







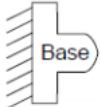
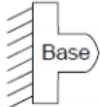
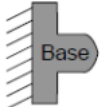
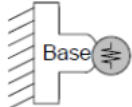
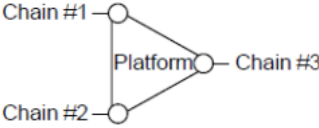
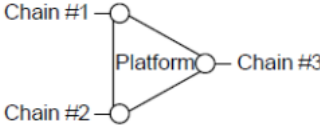
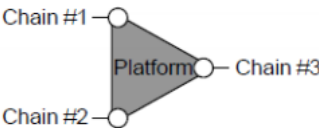
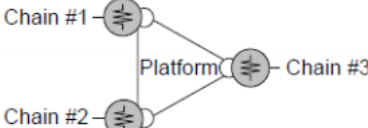
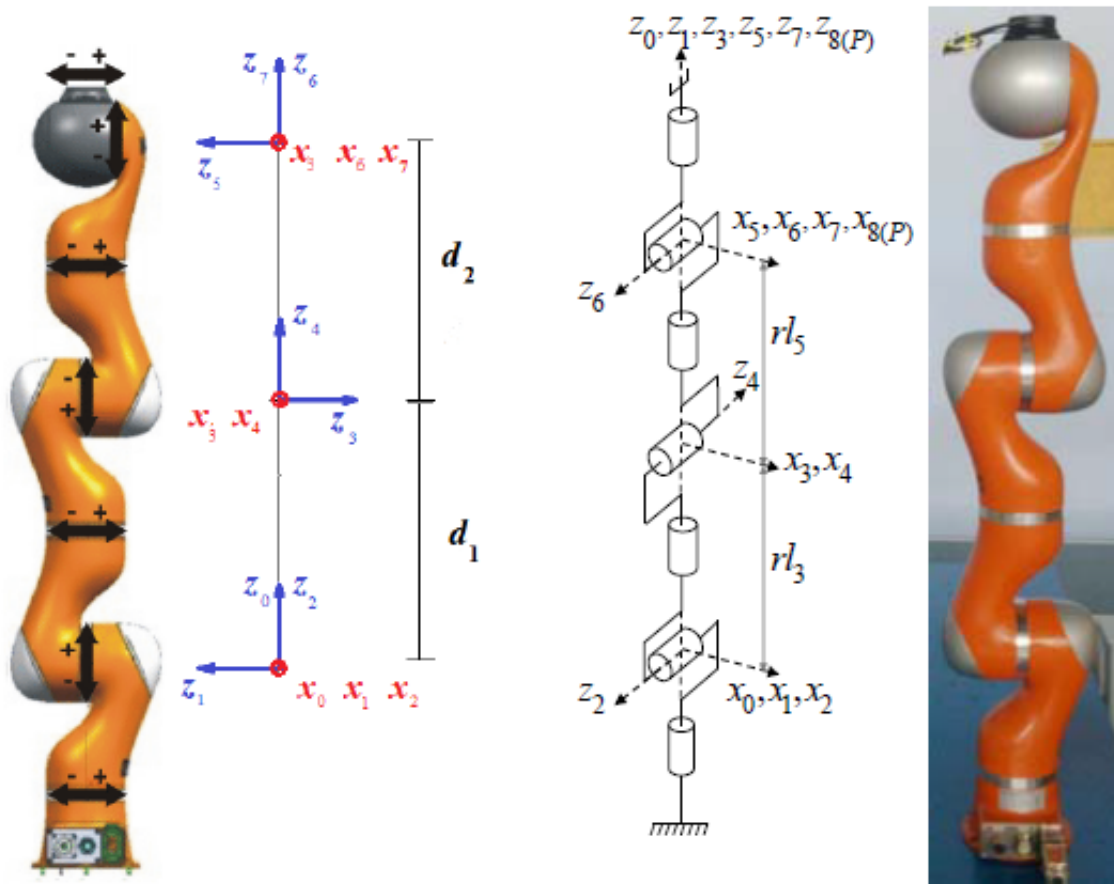


## VJM model of KUKA\_iiwa robot manipulator:

Manipulator components		VJM-model elements	
Component	Graphical presentation	Components	Graphical presentation
Actuated joint		Actuated joint + 6 d.o.f. virtual spring	
Passive joint (non-actuated)		Passive joint	
Rigid link		Rigid link	
Elastic link		Rigid link + 6 d.o.f. virtual spring	
Rigid base		Rigid base	
Elastic base		Rigid base + 6 d.o.f. virtual spring	
Rigid platform		Rigid platform	
Elastic platform		Rigid platform + set of 6 d.o.f. virtual spring (for each chain)	



$$\mathbf{K} = \begin{bmatrix} \frac{E \cdot S}{L} & 0 & 0 & 0 & 0 & 0 \\ 0 & \frac{12 \cdot E \cdot I_z}{L^3} & 0 & 0 & 0 & \frac{-6 \cdot E \cdot I_z}{L^2} \\ 0 & 0 & \frac{12 \cdot E \cdot I_y}{L^3} & 0 & \frac{6 \cdot E \cdot I_y}{L^2} & 0 \\ 0 & 0 & 0 & \frac{G \cdot J}{L} & 0 & 0 \\ 0 & 0 & \frac{6 \cdot E \cdot I_y}{L^2} & 0 & \frac{4 \cdot E \cdot I_y}{L} & 0 \\ 0 & \frac{-6 \cdot E \cdot I_z}{L^2} & 0 & 0 & 0 & \frac{4 \cdot E \cdot I_z}{L} \end{bmatrix}$$

$$\begin{bmatrix} \mathbf{0} & \mathbf{J}_\theta & \mathbf{J}_q \\ \mathbf{J}_\theta^T & -\mathbf{K}_\theta & \mathbf{0} \\ \mathbf{J}_q^T & \mathbf{0} & \mathbf{0} \end{bmatrix} \cdot \begin{bmatrix} \mathbf{F} \\ \boldsymbol{\theta} \\ \Delta \mathbf{q} \end{bmatrix} = \begin{bmatrix} \Delta \mathbf{t} \\ \mathbf{0} \\ \mathbf{0} \end{bmatrix}$$

$$\mathbf{K}_C = \mathbf{K}_C^0 - \mathbf{K}_C^0 \cdot \mathbf{J}_q \cdot \mathbf{K}_{Cq}$$

where  $\mathbf{K}_C^0 = (\mathbf{J}_\theta \cdot \mathbf{K}_\theta^{-1} \cdot \mathbf{J}_\theta^T)^{-1}$  is  
classical Cartesian stiffness matrix

The extended model of the KUKA manipulator:

$$\theta_7 \cdot R_{x,q_2} \cdot R_{x,\theta_8} \cdot T_{z,d_2} \cdot H_{3D,\theta_{14}} \cdot R_{z,q_3} \cdot R_{z,\theta_{15}} \cdot T_{z,d_3} \cdot H_{3D,\theta_{21}} \cdot R_{x,q_4} \cdot R_{x,\theta_{22}} \cdot T_{z,d_4} \cdot H_{3D,\theta_{28}} \cdot R_{z,q_5} \cdot R_{z,\theta_{29}} \cdot T_{z,d_5} \cdot H_{3D,\theta_{35}} \cdot R_{x,q_6} \cdot R_{x,\theta_{36}} \cdot T_{z,d_6}$$

with:  $H_{3D} = T_x \cdot T_y \cdot T_z \cdot R_x \cdot R_y \cdot R_z$

```
clear all, clc
Tbase = eye(4);
Ttool = eye(4);

%% links stiffness modeling
% Actuator stiff 1
k0 = 1e6;

%LINK1
%material and shape parameters
E = 70 *10e9; %Young's modulus
G = 25.5*10e9; %shear modulus
robot.d(1) = 10*10e-3;
robot.L(1) = 0.21;

%for cylinder
S = pi*robot.d(1)^2/4;
Iy = pi*robot.d(1)^4/64;
Iz = pi*robot.d(1)^4/64;
J = Iy + Iz;

k1 = [E*S/robot.L(1) 0 0 0 0 0;
0 12*E*Iz/robot.L(1)^3 0 0 0 6*E*Iy/robot.L(1)^2;
0 0 12*E*Iy/robot.L(1)^3 0 -6*E*Iy/robot.L(1)^2 0;
0 0 0 G*J/robot.L(1) 0 0;
0 0 -6*E*Iy/robot.L(1)^2 0 4*E*Iy/robot.L(1)^2 0;
0 6*E*Iy/robot.L(1)^2 0 0 0 4*E*Iz/robot.L(1)^2];

% Actuator stiff 2
k2 = 1e6;

%LINK2
%material and shape parameters
robot.d(2) = 10*10e-3;
robot.L(2) = 0.21;
S = pi*robot.d(2)^2/4;

k3 = [E*S/robot.L(2) 0 0 0 0 0;
0 12*E*Iz/robot.L(2)^3 0 0 0 6*E*Iy/robot.L(2)^2;
0 0 12*E*Iy/robot.L(2)^3 0 -6*E*Iy/robot.L(2)^2 0;
0 0 0 G*J/robot.L(2) 0 0;
0 0 -6*E*Iy/robot.L(2)^2 0 4*E*Iy/robot.L(2)^2 0;
0 6*E*Iy/robot.L(2)^2 0 0 0 4*E*Iz/robot.L(2)^2];

% Actuator stiff 3
k4 = 1e6;

%LINK3
%material and shape parameters
robot.d(3) = 10*10e-3;
robot.L(3) = 0.21;
S = pi*robot.d(3)^2/4;
```

```

k5 = [E*S/robot.L(3) 0 0 0 0 0;
0 12*E*Iz/robot.L(3)^3 0 0 0 6*E*Iy/robot.L(3)^2;
0 0 12*E*Iy/robot.L(3)^3 0 -6*E*Iy/robot.L(3)^2 0;
0 0 0 G*J/robot.L(3) 0 0;
0 0 -6*E*Iy/robot.L(3)^2 0 4*E*Iy/robot.L(3) 0;
0 6*E*Iy/robot.L(3)^2 0 0 0 4*E*Iz/robot.L(3)^2];

```

% Actuator stiff 4

```
k6 = 1e6;
```

%LINK4

%material and shape parameters

```
robot.d(4) = 10*10e-3;
```

```
robot.L(4) = 0.2;
```

```
S = pi*robot.d(4)^2/4;
```

```

k7 = [E*S/robot.L(4) 0 0 0 0 0;
0 12*E*Iz/robot.L(4)^3 0 0 0 6*E*Iy/robot.L(4)^2;
0 0 12*E*Iy/robot.L(4)^3 0 -6*E*Iy/robot.L(4)^2 0;
0 0 0 G*J/robot.L(4) 0 0;
0 0 -6*E*Iy/robot.L(4)^2 0 4*E*Iy/robot.L(4) 0;
0 6*E*Iy/robot.L(4)^2 0 0 0 4*E*Iz/robot.L(4)^2];

```

% Actuator stiff 5

```
k8 = 1e6;
```

%LINK5

%material and shape parameters

```
robot.d(5) = 10*10e-3;
```

```
robot.L(5) = 0.2;
```

```
S = pi*robot.d(5)^2/4;
```

```

k9 = [E*S/robot.L(5) 0 0 0 0 0;
0 12*E*Iz/robot.L(5)^3 0 0 0 6*E*Iy/robot.L(5)^2;
0 0 12*E*Iy/robot.L(5)^3 0 -6*E*Iy/robot.L(5)^2 0;
0 0 0 G*J/robot.L(5) 0 0;
0 0 -6*E*Iy/robot.L(5)^2 0 4*E*Iy/robot.L(5) 0;
0 6*E*Iy/robot.L(5)^2 0 0 0 4*E*Iz/robot.L(5)^2];

```

% Actuator stiff 6

```
k10 = 1e6;
```

%LINK6

%material and shape parameters

```
robot.d(6) = 10*10e-3;
```

```
robot.L(6) = 0.126;
```

```
S = pi*robot.d(6)^2/4;
```

```

k11 = [E*S/robot.L(6) 0 0 0 0 0;
0 12*E*Iz/robot.L(6)^3 0 0 0 6*E*Iy/robot.L(6)^2;
0 0 12*E*Iy/robot.L(6)^3 0 -6*E*Iy/robot.L(6)^2 0;
0 0 0 G*J/robot.L(6) 0 0;
0 0 -6*E*Iy/robot.L(6)^2 0 4*E*Iy/robot.L(6) 0;
0 6*E*Iy/robot.L(6)^2 0 0 0 4*E*Iz/robot.L(6)^2];

```

% Actuator stiff 7

```
k12 = 1e6;
```

%LINK7 (tool)

%material and shape parameters

```

robot.d(7) = 10*10e-3;
robot.L(7) = 0.05;
S = pi*robot.d(7)^2/4;

k13 = [E*S/robot.L(7) 0 0 0 0 0 0;
0 12*E*Iz/robot.L(7)^3 0 0 0 6*E*Iy/robot.L(7)^3;
0 0 12*E*Iy/robot.L(7)^3 0 -6*E*Iy/robot.L(7)^2 0;
0 0 0 G*J/robot.L(7) 0 0;
0 0 -6*E*Iy/robot.L(7)^2 0 4*E*Iy/robot.L(7)^3 0;
0 6*E*Iy/robot.L(7)^2 0 0 0 4*E*Iz/robot.L(7)^3];

```

```
% K theta matrixshow
```

```

Kt = [k0 zeros(1,42) zeros(1,6)
zeros(6,1) k1 zeros(6,36) zeros(6,6)
zeros(1,1) zeros(1,6) k2 zeros(1,35) zeros(1,6)
zeros(6,1) zeros(6,6) zeros(6,1) k3 zeros(6,29) zeros(6,6)
zeros(1,1) zeros(1,6) zeros(1,1) zeros(1,6) k4 zeros(1,28) zeros(1,6)
zeros(6,1) zeros(6,6) zeros(6,1) zeros(6,6) zeros(6,1) k5 zeros(6,22) zeros(6,6)
zeros(1,1) zeros(1,6) zeros(1,1) zeros(1,6) zeros(1,1) zeros(1,6) k6 zeros(1,21) zeros(1,6)
zeros(6,1) zeros(6,6) zeros(6,1) zeros(6,6) zeros(6,1) zeros(6,6) zeros(6,1) k7 zeros(6,15) zeros(6,6)
zeros(1,1) zeros(1,6) zeros(1,1) zeros(1,6) zeros(1,1) zeros(1,6) zeros(1,1) zeros(1,6) k8 zeros(1,14) zeros(1,6)
zeros(6,1) zeros(6,6) zeros(6,1) zeros(6,6) zeros(6,1) zeros(6,6) zeros(6,1) zeros(6,6) zeros(6,1) k9 zeros(6,8) zeros(6,6)
zeros(1,1) zeros(1,6) zeros(1,1) zeros(1,6) zeros(1,1) zeros(1,6) zeros(1,1) zeros(1,6) zeros(1,1) zeros(1,6) k10 zeros(1,7) zeros(1,6)
zeros(6,1) zeros(6,6) zeros(6,1) zeros(6,6) zeros(6,1) zeros(6,6) zeros(6,1) zeros(6,6) zeros(6,1) zeros(6,6) zeros(6,1) k11 zeros(6,6) zeros(6,6)
zeros(1,1) zeros(1,6) zeros(1,1) zeros(1,6) zeros(1,1) zeros(1,6) zeros(1,1) zeros(1,6) zeros(1,1) zeros(1,6) zeros(1,1) zeros(1,6) k12 zeros(1,6) zeros(1,6)
zeros(6,1) zeros(6,6) zeros(6,1) zeros(6,6) zeros(6,1) zeros(6,6) zeros(6,1) zeros(6,6) zeros(6,1) zeros(6,6) zeros(6,1) zeros(6,6) k13 zeros(6,6) zeros(6,6)];

```

```
Kt
```

```
Kt = 49x49 double
```

```

1.0e+10 * ...
0.0001 0 0 0 0 0 0 0
0 2.6180 0 0 0 0 0 0
0 0 0.4452 0 0 0 0.0467 0
0 0 0 0.4452 0 -0.0467 0 0
0 0 0 0 0.0012 0 0 0
0 0 0 -0.0467 0 0.0065 0 0
0 0 0.0467 0 0 0 0.0065 0
0 0 0 0 0 0 0 0.0001
0 0 0 0 0 0 0 0
0 0 0 0 0 0 0 0
:
:

```

```

%% lengths of links used in Forward kinematics, the thetas deviations and the configuration a
d = [robot.L(1), robot.L(2), robot.L(3), robot.L(4), robot.L(5), robot.L(6), robot.L(7)];
t= zeros(1, 49);
q= [ 0 0 0 0 0 0 0]

```

```
q = 1x7 double
```

```
0 0 0 0 0 0 0
```

```
% Jacobian and final result for Kc
```

```

Jth = Jt(Tbase,Ttool,q,t,d);
Kc =inv(Jth*inv(Kt)*Jth')

```

```
Kc = 6x6 double
```

```

1.0e+08 *
0.2702      0    -0.3107      0    -0.1074      0
0      0.0253      0    0.0145      0    0.0002
-0.3107      0    8.4001      0    -0.6457      0
0      0.0145      0    0.0112      0    0.0001
-0.1074      0    -0.6457      0    0.1447      0
0      0.0002      0    0.0001      0    0.0023

```

```

F =[1000; 1000; 0; 0; 0; 0];
% showing the deflection map
showDeflection(F, 'VJM')

```

