3D FDTD Analysis of TE_{10} Mode Propagation in X-Band Rectangular Waveguides

Samuel J. Wyss†
†School of Nuclear Engineering
Purdue University
West Lafayette, Indiana 47907
E-mail: wysss@purdue.edu

***Abstract*—Write your abstract text here.**

I. Introduction

To type basic text, you just type it into the TeX document like this. If you want to do different kinds of formatting you need to use the appropriate command, such as *italics* and **bold**. You can reference different parts of the document such as Section I or Section **??**. Depending on the TeX editor you are using, you may need to keep your different sub-files open for the editor to recognize the cross-reference labels you have declared in different sub-files.

To cite a reference, you just use the following command [1]. You can also cite multiple references at once like this [1]–[3]. The TeX compiler will automatically order your reference list for you based on the order that you call them in the document you are generating. If you change the document substantially and the references aren't getting automatically reordered, you may need to delete the .bbl file that gets generated when you compile to force the compiler to regenerate the .bbl file from scratch.

II. Mathematical Model

To model an infinitely long 3D waveguide *in silico*, the simulation domain must be divided up into regions where specific mathematical relations hold. In this particular system there are three such regions (1) PEC surrounded dielectric, (2) Total Field / Scattered Field (TF/SF) 1-way source, and (3) Mur Absorbing Boundary Condition (Mur ABC). Regions (2)-(3) are essential as modeling an A high level diagram of a PEC bordered rectangular waveguide can be found in Fig. 1(a) and a $\hat{y}$ sliced model where said relations hold can be found in Fig. 1(b). These governing relations are then discretized to formulate time-stepping formulas which allow the system to evolve transiently.

A. Model Formulation

1) PEC Surrounded Dielectric: As outlined in Fig. 1(b) the vast majority of the simulation domain is composed of a PEC enclosed dielectric, the governing equations of which are Ampère's and Faraday's Laws respectively. In differential form, these equations take the form

$$\nabla \times \mathbf{H} = \frac{\partial \mathbf{D}}{\partial t} + \mathbf{J} \tag{1}$$

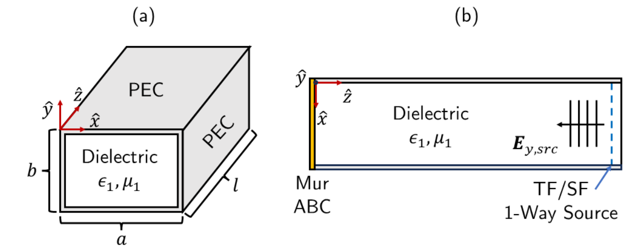

Fig. 1: Diagrams of (a) High-Level PEC Rectangular Waveguide (b) $\hat{y}$-Sliced Model with Labeled Regions

and

$$\nabla \times \mathbf{E} = -\frac{\partial \mathbf{B}}{\partial t} - \mathbf{M} \tag{2}$$

where $\mathbf{E}$ is the electric field, $\mathbf{D}$ is the electric flux density, $\mathbf{H}$ is the electric field, $\mathbf{B}$ is the magnetic flux density, $\mathbf{J}$ is the free electric current density, and $\mathbf{M}$ is the fictitious free magnetic current density.

For simplicity, this analysis focuses on diagonally-isotropic, time-invariant, and non-dispersive dielectrics within the waveguide. Under these stipulations, each set of fields and flux densities, ($\mathbf{E}$, $\mathbf{D}$), ($\mathbf{H}$, $\mathbf{B}$), can be related using the following constitutive relations

$$\mathbf{D} = \epsilon\mathbf{E}, \mathbf{B} = \mu\mathbf{H} \tag{3}$$

with ϵ and μ as the permittivity and permeability of the dielectric respectively.

In this analysis, no fictitious magnetic conductors will be considered as they are not pertinent, thus $\mathbf{M} = 0$. The free electric current density is treated as a linear superposition of Ohmic conduction $\mathbf{J}_{Ohm} = \sigma\mathbf{E}$ and and a source term $\mathbf{J}_{src}$

$$\mathbf{J} = \sigma\mathbf{E} \tag{4}$$

where σ is the diagonally-isotropic, time-invariant dielectric conductivity. In the described system, the inclusion of both a source current density and ohmic current density is not necessary as the wave is assumed to already be propagating in the waveguide from the TF/SF source, and Ohmic losses result in evanescent wave propagation along the waveguide's length. Despite this, these current density terms will be included in the governing set of equations for completeness. The full set of governing equations for waves propogating within the dielectric are as follows

$$\nabla \times \mathbf{H} = \epsilon \frac{\partial \mathbf{E}}{\partial t} + \sigma \mathbf{E} + \mathbf{J}_{src} \tag{5}$$

2) TF/SF 1-way Source: To inject energy into this system, a TF/SF scheme is used. For this particular application, the E_y field is used as a wave-port source (**TODO: EXPAND ME**). All total E_y field values are considered as a superposition of source field $E_{y,src}$ and that of a scattered field $E_{y,scat}$ as

$$E_y = E_{y,src} + E_{y,scat}. \tag{10}$$

https://www.tandfonline.com/doi/epdf/10.1163/156939300X00491?needAccess=true
ehere $E_{y,src}$ is injected into the system and the sca
Satisfying boundary conditoons

III. Numerical Results

A. Verification and Validation

1) Propogation Patterns:

2) Cutoff Frequency:

3) Dielectric Frequency Compression:

B. Case Study

IV. Conclusion

Overall, this is just a very simple document to get you going in LaTeX. There is a bit of a learning curve, but in my experience it is incredibly worthwhile for every graduate student to learn how to use this tool. There are still some times where I use Microsoft Word because it will be easier, but this is often very infrequent. At this point, I cannot imagine trying to write a journal paper within anything but LaTeX because of how much easier it is to control formatting, produce great looking equations, automatically handle cross-referencing and reference lists, etc.

V. Appendix

A. Code Structure

References

[1] J.-M. Jin, *Theory and Computation of Electromagnetic Fields*. John Wiley & Sons, 2011.

$$\nabla \times \mathbf{E} = -\mu \frac{\partial \mathbf{H}}{\partial t} \tag{6}$$

.

Each of these 3D vector equations can be broken down into $\hat{x}$, $\hat{y}$, and $\hat{z}$ component equations; the $\hat{y}$ components of $\mathbf{E}$ and $\mathbf{H}$ in Eqs. (5)-(6) are

$$\frac{\partial H_x}{\partial z} - \frac{\partial H_z}{\partial x} = \epsilon \frac{\partial E_y}{\partial t} + \sigma E_y + J_{y,src} \tag{7}$$

and

$$\frac{\partial E_x}{\partial z} - \frac{\partial E_z}{\partial x} = -\mu \frac{\partial H_y}{\partial t} \tag{8}$$

respectively.

These scalar equations are valid for all locations within the dielectric region excluding those inside of the PEC at which there is a Dirichlet boundary condition

$$E_x = E_y = 0. \tag{9}$$

[2] D. M. Pozar, *Microwave Engineering*. John Wiley & Sons, 2011.

[3] J.-M. Jin, *The Finite Element Method in Electromagnetics*. John Wiley & Sons, 2015.