

A Project
ON
Influence line Diagram for Indeterminate Beam
Using Muller Breslau Principle



Prepared in partial fulfillment of the

Study Project

Course No. - CE F266

Submitted By

Samarth Joshi

Prepared for

DR. S.N. Patel

BIRLA INSTITUTE OF TECHNOLOGY & SCIENCE, PILANI

(JUNE,2021)

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Introduction

The project shows the computation of the influence line diagram using the Muller Breslau principle for indeterminate beams and to build a code to compute values and graphs. According to the **Müller-Breslau principle**, an influence line will be a scaled form of the deflected beam shape, when resistance to the response is removed at the analysis point, and a relative unit deflection is applied for the shear influence line, or a unit rotation is applied for the moment influence line is introduced at the analysis point to determine an influence line. To remove shear resistance, a fictitious roller guide is applied, which allows vertical deflection at the analysis point while maintaining resistance to rotation. A fictitious hinge is applied to remove moment resistance. The hinge allows rotation at the analysis point with zero relative displacements. The resulting deflected shape provides the influence line for a unit point load.

There are various approaches to solve the beam's deflection after applying the Muller Breslau principle.

- Castigliano's method
- Moment-area theorem
- Conjugate beam method
- Double Integration
- Force Method

In the project double integration method is used for calculating bending, and there is another approach used in problem 3 and 4 by taking deflection of the beam as a cubic equation then assigning the boundary condition to the equations to find the coefficients of equations. The second approach makes all the calculation much easier in coding and calculation perspective.

Java and JavaFX handled for calculation and graph representation. User can give inputs in terms of length of the beam, distance of support, and distance analysis point. The output will be a graphical line chart representation with thousand intervals and can be modified to find any position. All calculation verified using STAAD Pro.

Problem Statement: 1

To find an influence line diagram of shear force for the point at distance “K” from the fixed end “A” (as shown in fig. 1).

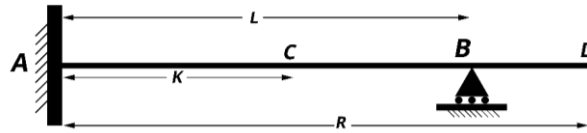


Fig. 1 Cantilever, simply supported Beam

R = Length of Beam,

L = Distance of support from origin from fixed end,

K = Distance of point for which ILD is calculated from fixed end,

EI = flexural rigidity of beam (assumed to be constant)

Solution: The solution will be in three parts for different position of K .

Applying Müller-Breslau principle,

Part 1: $K=0$,

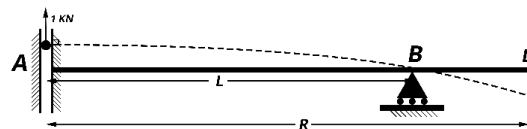


Fig. 2 Influence Line to the shear at C is to the same scale as deflected shape.

When x varies from 0 to K i.e., $0 \leq x < L$

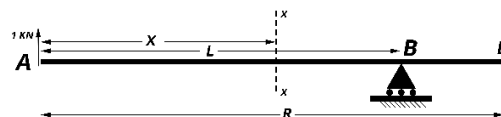


Fig. 3

By Double Integration Method,

$$M_x = - (L-x)$$

$$EI \frac{d^2y}{dx^2} = - (L-x)$$

$$EI \frac{dy}{dx} = -Lx + \frac{x^2}{2} + C_1 \quad \dots (1)$$

$$EI y(x) = -L \frac{x^2}{2} + \frac{x^3}{6} + C_1 x + C_2 \quad \dots (2)$$

Putting boundary condition in the equation (1) and (2)

$EI \frac{dy}{dx}$ at $x=0$ is 0 as there is fixed support. Hence, we get $C_1 = 0$

Again, $y(0)=0$ as there is fixed support. Hence, we get $C_2 = \frac{L^3}{3}$

$$EI y(x) = -L \frac{x^2}{2} + \frac{x^3}{6} + \frac{L^3}{3} \quad \dots (3)$$

When x varies from 0 to L i.e., $L \leq x < R$

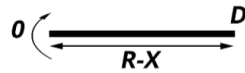


Fig. 5

By Double Integration Method,

$$M_x = 0$$

$$EI \frac{d^2y}{dx^2} = 0$$

$$EI \frac{dy}{dx} = C_5 \quad \dots (4)$$

$$EI y(x) = C_5 x + C_6 \quad \dots (5)$$

Using boundary condition,

When $x=L$, slope in equation (4) is equal to that of equation (1). Hence, we get $C_5 = -\frac{L^2}{2}$

When $x=L$, $y(L)=0$ as there is no displacement in y in equation (5) at a support, $C_6 = \frac{L^3}{2}$

$$EI y(x) = -\frac{L^2}{2}x + \frac{L^3}{2} \quad \dots (6)$$

To find the function of ILD we have to divide the function in equation (3), and (6) by scale factor which is equal to $y(L)$ in any of equation (3) or (6)

$$\text{Scale factor} = \frac{L^3}{3EI}$$

Hence, the **Influence Line Diagram for shear at C** is

$$y(x) = \left(-L \frac{x^2}{2} + \frac{x^3}{6} + \frac{L^3}{3}\right) \frac{3}{L^3} \quad \text{for } 0 < x < L$$

$$y(x) = \left(-\frac{L^2}{2}x + \frac{L^3}{2}\right) \frac{3}{L^3} \quad \text{for } L < x < R$$

Part 2: $0 < K < L$

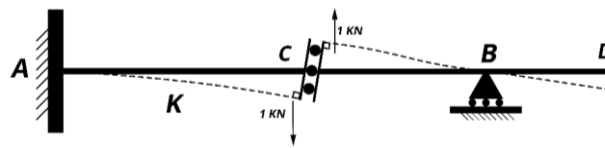


Fig. 2 Influence Line to the shear at C is to the same scale as deflected shape.

When x varies from 0 to K i.e., $0 \leq x < K$

By Double Integration Method,

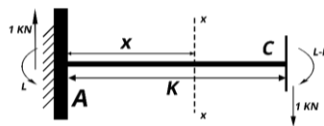


Fig. 3

$$M_x = x - L$$

$$EI \frac{d^2y}{dx^2} = x - L$$

$$EI \frac{dy}{dx} = \frac{x^2}{2} - Lx + C_1 \quad \dots (1)$$

$$EI y(x) = \frac{x^3}{6} - L \frac{x^2}{2} + C_1 x + C_2 \quad \dots (2)$$

Putting boundary condition in the equation (1) and (2)

$EI \frac{dy}{dx}$ at $x=0$ is 0 as there is fixed support. Hence, we get $C_1=0$.

Again, $y(0)=0$ as there is fixed support. Hence, we get $C_2=0$.

$$EI y(x) = \frac{x^3}{6} - L \frac{x^2}{2} \quad \dots (3)$$

When x is varies from 0 to K i.e., $K \leq x < L$

By Double Integration Method,

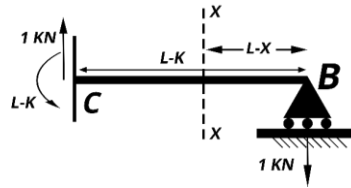


Fig. 4

$$M_x = x - L$$

$$EI \frac{d^2y}{dx^2} = x - L$$

$$EI \frac{dy}{dx} = \frac{x^2}{2} - Lx + C_3 \quad \dots (4)$$

$$EI y(x) = \frac{x^3}{6} - L\frac{x^2}{2} + C_3x + C_4 \quad \dots (5)$$

Using boundary condition,

When $x=K$, slope in equation (1) is equal to that of equation (4). Hence, we get $C_3=C_1=0$.

When $x=L$, $y(L)=0$ as there no displacement in y in equation (5) at roller support, $C_4=\frac{L^3}{3}$.

$$EI y(x) = \frac{x^3}{6} - L\frac{x^2}{2} + \frac{L^3}{3} \quad \dots (6)$$

When x is varies from 0 to K i.e., $L \leq x < R$

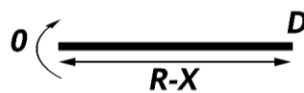


Fig. 5

By Double Integration Method,

$$M_x = 0$$

$$EI \frac{d^2y}{dx^2} = 0$$

$$EI \frac{dy}{dx} = C_5 \quad \dots (7)$$

$$EI y(x) = C_5x + C_6 \quad \dots (8)$$

Using boundary condition,

When $x=L$, slope in equation (7) is equal to that of equation (4). Hence, we get $C_5 = -\frac{L^2}{2}$

When $x=L$, $y(L)=0$ as there no displacement in y in equation (8) at a support, $C_6 = \frac{L^3}{2}$.

$$EI y(x) = -\frac{L^2}{2}x + \frac{L^3}{2} \quad \dots (9)$$

To find the function of ILD we have to divide the function in equation (3), (6) and (9) by scale factor which is equal to addition of $y(k)$ from equation (3) and (6).

$$\text{Scale factor} = \frac{L^3}{3EI}$$

Hence, the **Influence Line Diagram for shear at C** is

$$y(x) = \left(\frac{x^3}{6} - L\frac{x^2}{2}\right) \frac{3}{L^3} \quad \text{for } 0 < x < K$$

$$y(x) = \left(\frac{x^3}{6} - L\frac{x^2}{2} + \frac{L^3}{3}\right) \frac{3}{L^3} \quad \text{for } K < x < L$$

$$y(x) = \left(-\frac{L^2}{2}x + \frac{L^3}{2}\right) \frac{3}{L^3} \quad \text{for } L < x < R$$

Part 3: $K=L$,

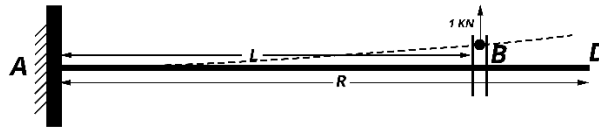


Fig. 2 Influence Line to the shear at C is to the same scale as deflected shape.

When x varies from 0 to K i.e., $0 \leq x < L$

By Double Integration Method,

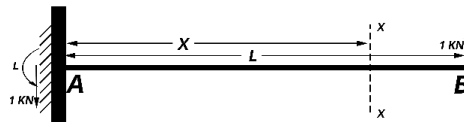


Fig. 3

$$M_x = -(x-L)$$

$$EI \frac{d^2y}{dx^2} = -(x-L)$$

$$EI \frac{dy}{dx} = -\frac{x^2}{2} + Lx + C_1 \quad \dots (1)$$

$$EI y(x) = -\frac{x^3}{6} + L\frac{x^2}{2} + C_1x + C_2 \quad \dots (2)$$

Putting boundary condition in the equation (1) and (2)

$EI \frac{dy}{dx}$ at $x=0$ is 0 as there is fixed support. Hence, we get $C_1=0$.

Again, $y(0)=0$ as there is fixed support. Hence, we get $C_2=0$.

$$EI y(x) = -\frac{x^3}{6} + L\frac{x^2}{2} \quad \dots (3)$$

When x is varies from 0 to K i.e., $L \leq x < R$

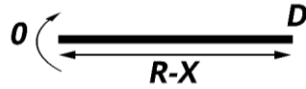


Fig. 5

By Double Integration Method,

$$M_x=0$$

$$EI \frac{d^2y}{dx^2} = 0$$

$$EI \frac{dy}{dx} = C_5 \quad \dots (4)$$

$$EI y(x) = C_5x + C_6 \quad \dots (5)$$

Using boundary condition,

When $x=L$, slope in equation (4) is equal to that of equation (1). Hence, we get $C_5 = \frac{L^2}{2}$

When $x=L$, $y(L)=0$ as there no displacement in y in equation (5) at a support, $C_6 = -\frac{L^3}{6}$

$$EI y(x) = \frac{L^2}{2}x - \frac{L^3}{6} \quad \dots (6)$$

To find the function of ILD we have to divide the function in equation (3), and (6) by scale factor which is equal to $y(L)$ in any of equation (3) or (6)

$$\text{Scale factor} = \frac{L^3}{3EI}$$

Hence, the **Influence Line Diagram for shear at C** is

$$y(x) = \left(-\frac{x^3}{6} + L\frac{x^2}{2}\right)\frac{3}{L^3} \quad \text{for } 0 < x < L$$

$$y(x) = \left(\frac{L^2}{2}x - \frac{L^3}{6}\right)\frac{3}{L^3} \quad \text{for } L < x < R$$

Problem Statement: 2

To find an influence line diagram of shear force for the point at distance “K” from the end “A” (as shown in Fig. 1).

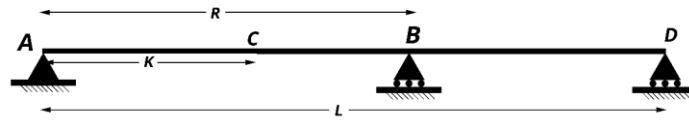


Fig. 1

L = Length of Beam,

R = Distance of middle support from origin from end A,

K = Distance of point for which ILD is calculated from end A,

EI = flexural rigidity of beam (assumed to be constant)

Solution: The solution will be in five parts for different position of K.

Applying Müller-Breslau principle,

PART 1: If $0 < K < L$,

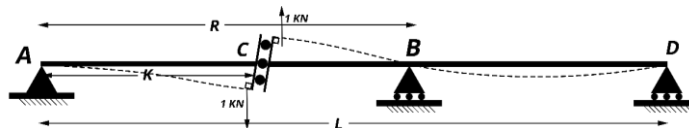


Fig. 2 Removing the support at C and applying the positive shear at C yields the deflected shape. Influence Line to the shear at C is to the same scale as deflected shape.

When x is varies from 0 to K i.e., $R \leq x < L$

By Double Integration Method,

$$M_x = \frac{R}{L-R} (L-x)$$

$$EI \frac{d^2y}{dx^2} = \frac{R}{L-R} (L-x)$$

$$EI \frac{dy}{dx} = \frac{R}{L-R} \left(Lx - \frac{x^2}{2} \right) + C_5 \quad \dots (1)$$

$$EI y(x) = \frac{R}{L-R} \left(L \frac{x^2}{2} - \frac{x^3}{6} \right) + C_5 x + C_6 \quad \dots (2)$$

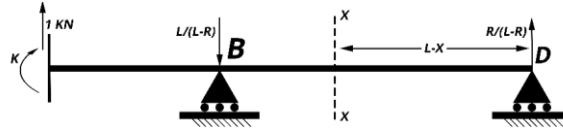


Fig. 3

Using boundary condition,

When $x=L$ and $x=R$ the value of $y(L)=0$ as there no displacement in y in equation (2) at a support.

We get,

$$\frac{R}{L-R} \left(\frac{L^2}{2} - \frac{L^3}{6} \right) + C_5 \cdot L + C_6 = 0$$

$$\frac{R}{L-R} \left(L \frac{R^2}{2} - \frac{R^3}{6} \right) + C_5 \cdot L + C_6 = 0$$

Solving the above equations. we get,

$$C_5 = \frac{R}{L-R} \left(L \frac{R^2}{2} - \frac{R^3}{6} - \frac{L^3}{3} \right)$$

$$C_6 = - \frac{R}{L-R} \left(\frac{L^3}{3} \right) - C_5 \cdot L$$

$$EI y(x) = \frac{R}{L-R} \left(L \frac{x^2}{2} - \frac{x^3}{6} \right) + C_5 \cdot x - \frac{R}{L-R} \left(\frac{L^3}{3} \right) - C_5 \cdot L \quad \dots (3)$$

When x is varies from 0 to K i.e., $K < x < R$

By Double Integration Method,

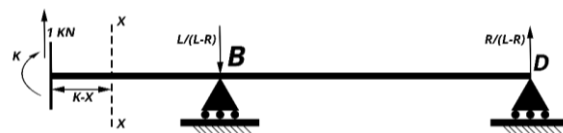


Fig. 4

$$M_x = x$$

$$EI \frac{d^2 y}{dx^2} = x$$

$$EI \frac{dy}{dx} = \frac{x^2}{2} + C_3 \quad \dots (4)$$

$$EI y(x) = \frac{x^3}{6} + C_3 x + C_4 \quad \dots (5)$$

Using boundary condition,

When $x=L$, slope in equation (1) is equal to that of equation (4),

$$\text{we get } C_3 = \frac{R}{L-R} \left(LR - \frac{R^2}{2} \right) + C_5 - \frac{R^2}{2}$$

When $x=L$, $y(L)=0$ as there no displacement in y in equation (7) at roller support,

$$\text{We get } C_4 = -\frac{R^3}{6} - \left\{ \frac{R}{L-R} \left(LR - \frac{R^2}{2} \right) + C_5 - \frac{R^2}{2} \right\} \cdot R$$

$$EI y(x) = \frac{x^3}{6} + \left\{ \frac{R}{L-R} \left(LR - \frac{R^2}{2} \right) + C_5 - \frac{R^2}{2} + C_5 - \frac{R^2}{2} \right\} x + -\frac{R^3}{6} - \left\{ \frac{R}{L-R} \left(LR - \frac{R^2}{2} \right) + C_5 - \frac{R^2}{2} \right\} \cdot R \quad \dots (6)$$

When x varies from 0 to K i.e., $0 \leq x < K$

By Double Integration Method,

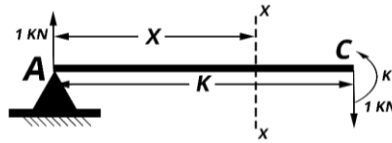


Fig. 5

$$M_x = x$$

$$EI \frac{d^2 y}{dx^2} = x$$

$$EI \frac{dy}{dx} = \frac{x^2}{2} + C_1 \quad \dots (7)$$

$$EI y(x) = \frac{x^3}{6} + C_1 x + C_2 \quad \dots (8)$$

Putting boundary condition in the equation (7) and (8),

$EI y(x)=0$ at $x=0$ as there is a support, we get $C_2=0$.

When $x=K$, slope in equation (4) is equal to that of equation (7), we get $C_1 = C_3$.

$$EI y(x) = \frac{x^3}{6} + \left\{ \frac{R}{L-R} \left(L \frac{R^2}{2} - \frac{R^3}{6} \right) + C_5 - \frac{R^2}{2} \right\} x \quad \dots (9)$$

To find the function of ILD we have to divide the function in equation (3), (6) and (9) by scale factor which is equal to addition of $y(k)$ from equation (6) and (9).

$$\text{Scale factor} = \frac{\frac{K^3}{6} + \left\{ \frac{R}{L-R} \left(L \frac{R^2}{2} - \frac{R^3}{6} \right) + C_5 - \frac{R^2}{2} \right\} K + \frac{K^3}{6} + \left\{ \frac{R}{L-R} \left(LR - \frac{R^2}{2} \right) + C_5 - \frac{R^2}{2} + C_5 - \frac{R^2}{2} \right\} K + - \frac{R^3}{6} - \left\{ \frac{R}{L-R} \left(LR - \frac{R^2}{2} \right) + C_5 - \frac{R^2}{2} \right\} R}{EI}$$

Hence, the **Influence Line Diagram for shear at C** from equation (3), (6) and (9) is

$$y(x) = \frac{\frac{x^3}{6} + \left\{ \frac{R}{L-R} \left(L \frac{R^2}{2} - \frac{R^3}{6} \right) + C_5 - \frac{R^2}{2} \right\} x}{\text{Scale factor} \cdot EI} \quad \text{for } 0 < x < K$$

$$y(x) = \frac{\frac{x^3}{6} + \left\{ \frac{R}{L-R} \left(LR - \frac{R^2}{2} \right) + C_5 - \frac{R^2}{2} + C_5 - \frac{R^2}{2} \right\} x - \frac{R^3}{6} - \left\{ \frac{R}{L-R} \left(LR - \frac{R^2}{2} \right) + C_5 - \frac{R^2}{2} \right\} R}{\text{Scale factor} \cdot EI} \quad \text{for } K < x < R$$

$$y(x) = \frac{\frac{R}{L-R} \left(L \frac{x^2}{2} - \frac{x^3}{6} \right) + C_5 \cdot x - \frac{R}{L-R} \left(\frac{L^3}{3} \right) - C_5 \cdot L}{\text{Scale factor} \cdot EI} \quad \text{for } R < x < L$$

$$\text{where } C_5 = \frac{R}{L-R} \left(L \frac{R^2}{2} - \frac{R^3}{6} - \frac{L^3}{3} \right)$$

PART 2: K=R,

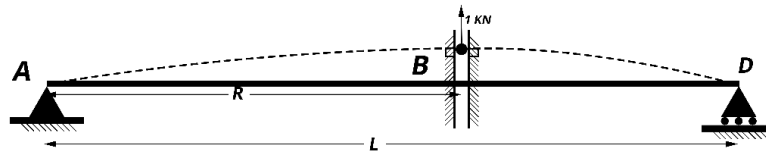


Fig. 6. Placing the roller guide at B and applying the positive shear at B yields the deflected shape. Influence Line to the shear at B is to the same scale as deflected shape

When x is varies from 0 to R i.e., $0 \leq x < R$

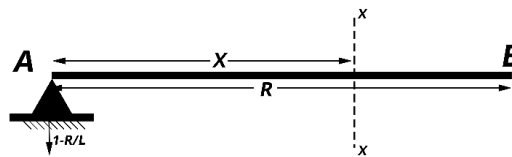


Fig. 7

By Double Integration Method,

$$M_x = -x \cdot \left(1 - \frac{R}{L} \right)$$

$$EI \frac{d^2y}{dx^2} = -x \cdot \left(1 - \frac{R}{L} \right)$$

$$EI \frac{dy}{dx} = -x^2 \cdot \left(1 - \frac{R}{L} \right) + C_1 \quad \dots (1)$$

$$EI y(x) = -x^3 \cdot (1 - \frac{R}{L}) + C_1 \cdot x + C_2 \quad \dots (2)$$

Using boundary condition,

When $x=0$ the value of $y(0)=0$ as there no displacement in y in equation (2) as it is at a support.

We get, $C_2=0$. $\dots (3)$

When x is varies from 0 to K i.e., $R < x < L$

By Double Integration Method,

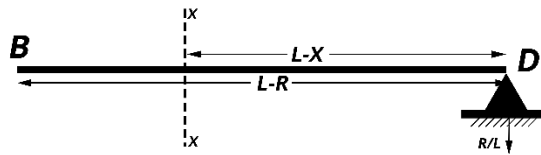


Fig. 8

$$M_x = -(L-x) \cdot \frac{R}{L}$$

$$EI \frac{d^2y}{dx^2} = -(L-x) \cdot \frac{R}{L}$$

$$EI \frac{dy}{dx} = -(Lx - \frac{x^2}{2}) \cdot \frac{R}{L} + C_3 \cdot x \quad \dots (4)$$

$$EI y(x) = -(L \frac{x^2}{2} - \frac{x^3}{6}) \cdot \frac{R}{L} + C_3 \cdot x + C_4 \quad \dots (5)$$

When $x=L$ the value of $y(L)=0$ as there no displacement in y in equation (3) as it is at a support.

We get,

$$C_3 \cdot L + C_4 = R \cdot \frac{L^2}{3} \quad \dots (6)$$

Also,

When $x=R$, slope in equation (1) is equal to that of equation (4) and also $y(x)$ will be equal in equation (2) and (5),

$$\text{We get } -\frac{R^3}{6} (1 - \frac{R}{L}) + C_1 R = -(L \frac{x^2}{2} - \frac{x^3}{6}) \cdot \frac{R}{L} + C_3 \cdot x + C_4 \quad \dots (7)$$

$$-(Lx - \frac{x^2}{2}) \cdot \frac{R}{L} + C_3 \cdot x = -x^2 \cdot (1 - \frac{R}{L}) + C_1 \quad \dots (8)$$

From the above equations (3), (6), (7) and (8)

$$C_1 = \frac{RL}{3} + \frac{R^3}{6L} - \frac{R^2}{2}$$

$$C_2 = 0$$

$$C_3 = \frac{RL^2}{3} - \frac{R^3}{6}$$

$$C_4 = -\frac{R^3}{6}$$

Hence,

$$y(x) = -x^3 \cdot \left(1 - \frac{R}{L}\right) + \left(\frac{RL}{3} + \frac{R^3}{6L} - \frac{R^2}{2}\right) \cdot x \quad \text{for } 0 < x < R \quad \dots (9)$$

$$y(x) = -\left(\frac{Lx^2}{2} - \frac{x^3}{6}\right) \frac{R}{L} + \left(\frac{RL^2}{3} - \frac{R^3}{6}\right) \cdot x - \frac{R^3}{6} \quad \text{for } R < x < L \quad \dots (10)$$

To find the function of ILD we have to divide the function in equation (9) and (10) by scale factor which is equal to addition of y(k) from equation (9) and (10).

$$\text{Scale factor} = \frac{-R^3 \cdot \left(1 - \frac{R}{L}\right) + \left(\frac{RL}{3} + \frac{R^3}{6L} - \frac{R^2}{2}\right) \cdot R}{EI}$$

Hence, the **Influence Line Diagram for shear at C from equation (9), and (10)** is

$$y(x) = \frac{-x^3 \cdot \left(1 - \frac{R}{L}\right) + \left(\frac{RL}{3} + \frac{R^3}{6L} - \frac{R^2}{2}\right) \cdot x}{\text{Scale factor} \cdot EI} \quad \text{for } 0 < x < R$$

$$y(x) = \frac{-\left(\frac{Lx^2}{2} - \frac{x^3}{6}\right) \frac{R}{L} + \left(\frac{RL^2}{3} - \frac{R^3}{6}\right) \cdot x - \frac{R^3}{6}}{\text{Scale factor} \cdot EI} \quad \text{for } R < x < L$$

PART 3: $R < K < L$,

By Similarity we can get ILD by replacing x to (L-x), R to (L-R) and K to (L-K) in the part 2.

We get,

Scale factor =

$$\frac{\frac{K^3}{6} + \left\{ \frac{(L-R)}{L-(L-R)} \left(L \frac{(L-R)^2}{2} - \frac{(L-R)^3}{6} \right) + C_5 - \frac{(L-R)^2}{2} \right\} \cdot K + \frac{K^3}{6} + \left\{ \frac{(L-R)}{L-(L-R)} \left(L(L-R) - \frac{(L-R)^2}{2} \right) + C_5 - \frac{(L-R)^2}{2} \right\} \cdot K + -\frac{(L-R)^3}{6} - \left\{ \frac{(L-R)}{L-(L-R)} \left(L(L-R) - \frac{(L-R)^2}{2} \right) + C_5 - \frac{(L-R)^2}{2} \right\} \cdot (L-R)}{EI}$$

Hence, the **Influence Line Diagram for shear at C from equation (8), (14) and (18)** is

$$y(x) = \frac{\frac{(L-x)^3}{6} + \left\{ \frac{(L-R)}{L-(L-R)} \left(\frac{(L-R)^2}{2} - \frac{(L-R)^3}{6} \right) + C_5 - \frac{(L-R)^2}{2} \right\} \cdot (L-x)}{\text{Scale factor} \cdot EI} \quad \text{for } K < x < L$$

$$y(x) = \frac{\frac{(L-R)^3}{6} + \left\{ \frac{(L-R)}{(L-R)} \right\} (L(L-R) - \frac{(L-R)^2}{2}) + C_5 - \frac{(L-R)^2}{2} + C_5 - \frac{(L-R)^2}{2} \cdot (L-R) - \frac{(L-R)^3}{6} - \left\{ \frac{(L-R)}{(L-R)} \right\} (L(L-R) - \frac{(L-R)^2}{2}) + C_5 - \frac{(L-R)^2}{2} \cdot (L-R)}{\text{Scale factor} \cdot EI} \quad \text{for } R < x < K$$

$$y(x) = \frac{\frac{(L-R)}{L-(L-R)} \left(L \frac{(L-x)^2}{2} - \frac{(L-x)^3}{6} \right) + C_5 \cdot (L-x) - \frac{(L-R)}{L-(L-R)} \left(\frac{L^3}{3} \right) - C_5 \cdot L}{\text{Scale factor : EI}} \quad \text{for } 0 < x < R$$

$$\text{where } C_5 = \frac{(L-R)}{L-(L-R)} \left(L \frac{(L-R)^2}{2} - \frac{(L-R)^3}{6} - \frac{L^3}{3} \right)$$

PART 4: $K = L$,

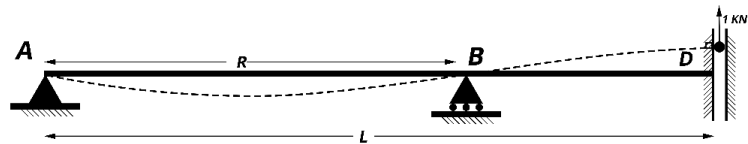


Fig. 9 Placing the roller guide at C and applying the positive shear at C yields the deflected shape. Influence Line to the shear at C is to the same scale as deflected shape.

When x varies from 0 to R i.e., $0 \leq x < R$

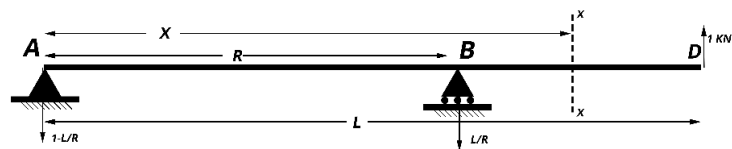


Fig. 4

By Double Integration Method,

$$M_x = -x \cdot (1 - \frac{R}{L})$$

$$EI \frac{d^2y}{dx^2} = -x \cdot (1 - \frac{R}{L})$$

$$EI \frac{dy}{dx} = -x^2 \cdot (1 - \frac{R}{L}) + C_1 \quad \dots (1)$$

$$EI y(x) = -x^3.(1-\frac{R}{L})+C_1.x+C_2 \quad \dots (2)$$

Using boundary condition,

When $x=0$ and $x=R$ the value of $y(0)=0$ as there no displacement in y in equation (2) as it is at a support.

We get,

$$C_1 = (1 - \frac{L}{R}) \cdot \frac{R^2}{6}$$

$$C_2 = 0$$

Hence,

$$EI y(x) = -x^3 \cdot (1 - \frac{R}{L}) + (1 - \frac{L}{R}) \frac{R^2 x}{6} \quad \dots (3)$$

When x is varies from 0 to K i.e., $R < x < L$

By Double Integration Method,

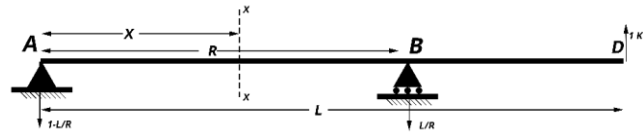


Fig. 10

$$M_x = (L-x)$$

$$EI \frac{d^2 y}{dx^2} = (L-x)$$

$$EI \frac{dy}{dx} = Lx - \frac{x^2}{2} + C_3 \quad \dots (4)$$

$$EI y(x) = (L \frac{x^2}{2} - \frac{x^3}{6}) + C_3 x + C_4 \quad \dots (5)$$

When $x=R$ the value of $y(L)=0$ as there no displacement in y in equation (3) as it is at a support.

We get,

$$C_3 R + C_4 = - (L \frac{R^2}{2} - \frac{R^3}{6}) \quad \dots (6)$$

Also, When $x=R$, slope in equation (10) is equal to that of equation (16) and also $y(x)$ will be equal,

We get,

$$Lx - \frac{x^2}{2} + C_3 = -x^2 \cdot (1 - \frac{R}{L}) + C_1 \quad \dots (7)$$

From the above equations (6) and (7),

$$C_3 = \frac{R^2}{6} - 2L \frac{R}{3}$$

$$C_4 = L \frac{R^2}{6}$$

Hence,

$$y(x) = -\frac{x^3}{6} \cdot (1 - \frac{L}{R}) + ((1 - \frac{L}{R}) \cdot \frac{R^2}{6}) \cdot x \quad \text{for } 0 < x < R \quad \dots (8)$$

$$y(x) = \left(\frac{Lx^2}{2} - \frac{x^3}{6} \right) + \left(\frac{R^2}{6} - 2L \frac{R}{3} \right) \cdot x + L \frac{R^2}{6} \quad \text{for } R < x < L \quad \dots (9)$$

To find the function of ILD we have to divide the function in equation (8) and (9) by scale factor which is equal to addition of $y(k)$ from equation (8) and (9).

$$\text{Scale factor} = \frac{\left(\frac{LR^2}{2} - \frac{R^3}{6} \right) + \left(\frac{R^2}{6} - 2L \frac{R}{3} \right) \cdot R + L \frac{R^2}{6}}{EI}$$

Hence, the **Influence Line Diagram for shear at C** from equation (8), and (9) is

$$y(x) = \frac{-\frac{x^3}{6} \cdot (1 - \frac{L}{R}) + ((1 - \frac{L}{R}) \cdot \frac{R^2}{6}) \cdot x}{\text{Scale factor} \cdot EI} \quad \text{for } 0 < x < R$$

$$y(x) = \frac{\left(\frac{Lx^2}{2} - \frac{x^3}{6} \right) + \left(\frac{R^2}{6} - 2L \frac{R}{3} \right) \cdot x + L \frac{R^2}{6}}{\text{Scale factor} \cdot EI} \quad \text{for } R < x < L$$

PART 5: If $K=0$,

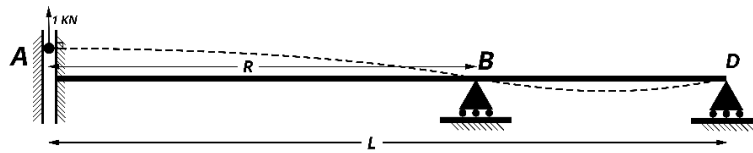


Fig. 11

By Similarity we can get ILD by replacing x to $(L-x)$, R to $(L-R)$ and K to $(L-K)$ in the part 4.

We get,

$$\text{Scale factor} = \frac{\left(\frac{L(L-R)^2}{2} - \frac{(L-R)^3}{6} \right) + \left(\frac{(L-R)^2}{6} - 2L \frac{(L-R)}{3} \right) \cdot (L-R) + L \frac{(L-R)^2}{6}}{EI}$$

Hence, the **Influence Line Diagram for shear at C** from equation (8), and (9) is

$$y(x) = \frac{-\frac{(L-x)^3}{6} \cdot \left(1 - \frac{L}{(L-R)}\right) + \left(1 - \frac{L}{(L-R)}\right) \cdot \frac{(L-R)^2}{6} \cdot (L-x)}{\text{Scale facto}(L-R) \cdot EI} \quad \text{for } R < x < L$$

$$y(x) = \frac{\left(\frac{L(L-x)^2}{2} - \frac{(L-x)^3}{6}\right) + \left(\frac{(L-R)^2}{6} - 2L\frac{(L-R)}{3}\right) \cdot (L-x) + L \cdot \frac{(L-R)^2}{6}}{\text{Scale facto}(L-R) \cdot EI} \quad \text{for } 0 < x < R$$

Problem Statement: 3

To find an influence line diagram of Bending Moment for the point at distance “K” from the fixed end “A” (as shown in fig. 1).

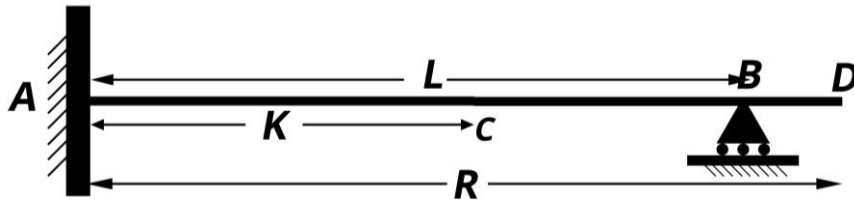


Fig. 1 Cantilever, simply supported Beam

R = Length of Beam,

L = Distance of support from origin from fixed end,

K = Distance of point for which ILD is calculated from fixed end,

EI = flexural rigidity of beam (assumed to be constant)

Solution: The solution will be in three parts for different position of K.

Applying Müller-Breslau principle,

Part 1: K=0

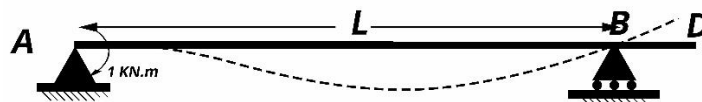


Fig. 2 Influence Line to the bending moment at 0 is to the same scale as deflected shape.

When x varies from 0 to K i.e., $0 \leq x < L$

As we know the M_x is a linear function of x (observation from the above problems and can be proved for any given beam)

By Double Integration it can be proved that deflection of beam is either a cubic function or a linear function

Let the equation for the deflected beam be,

$$y(x) = A_1x^3 + B_1x^2 + C_1x + D_1 \quad \dots (1)$$

The above equation will satisfy the following boundary condition

$$y(0) = D_1 = 0 \quad \dots (2)$$

$$y(L) = A_1L^3 + B_1L^2 + C_1L + D_1 = 0 \quad \dots (3)$$

$$\frac{d^2y}{dx^2} = 6A_1x + 2B_1 = 1 \text{ at } x=0 \quad \dots (4)$$

$$\frac{d^2y}{dx^2} = 6A_1x + 2B_1 = 0 \text{ at } x=L \quad \dots (5)$$

The equation (2), (3), (4), & (5) we can solve for $y(x)$ using matrix method

$$\begin{pmatrix} 0 & 0 & 0 & 1 \\ L^3 & L^2 & L & 1 \\ 0 & 2 & 0 & 0 \\ 6L & 2 & 0 & 0 \end{pmatrix} \begin{pmatrix} A_1 \\ B_1 \\ C_1 \\ D_1 \end{pmatrix} = \begin{pmatrix} 0 \\ 0 \\ 1 \\ 0 \end{pmatrix}$$

The value for the constants is calculated using inverse and multiplication matrix methods in java program.

When x varies from 0 to K i.e., $L \leq x < R$

Let the equation for the deflected beam be,

$$y(x) = A_3x^3 + B_3x^2 + C_3x + D_3 \quad \dots (1)$$

The above equation will satisfy the following boundary condition

$$y(L) = A_3L^3 + B_3L^2 + C_3L + D_3 = 0 \quad \dots (2)$$

derivatives will be equal at $x=K$

$$3A_3L^2 + 2B_3L + C_3 = 3A_1L^2 + 2B_1L + C_1 \quad \dots (3)$$

$$\frac{d^2y}{dx^2} = 6A_3x + 2B_3 = 0 \text{ at } x=L \quad \dots (4)$$

$$\frac{d^2y}{dx^2} = 6A_3x + 2B_3 = 0 \text{ at } x=R \quad \dots (5)$$

The equation (2), (3), (4), & (5) we can solve for $y(x)$ using matrix method

$$\begin{pmatrix} L^3 & L^2 & L & 1 \\ 3L^2 & 2L & 1 & 0 \\ 6L & 2 & 0 & 0 \\ 6R & 2 & 0 & 0 \end{pmatrix} \begin{pmatrix} A_3 \\ B_3 \\ C_3 \\ D_3 \end{pmatrix} = \begin{pmatrix} 0 \\ 3A_1K^2 + 2B_1K + C_1 \\ 0 \\ 0 \end{pmatrix}$$

The values for the constant is calculated using java.

After computation of all the constant for the cubic equations, Scale factor is calculated

$$\text{Scale factor} = (3A_1K^2 + 2B_1K + C_1)$$

Hence, the **Influence Line Diagram for shear at C from equation**

$$y(x) = (A_1x^3 + B_1x^2 + C_1x + D_1) / (3A_1K^2 + 2B_1K + C_1)$$

$$y(x) = (A_3x^3 + B_3x^2 + C_3x + D_3) / (3A_1K^2 + 2B_1K + C_1)$$

Part 2: $0 < K < L$

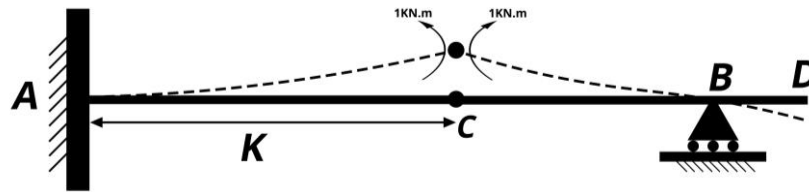


Fig. 2 Influence Line to the bending moment at C is to the same scale as deflected shape.

When x varies from 0 to K i.e., $0 \leq x < K$

As we know the M_x is a linear function of x (observation from the above problems and can be proved for any given beam)

By Double Integration it can be proved that deflection of beam is either a cubic function or a linear function

Let the equation for the deflected beam be,

$$y(x) = A_1x^3 + B_1x^2 + C_1x + D_1 \quad \dots (1)$$

The above equation will satisfy the following boundary condition

$$y(0) = D_1 = 0 \quad \dots (2)$$

$$\frac{dy}{dx} = 0 \text{ at } x=0 \quad \dots (3)$$

$$\frac{d^2y}{dx^2} = 6A_1x + 2B_1 = \frac{L}{L-K} \text{ at } x=0 \quad \dots (4)$$

$$\frac{d^2y}{dx^2} = 6A_1x + 2B_1 = 1 \text{ at } x=K \quad \dots (5)$$

The equation (2), (3), (4), & (5) we can solve for y(x) using matrix method

$$\begin{pmatrix} 0 & 0 & 0 & 1 \\ 0 & 0 & 1 & 0 \\ 0 & 2 & 0 & 0 \\ 6K & 2 & 0 & 0 \end{pmatrix} \begin{pmatrix} A_1 \\ B_1 \\ C_1 \\ D_1 \end{pmatrix} = \begin{pmatrix} 0 \\ 0 \\ 6A_1x + 2B_1 \\ 6A_1x + 2B_1 \end{pmatrix}$$

The value for the constants is calculated using inverse and multiplication matrix methods in java program.

When x varies from 0 to K i.e., $K \leq x < L$

Let the equation for the deflected beam be,

$$y(x) = A_2x^3 + B_2x^2 + C_2x + D_2 \quad \dots (1)$$

The above equation will satisfy the following boundary condition

$$y(L) = A_2L^3 + B_2L^2 + C_2L + D_2 = 0 \quad \dots (2)$$

displacement will be equal at x=K

$$A_2K^3 + B_2K^2 + C_2K + D_2 = A_1K^3 + B_1K^2 + C_1K + D_1 \quad \dots (3)$$

$$\frac{d^2y}{dx^2} = 6A_1x + 2B_1 = 0 \text{ at } x=L \quad \dots (4)$$

$$\frac{d^2y}{dx^2} = 6A_1x + 2B_1 = 1 \text{ at } x=K \quad \dots (5)$$

The equation (2), (3), (4), & (5) we can solve for y(x) using matrix method

$$\begin{pmatrix} L^3 & L^2 & L & 1 \\ K^3 & K^2 & K & 1 \\ 6L & 2 & 0 & 0 \\ 6K & 2 & 0 & 0 \end{pmatrix} \begin{pmatrix} A_2 \\ B_2 \\ C_2 \\ D_2 \end{pmatrix} = \begin{pmatrix} 0 \\ A_1K^3 + B_1K^2 + C_1K + D_1 \\ 0 \\ 1 \end{pmatrix}$$

The values for the constant is calculated using java.

When x varies from 0 to K i.e., $L \leq x < R$

Let the equation for the deflected beam be,

$$y(x) = A_3x^3 + B_3x^2 + C_3x + D_3 \quad \dots (1)$$

The above equation will satisfy the following boundary condition

$$y(L) = A_3L^3 + B_3L^2 + C_3L + D_3 = 0 \quad \dots (2)$$

derivatives will be equal at $x=K$

$$3A_3K^2 + 2B_3K + C_3 = 3A_2K^2 + 2B_2K + C_2 \quad \dots (3)$$

$$\frac{d^2y}{dx^2} = 6A_3x + 2B_3 = 0 \text{ at } x=L \quad \dots (4)$$

$$\frac{d^2y}{dx^2} = 6A_3x + 2B_3 = 0 \text{ at } x=R \quad \dots (5)$$

The equation (2), (3), (4), & (5) we can solve for $y(x)$ using matrix method

$$\begin{pmatrix} L^3 & L^2 & L & 1 \\ 3K^2 & 2K & 1 & 0 \\ 6L & 2 & 0 & 0 \\ 6R & 2 & 0 & 0 \end{pmatrix} \begin{pmatrix} A_3 \\ B_3 \\ C_3 \\ D_3 \end{pmatrix} = \begin{pmatrix} 0 \\ 3A_2K^2 + 2B_2K + C_2 \\ 0 \\ 0 \end{pmatrix}$$

The values for the constant is calculated using java.

After computation of all the constant for the cubic equations, Scale factor is calculated

$$\text{Scale factor} = (3A_1K^2 + 2B_1K + C_1) - (3A_2K^2 + 2B_2K + C_2)$$

Hence, the **Influence Line Diagram for shear at C from equation**

$$y(x) = (A_1x^3 + B_1x^2 + C_1x + D_1) / ((3A_1K^2 + 2B_1K + C_1) - (3A_2K^2 + 2B_2K + C_2))$$

$$y(x) = (A_2x^3 + B_2x^2 + C_2x + D_2) / ((3A_1K^2 + 2B_1K + C_1) - (3A_2K^2 + 2B_2K + C_2))$$

$$y(x) = (A_3x^3 + B_3x^2 + C_3x + D_3) / ((3A_1K^2 + 2B_1K + C_1) - (3A_2K^2 + 2B_2K + C_2))$$

Part 3: K=L

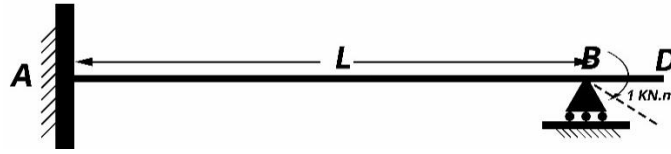


Fig. 2 Influence Line to the bending moment at L is to the same scale as deflected shape.

When x varies from 0 to K i.e., $0 \leq x < L$

As we know the M_x is a linear function of x (observation from the above problems and can be proved for any given beam)

By Double Integration it can be proved that deflection of beam is either a cubic function or a linear function

Let the equation for the deflected beam be,

$$y(x) = A_1x^3 + B_1x^2 + C_1x + D_1 \quad \dots (1)$$

The above equation will satisfy the following boundary condition

$$y(0) = D_1 = 0 \quad \dots (2)$$

$$y(L) = A_1L^3 + B_1L^2 + C_1L + D_1 = 0 \quad \dots (3)$$

$$\frac{d^2y}{dx^2} = 6A_1x + 2B_1 = 0 \text{ at } x=0 \quad \dots (4)$$

$$\frac{d^2y}{dx^2} = 6A_1x + 2B_1 = 0 \text{ at } x=L \quad \dots (5)$$

The equation (2), (3), (4), & (5) we can solve for y(x) using matrix method

$$\begin{pmatrix} 0 & 0 & 0 & 1 \\ L^3 & L^2 & L & 1 \\ 0 & 2 & 0 & 0 \\ 6L & 2 & 0 & 0 \end{pmatrix} \begin{pmatrix} A_1 \\ B_1 \\ C_1 \\ D_1 \end{pmatrix} = \begin{pmatrix} 0 \\ 0 \\ 0 \\ 0 \end{pmatrix}$$

The value for the constants is calculated using inverse and multiplication matrix methods in java program.

When x varies from 0 to K i.e., $L \leq x < R$

Let the equation for the deflected beam be,

$$y(x)=A_3x^3+B_3x^2+C_3x+D_3 \quad \dots (1)$$

The above equation will satisfy the following boundary condition

$$y(L)= A_3L^3+B_3L^2+C_3L+D_3 = 0 \quad \dots (2)$$

$$\frac{dy}{dx} = 3A_3L^2+2B_3L+C_3 = -1 \text{ at } x=0 \quad \dots (3)$$

$$\frac{d^2y}{dx^2} = 6A_3x+2B_3 = 0 \text{ at } x=L \quad \dots (4)$$

$$\frac{d^2y}{dx^2} = 6A_3x+2B_3 = 0 \text{ at } x=R \quad \dots (5)$$

The equation (2), (3), (4), & (5) we can solve for $y(x)$ using matrix method

$$\begin{pmatrix} L^3 & L^2 & L & 1 \\ 3L^2 & 2L & 1 & 0 \\ 6L & 2 & 0 & 0 \\ 6R & 2 & 0 & 0 \end{pmatrix} \begin{pmatrix} A_3 \\ B_3 \\ C_3 \\ D_3 \end{pmatrix} = \begin{pmatrix} 0 \\ -1 \\ 0 \\ 0 \end{pmatrix}$$

The values for the constant is calculated using java.

After computation of all the constant for the cubic equations, Scale factor is calculated

Scale factor = 1

Hence, the **Influence Line Diagram for shear at C from equation**

$$y(x)=0$$

$$y(x)=(A_3x^3+B_3x^2+C_3x+D_3)$$

Problem Statement: 4

To find an influence line diagram of Bending Moment for the point at distance “K” from the fixed end “A” (as shown in fig. 1).

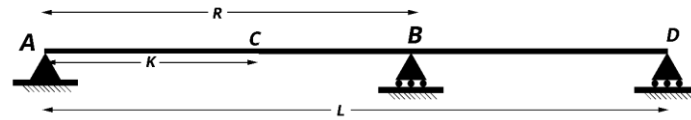


Fig. 1 Cantilever, simply supported Beam

R = Length of Beam,

L = Distance of support from origin from fixed end,

K = Distance of point for which ILD is calculated from fixed end,

EI = flexural rigidity of beam (assumed to be constant)

Solution: The solution will be in three parts for different position of K .

Applying Müller-Breslau principle,

Part 1: $K=0$

Moment at support will be zero when a unit load act upon beam.

Part 2: $0 < K < R$

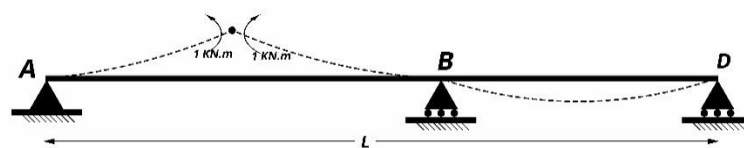


Fig. 2 Influence Line to the bending moment at C is to the same scale as deflected shape.

When x varies from 0 to K i.e., $R \leq x < L$

As we know the M_x is a linear function of x (observation from the above problems and can be proved for any given beam)

By Double Integration it can be proved that deflection of beam is either a cubic function or a linear function

Let the equation for the deflected beam be,

$$y(x) = A_1x^3 + B_1x^2 + C_1x + D_1 \quad \dots (1)$$

The above equation will satisfy the following boundary condition

$$y(R) = A_1R^3 + B_1R^2 + C_1R + D_1 = 0 \quad \dots (2)$$

$$y(L) = A_1L^3 + B_1L^2 + C_1L + D_1 = 0 \quad \dots (2)$$

$$\frac{d^2y}{dx^2} = 6A_1x + 2B_1 = \frac{R}{K} \text{ at } x=R \quad \dots (4)$$

$$\frac{d^2y}{dx^2} = 6A_1x + 2B_1 = 0 \text{ at } x=L \quad \dots (5)$$

The equation (2), (3), (4), & (5) we can solve for $y(x)$ using matrix method

$$\begin{pmatrix} L^3 & L^2 & L & 1 \\ R^3 & R^2 & R & 1 \\ 6L & 2 & 0 & 0 \\ 6R & 2 & 0 & 0 \end{pmatrix} \begin{pmatrix} A_2 \\ B_2 \\ C_2 \\ D_2 \end{pmatrix} = \begin{pmatrix} 0 \\ 0 \\ 0 \\ R/K \end{pmatrix}$$

The value for the constants is calculated using inverse and multiplication matrix methods in java program.

When x varies from 0 to K i.e., $K \leq x < R$

Let the equation for the deflected beam be,

$$y(x) = A_2x^3 + B_2x^2 + C_2x + D_2 \quad \dots (1)$$

The above equation will satisfy the following boundary condition

$$y(L) = A_2R^3 + B_2R^2 + C_2R + D_2 = 0 \quad \dots (2)$$

Slope will be equal at $x=K$

$$3A_2R^2 + 2B_2R + C_2 = 3A_3R^2 + 2B_3R + C_3 \quad \dots (3)$$

$$\frac{d^2y}{dx^2} = 6A_1x + 2B_1 = 0 \text{ at } x=R \quad \dots (4)$$

$$\frac{d^2y}{dx^2} = 6A_1x + 2B_1 = 1 \text{ at } x=K \quad \dots (5)$$

The equation (2), (3), (4), & (5) we can solve for $y(x)$ using matrix method

$$\begin{pmatrix} R^3 & R^2 & R & 1 \\ 3R^2 & 2R & 1 & 0 \\ 6R & 2 & 0 & 0 \\ 6K & 2 & 0 & 0 \end{pmatrix} \begin{pmatrix} A_2 \\ B_2 \\ C_2 \\ D_2 \end{pmatrix} = \begin{pmatrix} 0 \\ A_3R^2 + B_3R + C_3 \\ R/K \\ 1 \end{pmatrix}$$

The values for the constant is calculated using java.

When x varies from 0 to K i.e., $0 \leq x < K$

Let the equation for the deflected beam be,

$$y(x) = A_3x^3 + B_3x^2 + C_3x + D_3 \quad \dots (1)$$

The above equation will satisfy the following boundary condition

$$y(L) = A_3L^3 + B_3L^2 + C_3L + D_3 = 0 \quad \dots (2)$$

displacements will be equal at $x=K$

$$A_1K^3 + B_1K^2 + C_1K + D_1 = A_2K^3 + B_2K^2 + C_2K + D_2 \dots (3)$$

$$\frac{d^2y}{dx^2} = 6A_3x + 2B_3 = 0 \text{ at } x=0 \quad \dots (4)$$

$$\frac{d^2y}{dx^2} = 6A_3x + 2B_3 = 1 \text{ at } x=K \quad \dots (5)$$

The equation (2), (3), (4), & (5) we can solve for $y(x)$ using matrix method

$$\begin{pmatrix} 0 & 0 & 0 & 1 \\ 0 & 2 & 0 & 0 \\ 6K & 2 & 0 & 0 \\ R^3 & R^2 & R & 1 \end{pmatrix} \begin{pmatrix} A_3 \\ B_3 \\ C_3 \\ D_3 \end{pmatrix} = \begin{pmatrix} 0 \\ 0 \\ 1 \\ A_2K^3 + B_2K^2 + C_2K + D_2 \end{pmatrix}$$

The values for the constant is calculated using java.

After computation of all the constant for the cubic equations, Scale factor is calculated

$$\text{Scale factor} = (3A_1K^2 + 2B_1K + C_1) - (3A_2K^2 + 2B_2K + C_2)$$

Hence, the **Influence Line Diagram for shear at C from equation**

$$y(x) = (A_1x^3 + B_1x^2 + C_1x + D_1) / ((3A_1K^2 + 2B_1K + C_1) - (3A_2K^2 + 2B_2K + C_2))$$

$$y(x) = (A_2x^3 + B_2x^2 + C_2x + D_2) / ((3A_1K^2 + 2B_1K + C_1) - (3A_2K^2 + 2B_2K + C_2))$$

$$y(x) = (A_3x^3 + B_3x^2 + C_3x + D_3) / ((3A_1K^2 + 2B_1K + C_1) - (3A_2K^2 + 2B_2K + C_2))$$

Part 3: K=R

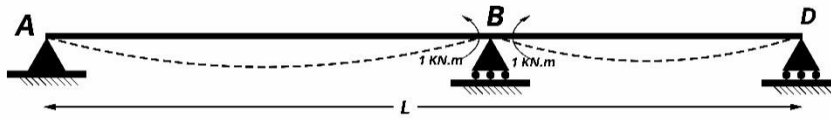


Fig. 2 Influence Line to the bending moment at L is to the same scale as deflected shape.

When x varies from 0 to K i.e., $0 \leq x < L$

As we know the M_x is a linear function of x (observation from the above problems and can be proved for any given beam)

By Double Integration it can be proved that deflection of beam is either a cubic function or a linear function

Let the equation for the deflected beam be,

$$y(x) = A_1x^3 + B_1x^2 + C_1x + D_1 \quad \dots (1)$$

The above equation will satisfy the following boundary condition

$$y(0) = D_1 = 0 \quad \dots (2)$$

$$y(R) = A_1R^3 + B_1R^2 + C_1R + D_1 = 0 \quad \dots (3)$$

$$\frac{d^2y}{dx^2} = 6A_1x + 2B_1 = 0 \text{ at } x=0 \quad \dots (4)$$

$$\frac{d^2y}{dx^2} = 6A_1x + 2B_1 = 0 \text{ at } x=R \quad \dots (5)$$

The equation (2), (3), (4), & (5) we can solve for $y(x)$ using matrix method

$$\begin{pmatrix} 0 & 0 & 0 & 1 \\ R^3 & R^2 & R & 1 \\ 0 & 2 & 0 & 0 \\ 6R & 2 & 0 & 0 \end{pmatrix} \begin{pmatrix} A_1 \\ B_1 \\ C_1 \\ D_1 \end{pmatrix} = \begin{pmatrix} 0 \\ 0 \\ -1/2 \\ 1 \end{pmatrix}$$

The value for the constants is calculated using inverse and multiplication matrix methods in java program.

When x varies from 0 to K i.e., $L \leq x < R$

Let the equation for the deflected beam be,

$$y(x) = A_3x^3 + B_3x^2 + C_3x + D_3 \quad \dots (1)$$

The above equation will satisfy the following boundary condition

$$y(R) = A_3R^3 + B_3R^2 + C_3R + D_3 = 0 \quad \dots (2)$$

$$y(L) = A_3L^3 + B_3L^2 + C_3L + D_3 = 0 \quad \dots (3)$$

$$\frac{d^2y}{dx^2} = 6A_3x + 2B_3 = -1/2 \text{ at } x=L \quad \dots (4)$$

$$\frac{d^2y}{dx^2} = 6A_3x + 2B_3 = 1 \text{ at } x=R \quad \dots (5)$$

The equation (2), (3), (4), & (5) we can solve for $y(x)$ using matrix method

$$\begin{pmatrix} R^3 & R^2 & R & 1 \\ L^3 & L^2 & L & 1 \\ 6L & 2 & 0 & 0 \\ 6R & 2 & 0 & 0 \end{pmatrix} \begin{pmatrix} A_3 \\ B_3 \\ C_3 \\ D_3 \end{pmatrix} = \begin{pmatrix} 0 \\ 0 \\ -1/2 \\ 1 \end{pmatrix}$$

The values for the constant is calculated using java.

After computation of all the constant for the cubic equations, Scale factor is calculated

$$\text{Scale factor} = 3A_1K^2 + 2B_1K + C_1 - 3A_2K^2 + 2B_2K + C_2$$

Hence, the **Influence Line Diagram for shear at C from equation**

$$y(x) = (A_1x^3 + B_1x^2 + C_1x + D_1) / ((3A_1K^2 + 2B_1K + C_1) - (3A_2K^2 + 2B_2K + C_2))$$

$$y(x) = (A_2x^3 + B_2x^2 + C_2x + D_2) / ((3A_1K^2 + 2B_1K + C_1) - (3A_2K^2 + 2B_2K + C_2))$$

Part 4: $R < K < L$

Replacing x by $L-x$ in part 2 we will get solution for the part 4.

Part 5: $K=L$

Moment at support will be zero when a unit load act upon beam.

Problem Statement: 4

To find arbitrary beam's deflection with known moment (using **slope deflection method**), after applying Muller Breslau principle.



We can prove that Internal Moment will be a linear function of \$x\$

By Double Integration we can say deflection of beam is either a cubic function or a linear function

Let the equation for the deflected beam be,

$$y(x) = A_1x^3 + B_1x^2 + C_1x + D_1 \quad \dots (1)$$

The above equation will satisfy the following boundary condition

$$y(0) = D_1 = 0 \quad \dots (2)$$

$$y(L) = A_1L^3 + B_1L^2 + C_1L + D_1 = 0 \quad \dots (3)$$

$$\frac{d^2y}{dx^2} = 6A_1x + 2B_1 = M_1 \text{ at } x=0 \quad \dots (4)$$

$$\frac{d^2y}{dx^2} = 6A_1x + 2B_1 = M_2 \text{ at } x=L \quad \dots (5)$$

The equation (2), (3), (4), & (5) we can solve for \$y(x)\$ using matrix method

$$\begin{pmatrix} 0 & 0 & 0 & 1 \\ L^3 & L^2 & L & 1 \\ 0 & 2 & 0 & 0 \\ 6L & 2 & 0 & 0 \end{pmatrix} \begin{pmatrix} A_1 \\ B_1 \\ C_1 \\ D_1 \end{pmatrix} = \begin{pmatrix} 0 \\ 0 \\ M_1 \\ M_2 \end{pmatrix}$$

From the above matrix we can find coefficient of cubic equation hence we can find beam's deflection after applying Muller Breslau Principle.

It can be concluded that we can find ILD for any beam after finding out the boundary conditions using methods such as Stiffness Matrix.

Application and Programming

Java is a programming language and a platform. Java is a high level, robust, object-oriented, and secure programming language. Java developed by Sun Microsystems (which is now the subsidiary of Oracle) in the year 1995. James Gosling is known as the father of Java. As previously mentioned, the code created on Java for performing the computations such as matrix multiplication using arrays and any such mathematical operations. It is essential to have prior knowledge of multi-dimensional arrays to understand mathematical solutions.

Java is an object-oriented programming language. Everything in Java is an object. Object-oriented means organizing software as a combination of different types of objects that incorporate both data and behavior. Object-oriented programming (OOPs) is a methodology that simplifies software development and maintenance by providing some rules.

Basic concepts of OOPs are:

- Object
- Class
- Inheritance
- Polymorphism
- Abstraction
- Encapsulation

Java is platform independent because it is different from other languages like C, C++, etc. which are compiled into platform specific machines while Java is a write once, run anywhere language. A platform is the hardware or software environment in which a program runs.

There are two types of platforms software-based and hardware-based. Java provides a software-based platform.

The Java platform differs from most other platforms in the sense that it is a software-based platform that runs on top of other hardware-based platforms. It has two components:

- Runtime Environment
- API (Application Programming Interface)

Java code can be executed on multiple platforms, for example, Windows, Linux, Sun Solaris, Mac/OS, etc. Java code is compiled by the compiler and converted into bytecode. This bytecode is a platform-independent code because it can be run on multiple platforms, i.e., Write Once and Run Anywhere (WORA).

JavaFX

The front end of the application made on JavaFX to create a simple user interface. JavaFX is a Java library used to develop Desktop applications and Rich Internet Applications (RIA). JavaFX is intended to replace swing in Java applications as a GUI framework. However, it provides more functionalities than swing. Like Swing, JavaFX also provides its components and does not depend upon the operating system. It is lightweight and hardware-accelerated. It supports various operating systems, including Windows, Linux, and Mac OS. The applications built in JavaFX can run on multiple platforms, including Web, Mobile and Desktops.

Scene Graph - It is the starting point of constructing a JavaFX application. It is a hierarchical tree of nodes that represent all the visual elements of the user interface. It also has the capability of handling events. In general, a scene graph defined as a collection of nodes. Each node has its separate id, style, and volume. Every node of a scene graph can only have a single parent and zero or more children. All the implementation on a scene graph is applied to its node. There are various classes present in javafx.scene package that is used for creating, modifying and applying some transformations on the node.

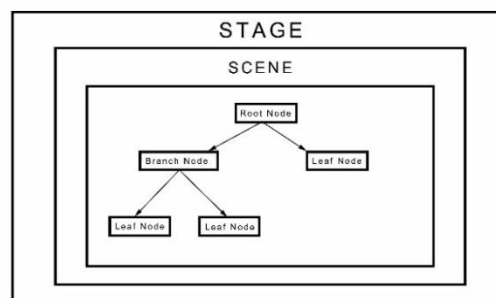


Fig. 1

JavaFX **Scene Builder** is used to design interface, tool that enables you to drag and drop graphical user interface (GUI) components onto a JavaFX scene. It can help you to quickly prototype interactive applications that connect GUI components to the application logic.

Eclipse is used as an integrated development environment which is used in computer programming. It contains a base workspace and an extensible plug-in system for customizing the environment.

Classes and Objects

There are total six JavaFX projects and each project consist of six to seven different classes in a src folder–

1. **Main.java** – To launch the program and set up basics prerequisite to launch an application.

```
package application;
import javafx.application.Application;

public class Main extends Application {
    @Override
    public void start(Stage primaryStage) throws Exception {

        Parent root = FXMLLoader.load(getClass().getResource("graph.fxml"));
        Scene scene = new Scene(root);
        scene.getStylesheets().add(getClass().getResource("application.css").toExternalForm());

        Image im= new Image(getClass().getResource("ild.png").toURI().toString());
        primaryStage.getIcons().add(im);

        primaryStage.setScene(scene);
        primaryStage.setTitle("Influence Line Diagram");
        // primaryStage.setResizable(false);
        primaryStage.show();
    }

    public static void main(String[] args) {
        launch(args);
    }
}
```

Fig. 2 Main.java

2. **Controller.java** – The main function of class is to control actions like to switch scene when the button is pressed. To perform a function the specific on action id must be assign in Scene Builder. Whenever the action is performed a set of action can be done using controller class.

```
package application;
import java.io.IOException;

public class Controller {

    @FXML
    public TextField beam;
    @FXML
    public TextField support;
    @FXML
    public TextField interest;
    public Stage stage;
    public Scene scene;
    public Parent root;
    public float arr[]=null;
    @FXML
    private CategoryAxis xAxi;
    @FXML
    private NumberAxis yAxi;
    @FXML
    private Pane pane;

    public void switchScene(ActionEvent e) throws IOException{
        ILD ilMethod = new ILD();
        float arr[] = ilMethod.main(Float.parseFloat(beam.getText()),Float.parseFloat(support.getText()),Float.parseFloat(interest.getText()));
        float beamL = Float.parseFloat(beam.getText());

        Graph gr = new Graph();
        gr.getValueOf("beam");

        Parent root = FXMLLoader.load(getClass().getResource("graph.fxml"));
        stage = (Stage)((Node)e.getSource()).getScene().getWindow();
        scene = new Scene(root);
        stage.setScene(scene);
    }
}
```

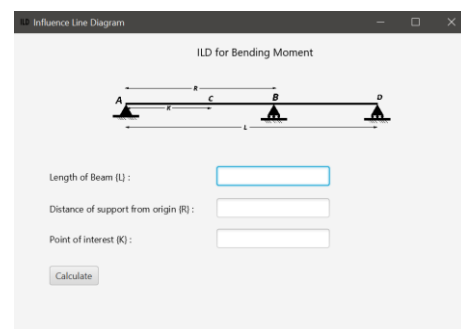


Fig. 3

3. **graph.java** – When all the calculation is computed in ILD.java it will return array of float values to graph.java where the graphical representation is done.

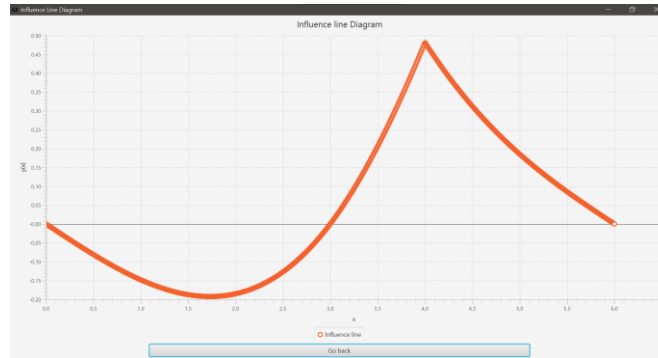


Fig. 4

4. **application.css and graph.fxml** – JavaFX FXML, which is an XML-based language that provides the structure for building a user interface separate from the application logic of your code. JavaFX has a rich set of extensions to CSS in support of features such as color derivation, property lookup, and multiple background colors and borders for a single node. These features add significant new power for developers and designers and are described in detail in this document. JavaFX Scene Builder is used to design interface, tool that enables you to drag and drop graphical user interface (GUI) components onto a JavaFX scene by creating changes in CSS and fxml files.
5. **ILD.java or ILD1.java** – All the calculative and mathematical operations part is in this class. This class will return output which will be used to create graph by graph.java class.
6. **Inverse.java** – It is class which takes a $n \times n$ matrix as input and will return inverse if matrix using mathematics.

Code Explanation

The first four problem mentioned in report are direct formula based. This section will be focused on explanation of beam with n number of supports. The problem divided into four parts Moment, Shear, Shear at Support, and Moment at Support. Each part divided into three subparts depending upon whether both ends pinned, left support Fixed, and both support fixed. Now, further explanation will be using an example (all reasons of parts and subparts will be similar)

Let there is four support and, the problem is to find an influence line diagram for a moment at any point of interest, say two.

At first, there are user inputs that are required-

- 1) Number of beams - 4
- 2) Point of Interest - 2
- 3) Length between each pair of nearest nodes or length of members- $L[1], L[2], L[3], L[4]$
- 4) whether ends are pinned or fixed.

```
//input from user

System.out.println("Enter number of beam : ");
int n = sc.nextInt();

System.out.println("Enter the beam number on which point of interest lies is : ");
int K = sc.nextInt();

L = new double[n+1];

// Distance between nodes
for (int i = 0; i < n+1; i++) {
    if (i!=K-1 && i!=K) {
        if (i<K-1) {
            System.out.println("Enter Length of " + (i+1) + " beam : ");
            L[i] = sc.nextFloat();
        }
        else{
            System.out.println("Enter Length of " + (i) + " beam : ");
            L[i] = sc.nextFloat();
        }
    }

    if(i==K-1) {
        System.out.println("Enter distance of point of interest from left nearest support: ");
        L[i] = sc.nextInt();
    }
    if(i==K) {
        System.out.println("Enter distance of point of interest from right nearest support: ");
        L[i] = sc.nextInt();
    }
}
```

Fig. 1 Inputs from user

As shown in the figure, there will be four elements and five nodes after applying the Muller Breslau principle, and it will consist of 11 forces and 11 displacement variables. When the beam deflects, the internal pin will allow a single deflection. However, the slope of each connected member will be different. Also, a slope at the roller will occur. The global axis set to the leftmost point of the beam.

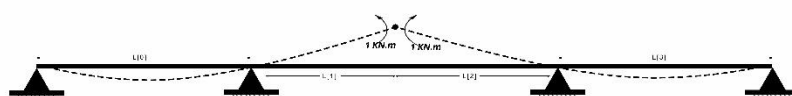


Fig. 2 Four pinned support continuous beam

To find beams deflection - after applying the Muller Breslau principle, we are using the stiffness matrix method to find slopes and vertical displacement at every single node, then will apply double integration on each element using boundary conditions to calculate the elements deflection equation.

First Step, Member Stiffness matrix is computed using the formula mentioned below in the figure -

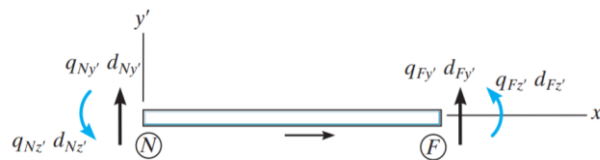


Fig. 3 Any arbitrary element

$$\begin{bmatrix} q_{Ny'} \\ q_{Nz'} \\ q_{Fy'} \\ q_{Fz'} \end{bmatrix} = \begin{bmatrix} \frac{12EI}{L^3} & \frac{6EI}{L^2} & -\frac{12EI}{L^3} & \frac{6EI}{L^2} \\ \frac{6EI}{L^2} & \frac{4EI}{L} & -\frac{6EI}{L^2} & \frac{2EI}{L} \\ -\frac{12EI}{L^3} & -\frac{6EI}{L^2} & \frac{12EI}{L^3} & -\frac{6EI}{L^2} \\ \frac{6EI}{L^2} & \frac{2EI}{L} & -\frac{6EI}{L^2} & \frac{4EI}{L} \end{bmatrix} \begin{bmatrix} d_{Ny'} \\ d_{Nz'} \\ d_{Fy'} \\ d_{Fz'} \end{bmatrix}$$

```
//Local Matrix
double [][4]local = new double[n+1][4][4];
for (int i = 0; i<n+1; i++) {
    local[i][0][0] = 12/(L[i]*L[i]*L[i]);
    local[i][0][1] = 6/(L[i]*L[i]);
    local[i][0][2] = -12/(L[i]*L[i]*L[i]);
    local[i][0][3] = 6/(L[i]*L[i]);
    local[i][1][0] = 6/(L[i]*L[i]);
    local[i][1][1] = 4/(L[i]);
    local[i][1][2] = -6/(L[i]*L[i]);
    local[i][1][3] = 2/(L[i]);
    local[i][2][0] = -12/(L[i]*L[i]*L[i]);
    local[i][2][1] = -6/(L[i]*L[i]);
    local[i][2][2] = 12/(L[i]*L[i]*L[i]);
    local[i][2][3] = -6/(L[i]*L[i]);
    local[i][3][0] = 6/(L[i]*L[i]);
    local[i][3][1] = 2/(L[i]);
    local[i][3][2] = -6/(L[i]*L[i]);
    local[i][3][3] = 4/(L[i]);
}
```

Fig. 4 Member Stiffness matrix or Local matrix

Second Step, to form Global Stiffness matrix –

After the structure stiffness matrix is determined, the loads at the nodes of the beam can be related to the displacements using the structure stiffness equation.

$$\mathbf{F}=\mathbf{K}*\mathbf{D} \dots\dots\dots()$$

	1	2	3	4	5	6	7	8	9	10	11
1	11	12	13	14							
2	21	22	23	24							
3	31	32	33 + 33	34 + 34	35	36					
4	41	42	43 + 43	44 + 44	45	46					
5			53	54	55 + 55	56	57	58	59		
6			63	64	65	66					
7					75		77	78	79		
8					85		87	88 + 88	89 + 89	8 10	8 11
9							9 8	9 9	9 10	9 11	
10							10 8	10 9	10 10	10 11	
11							11 8	11 9	11 10	11 11	

Global Matrix

```

//Global Matrix
float [][] global= new float[2*n+5][2*n+5];
for (int i = 0; i < n+1; i++) {
    int k;
    int l;
    if (i%2==0) {
        k = 2*i;
        l = 2*i+1;
    }
    else {
        k = 2*i+1;
        l = 2*i+2;
    }
    for (int m = 0; m < 4; m++) {
        for (int r = 0; r < 4; r++) {
            if (i%2==0&&l%2==0) {
                k=k+m;
                l=l+m;
            }
            if (i%2==0&&l%2==1) {
                l=l+m;
            }
            global[k][l] += local[i][m][r];
        }
    }
    if (i%2==0) {
        l=l+1;
    }
    else {
        l=l+2;
    }
    k++;
}

```

Fig.5 Global Stiffness matrix

Here Q and D are column matrices that represent both the known and unknown forces(both vertical forces and moments) and displacements(both slope and vertical displacements). Partitioning the stiffness matrix into the known and unknown elements of load and displacement, we have

$$F = K * D$$

Force[0]	11	12	13	14	0	0	0	0	0	0	0
0	21	22	23	24	0	0	0	0	0	0	0
Force[2]	31	32	33 + 33	34 + 34	35	36	0	0	0	0	0
0	41	42	43 + 43	44 + 44	45	46	0	0	0	0	0
0	0	0	53	54	55 + 55	56	57	58	59	0	0
1	0	0	63	64	65	66	0	0	0	0	0
-1	0	0	0	0	75	0	77	78	79	0	0
Force[7]	0	0	0	0	85	0	87	88 + 88	89 + 89	8 10	8 11
0	0	0	0	0	0	0	0	9 8	9 9	9 10	9 11
Force[9]	0	0	0	0	0	0	0	10 8	10 9	10 10	10 11
0	0	0	0	0	0	0	0	11 8	11 9	11 10	11 11

Force **Displacement**

Fig.6 Global Stiffness matrix

Code for computing displacements, solution of the fig.6

There will be either known force or known displacement in above matrix equation. There is an analogy that displacements are either zero or unknown. Then unknown displacements are calculated by diminishing the global matrix to smaller matrix GlobalK1 matrix.


```
// GlobalK1 Matrix
float globalk1[][] = new float[n+4][n+4];
int l=0;
int q=0;
for (int i = 0; i < n+4; i++) {

    if (i<K) {l=2*i+1;}
    if (i==K) {l=2*i;}
    if (i==K+1) {l=2*i-1;}
    if (i>=K+2) {l=2*i-2;}

    for (int j = 0; j < n+4; j++) {
        if (j<K) {q=2*j+1;}
        if (j==K) {q=2*j;}
        if (j==K+1) {q=2*j-1;}
        if (j>=K+2) {q=2*j-2;}

        globalk1[i][j] = global[l][q];
    }
}
```

```
// Inverse of GlobalK1 Matrix
float inverse[][] = new float[n+4][n+4];
inverse = Inverse.invert(globalk1);
System.out.println();
System.out.println("Inverse of globalk1 Matrix");
```

Fig. 8 Inverse function inverses any matrix

Fig. 7 GloblK1 Matrix and its Inverse

```
float[] displacement= new float[2*n+5];
System.out.println("Displacements");
for (int i = 0; i < n+4; i++) {

    for (int j = 0; j < n+4; j++) {

        if (i<K) {
            if (j<K) {displacement[2*i+1]+=inverse[i][j]*force[2*j+1];}
            if (j==K) {displacement[2*i+1]+=inverse[i][j]*force[2*j];}
            if (j==K+1) {displacement[2*i+1]+=inverse[i][j]*force[2*j-1];}
            if (j>=K+2) {displacement[2*i+1]+=inverse[i][j]*force[2*j-2];}

        }

        if (i==K) {
            if (j<K) {displacement[2*i]+=inverse[i][j]*force[2*j+1];}
            if (j==K) {displacement[2*i]+=inverse[i][j]*force[2*j];}
            if (j==K+1) {displacement[2*i]+=inverse[i][j]*force[2*j-1];}
            if (j>=K+2) {displacement[2*i]+=inverse[i][j]*force[2*j-2];}

        }

        if (i==K+1) {
            if (j<K) {displacement[2*i-1]+=inverse[i][j]*force[2*j+1];}
            if (j==K) {displacement[2*i-1]+=inverse[i][j]*force[2*j];}
            if (j==K+1) {displacement[2*i-1]+=inverse[i][j]*force[2*j-1];}
            if (j>=K+2) {displacement[2*i-1]+=inverse[i][j]*force[2*j-2];}

        }

        if (i>=K+2) {
            if (j<K) {displacement[2*i-2]+=inverse[i][j]*force[2*j+1];}
            if (j==K) {displacement[2*i-2]+=inverse[i][j]*force[2*j];}
            if (j==K+1) {displacement[2*i-2]+=inverse[i][j]*force[2*j-1];}
            if (j>=K+2) {displacement[2*i-2]+=inverse[i][j]*force[2*j-2];}

        }

    }

}
```

Fig. 9 Displacements by matrix multiplication of inverse and force

From the above matrix equation, we compute displacements which we can use in the above result of ILD problem 4 to compute the bending of beam.

```

//Finding Final Equation

//Value of x
float valueofx[] = new float[n+2];
valueofx[0]=0;
for (int i = 0; i < n+1; i++) {
    for (int m = 0; m < i+1; m++) {
        valueofx[i+1]+=L[m];

        }System.out.println("Value of x: "+valueofx[i+1]);
    }

float [][][] array1= new float[n+1][4][4];

for (int i = 0; i < n+1; i++) {
    array1[i][0][0] = valueofx[i]*valueofx[i]*valueofx[i];
    array1[i][0][1] = valueofx[i]*valueofx[i];
    array1[i][0][2] = valueofx[i];
    array1[i][0][3] = 1;
    array1[i][1][0] = 3*valueofx[i]*valueofx[i];
    array1[i][1][1] = 2*valueofx[i];
    array1[i][1][2] = 1;
    array1[i][1][3] = 0;
    array1[i][2][0] = valueofx[i+1]*valueofx[i+1]*valueofx[i+1];
    array1[i][2][1] = valueofx[i+1]*valueofx[i+1];
    array1[i][2][2] = valueofx[i+1];
    array1[i][2][3] = 1;
    array1[i][3][0] = 3*valueofx[i+1]*valueofx[i+1];
    array1[i][3][1] = 2*valueofx[i+1];
    array1[i][3][2] = 1;
    array1[i][3][3] = 0;
}

```

Fig. 10 Formulating Final equation variable as function of global x

```

float inv[][] = new float[n+1][n+1];
float abcd [][] = new float[n+1][4];

for (int i = 0; i < n+1; i++) {
    float [][] matrix = {{array1[i][0][0],array1[i][0][1],array1[i][0][2],array1[i][0][3]}, {array1[i][1][0],array1[i][1][1],array1[i][1][2],array1[i][1][3]},
    inv = Inverse.invert(matrix);

    for (int r = 0; r < 4; r++) {
        for (int r2 = 0; r2 < 4; r2++) {
            System.out.print("Inverse : ");
            System.out.print(inv[r][r2]+" ");
        } System.out.println();
    }System.out.println();

    for (int m2 = 0; m2 < 4; m2++) {
        int r=2*i;
        if (r%2*K) {r++;}
        for (int m3 = 0; m3 < 4; m3++) {
            abcd[i][m2]+= inv[m2][m3]*displacement[r];
            System.out.println("ABCD value for "+ i+"and "+r+" is :"+abcd[i][m2]);
            if (r==2*K&i==K) {r++;}
            r++;
        }
    }
}

```

Fig. 11 Computing coefficients of individual elements

```

System.out.println();
float Scalefactor = displacement[2*K+1]-displacement[2*K+2];
System.out.println("Values of Scalefactor: " + Scalefactor); System.out.println();

valueofy = new double[101*n+101] ;
double X1;
int r=0;

for (int i1 = 0; i1 < n+1; i1++) {
    X1= valueofx[i1];

    while (X1<valueofx[i1+1]) {
        valueofy[r] = (X1*X1*X1*abcd[i1][0]+X1*X1*abcd[i1][1]+X1*abcd[i1][2]+abcd[i1][3])/Scalefactor;
        System.out.println("Values of x "+X1+" for y: " + valueofy[r]);
        X1=X1+0.01*L[i1];
        r++;
    }
}

```

Fig. 12 Equation of Influence line using the above calculated coefficient

Summary

The **influence line diagram** is important part of analysis while designing structures like bridges crane rails, conveyor belts, floor girders, and other structures where loads will move along their span. The influence lines show where a load will create the maximum effect for any of the functions studied.

The major principle used across the project is Muller Breslau Principle which gives the result directly without calculating individually for different positions of unit load. Influence lines are based on Maxwell reciprocal work theorem. Also, Double Integration method is widely used, to find bending of beam with known boundary conditions.

Java and **JavaFX** are used to create backend and front end of application, respectively.

The project aims to develop a user interactive application which can compute graphs for influence lines for any indeterminate beam using the Muller Breslau principle. Initial approaches were based on manual calculation to formulate equation which can produce ILD values for corresponding positions, but for high indeterminacy it is difficult to calculate manually. Hence, Stiffness matrix method used to compute the displacements and then with help of ILD problem 4 result deflection of beam is calculated.

The results are verified using STAAD Pro and problems from book mentioned in references.

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