

Nonlinear Control Systems.

① Given dynamics

$$(m_x + m_\phi \sin^2(\phi)) \ddot{x} = -c_x \dot{x} + m_\phi g \cos(\phi) \sin(\phi) + m_\phi l \dot{\phi}^2 \sin(\phi) + u_x$$

$$m_x = -a_x u_x + \bar{m}_x$$

$$m_\phi l^2 \ddot{\phi} = -c_\phi \dot{\phi} - m_\phi l g \sin(\phi) - m_\phi l \cos(\phi) \ddot{x} + u_\phi$$

$$u_\phi = -a_\phi u_\phi + \bar{m}_\phi$$

For the 1st set of dynamics
tracking error

$$e = x_d - x$$

$$\dot{e} = \dot{x}_d - \dot{x}$$

$$\ddot{e} = \ddot{x}_d - \ddot{x}$$

multiply both sides by $(m_x + m_\phi \sin^2(\phi))$.

$$(m_x + m_\phi \sin^2(\phi)) \ddot{e} = (m_x + m_\phi \sin^2(\phi)) \ddot{x}_d - (m_x + m_\phi \sin^2(\phi)) \ddot{x}$$
①

Reference tracking error.

$$r = e + \alpha e$$

$$\Rightarrow \dot{r} = \dot{e} + \alpha \dot{e}$$

multiply both sides by $(m_x + m_\phi \sin^2(\phi))$.

$$(m_x + m_\phi \sin^2(\phi)) \dot{r} = (m_x + m_\phi \sin^2(\phi)) \dot{e} + (m_x + m_\phi \sin^2(\phi)) \alpha \dot{e}$$

Substituting eqn ①.

$$(m_x + m_\phi \sin^2(\phi)) \dot{r} = (m_x + m_\phi \sin^2(\phi)) \dot{x}_d - (m_x + m_\phi \sin^2(\phi)) \ddot{x} + (m_x + m_\phi \sin^2(\phi)) \alpha \dot{e}$$

$$(m_x + m_\phi \sin^2(\phi)) \dot{r} = (m_x + m_\phi \sin^2(\phi)) \ddot{x}_d - (-c_x \dot{x} + m_\phi g \cos(\phi) \sin(\phi) + m_\phi l \dot{\phi}^2 \sin(\phi) - \bar{m}_x)$$

$$+ (m_x + m_\phi \sin^2(\phi)) \alpha \dot{e} + r m_\phi \sin(\phi) \cos(\phi) - r m_\phi \sin(\phi) \cos(\phi)$$

$$Y = \left[(\ddot{x}_d + \alpha \dot{e}), (\dot{x} \sin(\phi) + \sin^2(\phi) \ddot{x}_d - g \cos(\phi) \sin(\phi) + \sin(\phi) \cos(\phi)), \right. \\ \left. (-\dot{\phi}^2 \sin(\phi)), \dot{x} \right]$$

$$\Theta = \begin{bmatrix} m_x \\ m_y \\ m_{pl} \\ C_x \end{bmatrix}$$

$$\Rightarrow (m_x + m_y \sin^2 \phi) \ddot{\gamma} = Y\theta - m_y \sin \phi \cos \phi \dot{\gamma} + \tilde{u}_x - \underline{u}_{x_0} \quad (2)$$

Let $\mathbf{e}_1 = \begin{bmatrix} e \\ \gamma \\ \tilde{\theta} \\ \tilde{u} \\ \tilde{a} \end{bmatrix}$

Lagrange function.

$$V = \frac{1}{2} e^2 + \frac{1}{2} (m_x + m_y \sin^2 \phi) \gamma^2 + \frac{1}{2} \tilde{\theta}^T \Gamma \tilde{\theta} + \frac{1}{2} \tilde{u}^2 + \frac{1}{2} \tilde{a}^2$$

$$\dot{V} = e \dot{e} + \frac{1}{2} (m_x + m_y \sin^2 \phi) (2\gamma \dot{\gamma}) + \frac{1}{2} (m_y (2 \sin \phi \cos \phi)) \dot{\gamma}^2 + \tilde{\theta}^T \Gamma \dot{\tilde{\theta}} + \tilde{u} \dot{\tilde{u}} + \frac{\tilde{a} \dot{\tilde{a}}}{r_a}$$

Substitute eqn (2).

$$\dot{V} = e(\gamma - \alpha e) + \gamma (Y\theta - m_y \sin \phi \cos \phi \dot{\gamma} + \tilde{u}_x - \underline{u}_{x_0}) + m_y \sin \phi \cos \phi \dot{\gamma}^2 + \tilde{\theta}^T \Gamma \tilde{\theta} + \tilde{u} \dot{\tilde{u}} + \frac{\tilde{a} \dot{\tilde{a}}}{r_a}$$

We know that

$$\tilde{\theta}^\circ = -\hat{\theta}^\circ \quad \text{and} \quad \tilde{a}^\circ = -\hat{a}^\circ$$

$$\text{as } \tilde{\theta} = \theta - \hat{\theta} \quad \tilde{a} = a - \hat{a}$$

$$\dot{V} = e(\gamma - \alpha e) + \gamma (Y\theta + \tilde{u}_x - \underline{u}_{x_0}) + \tilde{u}_x (\dot{u}_{x_0} + a_x u_x - \underline{u}_x) - \frac{\tilde{\theta}^T \Gamma \tilde{\theta} - \tilde{a} \dot{\tilde{a}}}{r_a}$$

Design $\bar{u}_{xd} = \bar{Y}\bar{\theta} + \bar{B}\bar{r} + \bar{e}$

$$\dot{v} = \alpha e^2 - \alpha r^2 + r_x (\bar{Y}\bar{\theta} + \bar{u}_x - (\bar{Y}\bar{\theta} + \bar{B}\bar{r} + \bar{e})) + \bar{u}_x (\bar{u}_{xd} + \alpha_x u_x - \bar{u}_x) - \bar{\Theta}^T \bar{\Gamma}^T \bar{\theta} - \bar{\alpha} \bar{a}$$

$$\dot{v} = -\alpha e^2 + r \bar{Y}\bar{\theta} - \bar{B}\bar{r}^2 + r \bar{u}_x + \bar{u}_x (\bar{u}_{xd} + \alpha_x u_x - \bar{u}_x) - \bar{\Theta}^T \bar{\Gamma}^T \bar{\theta} - \bar{\alpha} \bar{a}$$

Design $\bar{u}_x = \bar{a}_x u_x + \bar{u}_{dx} + r + \gamma \bar{u}_x$

$$\dot{v} = -\alpha e^2 + r \bar{Y}\bar{\theta} - \bar{B}\bar{r}^2 + r \bar{u}_x + \bar{u}_x (\bar{u}_{xd} + \alpha_x u_x - (\bar{a}_x u_x + \bar{u}_{dx} + r + \gamma \bar{u}_x)) - \bar{\Theta}^T \bar{\Gamma}^T \bar{\theta} - \bar{\alpha} \bar{a}$$

$$\dot{v} = -\alpha e^2 + r \bar{Y}\bar{\theta} - \bar{B}\bar{r}^2 + r \bar{u}_x + \bar{a}_x u_x \bar{u}_x - \bar{u}_x^2 - \bar{\Theta}^T \bar{\Gamma}^T \bar{\theta} - \bar{\alpha} \bar{a}$$

$$\dot{v} = -\alpha e^2 - \bar{B}\bar{r}^2 - \bar{u}_x^2 + r \bar{Y}\bar{\theta} + \bar{a}_x u_x \bar{u}_x - \bar{\Theta}^T \bar{\Gamma}^T \bar{\theta} - \bar{\alpha} \bar{a}$$

Design $\bar{a} = \gamma_a (\bar{u}_x u_x)$

$$\dot{v} = -\alpha e^2 - \bar{B}\bar{r}^2 - \bar{u}_x^2 + r \bar{Y}\bar{\theta} + \bar{a}_x u_x \bar{u}_x - \bar{\Theta}^T \bar{\Gamma}^T \bar{\theta} - \bar{\alpha} (\gamma_a (\bar{a}_x u_x))$$

$$\dot{v} = -\alpha e^2 - \bar{B}\bar{r}^2 - \bar{u}_x^2 + r \bar{Y}\bar{\theta} - \bar{\Theta}^T \bar{\Gamma}^T \bar{\theta}$$

Design $\bar{\theta} = \bar{\Gamma}^T \bar{r} + \bar{\Gamma} K_0 (y^T u - y^T \bar{\theta})$ for $t < T$

$$\dot{v} = -\alpha e^2 - \bar{B}\bar{r}^2 - \bar{u}_x^2 + r \bar{Y}\bar{\theta} - \bar{\Theta}^T \bar{\Gamma}^T (\bar{\Gamma}^T \bar{r} + \bar{\Gamma} K_0 (y^T u - y^T \bar{\theta}))$$

$$\dot{v} = -\alpha e^2 - \bar{B}\bar{r}^2 - \bar{u}_x^2 - \bar{\Theta}^T \bar{\Gamma}^T (\bar{\Gamma} K_0 (y^T \bar{\theta}))$$

$$\dot{v} = -\alpha e^2 - \bar{B}\bar{r}^2 - \bar{u}_x^2 - \bar{\Theta}^T K_0 y^T \bar{\theta}$$

For $t > T$.

$$\text{design } \hat{\theta} = \Gamma Y^T r + \Gamma K_0 (y^T u - y^T y \hat{\theta}) + \Gamma K_{CL} \sum_{i=1}^I y^T(t_i) y(t_i) \hat{\theta}$$

$$v = -\alpha e^2 - \beta r^2 - \gamma \tilde{u}^2 + r Y \hat{\theta} + \hat{\theta}^T \Gamma^T (\Gamma Y^T r + \Gamma K_0 (y^T u - y^T y \hat{\theta}) + \Gamma K_{CL} \sum_{i=1}^I y^T(t_i) y(t_i) \hat{\theta}).$$

$$v = -\alpha e^2 - \beta r^2 - \gamma \tilde{u}^2 + \hat{\theta}^T \Gamma^T (\Gamma K_0 y^T y \hat{\theta} + \Gamma K_{CL} \sum_{i=1}^I y^T(t_i) y(t_i) \hat{\theta})$$

$$v = -\alpha e^2 - \beta r^2 - \gamma \tilde{u}^2 + \hat{\theta}^T (K_0 y^T y \hat{\theta} + \sum_{i=1}^I y^T(t_i) y(t_i) \hat{\theta})$$

For time $t < T$.

$$v = -\alpha e^2 - \beta r^2 - \gamma \tilde{u}^2 + \hat{\theta}^T (K_0 y^T y \hat{\theta})$$

$$v \leq -\alpha e^2 - \beta r^2 - \gamma \tilde{u}^2$$

from Barbalat's Lemma.

$$\int_0^T v_j(\xi(t), \theta, t) dt \leq - \int_0^T (\alpha e^2(\theta) + \beta r^2(\theta) + \gamma \tilde{u}^2(\theta)) dt$$

$$v(\xi(0), 0) - v(\xi(T), T) \geq \int_0^T (\alpha e^2(\theta) + \beta r^2(\theta) + \gamma \tilde{u}^2(\theta)) dt.$$

Since $v(0), v(t) \in L_\infty \Rightarrow e, r, \tilde{u} \in L_2$.

~~$e, r \in L_\infty \Rightarrow e \in L_\infty \quad (r = e + de)$~~

~~e is Uniformly continuous.~~

~~$e, e^*, x_j, \dot{x}_j \in L_\infty \Rightarrow x, x^* \in L_\infty$~~

~~$x, \dot{x}, \ddot{x}_j, e, \dot{e}, \phi \in L_\infty \Rightarrow Y \in L_\infty$~~

~~$\hat{\theta} \in L_\infty \Rightarrow \hat{\theta} \in L_\infty$~~

~~$e, r, Y, \hat{\theta} \in L_\infty \Rightarrow \alpha \in L_\infty$~~

$$v \leq -\alpha e^2 - \beta r^2 - \gamma \tilde{u}^2$$

Therefore, all we can say about the system at $t < T$ is that it is locally stable.

For $t > T$

$$\dot{v} = -\alpha e^2 - \beta r^2 - \gamma \tilde{u}^2 + \tilde{\Theta} \left(k_0 y^T y + k_{CL} \sum_{i=1}^i y^T(t_i) y(t_i) \right) \tilde{\Theta}$$

$$V \leq \alpha c^2 - \beta r^2 - \gamma \tilde{u}^2 + \tilde{\Theta}\left(K_d \sum_{i=1}^j y^T(t_i) y(t_i)\right) \tilde{\Theta}$$

Using Barballet's Lemma.

$$\int_0^t r(\varrho(\theta), \theta), \theta) d\theta \leq - \int_0^t (\alpha e^2(\theta) + \beta \gamma^2(\theta) + \sqrt{\mu^2(\theta)} \alpha \\ + \sum_{i=1}^n y^i(t_i) y(t_i) \bar{\theta}^2(\theta)) d\theta$$

$$V(E(0), 0) - V(E(t), t) \geq \int_0^t (\lambda e^2(\theta) + \beta y^2(\theta) + \gamma \tilde{u}^2(\theta) + \sum_{j=1}^J y^T(t_j) y(t_j) \tilde{e}^2(\theta)) d\theta.$$

since $v(0), v(t) \in L_2 \Rightarrow e, x, u \in L_2$

$$c, r \in L_\infty \Rightarrow e^r \in L_\infty \quad (\because r = c + \lambda e).$$

e is uniformly continuous

$$c, c^*, x_0, \dot{x}_0 \in \ell_\infty, \Rightarrow x, \dot{x} \in \ell_\infty$$

$$\phi, \dot{\phi}, x, \dot{x}_0, \ddot{x}_0, \ddot{\phi} \in L_\infty \Rightarrow y \in L_\infty$$

$$c, r, Y, \tilde{\theta} \in L_0 \Rightarrow \tilde{a} \in L_0.$$

τ , μ , Θ are all uniformly continuous.

Therefore, from Barbalat's Lemma we can prove global asymptotic tracking (GAT).

(5)

For 2nd set of dynamics

$$m\ell^2 \ddot{\phi} = -c_\phi \dot{\phi} - mg \sin(\phi) - m\ell \cos(\phi) \ddot{x} + u_\phi$$

$$u_\phi = -\alpha \dot{u}_\phi + \tilde{u}_\phi$$

error tracking.

$$e_\phi = \dot{\phi}_d - \dot{\phi}$$

$$\dot{e}_\phi = \ddot{\phi}_d - \ddot{\phi}$$

$$\ddot{e}_\phi = \ddot{\phi}_d - \ddot{\phi}$$

multiply both sides by $m\ell^2$.

$$m\ell^2 \ddot{e}_\phi = m\ell^2 \ddot{\phi}_d - m\ell^2 \ddot{\phi} \quad \text{--- (3)}$$

Reference tracking error.

$$r = e + \alpha e.$$

$$r' = \dot{e} + \alpha \dot{e}$$

multiplying both sides by $m\ell^2$.

$$m\ell^2 r' = \alpha m\ell^2 \dot{e} + \alpha m\ell^2 \dot{e}$$

substituting eqn (3)

$$m\ell^2 \dot{r}' = m\ell^2 \dot{\phi}_d - m\ell^2 \ddot{\phi} + \alpha m\ell^2 \dot{e}$$

$$m\ell^2 \dot{r}' = m\ell^2 \dot{\phi}_d - (-c_\phi \dot{\phi} - mg \sin \phi - m\ell \cos \phi \ddot{x} + u_\phi - \tilde{u}_\phi + \tilde{u}_\phi) + \alpha m\ell^2 \dot{e}$$

$$m\ell^2 \dot{r}' = m\ell^2 \dot{\phi}_d + c_\phi \dot{\phi} + mg \sin \phi + m\ell \cos \phi \ddot{x} + \tilde{u}_\phi - u_\phi + \alpha m\ell^2 \dot{e}$$

$$m\ell^2 \dot{r}' = [(g \sin \phi + \cos \phi \ddot{x}) \quad (\dot{\phi}_d + \alpha \dot{e}_\phi) \quad \dot{\phi}] \begin{bmatrix} m\ell \\ m\ell^2 \\ c_\phi \end{bmatrix} - u_\phi + \tilde{u}_\phi$$

(4)

$$\text{Let } \mathbf{e}_j = \begin{pmatrix} e \\ r \\ \tilde{\theta} \\ \tilde{u} \\ \tilde{a} \end{pmatrix}$$

Lyapunov candidate.

$$V = \frac{1}{2} e^2 + \frac{1}{2} m \rho l^2 r^2 + \frac{1}{2} \tilde{\theta}^T \Gamma \tilde{\theta} + \frac{1}{2} \tilde{u}^2 + \frac{1}{2} \tilde{a}^2.$$

$$V^* = e^* e + \frac{1}{2} (m \rho l^2) r^* r + \tilde{\theta}^T \Gamma \tilde{\theta}^* + \tilde{u} \tilde{u}^* + \frac{\tilde{a} \tilde{a}^*}{\gamma a}.$$

$$\text{we know } \tilde{M}_{ij} = M_{ij} - M_p \Rightarrow \tilde{M}^* = M^* - M$$

$$\dot{V} = e(r - \alpha e) + \tilde{u}(M_j + a_p u - M) - \tilde{\theta}^T \Gamma \tilde{\theta}^* + (m \rho l^2) \dot{r} r + \frac{\tilde{a} \tilde{a}^*}{\gamma a}.$$

Substitute eqn ④.

$$\begin{aligned} \dot{V} &= e(r - \alpha e) + \tilde{u}(M_j + a_p u - M) - \tilde{\theta}^T \Gamma \tilde{\theta}^* - \frac{\tilde{a} \tilde{a}^*}{\gamma a} \\ &\quad + r(Y\theta - M_{jj} + \tilde{M}_j) \end{aligned}$$

$$\text{Design } M_{jj} = Y\theta + Br + c.$$

$$V^* = e(r - \alpha e) + \tilde{u}(M_j + a_p u - M) - \tilde{\theta}^T \Gamma \tilde{\theta}^* + r(Y\theta + \tilde{M}_j - (Y\theta + Br + c)) - \frac{\tilde{a} \tilde{a}^*}{\gamma a}.$$

$$\dot{V} = -\alpha e^2 + \tilde{u}(M_j + a_p u - M) - \tilde{\theta}^T \Gamma \tilde{\theta}^* - rY\theta + \tilde{u} \frac{\gamma a}{\gamma a} - Br^2 - \frac{\tilde{a} \tilde{a}^*}{\gamma a}.$$

$$V^* = -\alpha e^2 + \tilde{u}(M_j + a_p u - M) - \tilde{\theta}^T \Gamma \tilde{\theta}^* - rY\theta + \tilde{u} \gamma a - Br^2 - \frac{\tilde{a} \tilde{a}^*}{\gamma a}.$$

$$\text{Design } M = \hat{a}_p u + M_j + r + \gamma \tilde{u}.$$

$$V^* = -\alpha e^2 + \tilde{u}(M_j + a_p u - (\hat{a}_p u + M_j + r + \gamma \tilde{u})) - \tilde{\theta}^T \Gamma \tilde{\theta}^* - rY\theta - \tilde{u} r - Br^2 - \frac{\tilde{a} \tilde{a}^*}{\gamma a}.$$

$$V^* = -\alpha e^2 + \tilde{u} \tilde{u} - \gamma \tilde{u}^2 - Br^2 - rY\theta - \tilde{\theta}^T \Gamma \tilde{\theta}^* - \frac{\tilde{a} \tilde{a}^*}{\gamma a}.$$

(7)

$$\text{Design } \hat{a}^* = Y_a \bar{u} \bar{u}$$

$$V^* = -\alpha e^2 + \hat{a} \bar{u} \bar{u} - \gamma \bar{u}^2 - \beta r^2 - \gamma Y \bar{\theta} - \bar{\theta} \Gamma^T \bar{\theta} - \frac{\hat{a}}{Y_a} (\bar{u} \bar{u})$$

$$V^* = -\alpha e^2 - \gamma \bar{u}^2 - \beta r^2 - \gamma Y \bar{\theta} - \bar{\theta} \Gamma^T \bar{\theta}$$

$$\text{Design } \hat{\theta}^* = \Gamma Y^T \bar{r} + \Gamma K_0 (y^T \bar{u} - y^T \bar{y} \hat{\theta}) \quad \boxed{\text{for } t < T}$$

$$V^* = -\alpha e^2 - \beta r^2 - \gamma \bar{u}^2 + \gamma Y \bar{\theta} - \bar{\theta} \Gamma^T (\Gamma Y^T \bar{r} + \Gamma K_0 (y^T \bar{u} - y^T \bar{y} \hat{\theta}))$$

$$V^* = -\alpha e^2 - \beta r^2 - \gamma \bar{u}^2 - \bar{\theta} \Gamma^T (\Gamma K_0 (y^T \bar{y} \hat{\theta})).$$

$$\text{Design } \hat{\theta}^* = \Gamma Y^T \bar{r} + \Gamma K_0 (y^T \bar{u} - y^T \bar{y} \hat{\theta}) + \Gamma K_a \sum_{i=1}^j y^T(t_i) y(t_i) \bar{\theta} \quad \boxed{\text{for } t > T}$$

$$V^* = -\alpha e^2 - \beta r^2 - \gamma \bar{u}^2 + \bar{\theta} \Gamma^T (\Gamma Y^T \bar{r} + \Gamma K_0 (y^T \bar{u} - y^T \bar{y} \hat{\theta}) + \Gamma K_a \sum_{i=1}^j y^T(t_i) y(t_i) \bar{\theta}).$$

$$V^* = -\alpha e^2 - \beta r^2 - \gamma \bar{u}^2 + \bar{\theta} (K_0 y^T \bar{y} \hat{\theta} + K_a \sum_{i=1}^j y^T(t_i) y(t_i)) \bar{\theta}$$

For $t < T$

$$V^* = -\alpha e^2 - \beta r^2 - \gamma \bar{u}^2 - \bar{\theta} K_0 y^T \bar{y} \hat{\theta}.$$

So,

$$V^* \leq -\alpha e^2 - \beta r^2 - \gamma \bar{u}^2$$

all we know is PSD.

Therefore, all we can prove is local stability for $t < T$.

For $t > T$

$$V^* = -\alpha e^2 - \beta r^2 - \gamma \bar{u}^2 + \bar{\theta} (K_0 y^T \bar{y} \hat{\theta} + K_a \sum_{i=1}^j y^T(t_i) y(t_i)) \bar{\theta}$$

all we know is still PSD

not PSD but PD

So,

$$y' \leq -\alpha e^2 - \beta r^2 - \gamma \tilde{u}^2 + \tilde{\theta} (K_{CL} \sum_{j=1}^J y^*(t_j) y(t_j)) \tilde{\theta}.$$

Using Barbalat's lemma.

$$\int_0^t r(\varepsilon(s), 0), 0), 0) d\theta \leq - \int_0^t [\alpha e^2(s) + \beta r^2(s) + \gamma \tilde{u}^2(s) + \sum_{j=1}^J y^*(t_j) y(t_j)] \tilde{\theta}^2(s) ds.$$

$$V(\varepsilon(0), 0) - V(\varepsilon(t), t) \geq \int_0^t [\alpha e^2(s) + \beta r^2(s) + \gamma \tilde{u}^2(s) + \sum_{j=1}^J y^*(t_j) y(t_j)] \tilde{\theta}^2(s) ds.$$

Hence,

$$r(0), r(t) \in L_\infty \Rightarrow e, r, \tilde{u}, \tilde{\theta} \in L_2.$$

$$e, r \in L_\infty \Rightarrow e^\circ \in L_\infty (\because r = e^\circ + \alpha e).$$

e is uniformly continuous.

$$e, e^\circ, x_0, \dot{x}_0 \in L_\infty \Rightarrow x, \dot{x} \in L_\infty.$$

$$\phi, \dot{\phi}, x, \dot{x}, \dot{x}_0, \dot{\phi}_0, e, \dot{e} \in L_\infty \Rightarrow y \in L_\infty.$$

$$e \in L_\infty \Rightarrow \tilde{\theta} \in L_\infty$$

$$e, r, Y, \tilde{\theta} \in L_\infty \Rightarrow \tilde{u} \in L_\infty.$$

$r, \tilde{u}, \tilde{\theta}$, are all UC.

Therefore, from Barbalat's lemma we can prove global Asymptotic tracking (GAT).

(b) (ii) Used concurrent learning and backstepping to design my controller as suggested theoretically analysis, I was able to achieve GAT using, concurrent learning term "K_u" designed in my theta-hat-dot, I was able to retain the theta term in my analysis which enabled me to prove this GAT using Barbalat's lemma.

A different design term K_{cl} was added once enough data was collected to attain sufficient excitation.

$$\text{ie } \sum_{i=1}^j y^T(t_i) y(t_i) > \lambda$$

for a small enough λ value.