

Time:

1hr

Questions

1. Attempt all questions

2. Make suitable assumption if required

MM:16 Course  
Outcome

Q.1

8M CO1

- (i) Find the Norton equivalent with respect to terminals a-b in the circuit shown in Fig. 1 below. (2M)

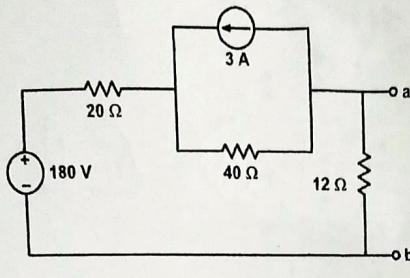


Fig. 1

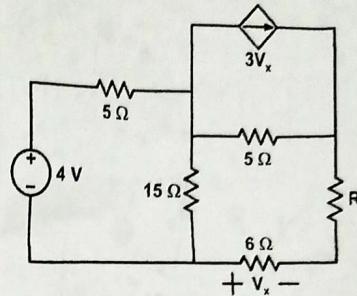
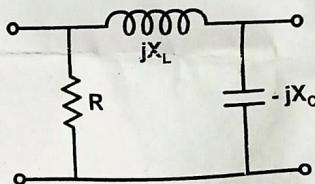


Fig. 2

- (ii) For the circuit shown in Fig. 2 above, determine the maximum power delivered to the variable resistor R. (3M)

- (iii) Determine the z-parameters of the network shown below. (3M)



8M CO2

Q.2

- (i) Develop the state equations for the following differential equation given below. (2M)

$$\frac{d^2y(t)}{dt^2} + \frac{4dy(t)}{dt} + 3y(t) = z(t)$$

- (ii) Develop the state equations for the circuit shown in Fig. 1 below. (3M)

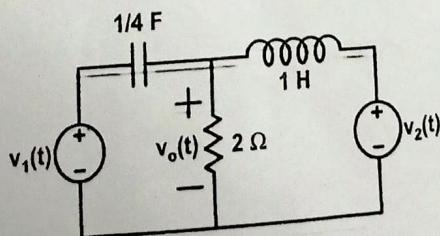


Fig. 1

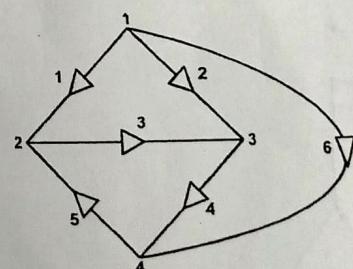


Fig. 2

- (iii) Find the incidence matrix and cut-set matrix for the given graph in Fig. 2 above. (3M)

Time:  
1hr1<sup>st</sup> Sessional Test (September 2023)MM:16 Course  
Outcome

Questions

1. Attempt all questions

2. Make suitable assumption if required

Q.1

- (i) Calculate
- $v$
- and
- $i_x$
- in the circuit of Fig. 1 shown below. (2M)

8M CO1

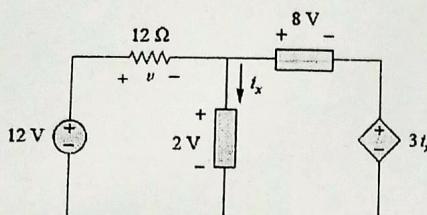


Fig. 1

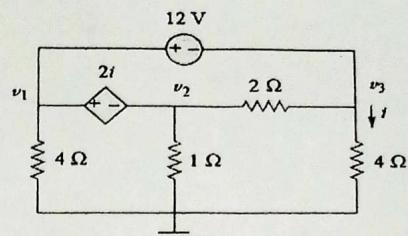


Fig. 2

- (ii) For the circuit shown in Fig. 2 above, find
- $v_1$
- ,
- $v_2$
- , and
- $v_3$
- using nodal analysis. (3M)

- (iii) For the circuit shown in Fig. below, find
- $V_o$
- (3M)

Q.2

8M CO2

- (i) A system has the transfer function

$$H(s) = \frac{s}{(s+1)(s+2)}$$

- (a) Find the impulse response of the system. (1M)

- (b) Determine the output
- $y(t)$
- , given that the input is
- $x(t)=u(t)$
- . (1M)

- (ii) The switch in Fig. 1 shown below has been in position a for a long time. At
- $t=0$
- , it moves to position b. Calculate
- $i(t)$
- for all
- $t>0$
- . (3M)

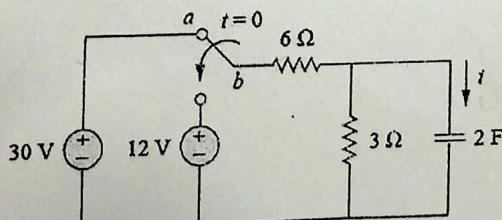


Fig. 1

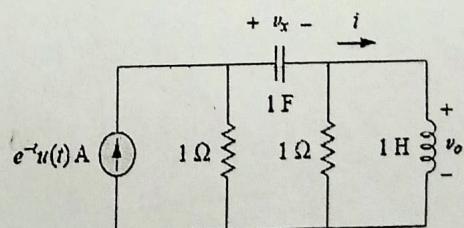


Fig. 2

- (iii) Find
- $v_o(t)$
- in the circuit of Fig. 2 shown above, if
- $v_x(0)=2$
- V and
- $i(0)=1$
- A. (3M)

## Basic

- charge ( $Q$ )  $\rightarrow i(t) = \frac{dQ}{dt}$
- $i(t) = \frac{dq}{dt}$

$$1C = -1.6 \times 10^{-19} C$$

$$\int i(t) dt = dq$$

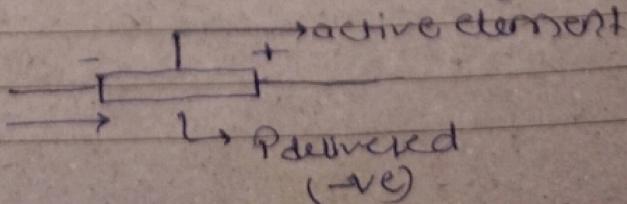
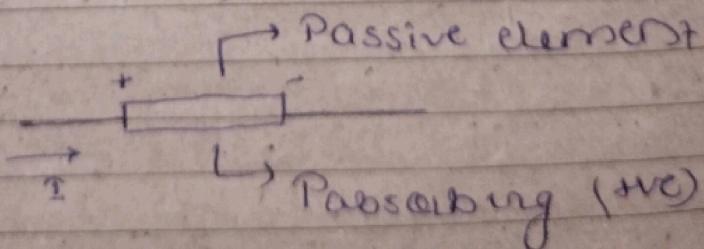
$$\left( \Phi = \int_{-\infty}^t i(u) du \right)$$

$$v \text{ (potential)} = \frac{dE}{dq}$$

$$(P(t) = \frac{dE}{dt})$$

$$= \frac{dE}{dq} \cdot \frac{dq}{dt}$$

$$(P(t) = v(t) \cdot I(t))$$



Pabsorbing (+ve)

Pdeivered (-ve)

## Basic

- charge ( $Q$ )  $\rightarrow i(t) = \frac{dQ}{dt}$
- $i(t) = \frac{dq}{dt}$

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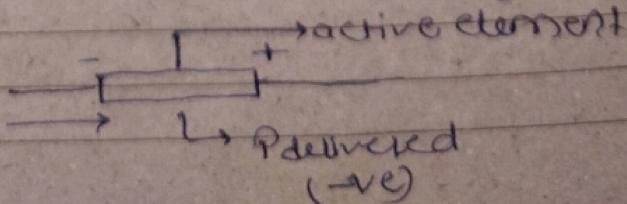
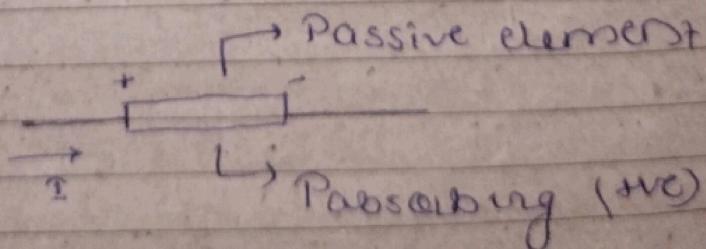
$$\int i(t) dt = dq$$

$$\left( \Phi = \int_{-\infty}^t i(u) du \right)$$

- v (potential)  $= \frac{dE}{dq}$
- $(P(t) = \frac{dE}{dt})$

$$= \frac{dE}{dq} \cdot \frac{dq}{dt}$$

$$(P(t) = v(t) \cdot I(t))$$

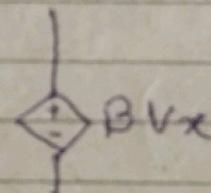
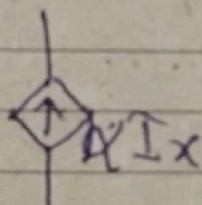


Passive (+ve)

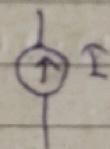
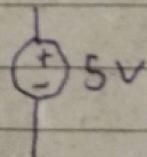
Powered (-ve)

- Those element which always absorb power then it is passive element
- Those element which always deliver power then it is active element
- \* Dependent source & independent source :

- It may be current , voltage source
- Dependent source depend on any parameter and this connect with any element of the circuit



- Independent source depend does not depend on any parameter.



$$\text{Q: } q = 5t \cdot \sin(4\pi t) \text{ mC}$$

$$i = ? \quad t = 0.5 \text{ s}$$

$$i = \frac{dq}{dt}$$

$$i = 5\sin(4\pi t) + 20\pi t \cos(4\pi t)$$

$$i = 5(\cancel{2t})^0 + 20\pi + \cos(\cancel{2\pi})$$

$$(i)_{t=0.5} = 10\pi \text{ mA}$$

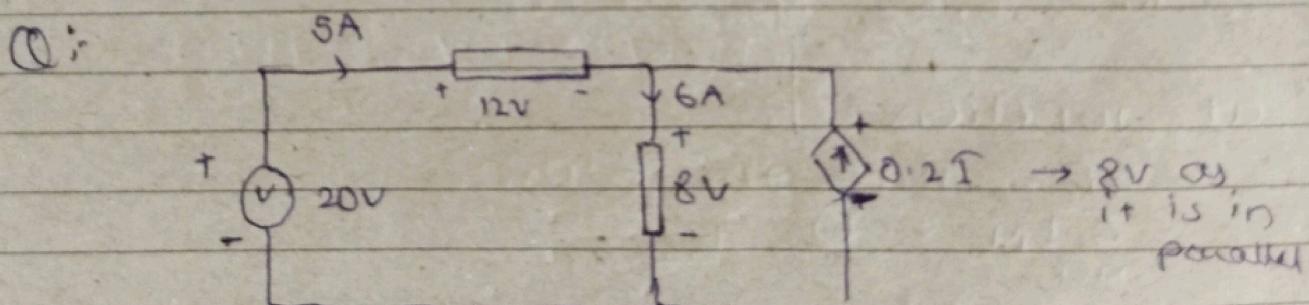
$$\textcircled{1}: i = (3t^2 - t)A, q = ?$$

$$t = 15.10 \text{ s}$$

$$\int dq = \int i dt$$

$$\textcircled{2} = \int (3t^2 - t)dt$$

$$\textcircled{2} = t^3 - \frac{t^2}{2} = \left[ (8-1) - \frac{(4-1)}{2} \right] \\ 7 - \frac{3}{2} \Rightarrow \underline{\underline{5.5 \text{ C}}}$$



$$P_{\text{absorb}} = 12 \times 5 + 6 \times 8 + 8 \times 1 \\ 60 + 48 \cancel{0}$$

$$P_{\text{absorb}} = 108 \cancel{W}$$

$$P_{\text{deliver}} = -20 \times 5 - 8 \times 1 = -108 W$$

To check

$$P_{\text{dissipated}} + P_{\text{absorbed}} = 0$$

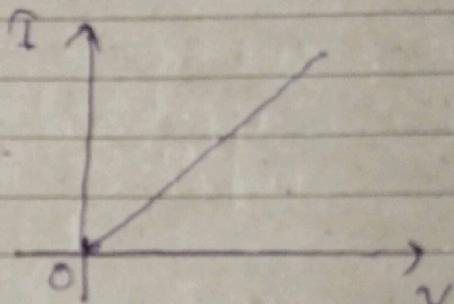
$$-108 + 108 = 0$$

\* Ohm's law :-

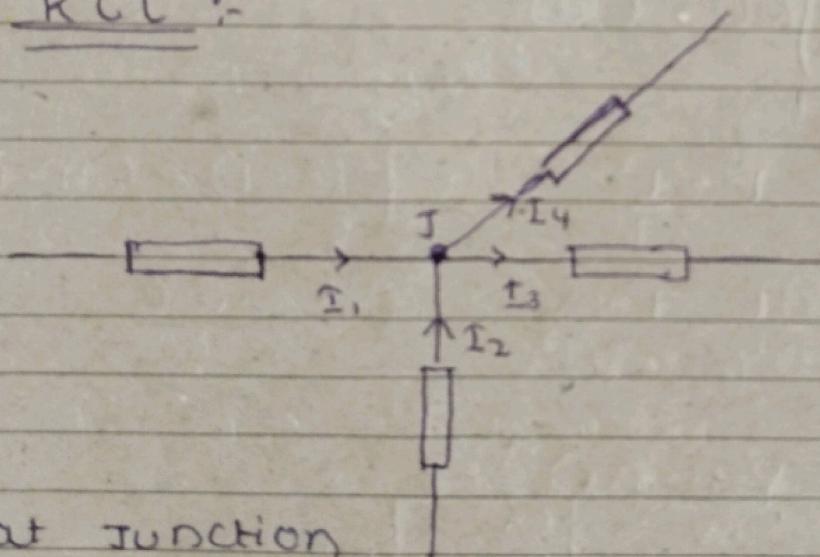
$$V \propto I$$

$$(V = IR)$$

$$\left( R = \frac{\rho L}{A} \right)$$



\* KCL :-



at JUNCTION

$$\sum_{n=1}^N I_n = 0$$

$$I_1 + I_2 - I_3 - I_4 = 0$$

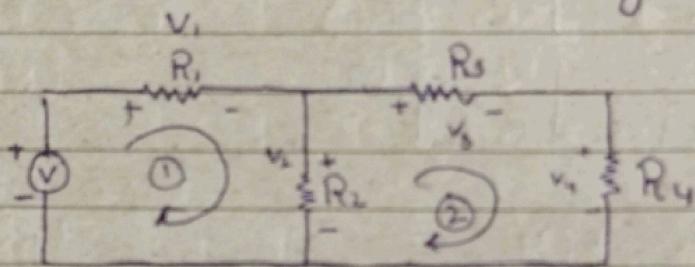
$$(I_1 + I_2 = I_3 + I_4)$$

$\Delta$   
Delta

Incoming current = Outgoing current

→ based on conservation of charge  
↳ neither be created nor destroyed

\* KVL (Kirchoff's voltage law) :-



in loop

$$\sum_{N=1}^m V_N = 0$$

in loop ①

$$V - V_1 - V_2 = 0$$

$$(V = V_1 + V_2)$$

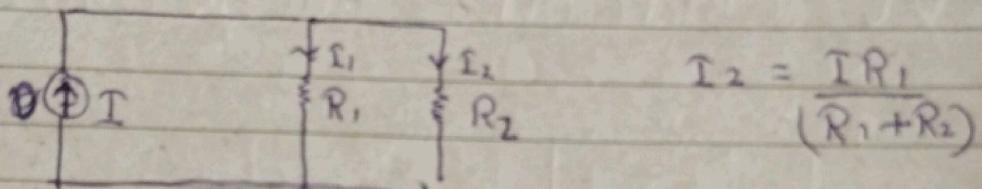
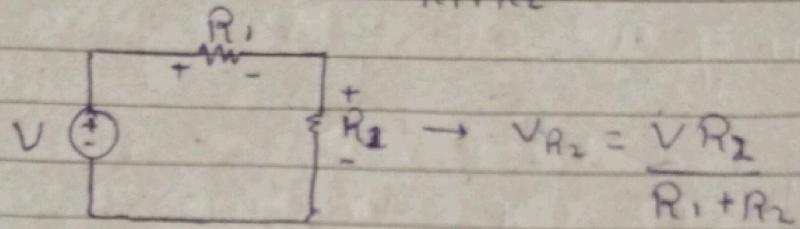
in loop ②

$$-V_3 - V_4 + V_2 = 0$$

$$(V_2 = V_3 + V_4)$$

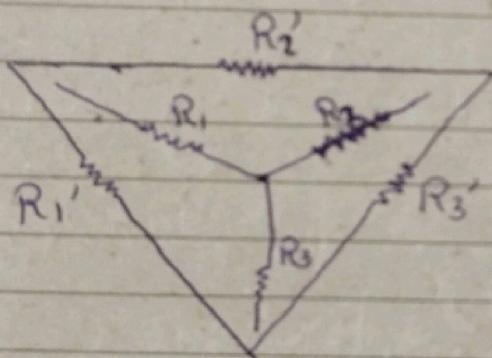
$$\rightarrow V_{R_1} = \frac{V R_1}{R_1 + R_2}$$

(B) \*



$$I_1 = \frac{I R_2}{(R_1 + R_2)}$$

### \* Star-Delta Transformation:-



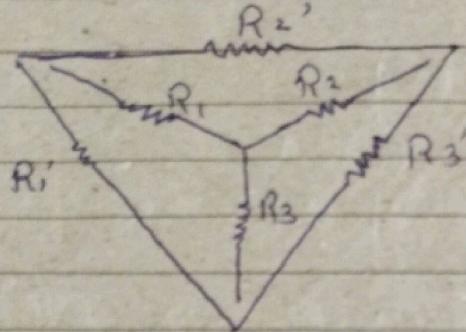
$$R_1' = \frac{R_1 R_2 + R_2 R_3 + R_1 R_3}{R_2}$$

$$R_2' = \frac{R_1 R_2 + R_2 R_3 + R_1 R_3}{R_3}$$

$$R_3' = \frac{R_1 R_2 + R_2 R_3 + R_1 R_3}{R_3}$$

$\Delta$   
 $P_{DE}$   
 $P_{DZ}$   
 Delta

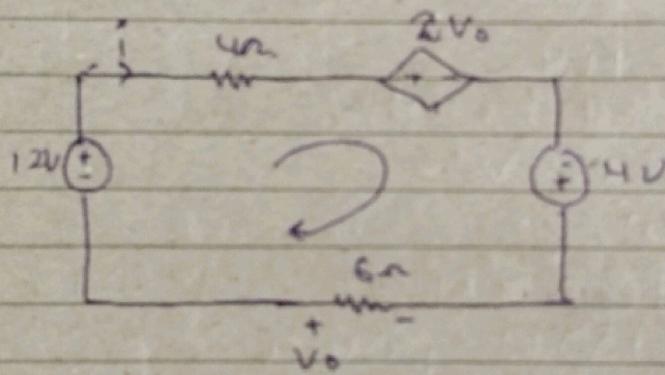
Delta-star transformation



$$R_1 = \frac{R_1' R_2'}{R_1' + R_2' + R_3'}$$

$$R_2 = \frac{R_1' R_3'}{R_1' + R_2' + R_3'}$$

Q:- Find  $i$ ,  $V_o$ ?



$$\begin{aligned} v &= -i \cdot 4 \\ i &= -v/4 \\ v &= -6i \end{aligned}$$

In this Loop

$$+12V - 4i - 2V_o + 4V + V_o = 0$$

$$12V - 4i + 12i + 4V - 6i = 0$$

$$16V + 2i = 0$$

$$(i = -8A)$$

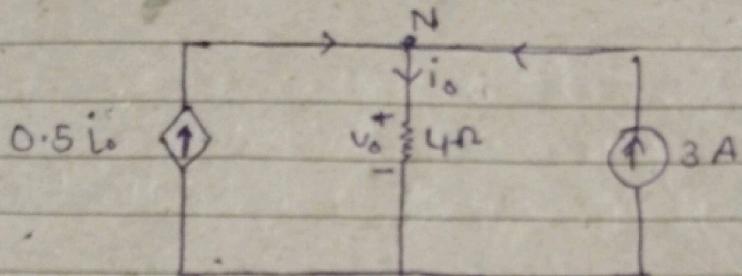
or,

$$V_o = -6i$$

$$(V_o = 48V)$$



Q:- Calculate  $i_o$  &  $v_o$



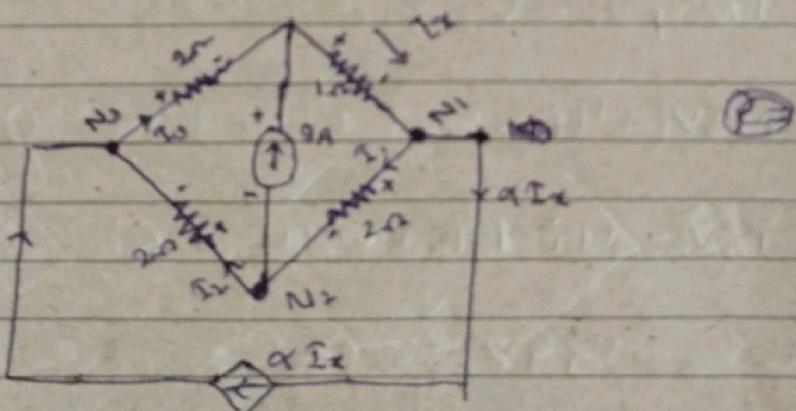
$$0.5i_o + 3 - i_o = 0$$

$$(i_o = 6 \text{ A})$$

$$v_o = +i_o \cdot 4$$

$$v_o = +24 \text{ V}$$

Q:- find  $\alpha$  for which 9A current source supplies 180W power



$$\begin{aligned} \text{so } P &= VI \\ 180 &= V(9) \end{aligned}$$

$$(V = 20 \text{ V})$$

$\Delta$   
P<sub>1</sub>, P<sub>2</sub>

at N, (Apply KCL)

$$I_2 = I_1 + \alpha I_x$$

$$(I_1 = (1-\alpha)I_x)$$

at N<sub>2</sub>

$$I_1 = g + I_2$$

$$I_2 = I_1 - g$$

$$(I_2 = (1-\alpha)I_x - g)$$

at N<sub>3</sub>

$$I_3 = I_2 + \alpha I_x$$

$$= (I_2 - \alpha I_x - g + \alpha I_x)$$

$$(I_3 = I_x - g)$$

→ Apply KVL in left loop

$$-2(I_x - g) - 20 - 2[(1-\alpha)I_x - g] = 0$$

$$-2I_x + 18 - 20 - 2[I_x - \alpha I_x - g] = 0$$

$$-2I_x - 2 - 2I_x + 2\alpha I_x + 18 = 0$$

$$-4I_x + 2\alpha I_x + 16 = 0 \quad \text{--- (1)}$$



In right loop

$$-\dot{I}_x - 2\dot{I}_1 + 20 = 0$$

$$-\dot{I}_x + 2\dot{I}_x + 2\alpha\dot{I}_x + 20 = 0$$

$$-3\dot{I}_x + 2\alpha\dot{I}_x + 20 = 0 \quad \text{--- (1)}$$

from eq (1) & (2) subtract both

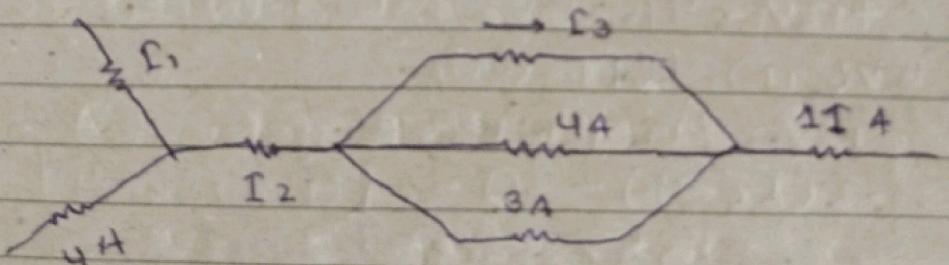
$$-\dot{I}_x + 4 = 0$$

$$(\dot{I}_x = 4)$$

NOW,

$$(x = 4)$$

Q:- find ( $I_1, I_2 \text{ & } I_3$ )



$$4A + 3A + I_3 = 11A$$

$$11 - 7A = I_3$$

$$(I_3 = 4A)$$

$\Delta$  Delta

$$\Sigma_2 = 4+4+3$$

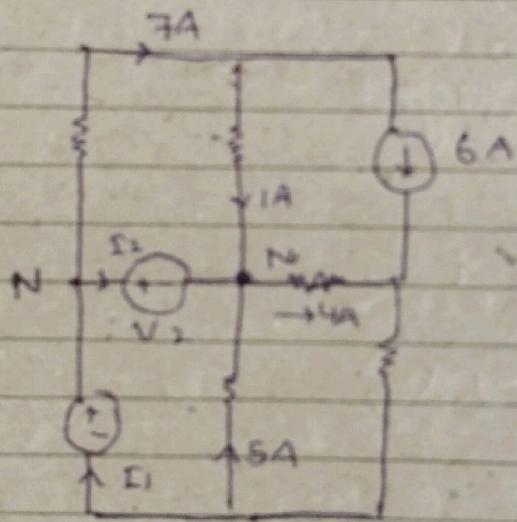
$$I_2 = 11 \text{ A}$$

$$\cancel{I_1 + I_2} - I_1 + 4 = 11$$

$$(I_1 = 7 \text{ A})$$

$$\rightarrow (7 \text{ A}, 11 \text{ A}, 4 \text{ A})$$

Q:- Find  $I_1$  &  $I_2$



at N,

$$\cancel{E_2} : I_2 + 5 + 1 = 4$$

$$E_2 = -2 \text{ A}$$

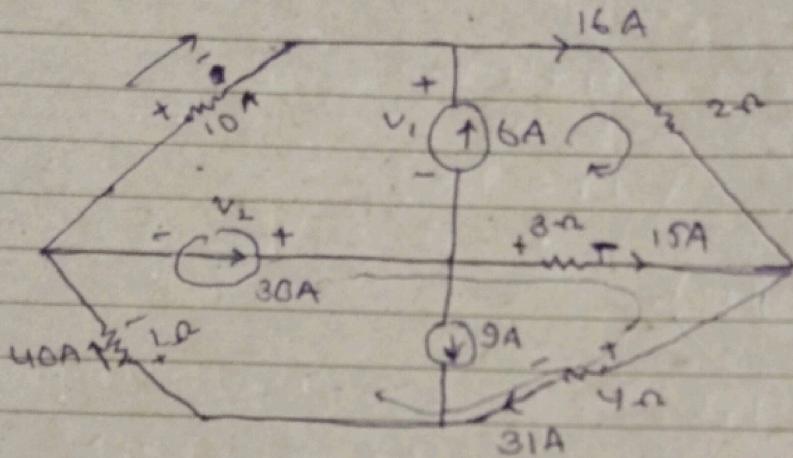
at N

$$I_1 = I_2 + 7$$

$$(I_1 = 5 \text{ A})$$



Q:- Find  $v_1$ ,  $v_2$ ?



In Loop top right

$$+v_1 - 32V + 45$$

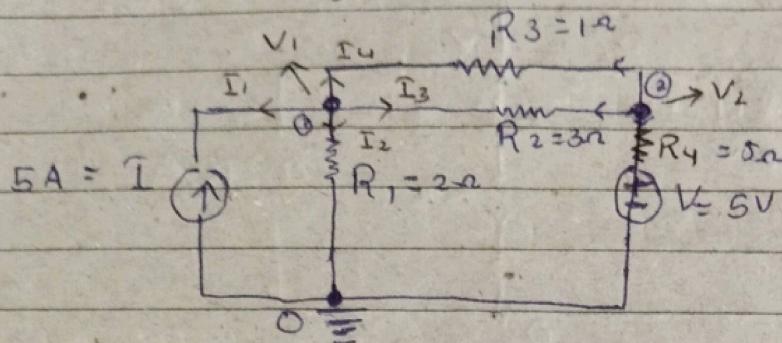
$$(v_1 = -13V)$$

In bottom loop

$$v_2 - 45 - 124 - 40$$

$$(v_2 = 209V)$$

## Nodal Analysis :-



at Node ①

$$I_1 + I_2 + I_3 + I_4 = 0$$

$$\frac{-5 + V_1 - 0}{2} + \frac{V_1 - V_2}{3} + \frac{V_1 - V_2}{1} = 0$$

$$-30 + 3V_1 + 2V_1 - 2V_2 + 6V_1 - 6V_2 = 0$$

$$11V_1 - 8V_2 - 30 = 0 \quad \textcircled{1}$$

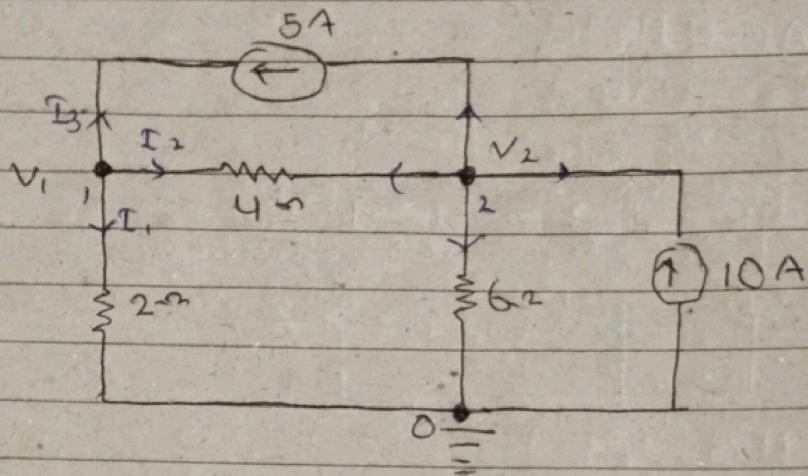
at Node ②

$$\frac{V_2 - V_1}{1} + \frac{V_2 - V_1}{3} + \frac{V_2 - 5 - 0}{5} = 0$$

$$15V_2 - 15V_1 + 5V_2 - 5V_1 + 3V_2 - 15 = 0$$

$$-20V_1 + 23V_2 - 15 = 0 \quad \textcircled{11}$$

(11)



at node - (1)

$$I_1 + I_2 + I_3 = 0$$

$$\frac{V_1 - 0}{2} + \frac{V_1 - V_2}{4} - 5 = 0$$

$$2V_1 + 2V_1 - 2V_2 - 20 = 0$$

$$3V_1 - V_2 = 20 \quad \text{--- (1)}$$

at node (2)

$$I_1 + I_2 + I_3 + I_4 = 0$$

$$= \frac{V_2 - 0}{6} + \frac{V_2 - V_1}{4} + 5 - 10 = 0$$

$$2V_2 + 3V_2 - 3V_1 - 60 = 0$$

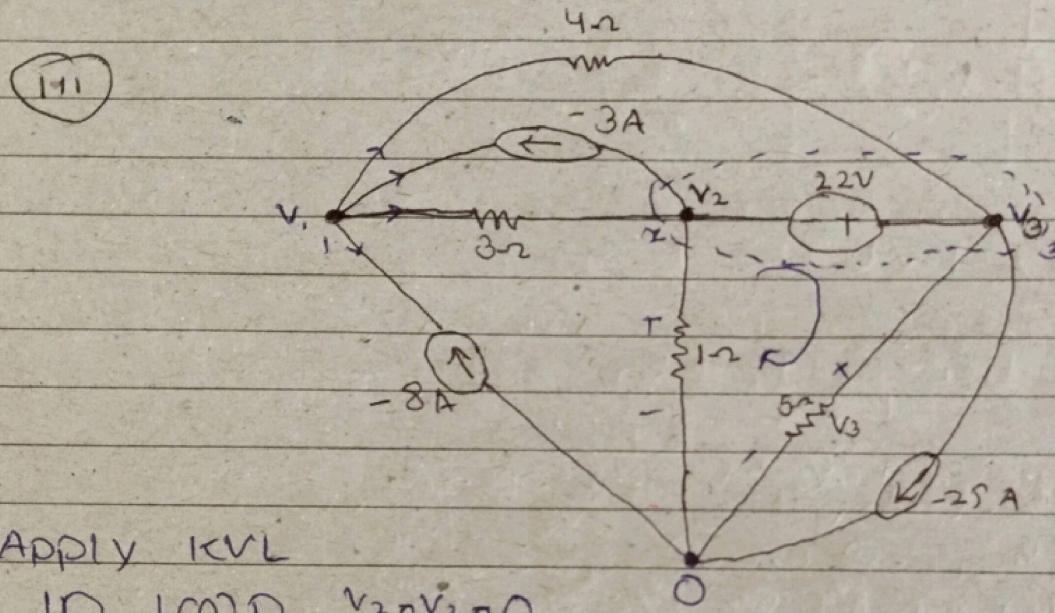
$$-3V_1 + 5V_2 - 60 = 0 \quad \text{--- (2)}$$

(11)

Note :-

Has node se outgoing current as a convention le wagle if convention current is in  $\leftarrow$  and given current direction  $\rightarrow$  current will become -ve

10A



Apply KVL

in loop  $v_2, v_3, 0$

$$22V - V_3 + V_2 = 0$$

$$V_2 - V_3 = 22 \quad \textcircled{1}$$

apply KCL at ①

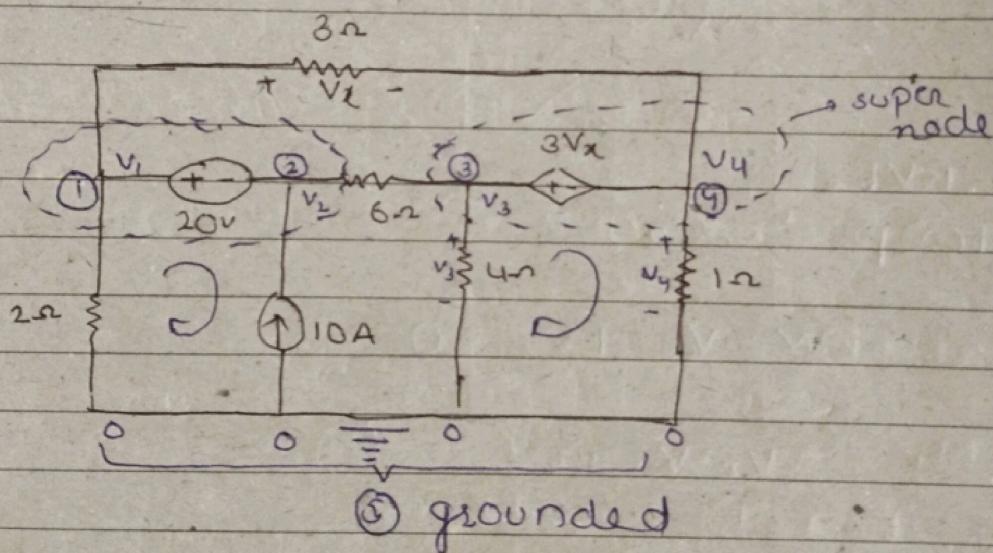
$$I_1 + I_2 + I_3 + I_4 = 0$$

$$+8 + \frac{V_1 - V_2}{3} + 3 + \frac{V_1 - V_3}{4} = 0$$

$$+132 + 7V_1 - 4V_2 - 3V_3 = 0 \quad \textcircled{11}$$

We assume node ② & ③ as super node, when ever there is a voltage source in btw 2 nodes it will become supernode (we act it 1 node)

(iv)



Apply KVL

$$-3V_x - V_4 + V_3 = 0$$

$$V_3 - V_4 \div 3V_x - ①$$

at node ① & ② as super node means  
at node ① & ② eqn be written in single  
eqn

$$\frac{V_1 - 0}{2} + \frac{V_1 - V_4}{3} + \frac{V_2 - V_3}{6} - 10 = 0$$

(11)

DL:  
PD: Delta

$$\Rightarrow 6v_1 + v_2 - v_3 - 2v_4 = 60 \quad \text{--- (ii)}$$

similarly

Node ③ & ④ are super node

$$\frac{v_3}{4} + \frac{v_3 - v_2}{6} + \frac{v_4 - v_1}{3} + \frac{v_4}{1} = 0$$

$$-4v_1 - 2v_2 + 5v_3 + 16v_4 = 0 \quad \text{--- (iii)}$$

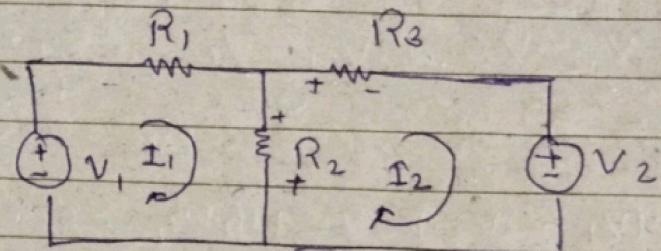
Apply KVL in loop  $v_1, v_2, 0$

$$-20 - v_2 + v_1$$

$$v_1 - v_2 = 20 \quad \text{--- (iv)}$$

### Mesh Analysis :

→ A mesh is a closed path during a circuit with no other path inside it



⇒ Apply KVL in both loop

$$(R_1 + R_2)I_1 + V_1 = 0 \quad \text{--- (1)}$$

$$-I_2R_2$$

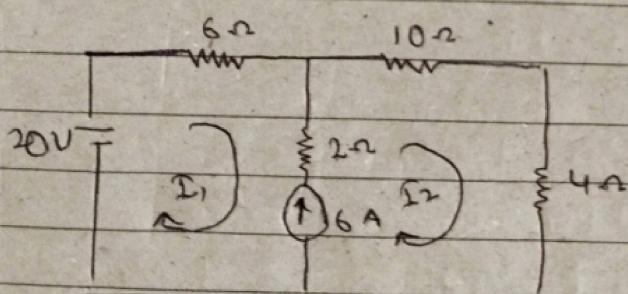
Apply KVL in other loop

$$-I_2(R_2 + R_3) - V_2 = 0 \quad \text{--- (2)}$$

$$-I_1R_2$$

Solve both eqn to get answer

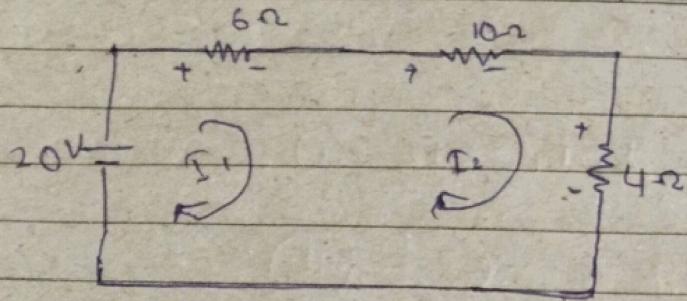
(1)



→ It is a supermesh type question mean whenever there is a current + super source in b/w 2 mesh it will become supermesh & to solve the question we remove that branch.

Apply super mesh concept

DL:  
PQ: Delta



Apply KVL in that loop

$$-6I_1 - 10I_2 - 14I_2 + 20 = 0 \quad \text{--- (1)}$$

For eqn (2) we know in super mesh branch

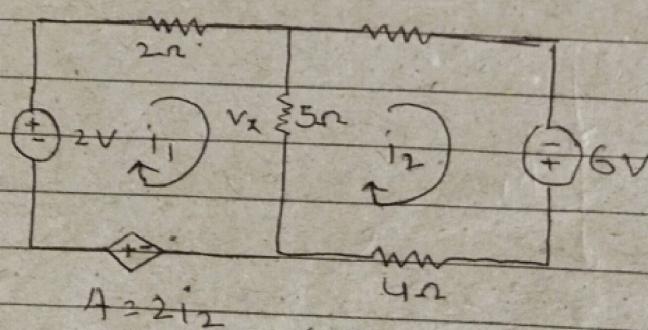
$$I_1 - I_2 = -6 \quad \text{--- (2)}$$

After solving both eqn

$$I_1 = -3.2$$

$$I_2 = 2.8$$

(III)



$$\text{if } A = 2i_2 \\ i_1 = ?$$

Apply KVL in loop (1)

$$+2 - 2i_1 - 5i_1 + 5i_2 + 2i_2 = 0$$

$$-7i_1 + 7i_2 = -2 \quad \text{--- (1)}$$



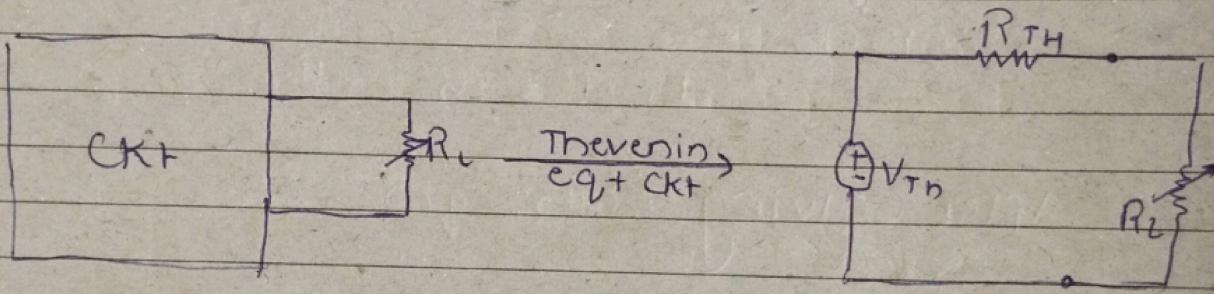
In loop ②

$$-3i_2 + 6 - 4i_2 + 5i_1 - 5i_2 = 0$$

$$5i_1 - 12i_2 = -6 \quad \text{--- (1)}$$

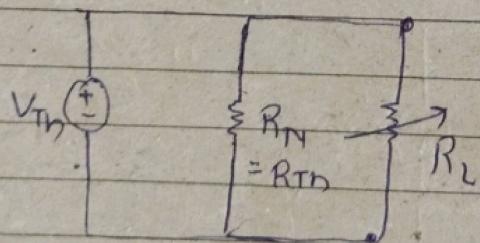
Solve both eqns to get  $i_1$ ,  $i_2$  & then find A

- Thevenin's & Norton's Theorem :-



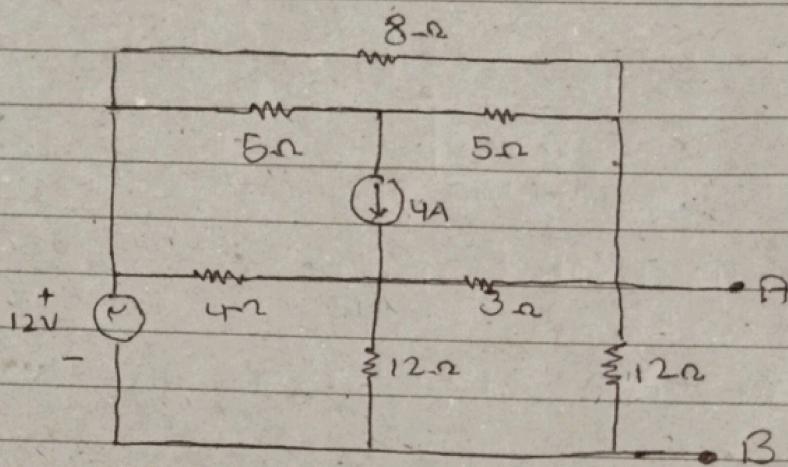
C  
F  
C  
F  
Norton  
Solutions

$$I_{RL} = \frac{V_{TH}}{(R_{TH} + R_L)}$$

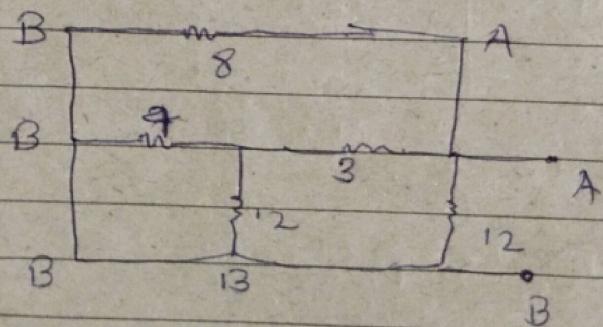
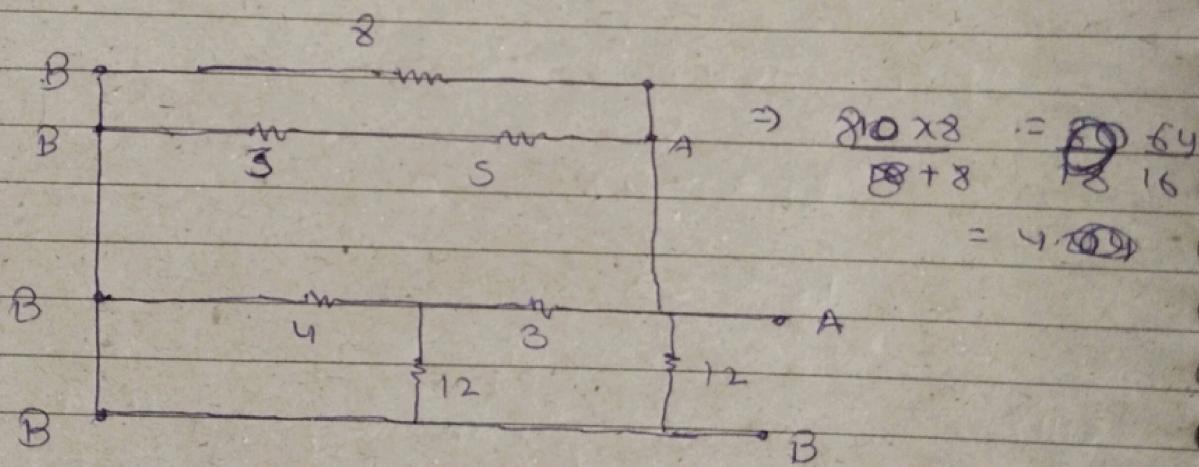


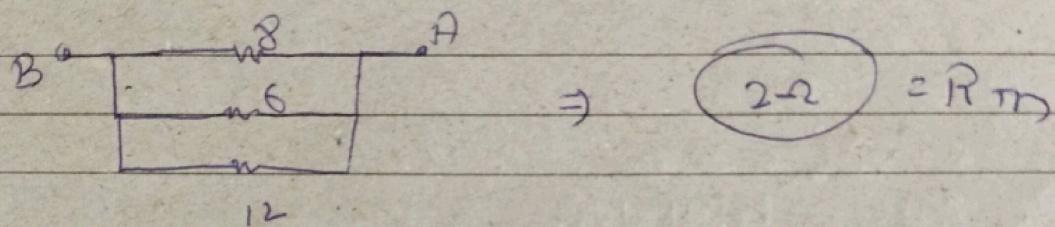
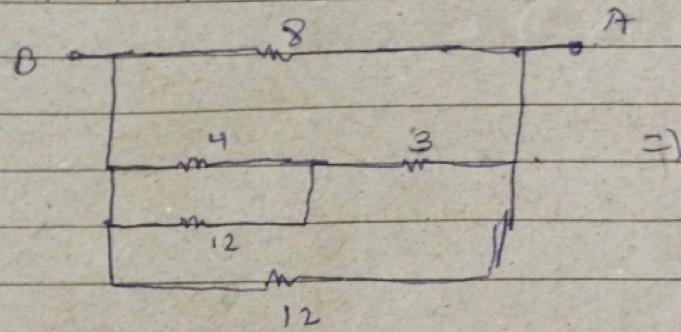


Q:- Find Thevinin's Eqn across A-B ?

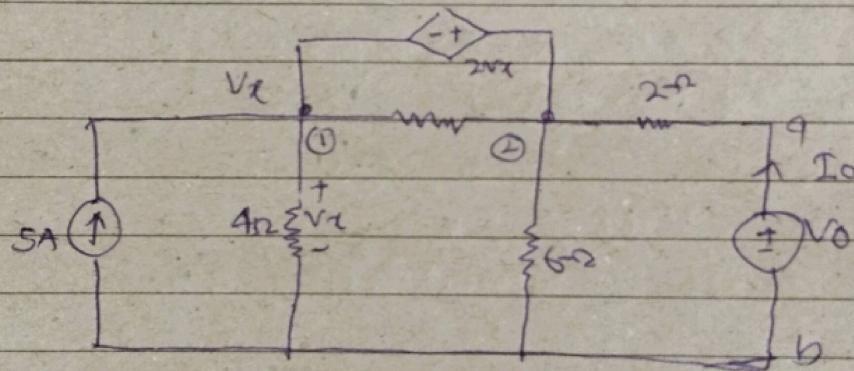


Sol To Find  $R_{Th}$  short voltage source & open current source (independent)

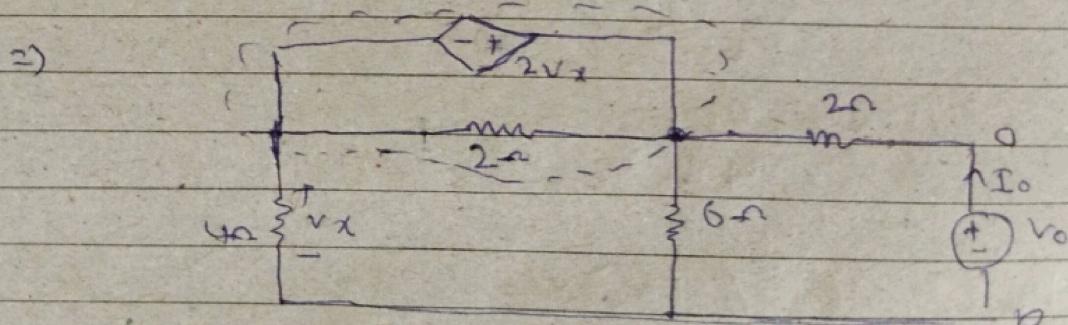




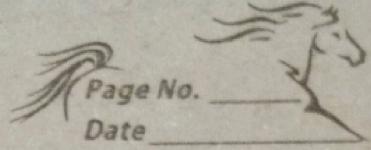
Q: Find Thevenin's Eqt across A-B



$\Rightarrow$  let  $V_0$  across  $0-1$  & open independent current source & node  $①$  &  $②$  are supernodes



To find  $R_{Th} = \frac{V_0}{I_0}$  ratio of  $V_0/I_0$



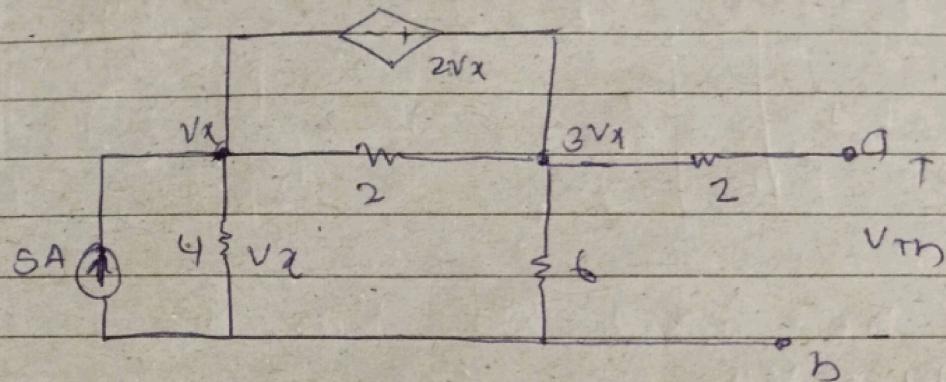
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Let  $v_y$  across node ②

at node ①

To find  $V_{Th}$



$V_{Th} = 3V_x$  from previous finding

as mode ① & ② are super nodes

$$\frac{V_x}{4} + \frac{V_x - V_{Th}}{2} - 5 + \frac{V_{Th} - V_x}{2} + \frac{V_{Th}}{6} = 0$$

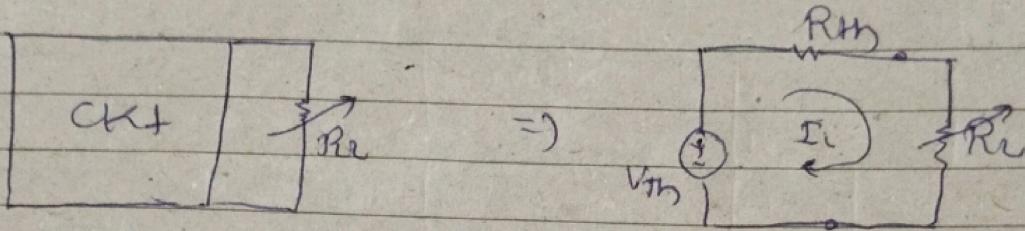
$$\frac{V_{Th}}{3 \times 4} + \frac{V_{Th}}{3 \times 2} - \frac{V_{Th}}{2} + \frac{V_{Th}}{2} - \frac{V_{Th}}{3 \times 2} + \frac{V_{Th}}{6} = 0$$

$$\Rightarrow \frac{V_{Th}}{12} + \frac{2V_{Th}}{6 \times 2} = 5$$

$$3V_{Th} = 12 \times 5$$

$$(V_{Th} = 20V)$$

## • Maximum power transfer theorem :-



$$I_C = \frac{V_m}{R_H + R_L}$$

$$P_L = I_C^2 \cdot R_L$$

$$P_L = \left[ \frac{V_m}{R_H + R_L} \right]^2 \cdot R_L$$

$$= \frac{V_m^2 \cdot R_L}{(R_H + R_L)^2}$$

For maximum power ( $R_L = R_H$ )

$$P_L = V_m^2 \cdot \frac{R_L}{(2R_L)^2} = \frac{V_m^2}{4} \frac{R_L}{R_L^2}$$

$$P_L = \frac{V_m^2}{4R_L^2}$$

$$P_L = V_m^2 / 4R_L^2$$

To max. power  $dP_L/dR_L = 0$

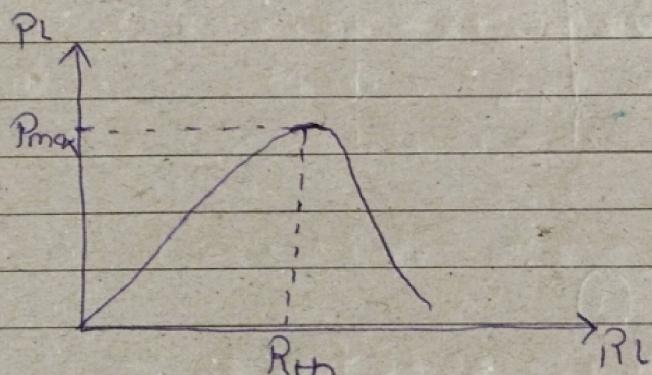
$$\frac{d}{dR_L} \left[ V_{TH}^2 \cdot \frac{R_L}{(R_{TH}+R_L)^2} \right]$$

$$= V_{TH}^2 \cdot [(R_L + R_{TH})^2 \cdot \frac{dR_L}{dR_L}] - R_L \cdot \frac{d}{dR_L} [R_{TH} + R_L]$$

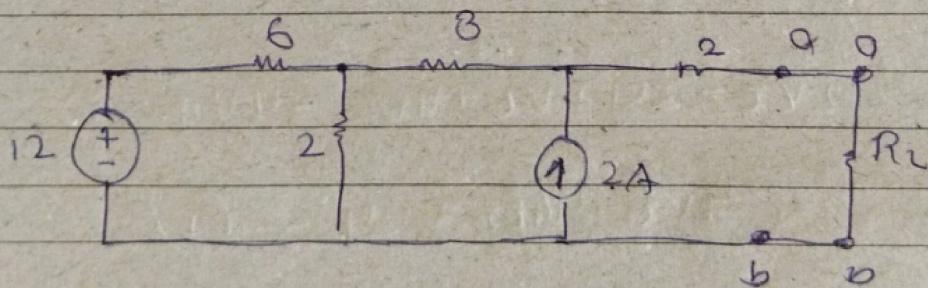
on solving it we get

$(R_{TH} = R_L)$  hence proved

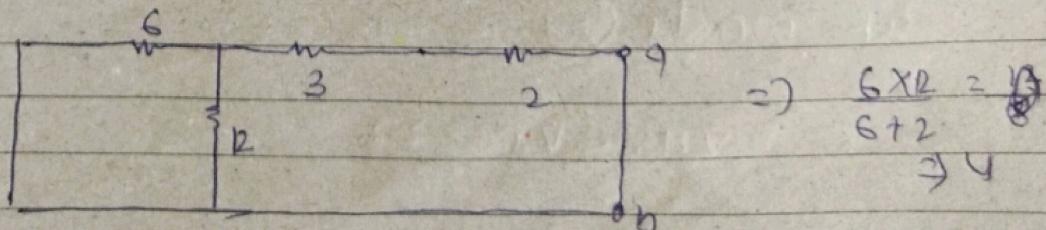
$P_L$  vs  $R_L$

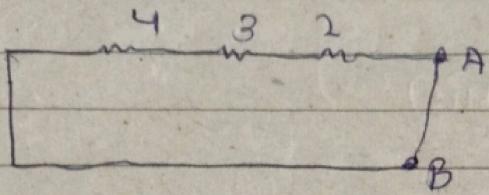


Q:



SOL:

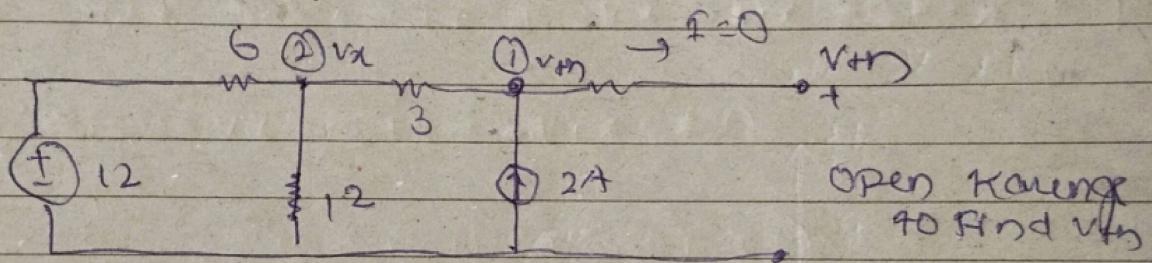




$$(R_{th} = g_n)$$

(thus  $R_L = g_n$ ) as  $R_{th} = R_L$

To find  $P_{max}$  we have to calculate  
 $v_{th}$



at node ①

$$\frac{V_x - 12}{6} + \frac{V_x}{12} + \frac{V_x - V_{th}}{3} = 0$$

$$2V_x - 24 + V_x + 4V_x - 4V_{th} = 0$$

$$7V_x - 4V_{th} = 24 \quad \textcircled{1}$$

at node ②

$$\frac{V_{th} - V_x}{3} = 2$$

$$V_{Th} - V_x = 6$$

$$V_{Th} - 6 = V_x \quad \text{--- (1)}$$

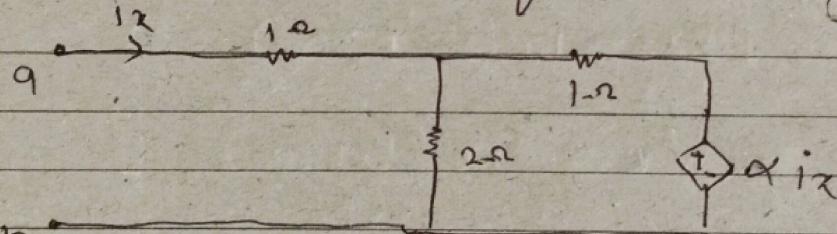
from eq (1) & (2)

$$(V_{Th} = 22V)$$

$$\text{to find } P_{max} = \frac{V_{Th}^2}{4R_L}$$

$$\Rightarrow \frac{22 \times 22}{4 \times 9} = 13.44 \text{ W}$$

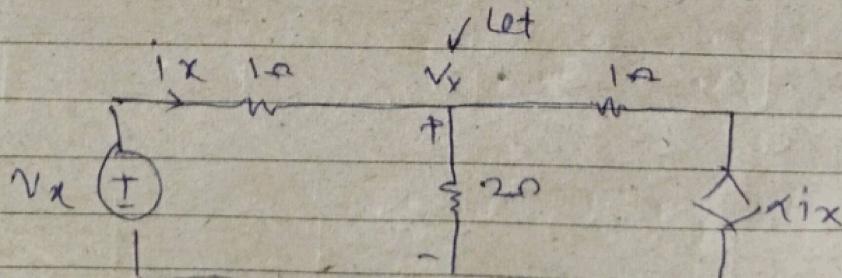
Q:- Find thevenin's eqt ckt as a func of t?



Note

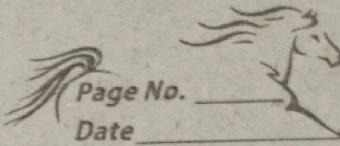
If there is no independent source in the ckt thus  $V_{Th}$  is always zero

Q1 to find  $R_{Th}$  let  $V_x$  across a/b



at node

$$\frac{V_y - V_x}{2} + \frac{V_y}{2} + V_y - \alpha i_x = 0 \quad \text{--- (1)}$$



also apply km in the leap

$$+v_x - i_x i_x - v_y = 0$$

$$v_y = v_x - i_x \quad \text{--- (1)}$$

Put (1) in (1)

$$\frac{v_x - i_x - v_x}{2} + \frac{v_x - i_x}{2} + \frac{v_x - i_x - 2i_x}{1} = 0$$

$$-2i_x + v_x - i_x + 2v_x - 2i_x - 2i_x = 0$$

$$3v_x - 5i_x - 2i_x i_x = 0$$

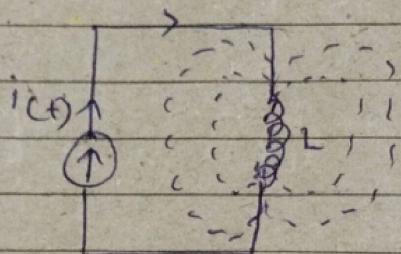
$$3v_x - i_x(5 + 2\alpha) = 0$$

$$3v_x = i_x(5 + 2\alpha)$$

$$R_m = \frac{v_x}{i_x} = \frac{(5 + 2\alpha)}{3} =$$



## Magnetically coupled ckt :-



$$V \propto \frac{d\Phi}{dt}$$

$$V \propto N$$

$$V = N \frac{d\Phi}{dt}$$

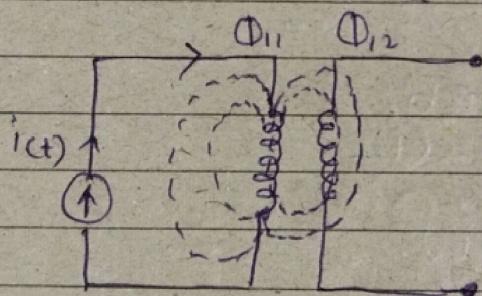
$$V = N \cdot \frac{d\Phi}{di} \cdot \frac{di}{dt}$$

Self inductance

$$\boxed{V = L \frac{di}{dt}}$$

L : inductance

Mutual inductance



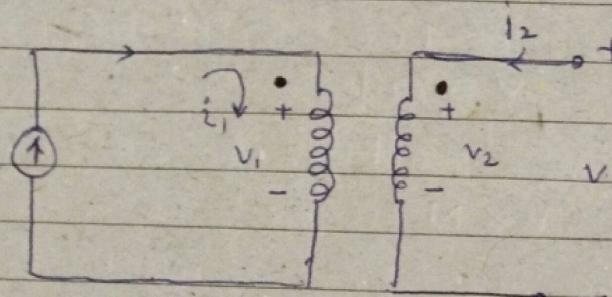
$$( V_1 = N_1 \frac{d\Phi_{11}}{dt} \cdot \frac{di}{dt} )$$

$$( V_2 = N_2 \frac{d\Phi_{12}}{dt} \cdot \frac{di}{dt} )$$

$$( V_2 = M_{12} \frac{di}{dt} )$$

$M_{12}$  : mutual  
inductance

• Dot convention for coil :-

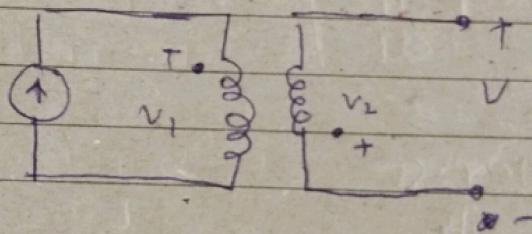


$i_1, i_2$  are time varying

$$(M = M_{12} = M_{21})$$

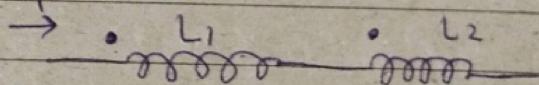
$$v_1 = L \frac{di_1}{dt} + M_1 \frac{di_2}{dt}$$

$v_{123}$

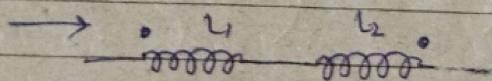


$$v_1 = L \frac{di_1}{dt} - M_1 \frac{di_2}{dt} - M_1 \frac{di_3}{dt}$$

concept  $\rightarrow$



$$(L_{eq} = L_1 + L_2 + 2M)$$



$$(L_{eq} = L_1 + L_2 - 2M)$$

• Concept

$$L = sL$$

$$C = \frac{1}{sC}$$

$$s = \sigma + j\omega$$

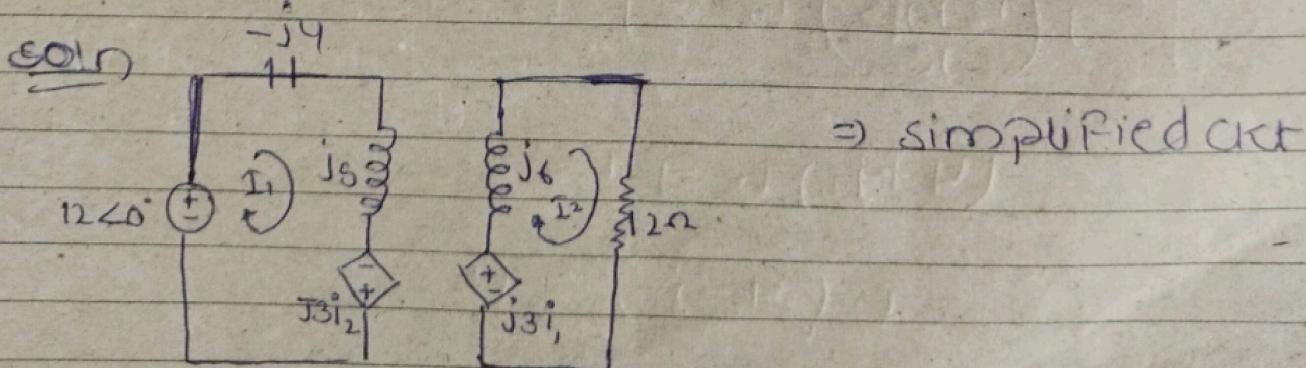
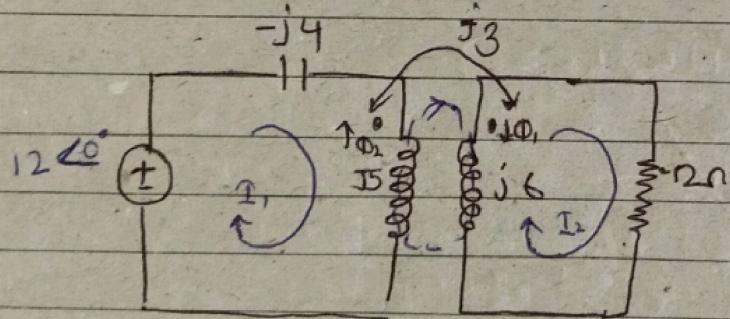
$$\sigma = 0$$

$$s = j\omega$$

$$X_L = j\omega L \quad X_M = j\omega M$$

$$X_C = \frac{1}{j\omega C} = -\frac{j}{\omega C}$$

Q: Solve the ckt to find  $I_1$  &  $I_2$



Apply KVL in loop 1

$$12 - (j4i_1) - j5i_1 + j3i_2 = 0$$

$$12 - j1_1 + j3i_2 = 0 \quad \text{--- (i)}$$

in loop 2

$$-j6i_2 - 12i_2 + j3i_1 = 0 \quad \text{--- (ii)}$$

on solving eq (i)

$$j1_1 - j3i_2 = 12$$

$$i_1 = \frac{(12 + j6)}{j3} i_2 \quad \text{--- (A)}$$

put (A) in (i)

~~$$+ j3i_1 - (12 + j6)i_2 = 0$$~~

~~$$j3 \left[ \frac{12 + j6}{j3} i_2 \right] -$$~~

$$j \left( \frac{12 + j6}{j3} \right) i_2 - j3i_2 = 12$$

$$(4 + j2)i_2 - j3i_2 = 12$$

$$i_2 (4 - j) = 12$$

$$|x - iy| = (\sqrt{x^2 + y^2})$$

$$\Theta = \tan^{-1}(y/x)$$

Page No.



$$I_2 = \frac{12 + j0}{4 - j} = \frac{\sqrt{12^2 + 0^2}}{\sqrt{4^2 + (-1)^2}}$$

$$I_2 = \frac{12}{\sqrt{17}}$$

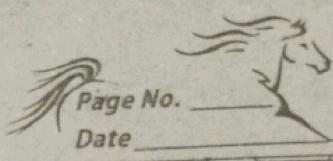
For angle,

$$\frac{\tan^{-1}(0)}{\tan^{-1}\left(\frac{1}{4}\right)} = \angle 14.04$$

$$I_2 = \frac{12 \angle 14.04}{\sqrt{17}}$$

put  $I_2$  in  $\textcircled{A}$

$$I_1 = \left(12 + j6\right) \left(\frac{12}{\sqrt{17}}\right)$$



## Laplace Transformation

$F(t) \xleftrightarrow[\text{inverse Laplace}]{\text{Laplace}} F(\omega)$  (frequency)

$$s = \sigma + j\omega$$

$$s = j\omega$$

$$x_C = \frac{1}{s} C$$

$$x_L = s L$$

$$x_C = \frac{1}{j\omega C}$$

$$x_L = j\omega L$$

$$F(s) = \int_{-\infty}^{\infty} f(t) e^{-st} dt$$

$$(F(s) = \int_0^{\infty} f(t) e^{-st} dt) \rightarrow \text{for unilateral C.R.}$$

$$F(s) = \int_0^{\infty} f(t) e^{-(\sigma + j\omega)t} dt$$

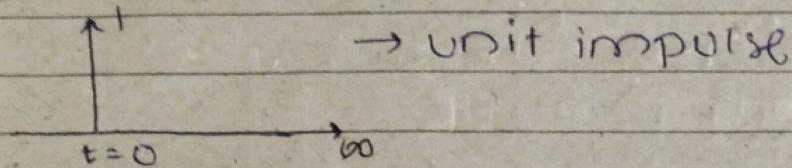
$$f(s) = \int_0^{\infty} f(t) e^{-\sigma t} e^{-j\omega t} dt \rightarrow |e^{-j\omega t}| = 1$$

$$\boxed{F(s) = \left| \int_0^{\infty} f(t) e^{-\sigma t} dt \right| < \infty} \rightarrow \text{absolutely integrable}$$



• Impulse signal :-

→ zero at an instant eg:- lightning



$$f(t) = \delta(t)$$

$$\left( \begin{array}{l} 1 \cdot \delta(t) \xleftrightarrow{-\infty \rightarrow \infty} 1 \\ A \cdot \delta(t) \xleftrightarrow{-\infty \rightarrow \infty} A \end{array} \right)$$

∴ since,

$$\therefore f(s) = \int_{-\infty}^{\infty} f(t) e^{-st} dt$$

$$\delta(t) \xleftrightarrow{-\infty \rightarrow \infty} \int_{0^-}^{\infty} \delta(t) e^{-st} dt$$

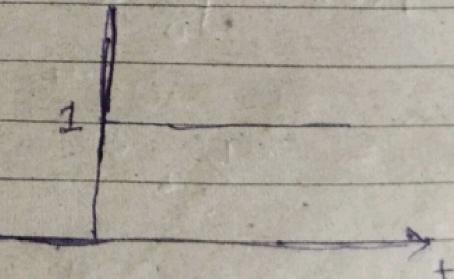
$$\begin{aligned} e^{-st} & , t=0 \\ e^{-0 \times s} & = 1 \\ e^0 & = 1 \end{aligned}$$

$$\left( \delta(t) \xleftrightarrow{-\infty \rightarrow \infty} \int_{0^-}^{\infty} \delta(t) e^{-0 \times s} dt = 1 \right)$$

• unit step signal

$$f(t) = u(t)$$

$$f(t) = \begin{cases} 1, & t > 0 \\ 0, & t < 0 \end{cases}$$



$$\therefore F(s) = \int_0^\infty f(t) e^{-st} dt$$

$$= \int_0^\infty 1 \cdot e^{-st} dt$$

$$= \frac{e^{-st}}{s} \Big|_0^\infty \Rightarrow \frac{e^{-s \times \infty}}{-s} + \frac{e^{-s \times 0}}{s}$$

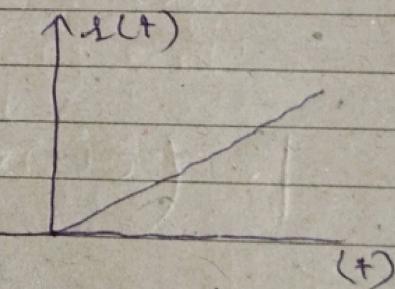
$$\Rightarrow \frac{1}{s}$$

$$\boxed{u(t) \xleftrightarrow{LT} \frac{1}{s}}$$

samp sing signal :

$$i(t) = t$$

$$\therefore f(s) = \int_0^\infty f(t) e^{-st} dt$$



$$f(s) = \int_0^\infty t e^{-st} dt$$

$$\int u v dx = u \int v dx - \int du \int v dx$$

[LATE]

$$f = \frac{1}{s^2}$$

$$\boxed{s(t) \xleftrightarrow{LT} \frac{1}{s^2}}$$



Q:- Find Laplace transform of  $f(t) = e^{-at} u(t)$   $a > 0$

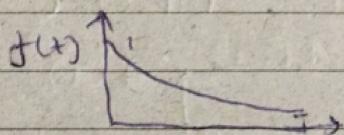
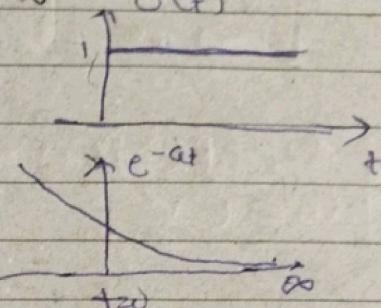
Sol  $f(s) = \int_0^\infty f(t) e^{-st} dt$

$$\int_a^\infty e^{-at} u(t) e^{-st} dt$$

( $u(t) \approx 1$ )

$$= \int_0^\infty e^{-at} e^{-st} dt$$

$$\int_0^\infty e^{-(a+s)t} dt$$

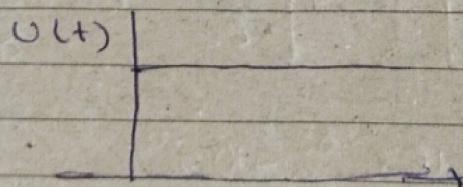


$$\left. \frac{e^{-(a+s)t}}{-s-a} \right|_0^\infty = \left( \frac{1}{s+a} \right)$$

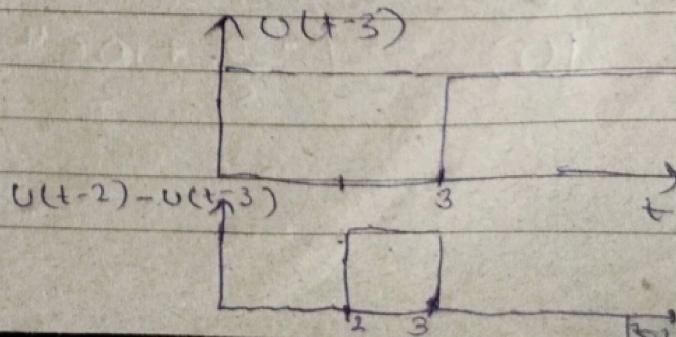
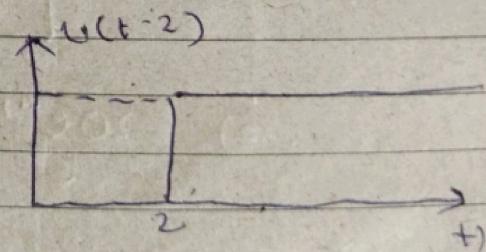
Q:- Find L.T?

$$F(t) = 10 [u(t-2) - u(t-3)]$$

Sol



$$u(t-2) \Rightarrow t-2=0 \quad t=2$$



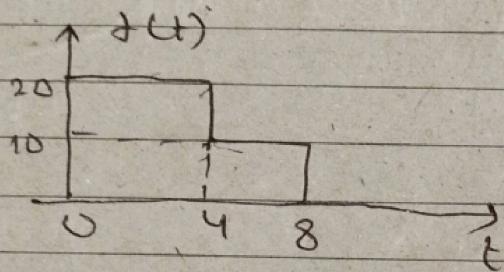
$$u(t-2)$$

$$-u(t-3)$$

$$F(s) = 10 \left[ \frac{e^{-2s}}{s} - \frac{e^{-3s}}{s} \right]$$

$$F(s) = \frac{10}{s} [e^{-2s} - e^{-3s}]$$

Q: Find L.T



60)  $f(s) = \int_0^4 f(t) e^{-st} dt + \int_4^8 f(t) e^{-st} dt$

$$20 \int_0^4 e^{-st} dt + 10 \int_4^8 e^{-st} dt$$

$$20 \left[ \frac{e^{-4s}}{s} - \frac{1}{s} \right] + 10 \left[ \frac{e^{-8s}}{s} - \frac{e^{-4s}}{s} \right]$$

$$\Rightarrow \frac{20e^{-4s}}{s} - \frac{20}{s} + \frac{10e^{-8s}}{s} - \frac{10e^{-4s}}{s}$$

$$f(s) = \left( -\frac{20}{s} + \frac{10e^{-4s}}{s} + \frac{10e^{-8s}}{s} \right)$$

Note

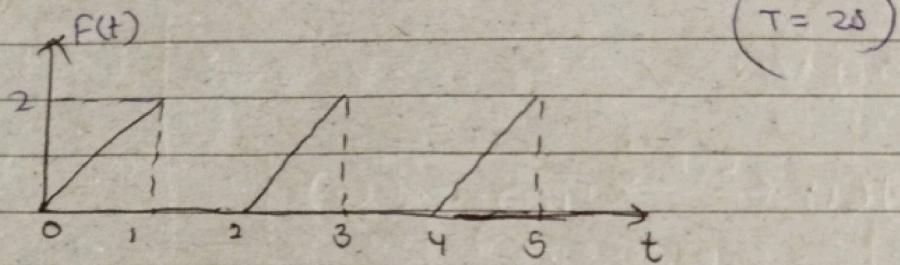
$$\left[ \frac{1}{1-e^{-Ts}} = \frac{1}{1-e^{-2s}} \right]$$

Date \_\_\_\_\_

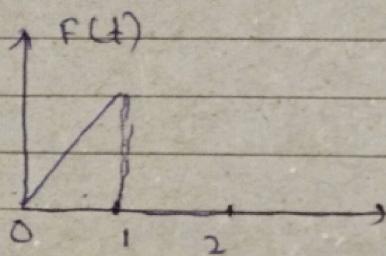
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Q:- Find L.T

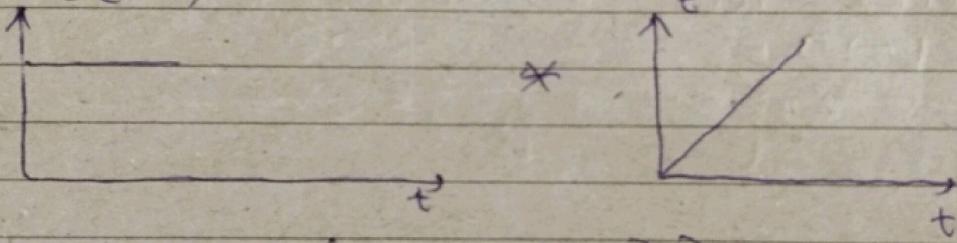


SOL  
⇒



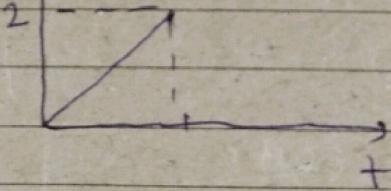
simulation of graph

$$\Rightarrow u(t) - u(t-1)$$



$$t(u(t) - u(t-1))$$

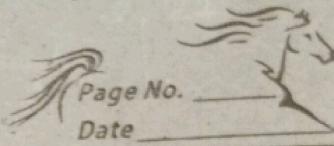
=



$$F(t) = t(u(t) - u(t-1))$$

$$2 \left[ t(u(t) - (t-1+1)u(t-1)) \right]$$

$$2 \left[ t(u(t)) - (t-1)u(t-1) + u(t-1) \right]$$



• Final value theorem :-

$t \rightarrow \infty$

$$\boxed{\lim_{t \rightarrow \infty} f(t) \xrightarrow{L.T} \lim_{s \rightarrow 0} s \cdot F(s)}$$

$$\begin{aligned} t &\leftrightarrow \frac{1}{s} \\ \infty &\leftrightarrow 0 \\ t=0 & \\ (s=0) & \end{aligned}$$

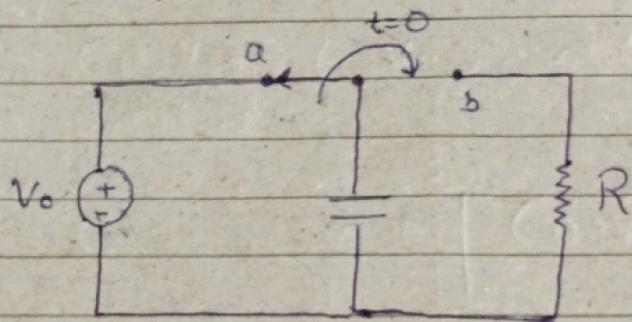
• Initial value theorem :-

$t \rightarrow 0$

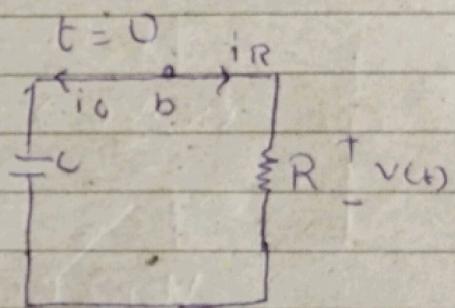
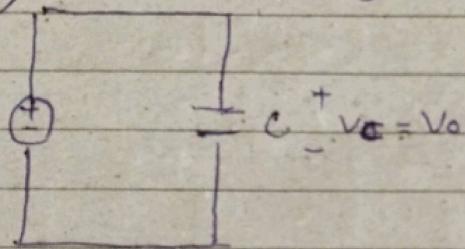
$$\boxed{\lim_{t \rightarrow 0} f(t) \xrightarrow{L.T} \lim_{s \rightarrow \infty} s \cdot f(s)}$$



## Source free R.C circuit :-



Capacitor initially charged to  $V_0$   
 $t < 0$ ,



we know

$$i = \frac{dq}{dt}$$

$$q = CV \Rightarrow \left( i_C = C \cdot \frac{dv}{dt} \right)$$

also

$$i_R = \frac{v(t)}{R}$$

Apply KCL at b

$$i_C + i_R = 0$$

$$C \cdot \frac{dv(t)}{dt} + \frac{v(t)}{R} = 0$$

across the capacitor

$$\frac{d(V(t))}{dt} \xrightarrow{\text{L.T.}} s \cdot V(s) - v(0^-) \quad \begin{matrix} \leftarrow \text{initial} \\ \text{condn} \end{matrix}$$

from ①

$$C \left[ s \cdot V(s) - v(0^-) \right] + \frac{V(s)}{R} = 0$$

$$C \left[ s \cdot V(s) - V_0 \right] + \frac{V(s)}{R} = 0$$

$$(s \cdot V(s)) - CV_0 + \frac{V(s)}{R} = 0$$

$$V(s) \left\{ C \cdot s + \frac{1}{R} \right\} = CV_0$$

$$V(s) = \frac{CV_0}{(Cs + \frac{1}{R})}$$

$$\boxed{V(s) = \frac{V_0}{s + \frac{1}{RC}}}$$

We have to find I.L.T of  $V(s)$

We know

$$\{se^{-at}\} = \frac{1}{s+a}$$

$$\mathcal{L} \left( \frac{1}{s+a} \right) = e^{-at}$$



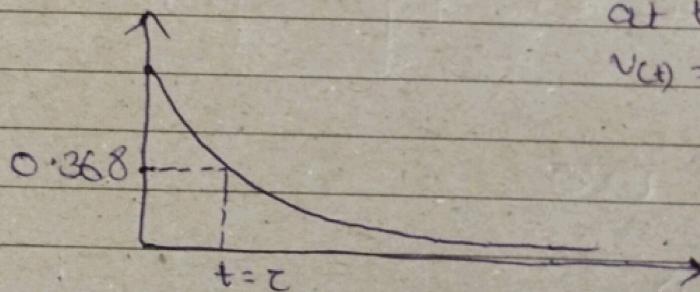
$$\mathcal{L}^{-1}\{V(s)\} = \mathcal{L}^{-1}\left\{\frac{V_0}{s + \frac{1}{RC}}\right\}$$

$$V(t) = V_0 e^{-\frac{t}{RC}}$$

$$\tau = \frac{1}{RC}$$

$$V(t) = V_0 e^{-\frac{t}{\tau}}$$

$V(t)$  vs t



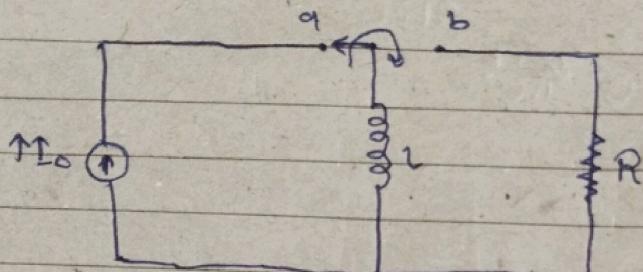
at  $t = \tau$

$$V(t) = V_0 e^{-1}$$

$$V(t) = 0.36 V_0$$

Source free R-L Ckt

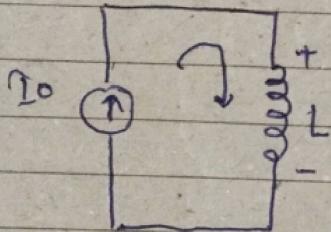
at  $t \leq 0$



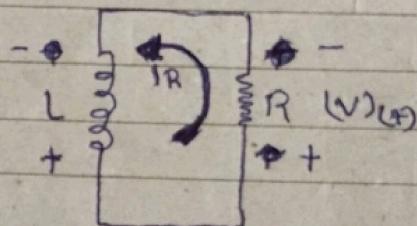
Let

Initially inductor  
has  $I_0$  current

at  $t \leq 0$



at  $t \geq 0$



Apply KVL when  $t \geq 0$

$$+V_L(+)+V(-)=0$$

$$\Rightarrow L \frac{di(t)}{dt} + iR = 0 \quad \text{--- (1)}$$

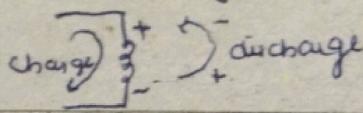
Applying Laplace transformation on (1)

$$\bullet \left\{ L \frac{di(t)}{dt} + i\omega R \right\} = 0$$

$$\left\{ sI(s) - I(0^-) \right\} + i\omega R$$

$$sLI(s) - L I_0 + I(s)\cdot R = 0$$

when inductor discharge its polarity will change



Date \_\_\_\_\_  
Page No. \_\_\_\_\_



$$I(s) = \frac{I_0}{(sL + R)}$$

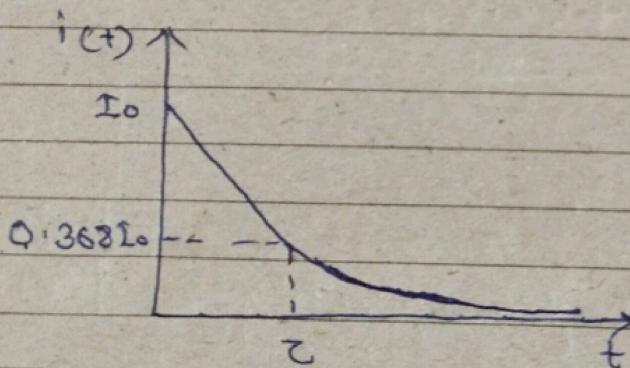
$$I(s) = \frac{I_0}{(s + R/L)} \quad \text{--- (11)}$$

taking inverse laplace transform of (11)

$$i(t) = I_0 e^{-Rt/L}$$

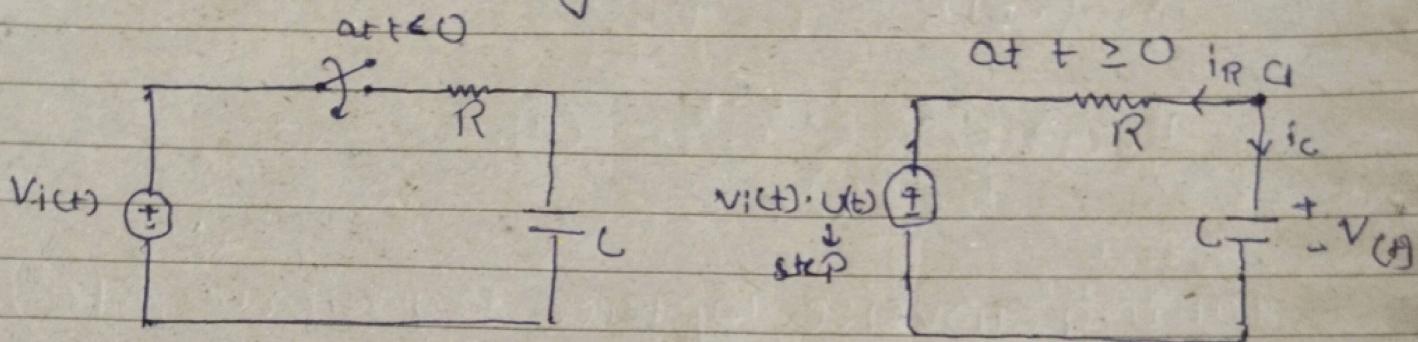
$$i_L(t) = I_0 e^{-t/\tau} \quad (\tau = L/R)$$

$$i(t) = I_0 e^{-t/\tau}$$



at  $t = \tau$   
 $i(t) = I_0 e^{-1}$

## Step Response of RC circuit :-



Cut node a apply KCL

$$i_R + i_C = 0$$

$$\frac{V(t) - V_i(t)U(t)}{R} + i_C = 0$$

$$\frac{V(t) - V_i(t) \cdot U(t)}{R} + C \cdot \frac{dV(t)}{dt} = 0$$

Apply Laplace

$$\frac{V(s) - \frac{V_i(s)}{s}}{R} + C \left\{ sV(s) - V(0^-) \right\} = 0$$

$$V(s) - \frac{V_i(s)}{s} + RC \left\{ sV(s) - V_0 \right\} = 0$$

$$V(s) - V_i(s) + RCsV(s) - RCV_0 = 0$$

$$V(s) \left\{ 1 + RCS \right\} = \frac{V_i(s)}{s} + RCV_0$$

$$i = \frac{dq}{dt}$$

$$q_v = Cu$$

$$r = \frac{dq_v}{dt}$$

$$i = C \cdot \frac{dv}{dt}$$

$$i_C = C \frac{dV(t)}{dt}$$

$$V_i \rightarrow s$$

$$V(t) \rightarrow s$$



$$V(s) = \frac{V_i(\omega)}{s(1+RCS)} + \frac{RCV_0}{(1+RCS)}$$

$$V(s) = \frac{RCV_0}{(1+RCS)} + \frac{V_i(s)}{s(1+RCS)}$$

→ apply partial fraction  
as  $s$  is in multiply)

Partial fraction for,

$$\frac{V_i(s)}{s(1+RCS)} = \frac{A}{s} + \frac{B}{(1+RCS)}$$

$$A|_{s=0} = \frac{V_i(\omega)}{1} = V_i(\omega)$$

$$B|_{s=1} = \frac{V_i}{-1/RC} = -RCV_i(\omega)$$

~~$$V(s) = \frac{RCV_i}{(1+RCS)}$$~~

$$V(s) = \frac{V_0}{(s + 1/RC)} + \frac{V_i(\omega)}{s} - \frac{RCV_i(\omega)}{(1+RCS)}$$

$$V(s) = \frac{V_0}{(s + 1/RC)} + \frac{V_i(\omega)}{s} - \frac{V_i(s)}{(s + 1/RC)} \quad \text{--- (1)}$$

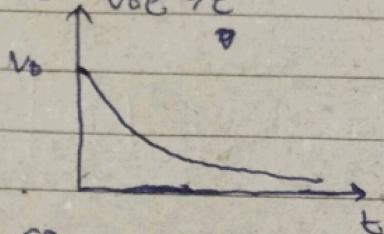
apply Laplace inverse on (1)

$$V(t) = V_0 e^{-t/\tau} + V_i(t)U(t) - V_i(t)e^{-t/\tau} \cdot U(t)$$

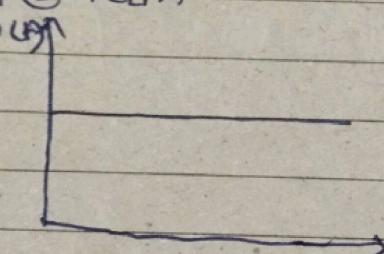
$$V(t) = V_0 e^{-t/\tau} + V_i(t) [1 - e^{-t/\tau}] \cdot U(t) \quad \tau = RC$$

Graph for final expression

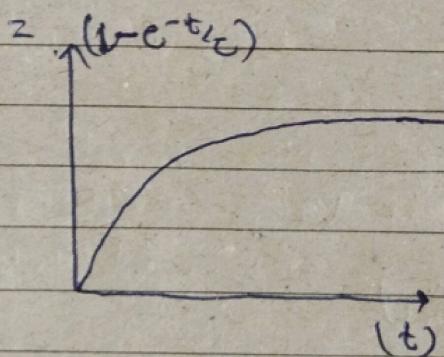
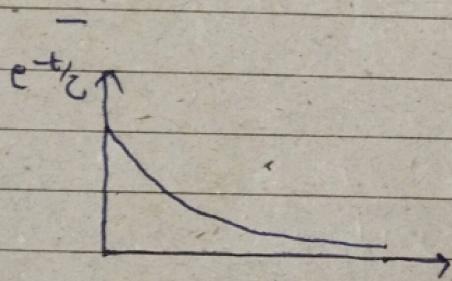
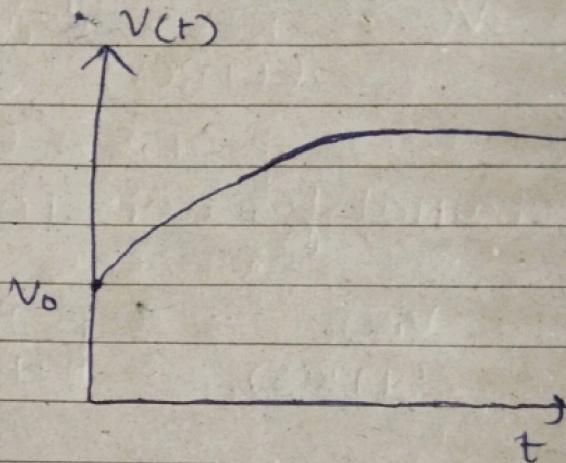
for ① term  $v_0 e^{-t/\tau}$



for ② term  $v_0(1 - e^{-t/\tau})$



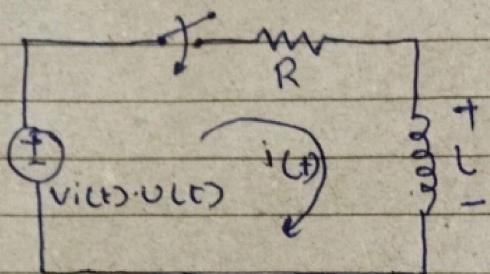
Final



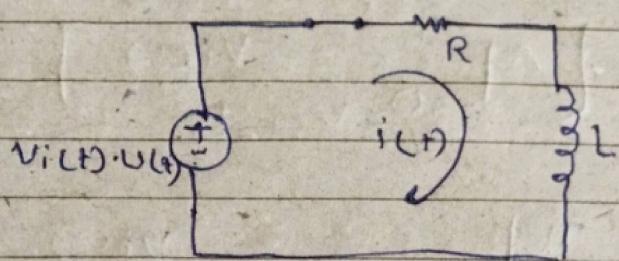


## Step Response of RL Circuit

at  $t=0$



at  $t > 0$ ,



Apply KVL,

$$V_i(t) \cdot U(t) - R i(t) - V_L(t) = 0$$

$$V_i(t) \cdot U(t) - R i(t) - L \frac{di}{dt} = 0$$

L.T

$$\frac{V_i(s)}{s} - R \hat{I}(s) - L \{ s \hat{I}(s) - I(0^-) \} = 0$$

$$\frac{V_i(s)}{s} - R \hat{I}(s) - s L \hat{I}(s) + L I_0 = 0$$

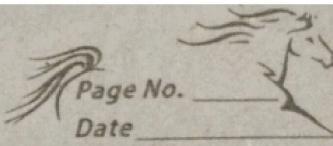
$$\frac{V_i(s)}{s} + L I_0 = R \hat{I}(s) + s L \hat{I}(s)$$

$$\frac{V_i(s)}{s} + L I_0 = \hat{I}(s) (R + sL)$$

$$\hat{I}(s) = \frac{V_i(s)}{s(R+sL)} + \frac{L I_0}{R+sL}$$

↳ Apply partial fraction

P.F



$$\frac{V_i(s)}{s(R+SL)} = \frac{A}{s} + \frac{B}{R+SL}$$

$$[ A ]_{s=0} = \frac{V_i(s)}{R}$$

$$[ B ]_{s=R/L} = \frac{V_i(s)}{R/L}$$

$$[ B = -\frac{L}{R} V_i(s) ]$$

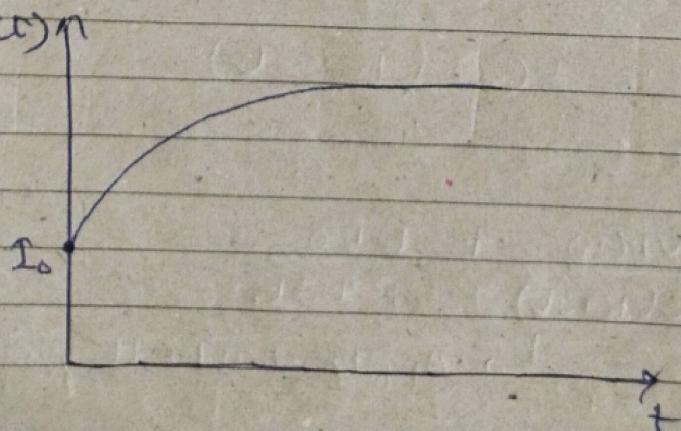
$$I(s) = \frac{I_0}{(s+R/L)} + \frac{V_i(s)}{R} \frac{1}{s} - \frac{L}{R} \frac{V_i(s)}{(R/L+s)}$$

APPLY ILT

$$i(t) = I_0 e^{-R/L t} + \frac{V_i(t)}{R} \cdot u(t) - \frac{V_i(t)}{R} e^{-R/L t} \cdot u(t)$$

$$i(t) = I_0 e^{-R/L t} + \frac{V_i(t)}{R} [ 1 - e^{-R/L t} ] u(t)$$

$$\underline{i(t) vst} \rightarrow i(t) u(t)$$





Note

$$t = \infty, t = 0$$

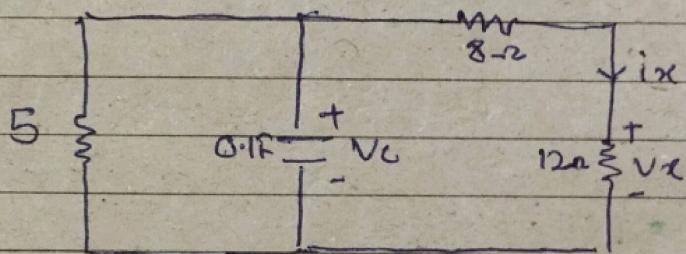
RC

$$V(t) = V(\infty) - [V(\infty) - V_0] e^{-t/\tau}$$

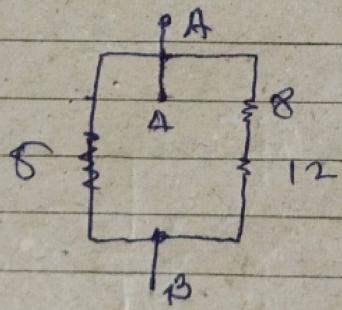
RL

$$i(t) = i(\infty) - [i(\infty) - i(0)] e^{-t/\tau}$$

Q :- Given  $V_{CC} = 15V$ . Find  $V_C, V_x, i_x$  for  $t > 0$



Sol To find  $\tau$  we have to find  $R_{\text{net}}$ ,  
to find  $R_{\text{net}}$  we open capacitors  
find  $R_{\text{net}}$   $R_{\text{net}}$  across it.



$$\Rightarrow 8 + 12 = 20$$

$$R_{\text{net}} = \frac{20 \times 8}{20 + 5} = 4 \Omega$$

$$\tau = RC$$

$$\tau = 4 \times 0.1$$

$$\tau = 0.4 \text{ s}$$

$$\therefore V(t) = V_0 e^{-t/\tau} \quad \text{or} \quad \tau = 0.4$$

$$V(t) = 15 e^{-t/0.4}$$

$$(V_C(t) = V(t) = 15 e^{-2.5 t})$$

For,

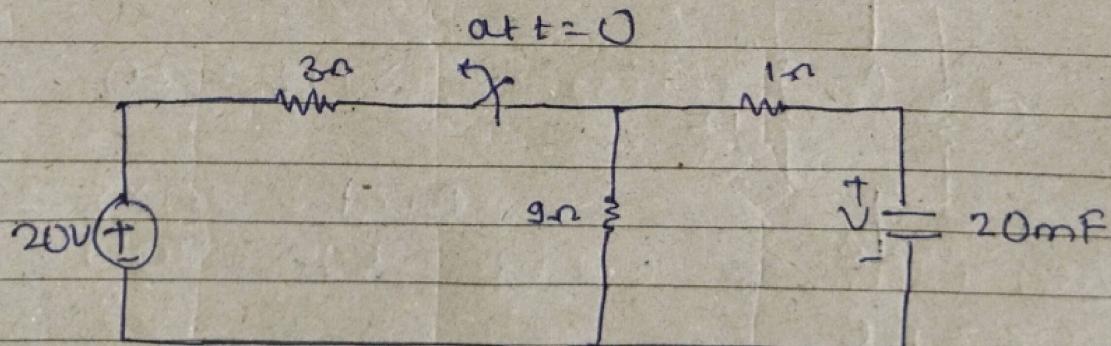
$$V_x = V_C(t) \cdot \frac{12}{8+12} = \frac{12}{20} V_0$$

$$(V_x = 9 e^{-2.5 t})$$

$$i_x = \frac{V_C(t) - V_{C0}}{8} = \frac{15 e^{-2.5 t} - 9 e^{-2.5 t}}{8}$$

$$(i_x = \frac{3}{4} e^{-2.5 t})$$

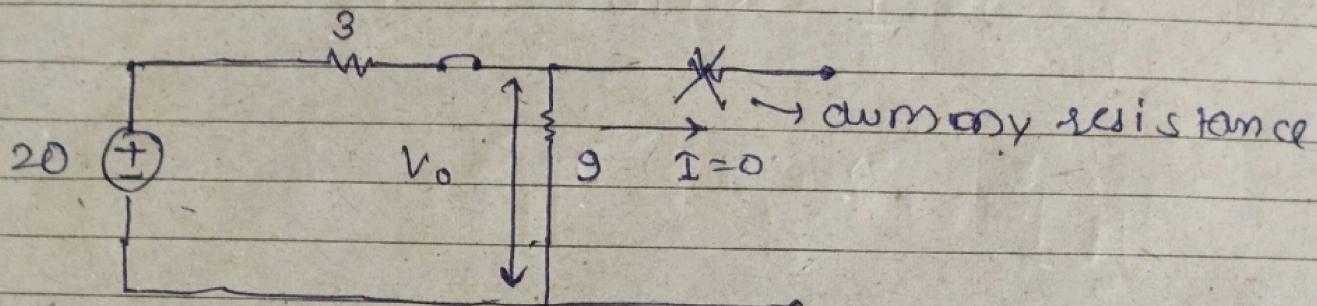
$\Phi$ :  $V(t)$ , initial energy stored in capacitor at  $t=0$





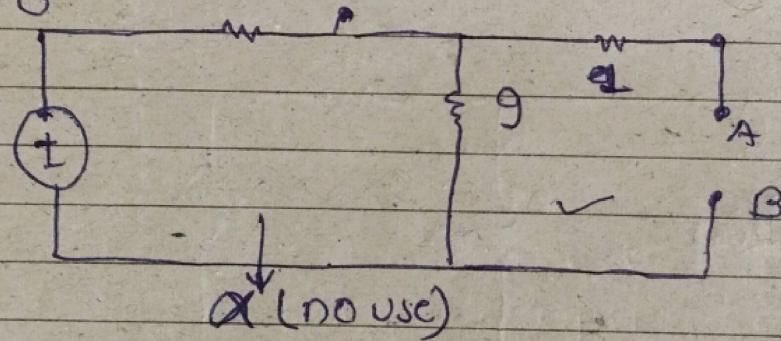
SOL at  $t < 0$

capacitor connected with DC  
thus it behave as open ckt as  $X_C = \infty$



$$V_o = 20 \times \frac{9}{(9+3)} \Rightarrow 15V$$

at  $t > 0$



$$R_{th} = 9 + 1$$

$$R_{th} = 10\Omega$$

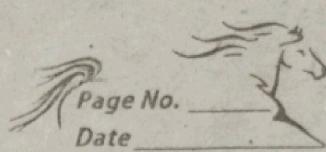
$$\tau = R_{th} C = 10 \times 20 \times 10^{-3}$$

$$\tau = 0.2s$$

$$V(t) = V_o e^{-t/\tau}$$

$$V(t) = 15 e^{-t/0.2} \Rightarrow (V(t) = 15 e^{-5t})$$

Use KVL during induction



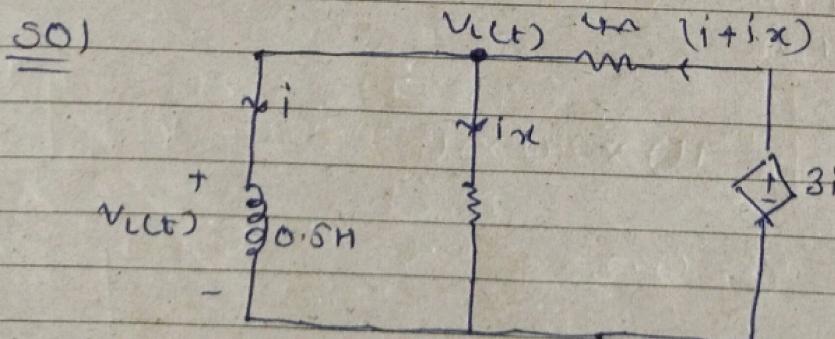
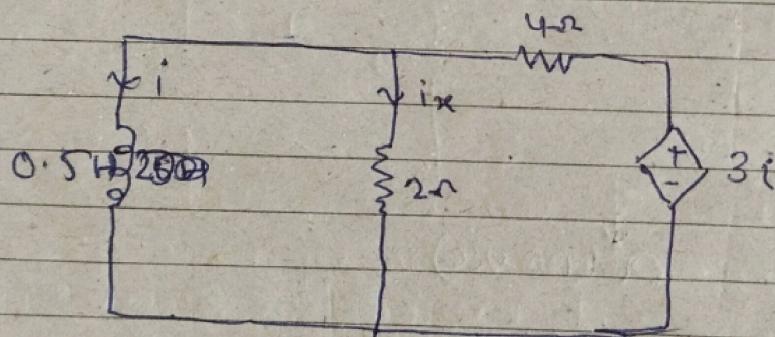
Energy,

$$= \frac{1}{2} \times N_0^2 \times \frac{20}{\pi} \times 20 \times 10^{-3} \times 15 \times 15$$

$$(E = 2.25 \text{ J})$$

H.A

Q: Assuming  $i(0) = 10 \text{ A}$  find  $i(t)$  &  $i_m(t)$  in the circuit



APPLY KVL in outer loop

$$+V_L(t) + 4(i + i_x) - 3i = 0$$

$$V_L(t) = L \frac{di}{dt} = L \{ S I(\omega) - i(0^-) \}$$

$$L \frac{di}{dt} + 4i + 4ix - 3i = 0$$

$$L \frac{di}{dt} + i + 4ix = 0$$

$$L \{ S I(\omega) - i(0^-) \} + I(\omega) + 4Ix(\omega) = 0 \quad \textcircled{1}$$

Also,

$$i_R(t) = \frac{V_L(t)}{2}$$

$$V_L(t) = L \frac{di}{dt}$$

$$I_R(t) = \frac{L di/dt}{2} = \frac{L}{2} \{ S I(\omega) - i(0^-) \}$$

$$= \frac{L}{2} S I(\omega) - \frac{L}{2} i(0^-)$$

$$Ix(\omega) = \frac{SL}{2} I(\omega) - SL \quad \text{put in } \textcircled{1}$$

$$SL I(\omega) - Li(0^-) + I(\omega) + 4 \left\{ \frac{SL}{2} I(\omega) - SL \right\} = 0$$

$$SL I(\omega) - 10L + I(\omega) + 2SL I(\omega) - 20L = 0$$

$$3SL I(\omega) - 30L + I(\omega) = 0$$

$$I(\omega) \{ 3SL + 1 \} = 30L$$

$$I(\omega) = \frac{30L}{3SL + 1} = \frac{30 \times 0.5}{(3 \times 0.5 \times 8 + 1)}$$

$$\bar{I}(s) = \frac{15}{s + \frac{3}{2}}$$

$$I(s) = \frac{15 \times 2/3}{s + 2/3} = \frac{10}{s + 2/3} \quad \textcircled{11}$$

Inverse Laplace transform of ⑪

$$(i(t) = 10e^{-2/3 t})$$

NOW we have

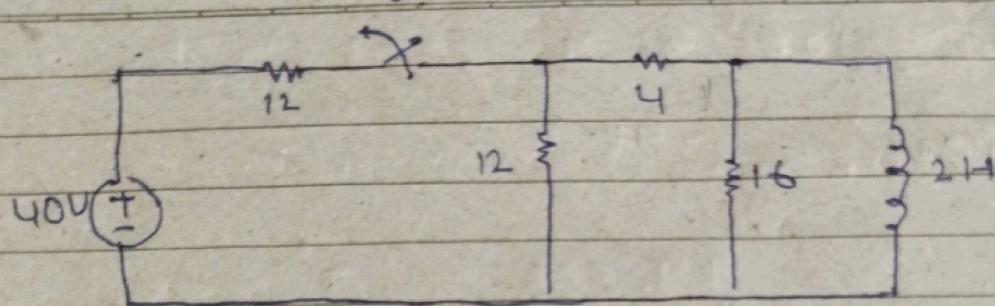
$$I_x(s) = \frac{5L}{2} \bar{I}(s) - 5L$$

$$I_x(s) = \frac{1}{4}s \bar{I}(s) - 25$$

APPLY I.L.T

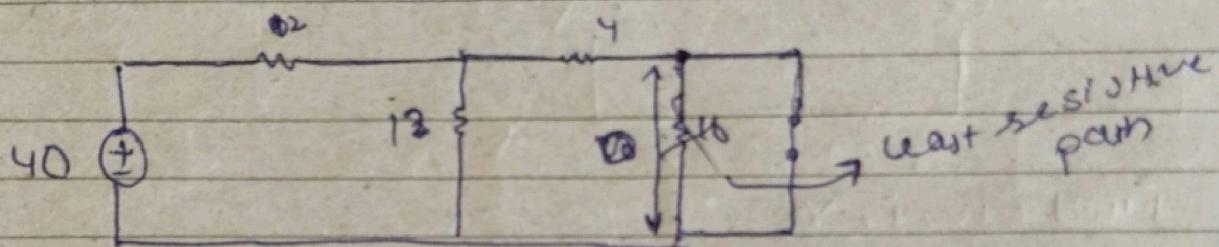
$$I_x(t) = \frac{1}{4}$$

Q:-



find  $i_{(e)}|_{t>0} = ?$

inductor behave like  
close ckt



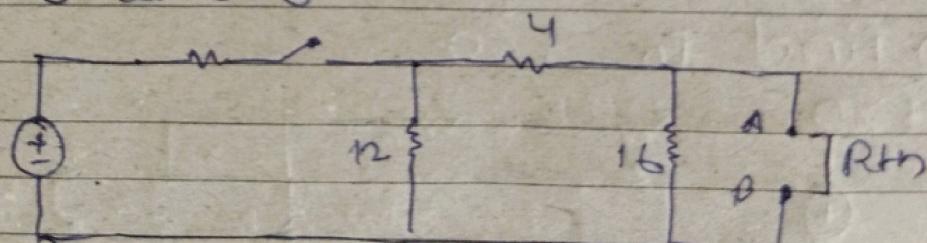
$$\frac{12 \times 4}{16} = 3 \text{ A}$$

$$R_{eq} = 3 + 2 = 5 \Omega$$

~~$$I = \frac{40}{5} = 8 \text{ A}$$~~

~~$$(I^0 = \frac{8 \times 12}{16} = 6 \text{ A})$$~~

To find  $Z$  at  $t > 0$



$$R_m = \frac{16}{2} = 8 \Omega$$

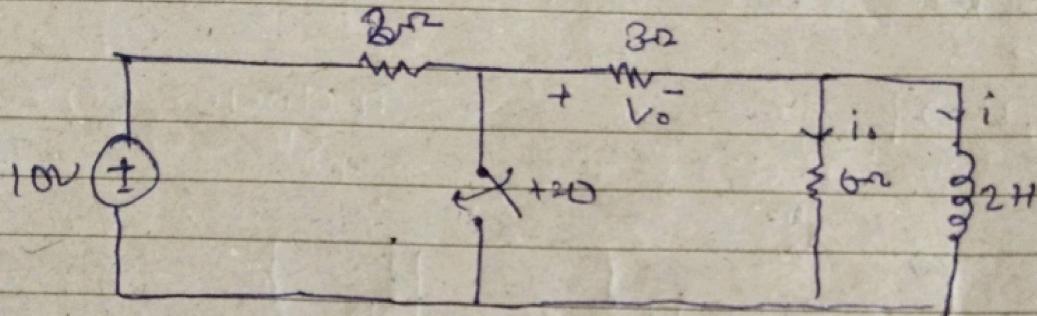
$$Z = \frac{L}{R} = \frac{1}{4}$$

NOW,

$$i(t) = i_0 e^{-t/\tau}$$

$$(i_{in} = 5 e^{-4t})$$

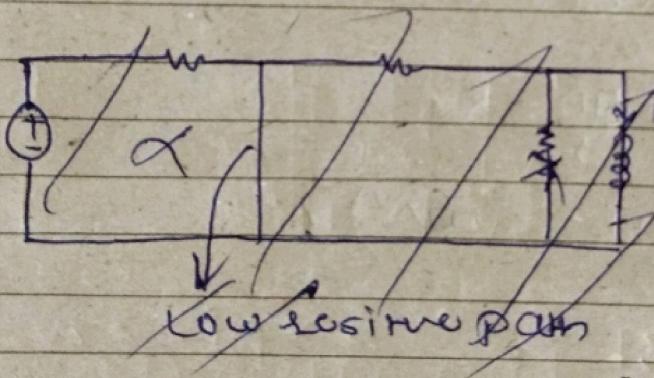
Q:



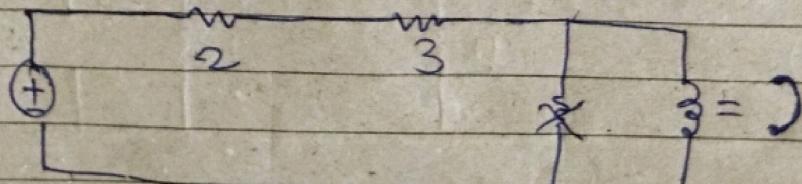
Find  $i_0, i, V_o$

at  $t \geq 0$  close

~~Ans~~  $i_0 = 0$  because  $2H$  get shorted and current follow low resistive path



To find  $I_0 \ t < 0$

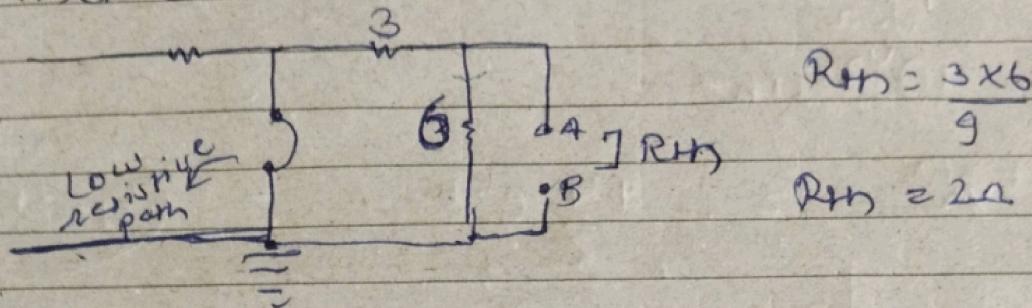


$$R_{eq} = 5\Omega$$

$$I_0 = \frac{10}{5} = 2A$$



To find  $\tau$



$$\tau = L/R = \frac{2}{2} = 1$$

$$i(+)=I_0 e^{-t/\tau}$$

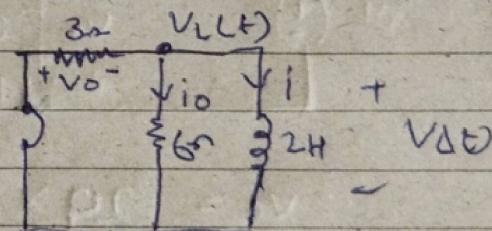
$$i(+)=2e^{-t}$$

$$(V_0 = 2 \times 3 = 6V)$$

Now find

$$\begin{aligned} i_0 &= ? \\ V_0 &=? \quad t > 0 \end{aligned}$$

$$i(+)=2e^{-t}$$



$$i_0 = \frac{V_L(t)}{6} = i_0 = \frac{L di/dt}{6}$$

$$i_0 = \frac{2 \cdot d(2e^{-t})/dt}{6}$$

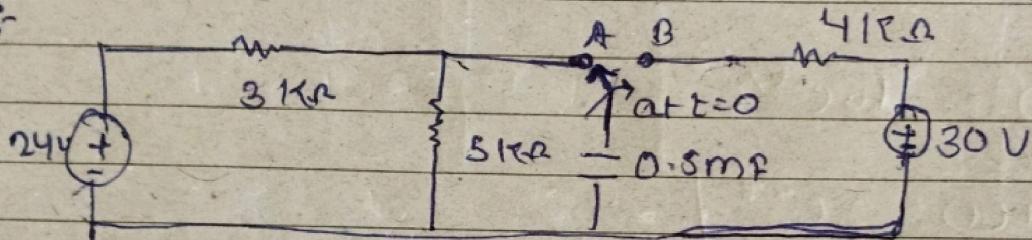
$$i_0 = -\frac{4(e^{-t})}{6} = \left(-\frac{2}{3}e^{-t}\right)$$

$$\frac{(i_0 + i(t))}{+ 3\Omega} = V_o$$

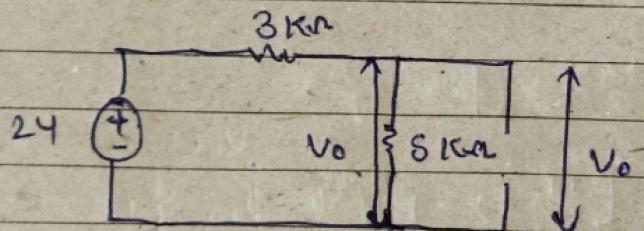
$$\Rightarrow \frac{(-\frac{2}{3} + 2) e^{-t}}{3}$$

$$V_o = \frac{+4}{3} e^{-t} = 4e^{-t}$$

Q:

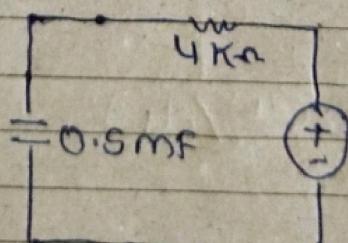


at  $t < 0$



$$V_o = 24 \times \frac{5}{5+3} \Rightarrow 12 \times \frac{1}{2} = 6 \text{ V}$$

at  $t > 0$



at node C

We know as it is not source free RC circuit  
 $V(t) = V_{(0)} - [V_{\infty} - V_0] e^{-t/\tau}$

$$V(t) = 30 - [30 - 15] e^{-t/2}$$

$$\left. \begin{aligned} V(t) &= 30 - 15 \\ &= 30 - 15 e^{-t/2} \end{aligned} \right)$$

$$C = RC$$

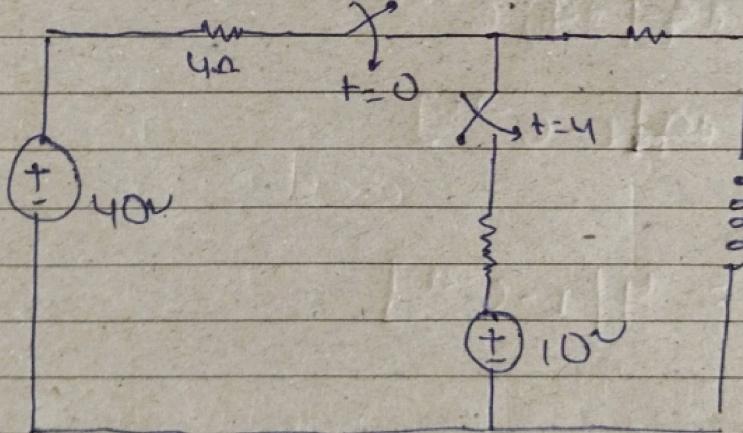
$$\tau = 4 \times 2 \times 0.5 \text{ ms}$$

$$\tau = 2$$

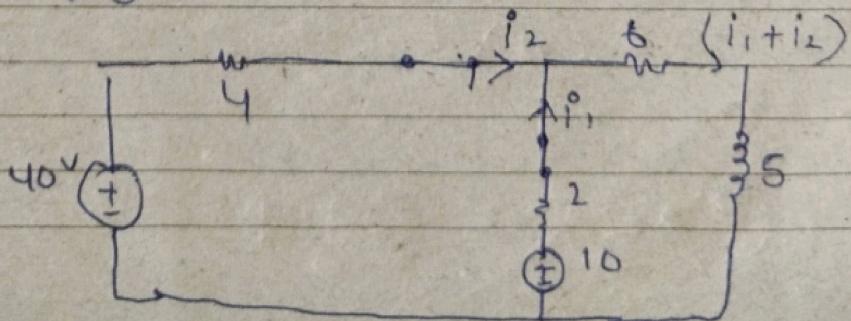
$$V(t)|_{15} = 30 - 15 e^{-\frac{1}{2}}$$

$$(V(t)|_{45} = 30 - 15 e^{-2})$$

Q:-



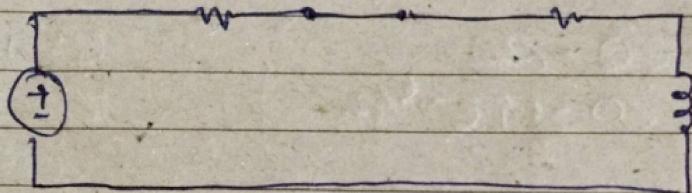
at  $t > 0$



# APPLICATION IN CIRCUITS

Q1 - Q10 -

$$4 > t \geq 0$$



$$i_{\infty} = \frac{10}{5} = 2A$$

$$\tau = L/R = \frac{10}{5} = 2$$

$$i(t) = i_{\infty} - (i_{\infty} - i_0) e^{-t/\tau}$$

$$2 - (2 - 1) e^{-2t}$$

$$1 - e^{-2t}$$

$$i(t) = 2[1 - e^{-2t}]$$

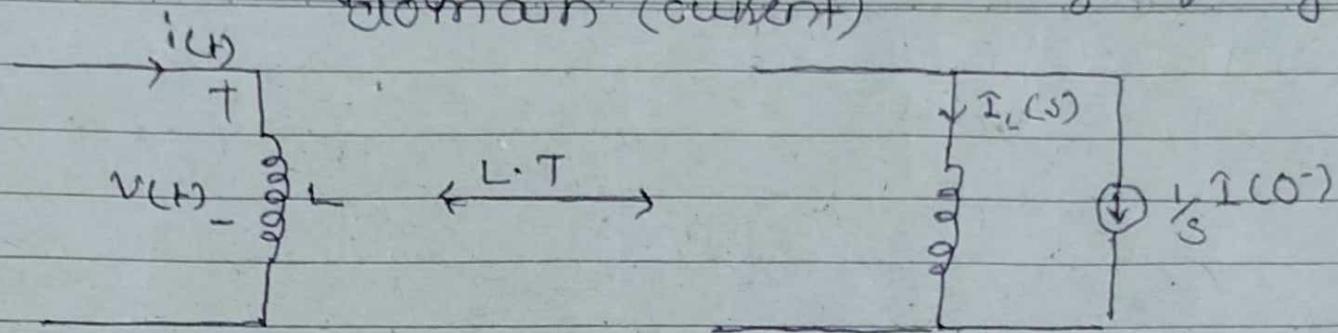
inductor L KO SL se replace kardenge

Date \_\_\_\_\_

Page No. \_\_\_\_\_



\* ~~Capa~~ changing time domain ~~to~~ frequency domain (current)



$$V(t) = L \frac{di}{dt}$$

Applying  $L \cdot T$

$$V(s) = L \{ sI(s) - I(0^+) \}$$

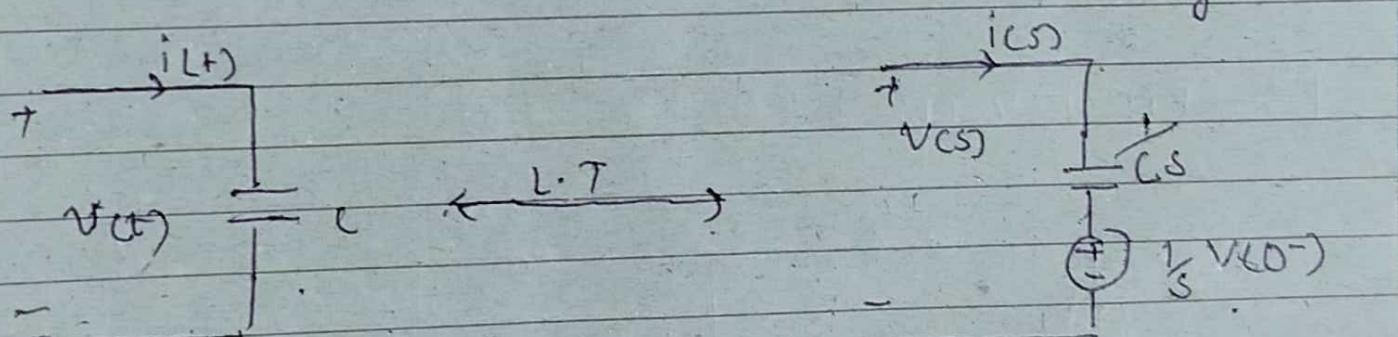
$$V(s) = sL I(s) - L \cdot I(0^+)$$

$$I_s + S L = V(s) + L \hat{I}(0^+)$$

$$I(s) = \frac{1}{sL} V(s) + \frac{1}{s} I(0^+)$$

$$I(s) = I_L(s) + \frac{1}{s} I(0^+)$$

\* In case of capacitor:



$$i = \frac{dq}{dt}$$

$$q = CV$$

$$i(t) = C \frac{dV(t)}{dt}$$

$$I(s) = C \{ sV(s) - v(0^-) \}$$

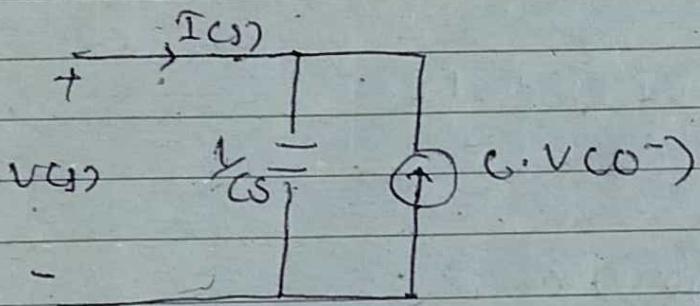
$$I(s) = (sV(s)) - (v(0^-))$$

$$V_s = \frac{I(s)}{Cs} + \frac{v(0^-)}{s}$$

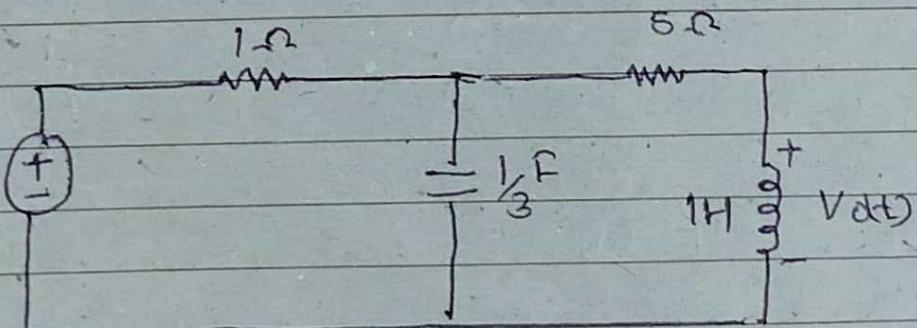
$$V(s) = \frac{1}{Cs} I(s) + \frac{v(0^-)}{s}$$

$$I(s) = \frac{V(s)}{\frac{1}{Cs}} - C \cdot v(0^-)$$

current domain



Q:- Find  $v_o(t)$  ?



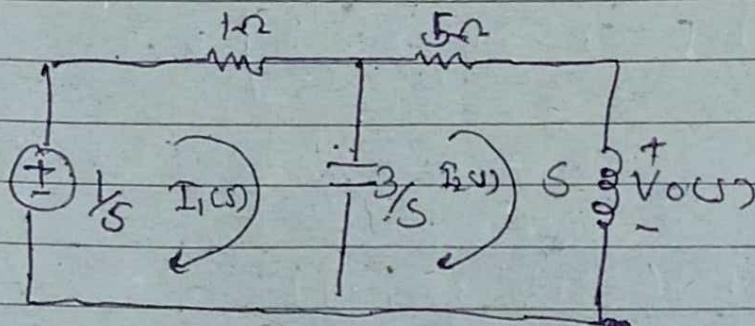


$$\underline{S(s)} \quad U(s) \xleftrightarrow{LT} \frac{1}{s}$$

$$1, 5 \text{ n} \xleftrightarrow{LT} 1, 5 \text{ n}$$

$$\frac{1}{3} F \xleftrightarrow{LT} \frac{1}{cs} = \frac{1}{\frac{1}{3}s} = 3s$$

$$1H \xleftrightarrow{LT} SL = s$$



as initial condn is not given then initial value is zero

Apply KVL

$$\frac{1}{s} - I_1(s) - \frac{3}{s} (I_1(s) - I_2(s)) = 0 \quad (1)$$

$$-5I_2(s) - I_2(s)s - \frac{3}{s} (I_2(s) - I_1(s))$$

$$-5I_2(s) - I_2(s)s - \frac{3}{s} I_2(s) + \frac{3}{s} I_1(s) = 0$$

$$\frac{3}{s} I_1(s) = \left(5 + s + \frac{3}{s}\right) I_2(s)$$

$$I_1(s) = \left(s + s + \frac{3}{s}\right) \frac{1}{3} I_2(s) \quad \text{put in } (1)$$

$$I_5 = \left( \frac{1}{8} + \frac{3}{s} \right) \frac{5}{3} \left( s^2 + 5s + 3 \right) I_2(s) - \frac{3}{s} I_2(s)$$

$$I_5 = \frac{(s+3)}{s} \cdot \frac{8}{3} \left( s^2 + 5s + 3 \right) I_2(s) - \frac{3}{s} I_2(s)$$

$$I = (s+3) \frac{1}{3} (s^2 + 5s + 3) I_2(s) - 3 I_2(s)$$

$$I = \left[ \frac{(s+3)(s^2 + 5s + 3) - 9}{3} \right] I_2(s).$$

$$I_2(s) = \frac{3}{[(s+3)(s^2 + 5s + 3) - 9]}$$

$$I_2(s) = \frac{3}{s^3 + 5s^2 + 3s + 3s^2 + 15s + 8 - 8}$$

$$I_2(s) = \frac{3}{s^3 + 8s^2 + 18s}$$

$$I_2(s) = \frac{3}{s(s^2 + 8s + 18)}$$

$$V_0(s) = s I_2(s) = \frac{3}{s(s^2 + 8s + 18)} \cancel{s}$$

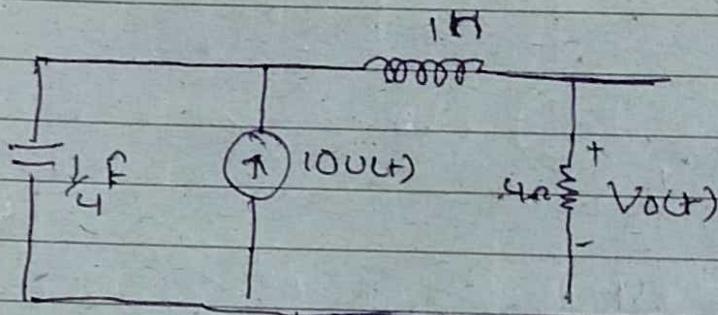
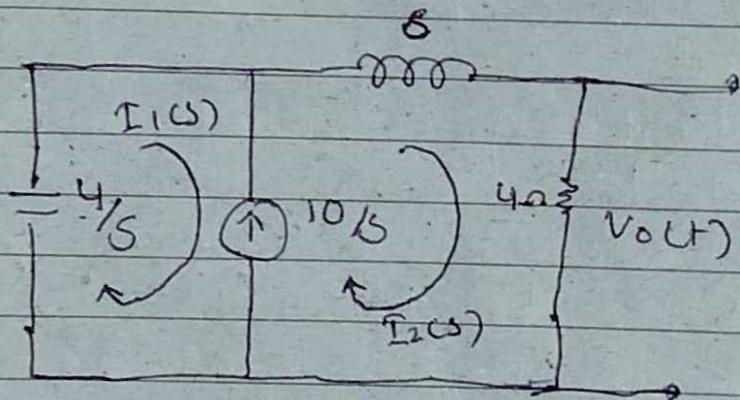


$$V(s) = \frac{3}{s^2 + 8s + 16 + 2}$$

$$V(s) = \frac{1}{\sqrt{2}} \frac{3 \times \sqrt{2}}{(s+4)^2 + (\sqrt{2})^2}$$

1. L.T

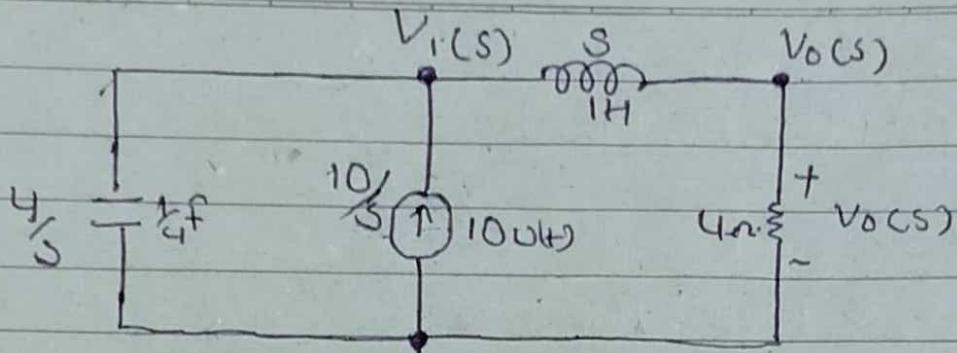
$$V_o(t) = \frac{3}{\sqrt{2}} e^{-4t} \cdot \sin \sqrt{2} t \cdot V(t)$$

Q:- Find  $V_o(t)$ SOL

$$-\frac{4}{s} I_1(s) -$$

$$I_2 - I_1 = 10$$

~~DO NOT~~ apply superposition it become complicated



Apply nodal analysis :-

$$\frac{V_1}{4/s} - \frac{10}{s} + \frac{V_1 - V_o}{s} = 0$$

$$\frac{sV_1}{4} - \frac{10}{s} + \frac{V_1}{s} - \frac{V_o}{s} = 0$$

$$V_1 \left( \frac{s}{4} + \frac{1}{s} \right) - \frac{V_o}{s} = \frac{10}{s}$$

$$V_1 \left( \frac{s^2 + 4}{4s} \right) - \frac{V_o}{s} = \frac{10}{s}$$

$$V_1 \left( \frac{(s^2 + 4s)}{4s} \right) - \frac{V_o}{s} = \frac{10}{s}$$

$$V_1(s^2 + 4) - 4V_o = 40 \quad \text{--- (1)}$$

$$\frac{V_o - V_1}{s} + \frac{V_o}{4} = 0$$

$$\frac{V_o}{s} - \frac{V_1}{s} + \frac{V_o}{4} = 0$$



$$V_o \left( \frac{1}{s} + \frac{1}{4} \right) = \frac{V_L}{s}$$

$$\frac{V_o(4+s)}{4s} = \frac{V_L}{s} \quad \text{--- (1)}$$

$$(1) - (1)$$

$$V_o \left( \frac{s+4}{4} \right) (s^2 + 4) - 4V_o = 40$$

$$V_o(s^2 + 4s + 4s^2 + 16 - 16) = 160$$

$$V_o = \frac{160}{s(s^2 + 4s + 4)}$$

$$V_o = \frac{160}{s(s+2)^2}$$

Partial fraction

$$\frac{160}{s(s+2)^2} = \frac{A}{s} + \frac{B}{s+2} + \frac{C}{(s+2)^2}$$

$$160 = A(s+2)^2 + B(s+2)s + Cs$$

$$160 = -2c^2$$

$$(c=80)$$

$$160 = A4$$

$$(A=40)$$

$$160 = 360 + 3B - 80$$

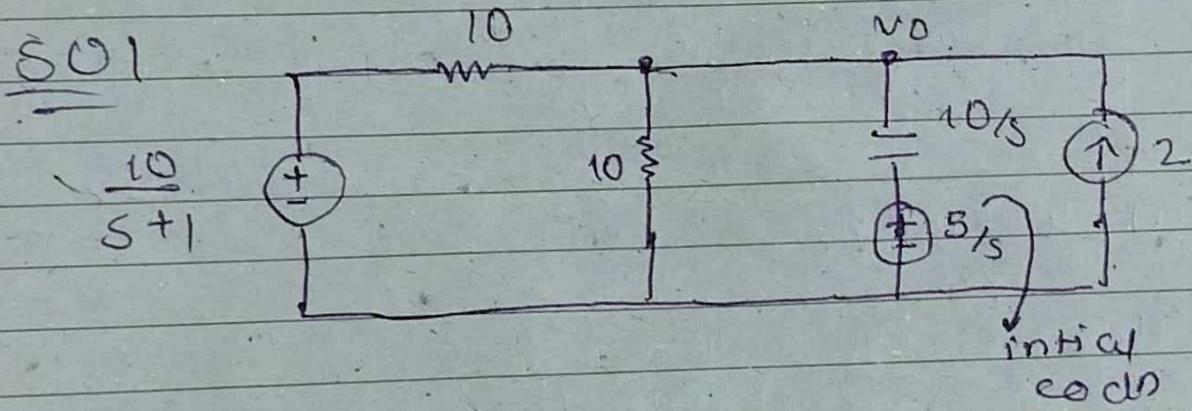
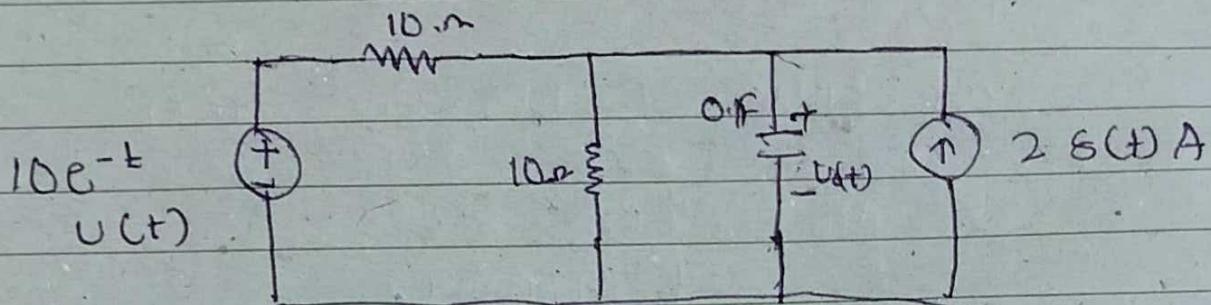
$$B = -40$$

$$V_o(s) = \frac{40}{s} - \frac{40}{s+2} - \frac{80}{(s+2)^2}$$

ILT

$$V_o(t) = 40 \left( 1 - e^{-2t} - 2e^{-2t} \right)$$

Q:- Find  $V_o(t)$ , given  $V_o(0^-) = 5V$



$$\frac{V_o - 10}{s+1} + \frac{V_o}{10} + \frac{V_o - 5/s}{10/s} - 2 = 0$$

$$\frac{V_o}{10} - \frac{1}{s+1} + \frac{V_o}{10} + \frac{5V_o}{10} - \frac{1}{2} - 2 = 0$$

$$V_o \left( \frac{1}{5} + \frac{s}{10} \right) \approx \frac{3}{2} + \frac{1}{s+1}$$



$$V_o(s) = \frac{10}{(s+1)(s+2)} + \frac{s(10)}{2, s+2}$$

$$V_o(s) = \frac{10}{(s+1)(s+2)} + \frac{2s}{(s+2)}$$

$$\frac{10}{(s+1)(s+2)} = \frac{A}{s+1} + \frac{B}{s+2}$$

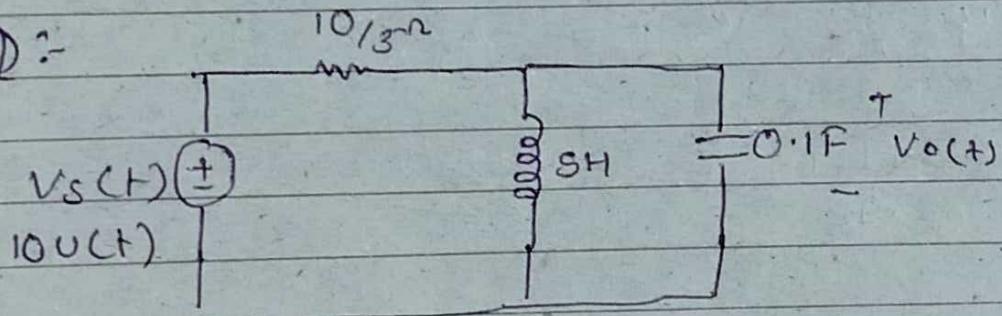
$$10 = A(s+2) + B(s+1)$$

$$(A = 10), \quad 10 = -B \\ (B = -10)$$

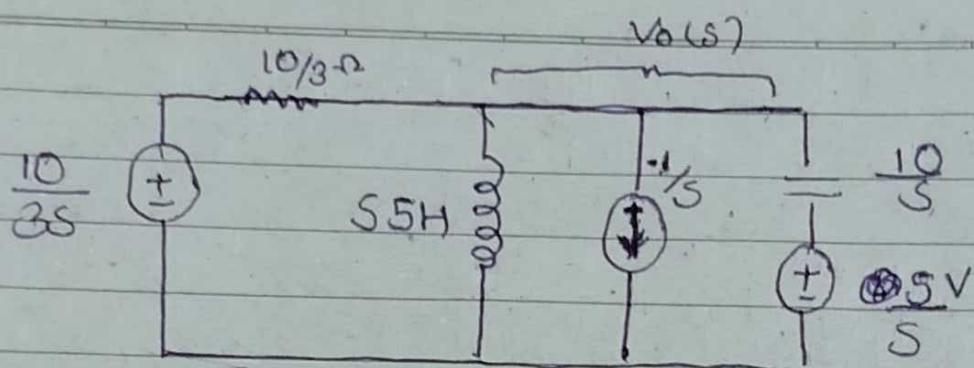
$$V_o(s) = \frac{10}{s+1} - \frac{10}{(s+2)} + \frac{2s}{s+2}$$

$$= \{10e^{-t} + 15e^{-2t}\} v_o(t)$$

Q:



assume that at  $t=0$ ,  $-1A$  flow through inductor &  $+5V$  is across the capacitor



Applying nodal analysis

$$\frac{V_{o(s)}}{10/3} - \frac{10/3}{10/3} + \frac{V_{o(s)}}{5s} + \left(-\frac{1}{s}\right) + \frac{V_{o(s)} - 5/s}{10/s} = 0$$

$$-\frac{3}{10}V_{o(s)} - \frac{10/s}{10/3} + \frac{V_{o(s)}}{5s} - \frac{1}{s} + \frac{5}{10}V_{o(s)} - \frac{8}{10}\frac{1}{s} = 0$$

$$-\frac{3}{10}V_{o(s)} - \frac{3}{5} + \frac{V_{o(s)}}{5s} - \frac{1}{s} + \frac{5}{10}V_{o(s)} + \frac{1}{2} = 0$$

$$-\frac{3}{10}V_{o(s)} + \frac{1}{5s}V_{o(s)} + \frac{5}{10}V_{o(s)} = \frac{4+1}{2}$$

$$V_{o(s)} \left\{ \frac{3}{10} + \frac{1}{5s} + \frac{5}{10} \right\} = \frac{8+5}{2s}$$

$$V_{o(s)} \left\{ \frac{3s+1+s^2}{5+10s} \right\} = \frac{s+8}{2s}$$

$$V_{o(s)} = \frac{5(s+8)}{s^2 + 3s + 2}$$

$$\frac{5(s+8)}{(s+1)(s+2)} = \frac{A}{(s+1)} + \frac{B}{(s+2)}$$



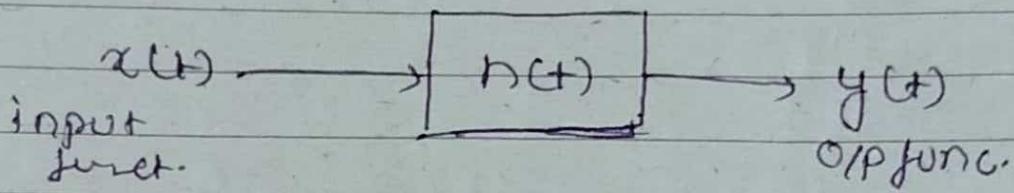
$$A|_{S=1} = 5 \times 7 = 35, \quad B = -30$$

$$v_0(s) = \frac{35}{(s+1)} - \frac{30}{s+2}$$

T.T.T

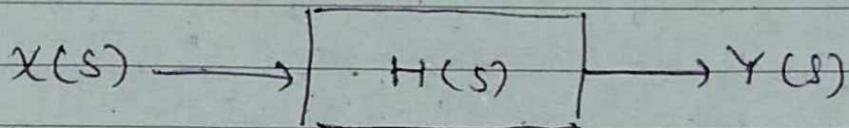
$$[35e^{-t} - 30e^{-2t}]u(t)$$

## Transfer Function



$$y(t) = x(t) * h(t)$$

$$Y(s) = X(s) \cdot H(s)$$



$$\boxed{H(s) = \frac{Y(s)}{X(s)}} \rightarrow \text{"Transfer function"}$$

Q:- If input/O/P func is  $y(t) = 10e^{-t} \cos 4t u(t)$

$$x(t) = e^{-t} \cdot u(t)$$

Find transfer func. & impulse response

$$H(s) = \frac{Y(s)}{X(s)} \quad \rightarrow \textcircled{1}$$

$$Y(s) = 10 \cdot \frac{(s+1)}{(s+1)^2 + 4^2} = \frac{10(s+1)}{(s+1)^2 + 4^2}$$

$$X(s) = \frac{1}{(s+1)}$$

Put in eq. ①



$$H(s) = \frac{10(s+1)}{(s+1)^2 + 4^2}$$

$\cancel{(s+1)}$

$$H(s) = 10 \left\{ \frac{(s+1)^2 + 16 - 16}{(s+1)^2 + 4^2} \right\}$$

$$H(s) = 10 \left\{ \frac{(s+1)^2 + 16}{(s+1)^2 + 4^2} - \frac{16}{(s+1)^2 + 4^2} \right\}$$

$$H(s) = 10 \left\{ 1 - \frac{16}{(s+1)^2 + 4^2} \right\} = \left\{ 1 - \frac{4 \times 4}{(s+1)^2 + 4^2} \right\}$$

I.L.T.

$$h(t) = 10 \left\{ \delta(t) - 4e^{-t} \sin 4t \right\}$$

$$h(t) = 10\delta(t) - 40e^{-t} \sin 4t \cdot u(t)$$

$\Rightarrow$  impulse response means  $x(t) = \delta(t)$  &  
 $x(s) = 1$  thus  $y(t) = h(s)$ ,  $y(t) = h(t)$

↑ impulse response

thus,

$$y(t) = 10\delta(t) - 40e^{-t} \sin 4t \cdot u(t)$$

Q:  $H(s) = \frac{2s}{(s+6)}$  Find  $y(t)$ , when  $x(t) = 10e^{-3t}u(t)$

SOL  $H(s) = \frac{2s}{s+6}$

L.T

~~$n(t) = 2e^{-6t}$~~

~~$x(t) = 1$~~

thus,

~~$y(t) = n(t)$~~

~~$y(t) = 2e^{-6t}$~~

$Y(s) = X(s) \cdot H(s)$

$$\frac{10}{s+3} \cdot \frac{2s}{s+6} = \frac{20s}{(s+3)(s+6)}$$

$$Y(s) = \frac{-20}{s+3} + \frac{40}{s+6}$$

$$y(t) = (-20e^{-3t} + 40e^{-6t})u(t)$$

when impulse response

$$H(s) = h(s)$$

$$Y(s) = \frac{2s}{s+6}$$

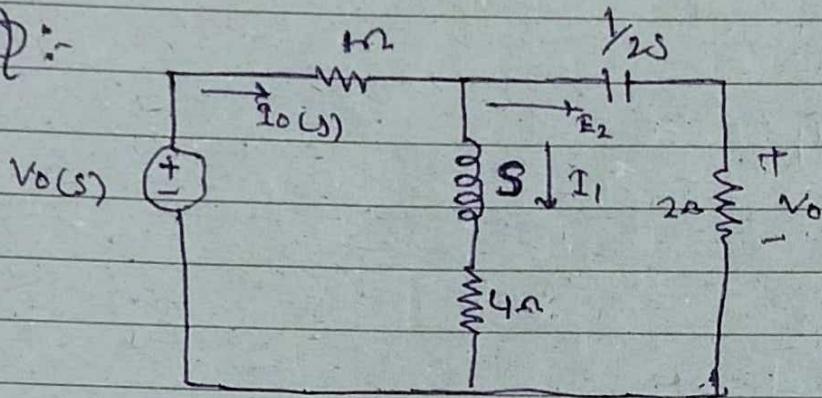


$$= \frac{2s}{s+6}$$

$$\Rightarrow 2 \left( \frac{s+6 - 6}{s+6} \right) \Rightarrow 2 \left( 1 - \frac{6}{s+6} \right)$$

$$\Rightarrow 28(t) - 12e^{-6t} + v(t)$$

Q:-



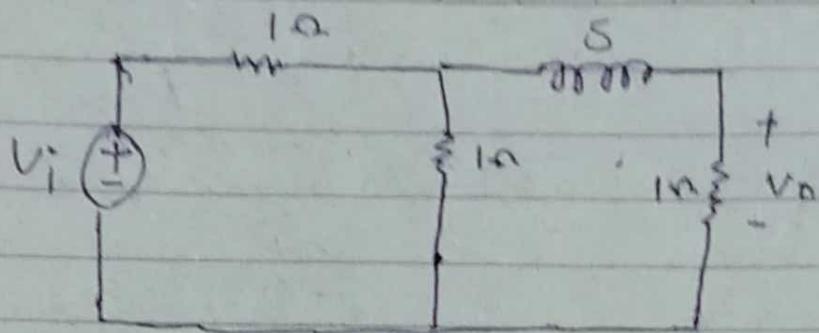
$$\Rightarrow \text{Find Chain } H(s) = \frac{V_o(s)}{I_o(s)}$$

~~SOL~~  $I_2 = \frac{I_o(s) \cdot (s+4)}{\left( s+4 + \frac{1}{2s} + 2 \right)}$   $\rightarrow$  Current divider rule

$$\text{At } V_o(s) = I_2 \cdot 2 = 2 \frac{I_o(s) (s+4)}{\left( s+4 + \frac{1}{2s} + 2 \right)}$$

$$(H(s)) = \frac{V_o(s)}{I_o(s)} = \frac{2(s+4)}{\left( s+4 + \frac{1}{2s} + 2 \right)}$$

Q:



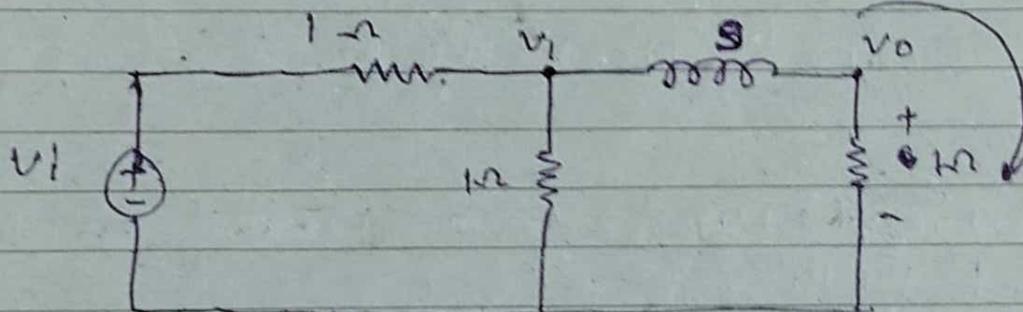
Find (a)  $H(s) = \frac{V_o}{V_i} = ?$

(b) impulse response

(c)  $V_i(t) = U(t)$

(d)  $V_i(t) = 8\cos 2t$

SOL



Apply nodal at  $V_i$

$$\frac{V_1 - V_i}{1} + \frac{V_1}{1} + \frac{V_1 - 0}{(s+1)} = 0$$

$$V_1 - V_i + V_1 + \frac{V_1}{s+1}$$

$$2V_1 - V_i + \frac{V_1}{s+1} = 0$$

$$2V_1 + \frac{V_1}{s+1} = V_i$$

$$10 \left\{ \frac{2s+2+1}{s+1} + v_1 \right\} = v_i$$

$$v_i \left\{ \frac{2s+2+1}{s+1} \right\} = v_i$$

$$v_i \left\{ \frac{2s+3}{s+3} \right\} = v_i$$

$$v_o = \frac{(s+1)v_i}{(2s+3)}$$

Apply voltage divider rule

$$v_o = v_i \cdot \frac{1}{s+1} \text{ towards } R$$

$$v_o = \frac{(s+1)v_i}{(2s+3)} \cdot \frac{1}{s+3}$$

$$\frac{v_o}{v_i} = \frac{1}{(2s+3)} = \frac{1}{2} \left[ \frac{1}{s+\frac{3}{2}} \right]$$

$$(a) H(s) = \left( \frac{v_o}{v_i} = \frac{1}{2} \left[ \frac{1}{s+\frac{3}{2}} \right] \right)$$

Apply ILT

$$h(t) = \frac{1}{2} e^{-\frac{3}{2}t} u(t)$$

$$(b) x(t) =$$

$$y(t) = \frac{1}{2} e^{-\frac{3}{2}t} u(t)$$

$$v = v_i(t) = u(t)$$

$$v_i(s) = \frac{1}{s}$$

$$Y(s) = H(s) \cdot X(s)$$

$$Y(s) = \frac{1}{2s+3} \cdot \frac{1}{s} = \frac{1}{2s(s+3/2)}$$

Apply P.F then Laplace transform,

$$y(t) = \frac{1}{3} [1 - e^{-3t/2}] u(t)$$

$$(a) v_i(t) = 8 \cos 2t$$

$$Y(s) = \frac{8s}{s^2 + 4} + \frac{1}{2(s+3/2)}$$

$$Y(s) = \frac{4s}{(s+3/2)(s^2+4)}$$

Applying P.F

$$\frac{4s}{(s+3/2)(s^2+4)} = \frac{A}{s+3/2} + \frac{Bs+C}{s^2+4}$$

$$-A = B = \frac{24}{25}$$

~~Ans~~



## Network Stability

$$C^{-at} \leftrightarrow \frac{1}{s+a}$$

how we find signal is stable not

$\frac{1}{(s+a)}$  to find poles <sup>Equate</sup> ~~But~~ Denominator = 0

$$s+a = 0 ,$$

$[s = -a]$  pole is  $\text{ve}$

if poles of the system is  $\text{ve}$  then system is  $\text{ve}$  & converging graph & vice versa

$$H(s) = \frac{N(s)}{D(s)} = \frac{(s+a_1)(s+a_2)(s+a_3) \dots (s+a_n)}{(s+b_1)(s+b_2)(s+b_3) \dots (s+b_m)}$$

$$s = -a_1, -a_2, -a_3, -a_4 \dots -a_n$$

↑

zeros of the system & it does not give any idea about the stability of system

$$s = -b_1, -b_2, -b_3, -b_4 \dots -b_m$$

↓

Pole's of the system it give idea of the stability of the system

Two port Network :-

$\tilde{Z}$  - parameter

$Y$  - " "

$H$  - " "

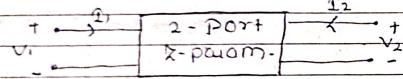
$G$  - " "

$ABCD$  - " "

①  $Z$ -parameter :-

↳ Impedance parameters :-

$$Z = V/I \Rightarrow V = Z \cdot I$$



$$\begin{bmatrix} V_1 \\ V_2 \end{bmatrix} = \begin{bmatrix} Z_{11} & Z_{12} \\ Z_{21} & Z_{22} \end{bmatrix} \cdot \begin{bmatrix} I_1 \\ I_2 \end{bmatrix}$$

$$V_1 = Z_{11}I_1 + Z_{12}I_2 \quad (1)$$

$$V_2 = Z_{21}I_1 + Z_{22}I_2 \quad (2)$$

Now from eqns (1)

$$Z_{11} = \left. \frac{V_1}{I_1} \right|_{I_2=0}$$

$Z_{11}$ : input driving impedance when O/P port is open

$$(a) R_{12} = \left. \frac{V_1}{I_2} \right|_{I_1=0}$$

→ Reverse transfu. impedance when I/P is open

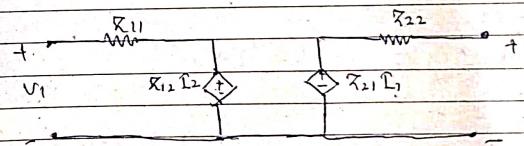
$$(b) Z_{21} = \left. \frac{V_2}{I_1} \right|_{I_2=0}$$

→ Forward transfu. impedance when O/P is open

$$(c) Z_{22} = \left. \frac{V_2}{I_2} \right|_{I_1=0}$$

→ O/P driving impedance when I/P is open

Circuit for the same -



## 11 Y parameter:

↳ Admittance parameter

$$Y = \frac{I}{V} = \frac{\dot{I}}{V} \Rightarrow (\dot{I} = Y \cdot V)$$

$$\begin{bmatrix} I_1 \\ I_2 \end{bmatrix} = \begin{bmatrix} Y_{11} & Y_{12} \\ Y_{21} & Y_{22} \end{bmatrix} \begin{bmatrix} V_1 \\ V_2 \end{bmatrix}$$

$$I_1 = Y_{11}V_1 + Y_{12}V_2 \quad \text{--- (1)}$$

$$I_2 = Y_{21}V_1 + Y_{22}V_2 \quad \text{--- (2)}$$

from the eqn

$$\text{a) } Y_{11} = \frac{I_1}{V_1} \Big|_{V_2=0}$$

→ input driving admittance, when O/P port is short ckt

$$\text{b) } Y_{21} = \frac{I_2}{V_1} \Big|_{V_2=0}$$

→ forward transfer admittance, when O/P is short ckt

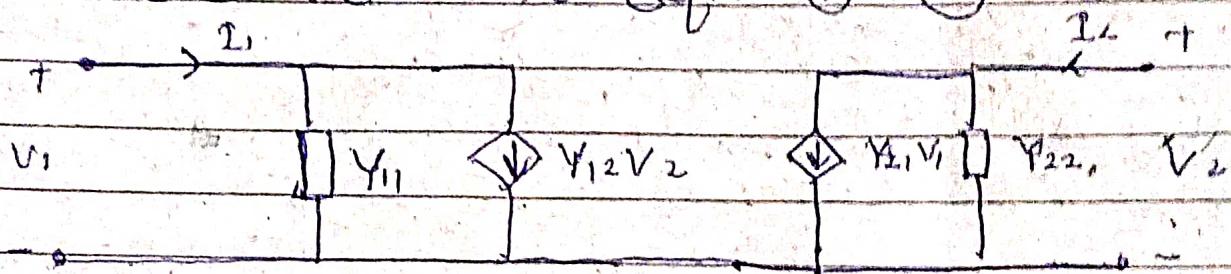
$$\text{c) } Y_{12} = \frac{I_1}{V_2} \Big|_{V_1=0}$$

Reverse transfer admittance, when I/P short ckt

$$Y_{22} = \frac{I_2}{V_2} \Big|_{V_1=0}$$

→ O/p driving admittance ; when I/P short ckt

\* Model for the eqn ① & ⑪



(iii) b-parameter :-

↳ hybrid parameter.

$$\begin{bmatrix} V_1 \\ I_2 \end{bmatrix} = \begin{bmatrix} h_{11} & h_{12} \\ h_{21} & h_{22} \end{bmatrix} \begin{bmatrix} I_1 \\ V_2 \end{bmatrix}$$

$$V_1 = h_{11} I_1 + h_{12} V_2 \quad \text{--- } ①$$

$$I_2 = h_{21} I_1 + h_{22} V_2 \quad \text{--- } ⑪$$

a)  $h_{11} = \frac{V_1}{I_1} \Big|_{V_2=0}$

→ I/P driving Impedance, when o/p is short ckt

b)  $h_{12} = \frac{V_1}{V_2} \Big|_{I_1=0}$

→ reverse voltage gain, when I/P is open ckt

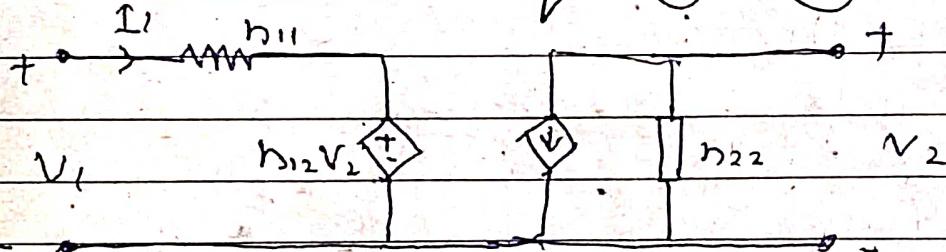
c)  $b_{21} = \frac{I_2}{I_1} \Big|_{V_2=0}$

→ forward current gain when O/P shorted

d)  $b_{22} = \frac{I_2}{V_2} \Big|_{I_1=0}$

→ O/P admittance when T/P is open  
ckt

\* Model for the eqn ① 8(11)



(IV) g-parameter (inverse h-parameter)

$$\begin{bmatrix} I_1 \\ V_2 \end{bmatrix} = \begin{bmatrix} g_{11} & g_{12} \\ g_{21} & g_{22} \end{bmatrix} \begin{bmatrix} V_1 \\ I_2 \end{bmatrix}$$

$$I_1 = g_{11}V_1 + g_{12}I_2 \quad \text{--- } ①$$

$$V_2 = g_{21}V_1 + g_{22}I_2 \quad \text{--- } ②$$

a)  $g_{11} = \frac{I_1}{V_1} \Big|_{I_2=0}$

→



b)  $g_{11} = \frac{I_1}{V_2} \Big|_{V_1=0}$

→

c)  $g_{21} = \frac{V_2}{I_2} \Big|_{V_1=0}$

→

d)  $g_{22} = \frac{V_2}{I_2} \Big|_{V_1=0}$

(i) ABCD parameters :-

$$\begin{bmatrix} V_1 \\ I_1 \end{bmatrix} = \begin{bmatrix} A & B \\ C & D \end{bmatrix} \begin{bmatrix} V_2 \\ -I_2 \end{bmatrix}$$

$$V_1 = AV_2 + B(-I_2) \quad \text{--- (I)}$$

$$I_1 = CV_2 + D(-I_2) \quad \text{--- (II)}$$



symmetrical

reciprocal

$$\begin{bmatrix} \chi_{11} & \chi_{12} \\ \chi_{21} & \chi_{22} \end{bmatrix}$$

$$\begin{bmatrix} \gamma_{11} & \gamma_{12} \\ \gamma_{21} & \gamma_{22} \end{bmatrix}$$

$$\begin{bmatrix} h_{11} & h_{12} \\ h_{21} & h_{22} \end{bmatrix}$$

$$\begin{bmatrix} g_{11} & g_{12} \\ g_{21} & g_{22} \end{bmatrix}$$

$$\begin{bmatrix} A & B \\ C & D \end{bmatrix}$$

symmetrical  
NTW

$$\chi_{11} = \chi_{22}$$

$$\gamma_{11} = \gamma_{22}$$

$$h_{11}h_{22} - h_{21}h_{12} = 1$$

$$\chi_{21} = \chi_{12}$$

$$\gamma_{21} = \gamma_{12}$$

$$h_{21} = -h_{12}$$

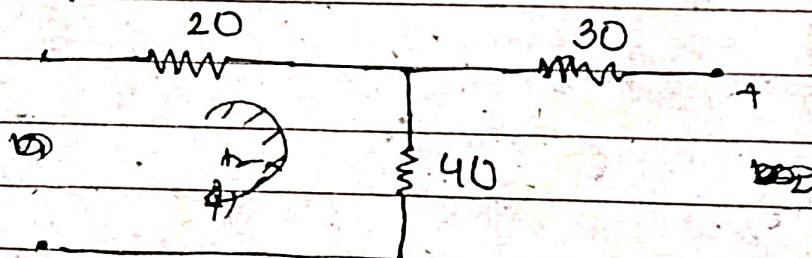
$$g_{11}g_{22} - g_{12}g_{21} = 1$$

$$g_{21} = -g_{12}$$

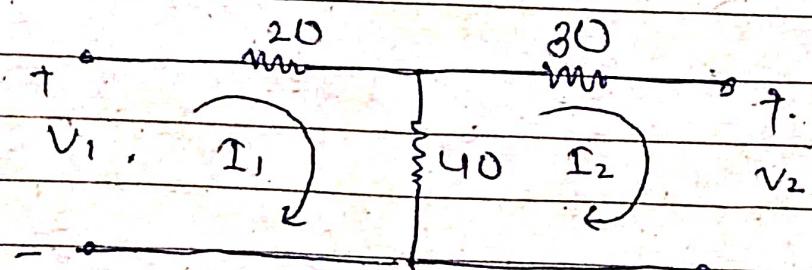
$$A = D -$$

$$AD - BC = 1$$

Q: Find  $\chi$ -parameter



Sol



$$V_1 - 20I_1 - 40(I_1 + I_2) = 0$$

$$V_1 = 60I_1 + 40I_2 \quad \text{--- (1)}$$

$$V_2 = 30I_2 - 40(I_1 + I_2) = 0$$

$$V_2 = 40I_1 + 70I_2 \quad \text{--- (ii)}$$

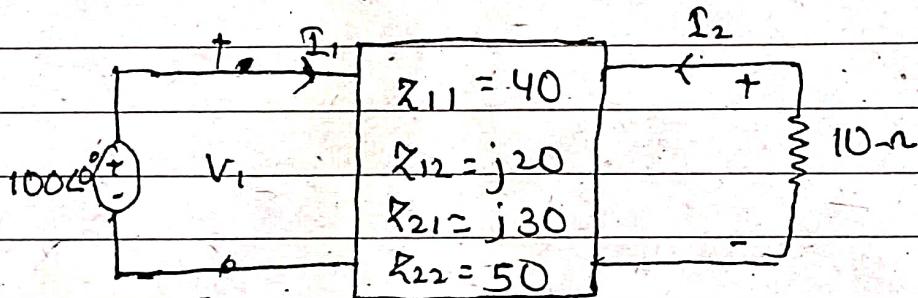
Now,

$$\chi_{11} = 60, \quad \chi_{12} = 40$$

$$\chi_{21} = 40, \quad \chi_{22} = 70$$

As  $\chi_{12} = \chi_{21}$  it is reciprocal circuit

Q: Find  $I_1$  &  $I_2$



$$50I_1 - V_1 = \chi_{11}I_1 + \chi_{12}I_2$$

$$V_2 = \chi_{21}I_1 + \chi_{22}I_2$$

$$\therefore V_2 = -I_2 \times 10$$

$$= -10I_2$$

$$100 = 40I_1 + j20I_2 \quad \text{--- (i)}$$

$$-60I_2 = j30I_1$$

$$I_1 = 2jI_2$$

$$(V_2 = j30I_1 + 50I_2)$$

$$-10I_2 = j30I_1 + 50I_2 \quad \text{--- (ii)}$$

$$60I_2 + j30I_1 = 0$$

$$40I_1 + j20I_2 = 100$$

From this

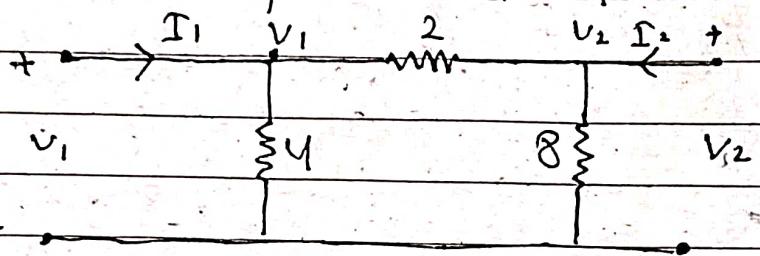


$$I_1 = 2j I_2$$

$$I_2 = -j \quad \Rightarrow \quad I_2 = 1 \angle +90^\circ = 1 \angle 90^\circ$$

$$|I_2 - 2j|^2 = 2A$$

Q :- Find Y-parameter?

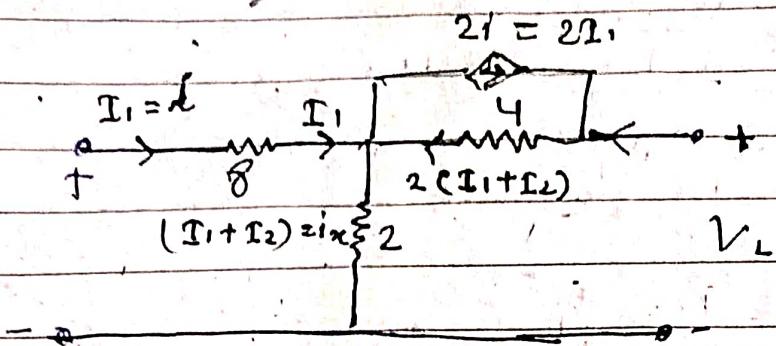


$$\frac{V_1}{4} + \frac{V_1 - V_2}{2} - I_2 = 0$$

$$\frac{V_1}{4} + \frac{2V_1}{2x2} - \frac{V_2}{2} = I_1$$

$$\left( \frac{3V_1}{4} - \frac{1}{2}V_2 = I_1 \right)$$

Q: Find Y parameter



Apply KCL

$$I_1 + 2I_1 + I_2 = ix + 2I_1$$

$$ix = (I_1 + I_2) \quad \text{--- (1)}$$

$$V_1 - 8I_1 - 2(I_1 + I_2) = 0$$

$$V_1 = 10I_1 + 2I_2 \quad \text{--- (II)}$$

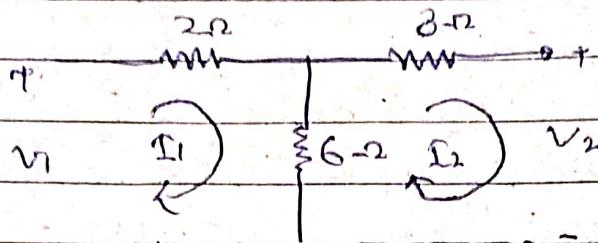
$$V_2 = 4(2I_1 + I_2) - 2(I_1 + I_2) = 0$$

$$V_2 = 8I_1 + 4I_2 + 2I_1 + 2I_2$$

$$V_2 = 10I_1 + 6I_2 \quad \text{--- (III)}$$



Q: Find b-parameter?



Sol Apply KVL

$$v_1 - 2I_1 - 6(I_1 + I_2) = 0$$

$$v_1 = 8I_1 + 6I_2 \quad \text{--- (1)}$$

$$(b_{11} = 8) \text{ or } b_{11} = \frac{v_1}{I_1} \Big|_{I_2=0}$$

$$v_2 - 3I_2 - 6I_2 - 8I_1 = 0$$

$$v_2 - 9I_2 - 6I_1 = 0$$

$$I_2 = \frac{v_2 - 6I_1}{9}$$

$$I_2 = \frac{1}{9}v_2 - \frac{2}{3}I_1$$

$$(b_{21}) = -\frac{2}{3}, \quad (b_{22} = \frac{1}{9})$$

• Interconnection of 2 port Network :-

→ Series-series connection  $\rightarrow Z$ -parameter

→ parallel parallel  $\rightarrow Y$

→ series-parallel  $\rightarrow \Gamma / P - Z, O / P - Y$

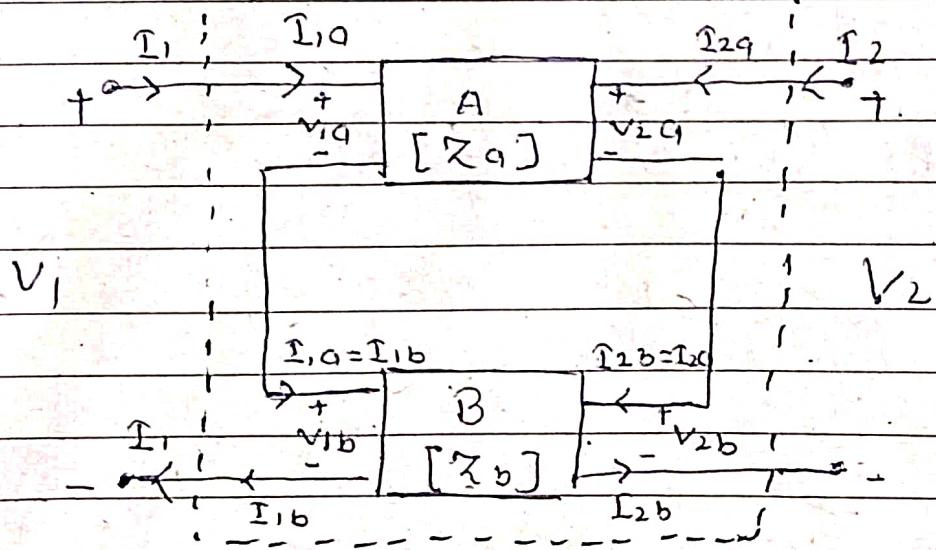
→ parallel series  $\rightarrow \Gamma / P Y, O / P - Z$

→ cascade  $\rightarrow ABCD$  parameters

### Note

We connect  $Z$  in series &  $Y$  in parallel

①



Now Apply KVL

$$V_1 - V_{1a} - V_{1b} = 0$$

$$(V_1 = V_{1a} + V_{1b})$$

$$(V_2 - V_{2a} + V_{2b} = 0)$$

$$(I_1 = I_{1a} = I_b)$$

$$(I_2 = I_{2a} = I_{2b})$$

thus we can write the eqns for  $\chi$  parameters as it is 2, 2 port network

$$V_{1a} = \chi_{11a} I_{1a} + \chi_{12a} \cdot I_{2a} \quad \text{--- (1)}$$

$$V_{2a} = \chi_{21a} I_{1a} + \chi_{22a} I_{2a} \quad \text{--- (2)}$$

$$V_{1b} = \chi_{11b} I_{1b} + \chi_{12b} I_{2b} \quad \text{--- (3)}$$

$$V_{2b} = \chi_{21b} I_{1b} + \chi_{22b} I_{2b} \quad \text{--- (4)}$$

add eqn (1) & (3)

$$V_{1a} + V_{1b} = \chi_{11a} I_{1a} + \chi_{11b} I_{1b} + \chi_{12a} I_{2a} + \chi_{12b} I_{2b}$$

$$\text{as } V_{1a} + V_{1b} = V_1$$

$$V_1 = (\chi_{11a} + \chi_{11b}) I_1 + (\chi_{12a} + \chi_{12b}) I_2$$

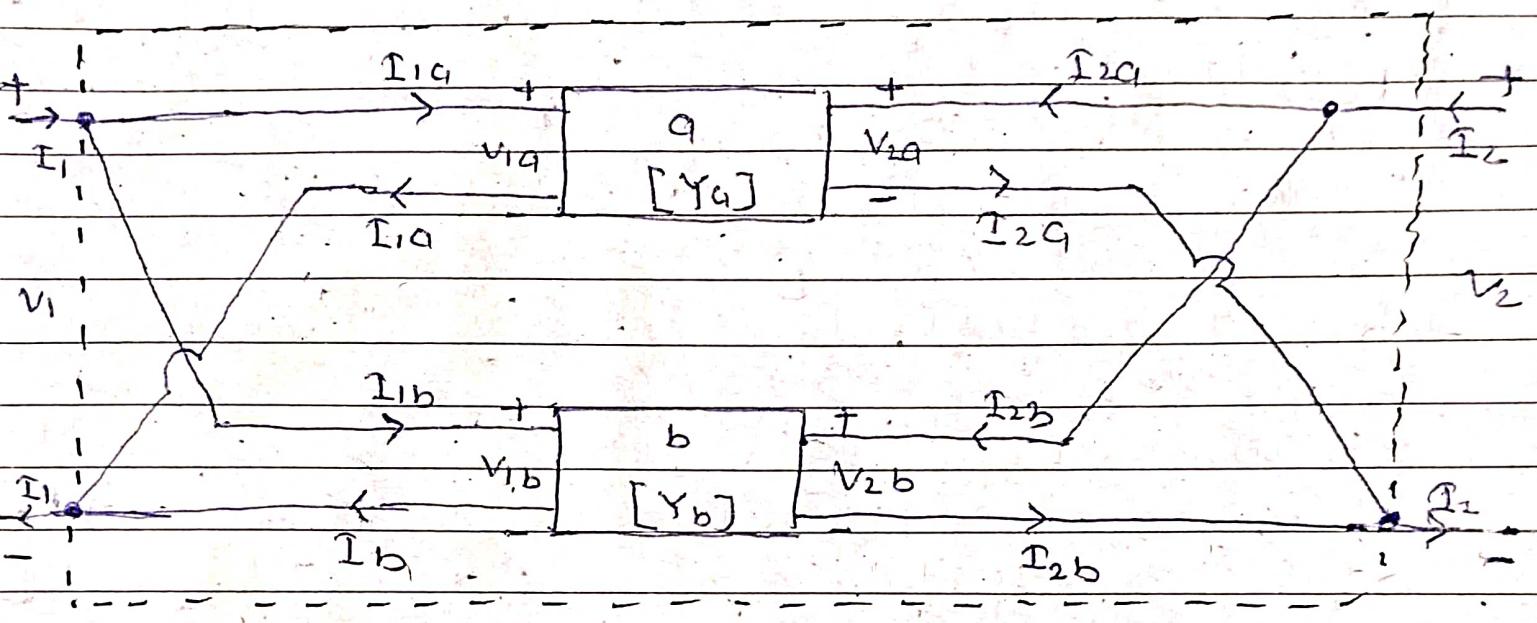
Now similarly for eqn 2 & (4)

$$V_{2a} + V_{2b} = \chi_{21a} I_{1a} + \chi_{21b} I_{1b} + \chi_{22a} I_{2a} + \chi_{22b} I_{2b}$$

$$V_2 = (\chi_{21a} + \chi_{21b}) I_1 + (\chi_{22a} + \chi_{22b}) I_2$$

$$[Z] = \begin{bmatrix} (Z_{11a} + Z_{11b}) & (Z_{12a} + Z_{12b}) \\ (Z_{21a} + Z_{21b}) & (Z_{22a} + Z_{22b}) \end{bmatrix}$$

## (ii) parallel parallel connection -



Now on analysis

$$V_1 = V_{1a} = V_{1b}$$

$$V_2 = V_{2a} = V_{2b}$$

$$I_1 = I_{1a} + I_{1b}$$

$$I_2 = I_{2a} + I_{2b}$$



Now we can write eqn for  $\Sigma$ -parameter

$$I_{1a} = Y_{11a} \cdot V_{1a} + Y_{12a} \cdot V_{2a} \quad \text{--- (1)}$$

$$I_{2a} = Y_{21} V_{1a} + Y_{22a} \cdot V_{2a} \quad \text{--- (2)}$$

$$I_{1b} = Y_{11b} \cdot V_{1b} + Y_{12b} \cdot V_{2b} \quad \text{--- (3)}$$

$$I_{2b} = Y_{21b} V_{1b} + Y_{22b} \cdot V_{2b} \quad \text{--- (4)}$$

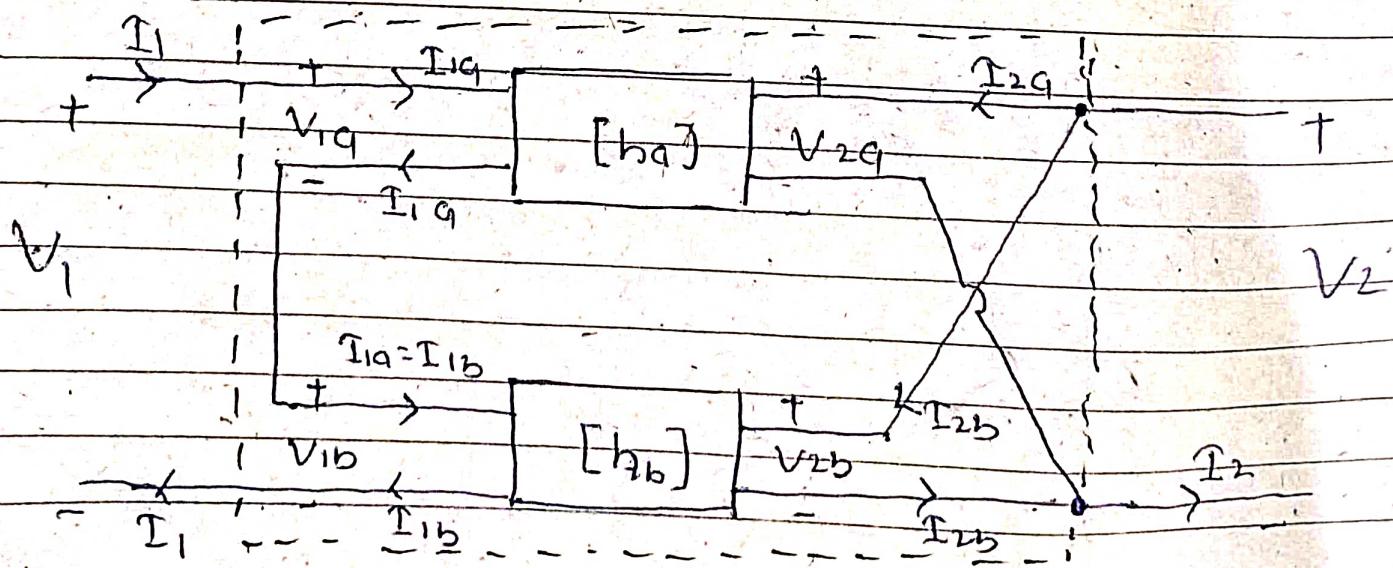
Now Add eqn (1) & (3)

$$I_1 = (I_{1a} + I_{1b}) = (Y_{11a} + Y_{11b}) V_1 + (Y_{12a} + Y_{12b}) V_2$$

$$I_2 = (I_{2a} + I_{2b}) = (Y_{21} + Y_{21b}) V_1 + (Y_{22a} + Y_{22b}) V_2$$

$$[Y] = \begin{bmatrix} (Y_{11a} + Y_{11b}) & (Y_{12a} + Y_{12b}) \\ (Y_{21} + Y_{21b}) & (Y_{22a} + Y_{22b}) \end{bmatrix}$$

### (3) Series - Parallel



ON analysis,

$$I_1 = I_{1a} = I_{1b}$$

$$V_1 - V_{1a} - V_{1b} = 0$$

$$V_1 = (V_{1a} + V_{1b})$$

$$I_2 = I_{2a} + I_{2b}, \quad V_2 = V_{2a} = V_{2b}$$

NOW,

$$V_{1a} = h_{11a} I_{1a} + h_{12a} V_{2a}$$

$$\circ V_{1b} = h_{11b} I_{1b} + h_{12b} V_{2b}$$

$$I_{2a} = h_{21a} I_{1a} + h_{22a} V_{2a}$$

$$I_{2b} = h_{21b} I_{1b} + h_{22b} V_{2b}$$

Add

(1) & (2)

$$V_{1a} + V_{1b} = V_1 = (h_{11a} + h_{11b}) I_1 + (h_{12a} + h_{12b}) V_2$$

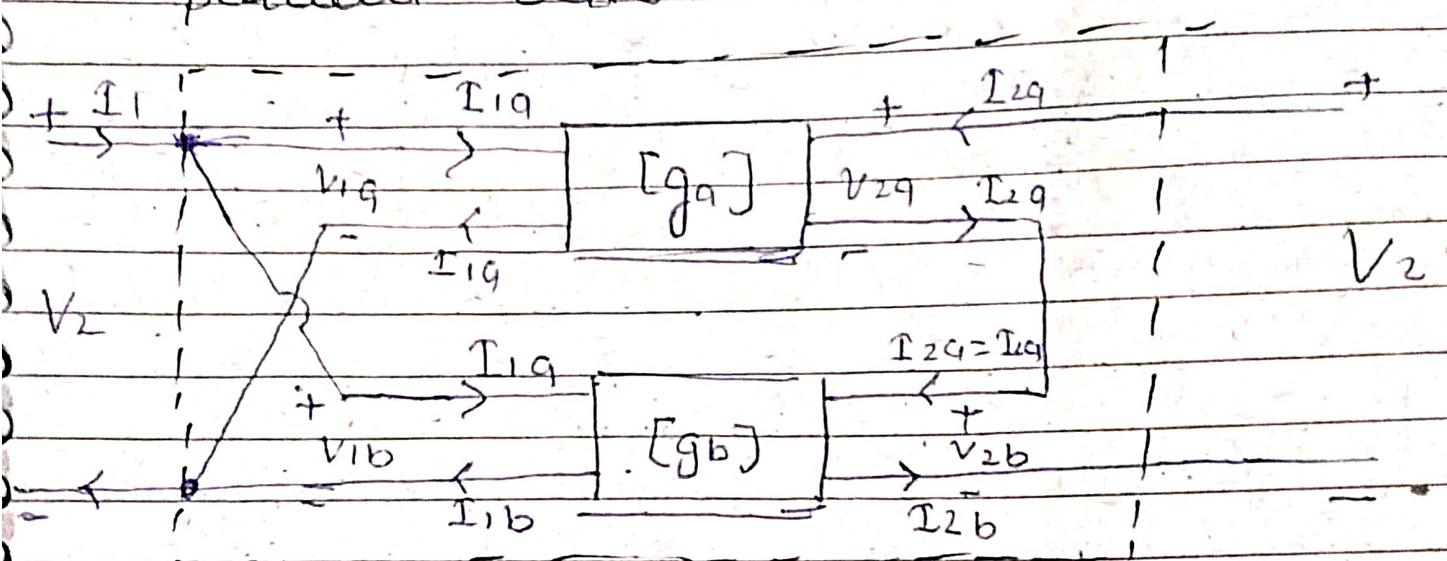
(1) & (4)

$$I_{2a} + I_{2b} = I_2 = (h_{21a} + h_{21b}) I_1 + (h_{22a} + h_{22b}) V_2$$

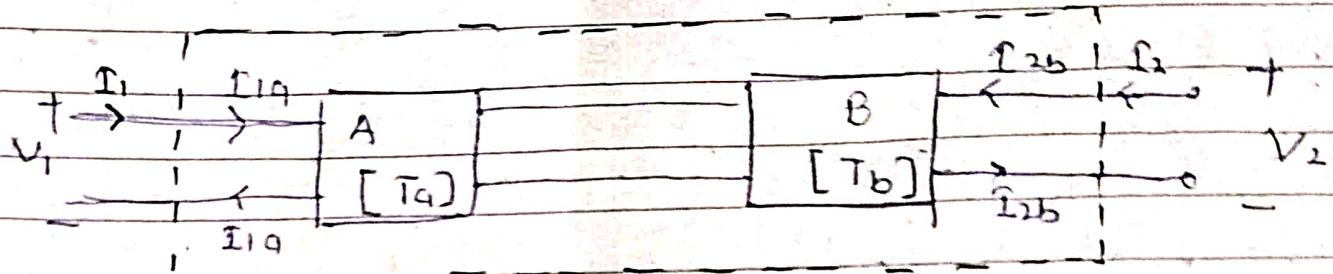
$$[h] = \begin{bmatrix} (h_{11a} + h_{11b}) & (h_{12a} + h_{12b}) \\ (h_{21a} + h_{21b}) & (h_{22a} + h_{22b}) \end{bmatrix}$$



→ parallel - series connection ↵



## ⑤ Cascade



$$[T] = [T_A] [T_B]$$

$$[T] = \begin{bmatrix} A_a & B_a \\ C_a & D_a \end{bmatrix} \begin{bmatrix} A_b & B_b \\ C_b & D_b \end{bmatrix}$$



## UNIT - 3

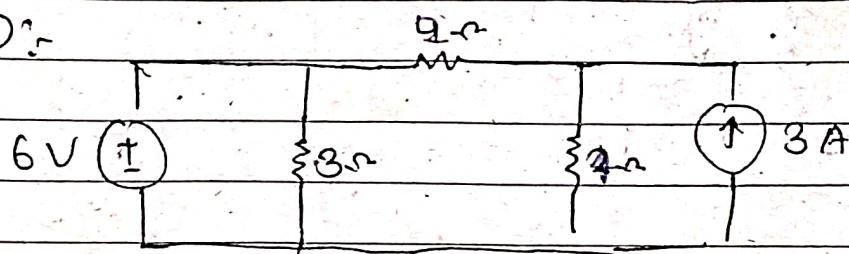
### Superposition theorem -

Condition to apply superpos. theorem

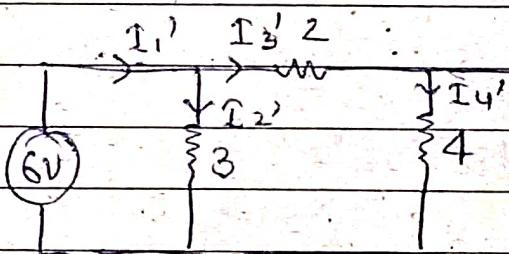
→ linear Ntw

→ Independent sources

Q:-



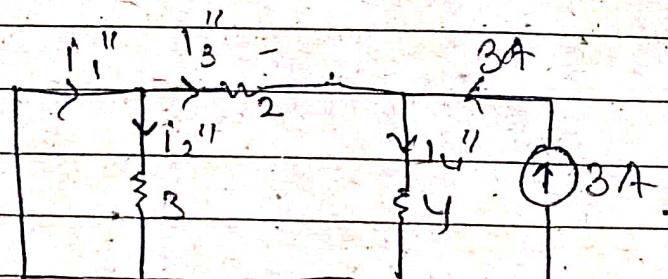
SOL



$$\left( i_2' = \frac{6}{3} = 2A \right), \quad \left( i_3' = i_4' = \frac{6}{6} = 1A \right)$$

$$( i_2' = 3A )$$

Case - 2



$$i_2'' = 0, \quad i_4'' = 1A$$

$$i_1'' = i_3'' = -2A$$

$$i_1 = i_1' + i_1''$$

$$= 3 + (-2)$$

$$i_2 = i_2' + i_2''$$

$$i_2 = 2 + 0 = 2A$$

$$(i_1 = 1A)$$

$$(i_2 = 2A)$$

$$i_4 = i_4' + i_4''$$

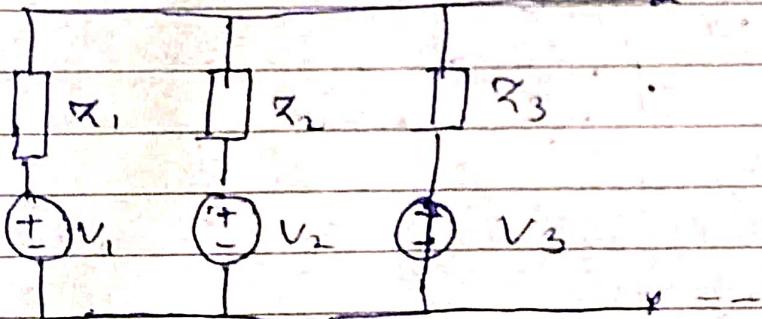
$$1 + 1$$

$$(i_4 = 2A)$$

$$i_3 = i_3' + i_3'' = 1 + (-2)$$

$$(i_3 = -1A)$$

### Millman's theorem :-



According to this theorem we can  
this multiple combination of  $R$ ,  
 $V$  in ~~sig~~ single voltage & single  
impedance.

$$\frac{1}{Z_1} = 1, \quad \frac{1}{Z_2} = 1, \quad \frac{1}{Z_3} = \frac{1}{R_3}$$



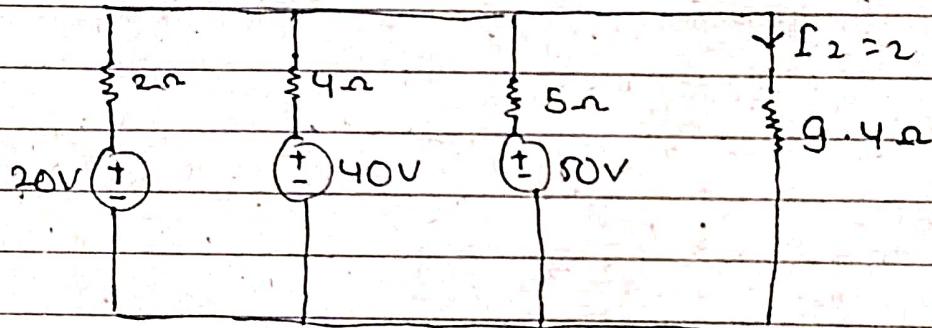
$$Y = Y_1 + Y_2 + Y_3$$

$$(Y = \frac{1}{Z_1} + \frac{1}{Z_2} + \frac{1}{Z_3})$$

$$E = \frac{V_1 Y_1 + V_2 Y_2 + V_3 Y_3}{Y}$$

$$(E = \frac{V_1 Y_1 + V_2 Y_2 + V_3 Y_3}{Y_1 + Y_2 + Y_3})$$

Q:



$$\text{Sol} \quad Y_1 = \frac{1}{Z_1} = \frac{1}{2} = 0.5$$

$$Y_2 = \frac{1}{Z_2} = \frac{1}{4} = 0.25$$

$$Y_3 = \frac{1}{Z_3} = \frac{1}{5} = 0.2$$

$$Y = 0.5 + 0.25 + 0.2$$

$$(Y = 0.95)$$

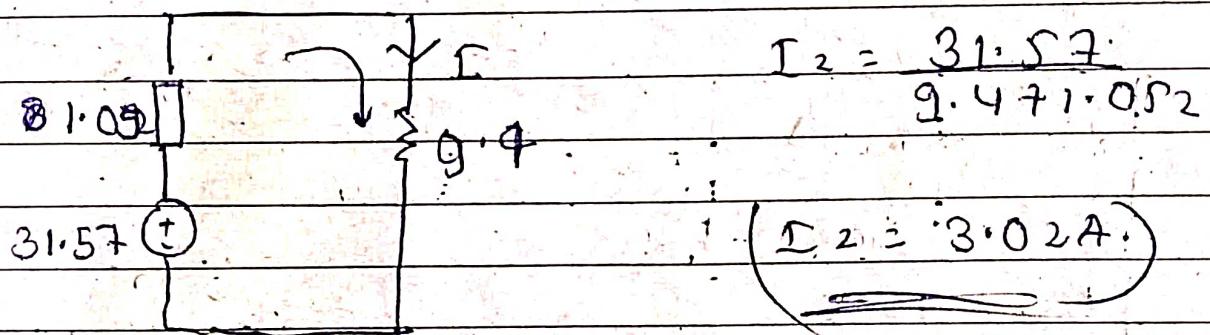
$$Z = \frac{1}{Y} = \frac{1}{0.95} = 1.052$$

$$V_2 = \frac{V_1 Y_1 + V_2 Y_2 + V_3 Y_3}{(Y_1 + Y_2 + Y_3)}$$

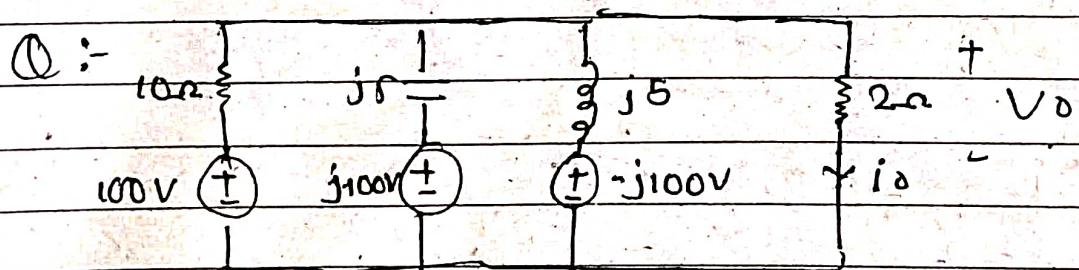
$$V = \frac{20 \times 0.5 + 40 \times 0.25 + 50 \times 0.12}{0.95}$$

$$V = \frac{30}{0.95} = 31.57$$

Equivalent Ckt



HA



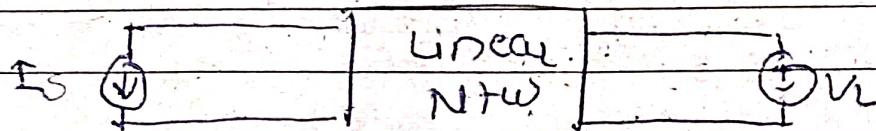
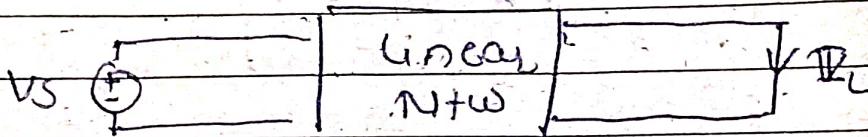
Find  $V_o, I_o = ?$



\* Free response

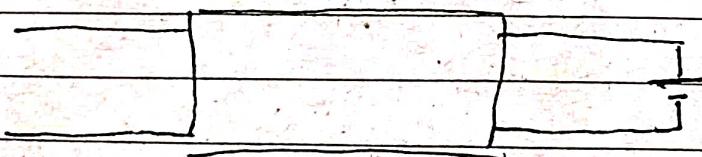
\* Reciprocity theorem -

→ Response = constant  
 Excitation



$$\frac{I_L}{V_s} = \frac{I_s}{V_L}$$

Q:

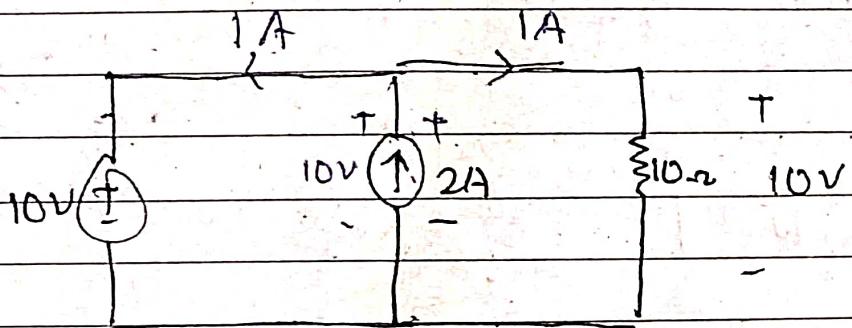


Tellegan's theorem :-

$\rightarrow (\text{Power absorb} = \text{Power delivered})$

Note

(+) sign me current enter kar raha  
hai Power & (-) sign se current  
nikal raha hai Power



$$P_{10v} = 10 \times 1 = 10W \rightarrow \text{Absorbed}$$

$$P_{10v} = 10 \times 3 = 30W \rightarrow \text{Delivered}$$

$$P_{10v} = 10 \times 1 = 10W \quad \text{Absorbed}$$

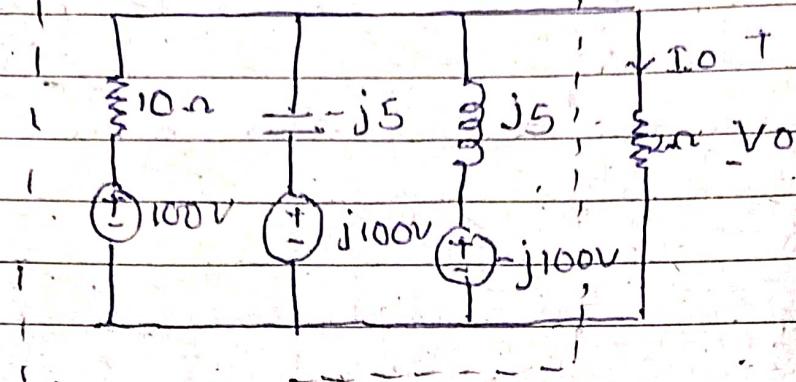
Absorbed = Delivered

$$20W = 10W + 10W$$

$$(20W = 20W)$$



Q:



$$V = V_1 Y_1 + V_2 Y_2 + V_3 Y_3$$

$$(Y_1 + Y_2 + Y_3) = Y = \frac{1}{Z}, Z = \frac{1}{Y}$$

$$Y_1 = \frac{1}{Z_1} = \frac{1}{10} = 0.1 \Omega$$

$$Y_2 = \frac{1}{Z_2} = \frac{1}{-j5} = j0.2$$

$$Y_3 = \frac{1}{Z_3} = \frac{1}{j5} = -j0.2$$

$$Y = 0.1 + j0.2 - j0.2 = 0.1$$

$$Z = \frac{1}{Y} = \frac{1}{0.1} = 10$$

$$V = \frac{(100 \times 0.1 + j100 \times j0.2 + (-j100) \times (-j0.2))}{0.1}$$

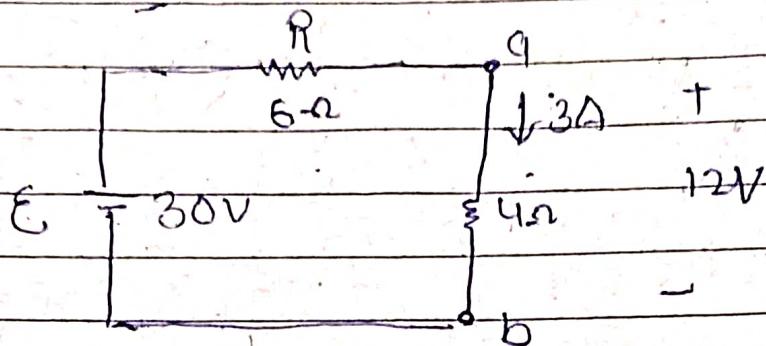
$$V = \frac{10 - 20 - 20}{0.1} = \frac{-30}{0.1} = -300 \text{ V}$$

Equivalent CKT,



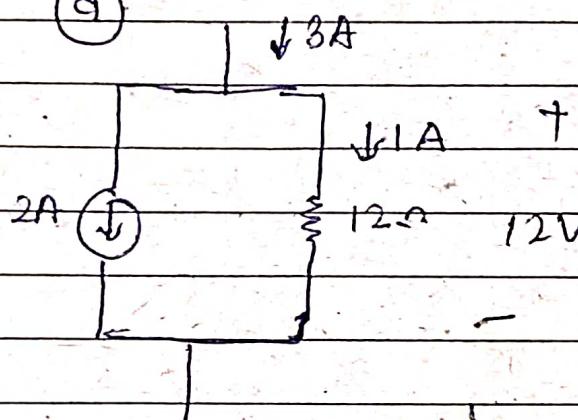


## Substitution Theorem

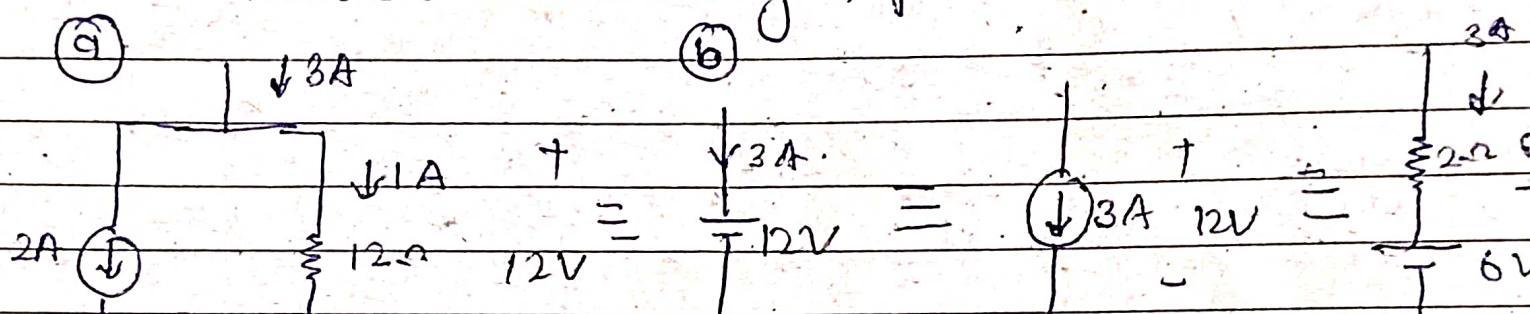


a & b section may represent as

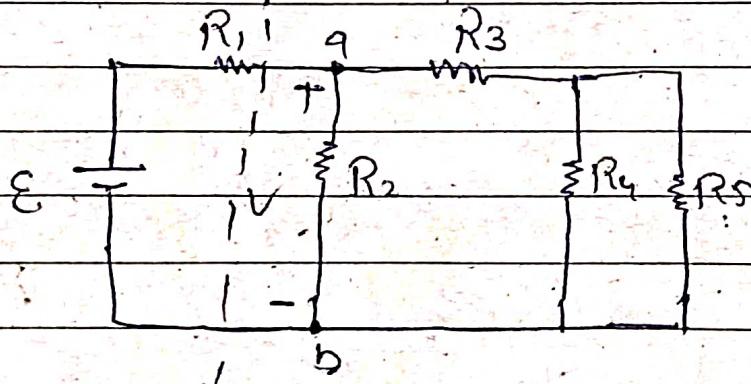
(a)



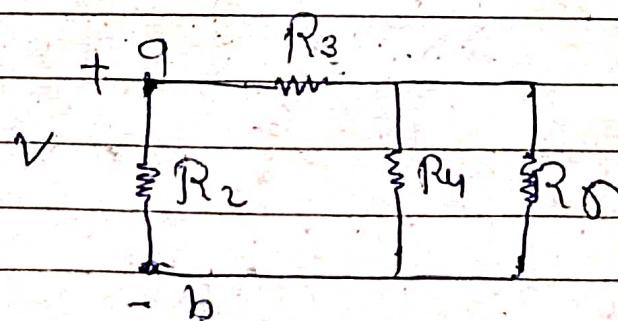
(b)



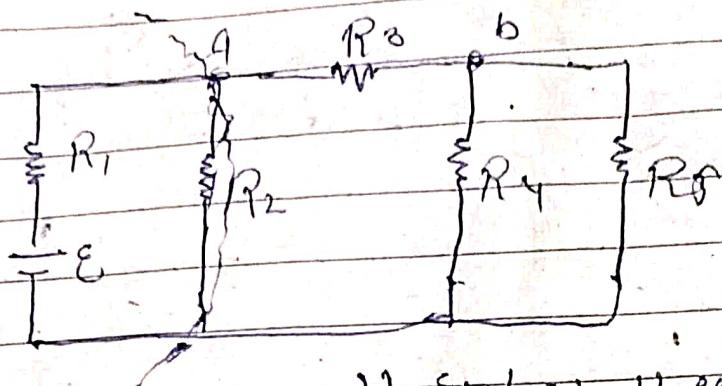
Ex:-



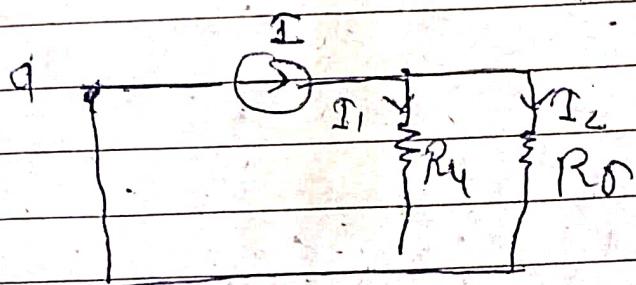
## III Substitution theorem



## Illustration 2



↓ subst. theorem

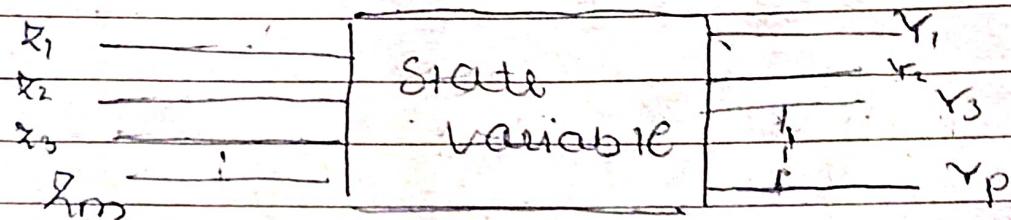
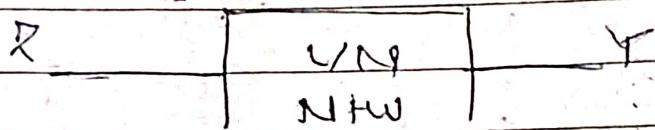


$$I_1 = \frac{I \times R_4}{R_5 + R_4}$$

$$I_2 = \frac{I \times R_5}{R_5 + R_4}$$



## State variable :-



$$x(t) = \begin{bmatrix} x_1(t) \\ x_2(t) \\ x_3(t) \\ \vdots \\ x_m(t) \end{bmatrix}, \quad \dot{x}(t) = \begin{bmatrix} \dot{x}_1(t) \\ \dot{x}_2(t) \\ \dot{x}_3(t) \\ \vdots \\ \dot{x}_m(t) \end{bmatrix}$$

$$\left( \dot{x}(t) = \frac{dx(t)}{dt} \right), \quad x(t) = \begin{bmatrix} x_1(t) \\ x_2(t) \\ x_3(t) \\ \vdots \\ x_m(t) \end{bmatrix}$$

$$Y(t) = \begin{bmatrix} y_1(t) \\ y_2(t) \\ y_3(t) \\ \vdots \\ y_p(t) \end{bmatrix}$$

$$\dot{x} = Ax + Bu$$

$$y = cx + du$$

A = system matrix

B = input coupling matrix

C = O/P matrix

D = feed forward matrix

$[A]n \times n, [B]n \times m$

$[C]p \times n, [D]p \times m$

$$\dot{x} = Ax + Bu$$

apply L.T.

$$s_x(s) = Ax(s) + Bu(s)$$

$$s_x(s) - Ax(s) = Bu(s)$$

$$x(s) \begin{bmatrix} s\cdot I - A \\ \xrightarrow{\text{identity matrix}} \end{bmatrix} = Bu(s)$$

$$\frac{y(s)}{z(s)} = x(s)$$

$$Y(s) = X(s)Z(s)$$

$$X(s) = (s\cdot I - A)^{-1} \cdot B \cdot Z(s)$$

$$X(s) = (s\cdot I - A)^{-1} \cdot B \cdot Z(s)$$

$$Y(s) = C \cdot X(s) + D \cdot Z(s)$$

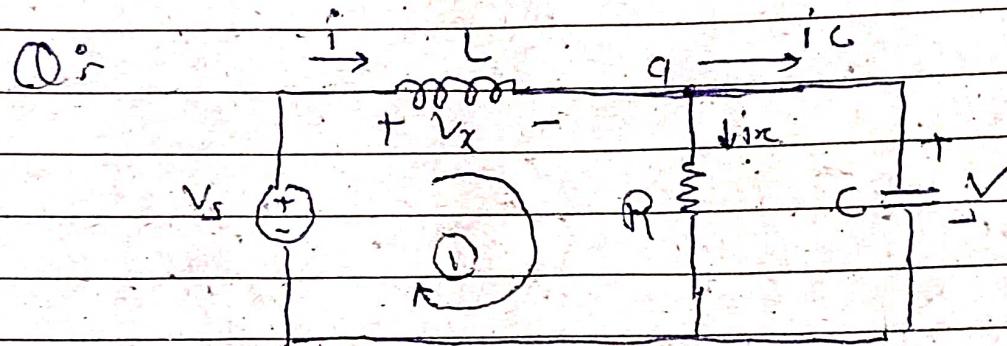
$D \rightarrow 0$ , maximum case

$$Y(s) = C \cdot X(s)$$

$$Y(s) = C \cdot (s\cdot I - A)^{-1} \cdot B \cdot Z(s)$$

## Note

storing elements are capacitor & inductor.



so

$$L \rightarrow i \rightarrow v_L = L \frac{di}{dt} = L \cdot i(t)$$

$$C \rightarrow v \rightarrow i = C \frac{dv}{dt} = C \dot{v}(t)$$

KCL at q,

$$i = i_x + i_C$$

$$i = \frac{V}{R} + C \cdot \frac{dv(t)}{dt}$$

$$i = \frac{V}{R} + C \dot{v}(t)$$

$$C \cdot \dot{v}(t) = i - \frac{V}{R}$$

$$\Rightarrow \left( v(t) = -\frac{V}{RC} + \frac{i}{C} \right)$$

KVL at loop ①

$$V_s - V_L - V = 0$$

$$V_s - V = V_L$$

$$\therefore V_L = L \frac{di}{dt}$$

$$V_L = L i(t)$$

$$i(t) = -V + V_s$$

$$i'(t) = \frac{V}{L} + \frac{V_s}{L} \quad \text{--- } 2$$

NOW,

$$V' = -\frac{1}{RC} V + \frac{1}{C} i$$

$$i' = -\frac{1}{L} V + \frac{1}{V} V_s$$

We can this in form

$$x = Ax + B \beta$$

$$\begin{bmatrix} V' \\ i' \end{bmatrix} = \begin{bmatrix} -\frac{1}{RC} & \frac{1}{C} \\ -\frac{1}{L} & 0 \end{bmatrix} \begin{bmatrix} V \\ i \end{bmatrix} + \begin{bmatrix} 0 \\ \frac{1}{V} V_s \end{bmatrix}$$



$$i_R = \frac{V}{R} = \frac{1}{R} V + 0 \cdot I$$

$$i_R = \begin{bmatrix} 1/R & 0 \end{bmatrix} \begin{bmatrix} V \\ I \end{bmatrix}$$

Let  $R = 1\Omega$ ,  $C = 0.25F$ ,  $L = 0.5H$

$$A = \begin{bmatrix} -4 & 4 \\ -2 & 0 \end{bmatrix}, \quad B = \begin{bmatrix} 0 \\ 2 \end{bmatrix}$$

$$C = \begin{bmatrix} 1, 0 \end{bmatrix}$$

$$Y(s) = C(SI - A)^{-1} \cdot B \cdot Z(s)$$

$$H(s) = \frac{Y(s)}{Z(s)}$$

$$H(s) = C(SI - A)^{-1}$$

$$S \begin{bmatrix} 1 & 0 \\ 0 & 1 \end{bmatrix} = \begin{bmatrix} S & 0 \\ 0 & S \end{bmatrix}$$

$$SI - A = \begin{bmatrix} S & 0 \\ 0 & S \end{bmatrix} - \begin{bmatrix} -4 & 4 \\ -2 & 0 \end{bmatrix}$$

$$= \begin{bmatrix} S & 4 \\ -2 & S+2 \end{bmatrix}$$

$$|SI - A| = S^2 + 4S + 8$$

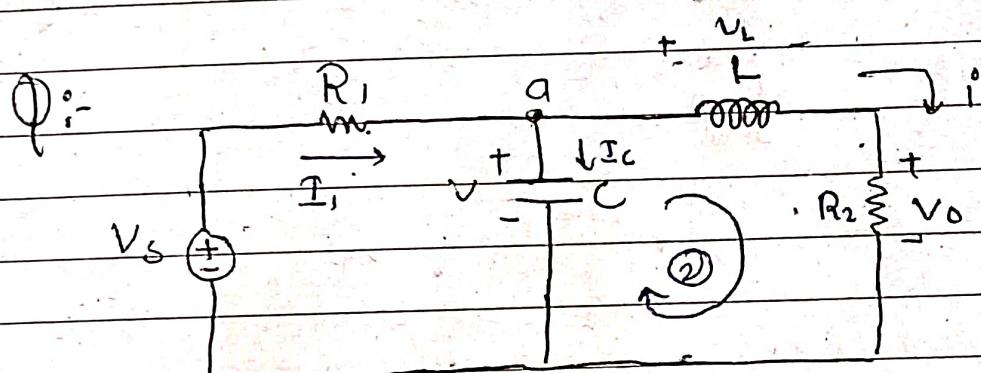
$$(SI - A)^{-1} = \frac{\text{adj}(SI - A)}{\det(SI - A)} = \begin{bmatrix} 5 & 4 \\ -2 & 5+q \end{bmatrix}$$

$$S^2 + 4S + 8$$

$$\begin{bmatrix} 1 & 0 \\ 0 & 1 \end{bmatrix} \begin{bmatrix} 0 & 8 \\ 0 & 2S+8 \end{bmatrix}$$

$$S^2 + 4S + 8$$

$$H(s) = \frac{8}{S^2 + 4S + 8}$$



Find  $H(s)$ ?  $R_1 = 1$ ,  $R_2 = 2$   $C = 0.5$ ,  $L = 0.2$

Sol) Apply KCL at a,

$$I_1 = I_C + i$$

$$I_1 = C \cdot \frac{dv}{dt} + i$$

$$I_1 = \frac{Vs - v}{R_1}$$

$$\frac{Vs - v}{R_1} = C \cdot \dot{v}(t) + i$$

$$C \dot{v}(t) = \frac{-v}{R_1} - i + \frac{Vs}{R_1}$$



$$\left. \dot{V}(t) = -\frac{V}{R_1 C} - \frac{i}{C} + \frac{V_s}{R_1 C} \right) \quad (1)$$

Apply KVL at loop-2,

$$+V - V_L - V_o = 0$$

$$V_L = V - V_o$$

$$L \frac{di}{dt} = V - V_o$$

$$i_{(4)} = \frac{V - V_o}{L} \quad | \quad V_o = i R_2 \quad (3)$$

$$\left. i_{(4)} = \frac{V - i R_2}{L} \right) \quad (2)$$

We know  $\dot{x} = Ax + Bz$

$$\begin{bmatrix} \dot{V}(t) \\ \dot{i}(t) \end{bmatrix} = \begin{bmatrix} -\frac{1}{R_1 C} & -\frac{1}{C} \\ \frac{1}{L} & -\frac{R_2}{L} \end{bmatrix} \begin{bmatrix} V \\ i \end{bmatrix} + \begin{bmatrix} \frac{1}{R_1 C} \\ 0 \end{bmatrix} V_s$$

$$\therefore Y = CX$$

$$V_o = \begin{bmatrix} 0 & R_2 \end{bmatrix} \begin{bmatrix} V \\ i \end{bmatrix}$$

$$A = \begin{bmatrix} -2 & -2 \\ 5 & -10 \end{bmatrix}, \quad B = \begin{bmatrix} 2 \\ 0 \end{bmatrix}, \quad C = \begin{bmatrix} 0 & 2 \end{bmatrix}$$

We know,

$$H(s) = C \cdot (sI - A)^{-1} \cdot B$$

$$(sI - A) = \begin{bmatrix} s & 0 \\ 0 & s \end{bmatrix} - \begin{bmatrix} -2 & -2 \\ 5 & -10 \end{bmatrix} \Rightarrow \begin{bmatrix} s+2 & 2 \\ -5 & s+10 \end{bmatrix}$$

$$\frac{(sI - A)^{-1}}{|sI - A|} = \text{adj}(sI - A) = \frac{\begin{bmatrix} (s+10) & -2 \\ 5 & (s+2) \end{bmatrix}}{s^2 + 12s + 30}$$

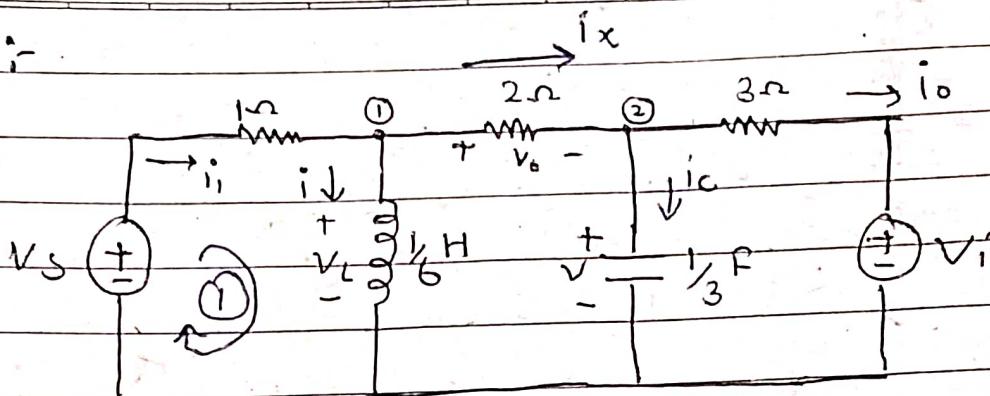
$$H(s) = \begin{bmatrix} 0 & 2 \end{bmatrix} \frac{\begin{bmatrix} (s+10) & -2 \\ 5 & (s+2) \end{bmatrix}}{s^2 + 12s + 30} \begin{bmatrix} 2 \\ 0 \end{bmatrix}$$

$$H(s) = \frac{\begin{bmatrix} 0 & 2 \end{bmatrix} \begin{bmatrix} 2(s+10) \\ 10 \end{bmatrix}}{s^2 + 12s + 30}$$

$$H(s) = \frac{20}{(s^2 + 12s + 30)}$$



Q:-



Apply KVL at Loop 1

$$V_s - i_1 x_1 - V_L = 0$$

$$V_s - i_1 = L \frac{di}{dt}$$

$$(V_s - i_1 = L \dot{i}_1) \rightarrow (1)$$

KVL at Loop 2

$$V_s - i_1 - V_s - V = 0$$

$$V_s - V - V_o = i_1 \rightarrow (2)$$

We know,

$$i_x = i_1 - i_2, \quad V_o = (i_1 - i_2) R \quad \text{put in (2)}$$

$$i_1 = V_s - V - V_o$$

$$i_1 = V_s - V - (i_1 - i_2)$$

$$3i_1 = V_s - V + 2i_2$$

$$\left[ i_1 = \frac{V_s - V + 2i_2}{3} \right] \rightarrow \text{put in (1)}$$

$$i_{CT} = V_s - \left[ \frac{(V_s - V + 2i)}{3} \right]$$

$$= V_s - \frac{V_s}{3} + \frac{V}{3} - \frac{2i}{3}$$

$$i_{CT} = \frac{V_s}{2} - \frac{V_s}{3} + \frac{V}{3} - \frac{2i}{3}$$

$$i_{CT} = \frac{3V_s - V_s}{3L} + \frac{V}{3L} - \frac{2i}{3L}$$

as  $\sigma L = i_0 / 6$  put in above eqn

$$(i_{CT} = 2V - 4i_0 + 4V_s)$$

— A

NOW APPLY KVL AT (2)

$$(i_1 - i_0) = I_{CT} + i_0 \quad | \quad i_0 = \frac{V - V_i}{3}$$

$$i_1 - i_0 = C \frac{dV}{dt} + i_0$$

$$\left( \frac{V_s - V + 2i_0}{3} - i_0 \right) = C \dot{V}(t) + \frac{V - V_i}{3}$$

$$\frac{V_s - V + 2i_0}{3} - \frac{V}{3} + \frac{V_i}{3} = C \dot{V}(t)$$

$$\frac{V_s}{3} - \frac{V}{3} - \frac{2i_0}{3} - \frac{V}{3} + \frac{V_i}{3} = C \dot{V}(t)$$

$$C \dot{V}(t) = \frac{V_s}{3} - \frac{2V}{3} + \frac{V_i}{3} - \frac{i_0}{3}$$



$$\text{as } C = \frac{1}{3} F$$

$$\frac{1}{3} \dot{V}(t) = \frac{V_S}{3} - \frac{2V}{3} + \frac{Vi}{3} - \frac{i}{3}$$

$$(\dot{V}(t) = V_S - 2V + Vi - i) \longrightarrow \textcircled{B}$$

Now for  $V_0$ ,

$$V_0 = 2i, -2i$$

$$= 2 \left[ \frac{V_S - V + 2i}{3} \right] - 2i$$

$$= \frac{2}{3} V_S - \frac{2}{3} V + \frac{4}{3} i - 2i$$

$$V_0 = \frac{2}{3} V_S - \frac{2}{3} V - \frac{2}{3} i \longrightarrow \textcircled{C}$$

$$\begin{bmatrix} \dot{V}(t) \\ i(t) \end{bmatrix} = \begin{bmatrix} -2 & -1 \\ 2 & -4 \end{bmatrix} \begin{bmatrix} V \\ i \end{bmatrix} + \begin{bmatrix} 1 & 1 \\ 4 & 0 \end{bmatrix} \begin{bmatrix} V_S \\ Vi \end{bmatrix}$$

$$\begin{bmatrix} V_0 \\ i_0 \end{bmatrix} = \begin{bmatrix} -2/3 & -2/3 \\ 1/3 & 0 \end{bmatrix} \begin{bmatrix} V \\ i \end{bmatrix} + \begin{bmatrix} 2/3 & 0 \\ 0 & -1/3 \end{bmatrix} \begin{bmatrix} V_S \\ Vi \end{bmatrix}$$

$$Q: \frac{d^2y(t)}{dt^2} + 3\frac{dy(t)}{dt} + 2y(t) = 5x(t)$$

SOL

$$\text{Let } x_1 = y(t)$$

$$x_2 = \dot{x}_1 = \dot{y}(t)$$

$$\ddot{x}_2 = \ddot{x}_1 = \ddot{y}(t)$$

NOW from given eqn,

$$\ddot{x}_2 + 3\dot{x}_2 + 2x_1 = 5x(t)$$

$$\ddot{x}_2 = -3\dot{x}_2 - 2x_1 + 5x(t)$$

$$\dot{x}_1 = x_2 + 0x_1 + 0x(t)$$

$$\begin{bmatrix} \dot{x}_1 \\ \dot{x}_2 \end{bmatrix} = \begin{bmatrix} 0 & 1 \\ -2 & -3 \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \end{bmatrix} + \begin{bmatrix} 0 \\ 5 \end{bmatrix} x(t)$$

$$Y = \begin{bmatrix} 1 & 0 \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \end{bmatrix}$$

$$H(s) = C \left[ (sI - A)^{-1} \right] \cdot B$$

$$(sI - A) = \begin{bmatrix} s & 0 \\ 0 & s \end{bmatrix} - \begin{bmatrix} 0 & 1 \\ -2 & -3 \end{bmatrix} = \begin{bmatrix} s & -1 \\ 2 & s+3 \end{bmatrix}$$

$$(sI - A)^{-1} = \frac{1}{s^2 + 3s + 2} \begin{bmatrix} s+3 & 1 \\ -2 & s \end{bmatrix}$$



$$H(s) = \frac{\begin{bmatrix} 1 & 0 \end{bmatrix} \begin{bmatrix} s+3 & 1 \\ -2 & s \end{bmatrix} \begin{bmatrix} 0 \\ 5 \end{bmatrix}}{s^2 + 3s + 2}$$

$$\frac{\begin{bmatrix} 1 & 0 \end{bmatrix} \begin{bmatrix} 5 \\ 5s \end{bmatrix}}{s^2 + 3s + 2}$$

$$H(s) = \frac{5}{s^2 + 3s + 2}$$

Q:-  $\frac{d^3y(t)}{dt^3} + 18\frac{d^2y}{dt^2} + 20\frac{dy}{dt} + 5y = z(t)$   
Find, [A], [B] & [C]

So,  $x_1 = y(t)$

$x_2 = \dot{x}_1 = y'(t)$

$x_3 = \ddot{x}_1 = \ddot{y}(t)$

$\ddot{x}_3 + 18\ddot{x}_3 + 20x_2 + 5x_1 = z(t)$

$$\ddot{x}_3 + 18\ddot{x}_3 + 20x_2 + 5x_1 = z(t)$$

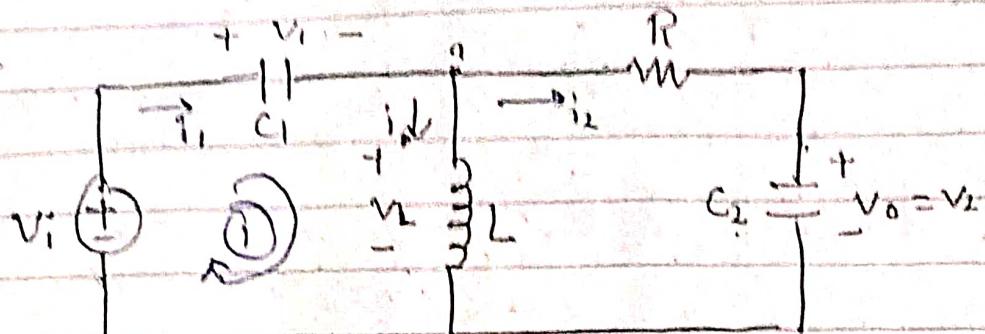
$$x_3 = z(t) - 18x_3 - 20x_2 - 5x_1$$

$$\begin{bmatrix} \ddot{x}_3 \\ \ddot{x}_2 \\ \ddot{x}_1 \end{bmatrix} = \begin{bmatrix} -18 & -20 & -5 \\ 0 & 0 & 0 \\ 0 & 0 & 0 \end{bmatrix} \begin{bmatrix} x_3 \\ x_2 \\ x_1 \end{bmatrix} + \begin{bmatrix} 1 \\ 0 \\ 0 \end{bmatrix} z(t)$$

$$y = \begin{bmatrix} 1 & 0 & 0 \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \\ x_3 \end{bmatrix}$$

[C]

Q: Find  $H(s)$



so

KVL in loop P①

$$v_i - v_1 - v_L = 0$$

$$v_i - v_1 = v_L = L \frac{di}{dt}$$

$$v_i = v_1 = L \frac{di}{dt}$$

$$\left( \dot{i}(t) = -\frac{v_1}{L} + \frac{v_i}{L} \right) \quad \text{--- (A)}$$

at node 1

$$i_1 = i + i_2$$

$$i_1 = C \frac{dv_1}{dt} \quad \text{--- (1)}$$

Apply KVL in outer loop

$$v_i - v_1 - i_2 R - v_2 = 0$$

$$v_i - v_1 - v_2 = i_2 R$$

$$\left( i_2 = \frac{v_i - v_1 - v_2}{R} \right)$$

also,

$$i_2 = \frac{C_2 dV_2}{dt}$$

$$\frac{i_2}{C_2} = V_2(t)$$

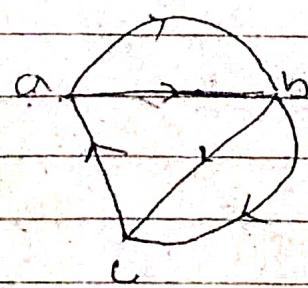
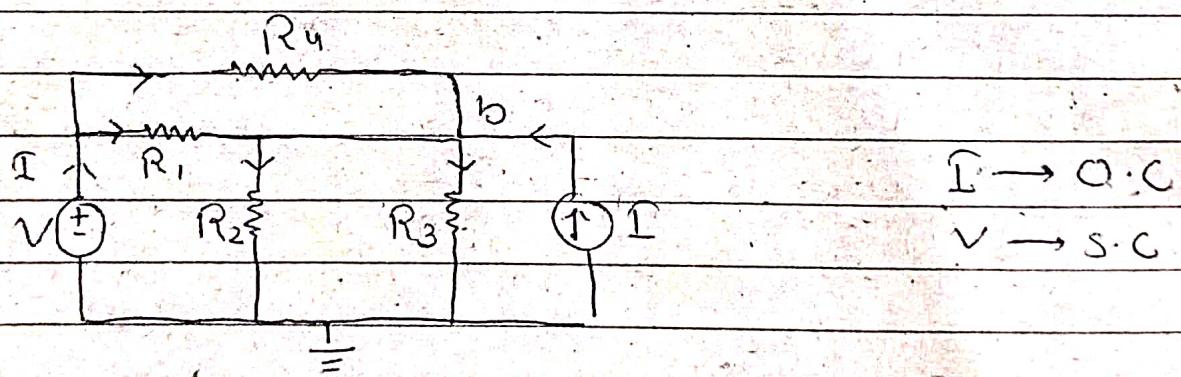
$$V_2(t) = V_i - \frac{V_i - V_1}{R C_2} - \frac{V_1 - V_2}{R C_2} \quad \text{--- (b)}$$

from ①

$$j(V_1(t)) = \frac{i_1}{C_1} + \frac{V_i - V_1}{R C_1} - \frac{V_1 - V_2}{R C_1} \quad \text{--- (c)}$$

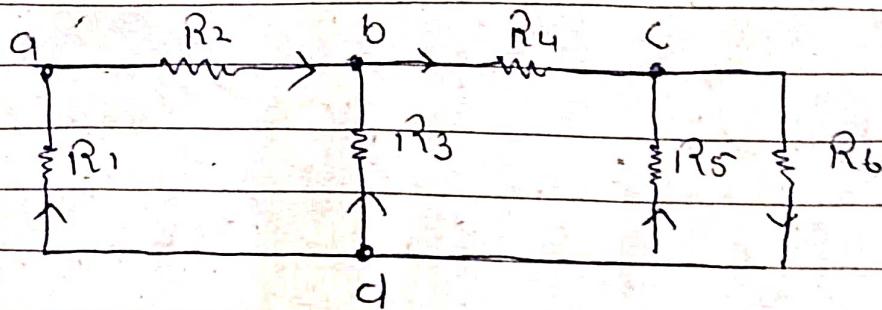
$$\begin{bmatrix} V_1 \\ i_2 \\ i_1 \end{bmatrix} = \begin{bmatrix} -1/R C_1 & -1/R C_1 & 1/C_1 \\ -1/R C_2 & -1/R C_2 & 0 \\ -1/L & 0 & 0 \end{bmatrix} \begin{bmatrix} V_1 \\ V_2 \\ V_3 \end{bmatrix} + \begin{bmatrix} 1/R C_1 \\ 1/R C_2 \\ 1/L \end{bmatrix} V_i$$

### Graph theory :

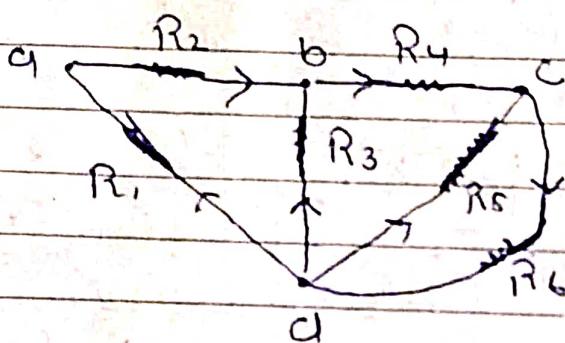


directed graph

## Incidence Matrix



→ directed graph ↴



4-node  
6-branch branches

branch →

→ incidence matrix

node ↓

	1	2	3	4	5	6
a	-1	1	0	0	0	0
b	0	-1	-1	1	0	0
c	0	0	0	-1	-1	1
d	1	0	1	0	1	-1

NOTE:-

Jis node se current nikal raha hai

uss ko (+) unge  
jis me enter

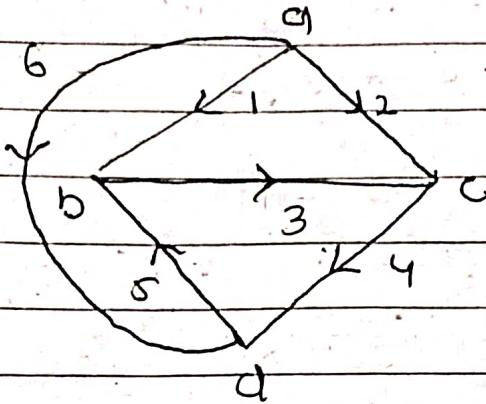
kar raha hai  
uss ko (-)

→ If we eliminate the reference node element then this matrix ~~base~~ becomes reduce incidence matrix

$$\begin{bmatrix} -1 & +1 & 0 & 0 & 0 & 0 \\ 0 & -1 & -1 & 1 & 0 & 0 \\ 0 & 0 & 0 & -1 & -1 & 1 \end{bmatrix} \rightarrow \text{Reduce incidence matrix}$$



Q:- form its incidence matrix



$$\begin{array}{c|cccccc}
 & 1 & 2 & 3 & 4 & 5 & 6 \\
 \hline
 a & 1 & 1 & 0 & 0 & 0 & 1 \\
 [A] = b & -1 & 0 & 1 & 0 & -1 & 0 \\
 c & 0 & -1 & -1 & 1 & 0 & 0 \\
 d & 0 & 0 & 0 & -1 & 1 & -1
 \end{array} \rightarrow \text{incidence matrix}$$

Now apply KCL at node a

$$i_1 + i_2 + i_6 = 0$$

KCL at node b

$$-i_1 - i_5 + i_3 = 0$$

KCL at node c

$$-i_2 + i_4 - i_3 = 0$$

KCL at node d

$$-i_6 - i_4 + i_5 = 0$$

$$[A] [i_o] = 0$$

$$\begin{bmatrix} 1 & 1 & 0 & 0 & 0 & 1 \\ -1 & 0 & 1 & 0 & -1 & 0 \\ 0 & -1 & -1 & 1 & 0 & 0 \\ 0 & 0 & 0 & -1 & 1 & -1 \end{bmatrix} \begin{bmatrix} i_1 \\ i_2 \\ i_3 \\ i_4 \\ i_5 \\ i_6 \end{bmatrix} = 0$$

~~This~~ After solving this we get all KCL eqns.

# KVL in all branches :-

b<sub>1</sub> → branch 1

$$V_{b_1} = V_a - V_b$$

$$V_{b_2} = V_a - V_c$$

$$V_{b_3} = V_b - V_c$$

$$V_{b_4} = V_c - V_d$$

$$V_{b_5} = V_d - V_b$$

$$V_{b_6} = V_a - V_d$$

$$[A] = \begin{bmatrix} 1 & 1 & 0 & 0 & 0 & 1 \\ -1 & 0 & 1 & 0 & -1 & 0 \\ 0 & -1 & -1 & 1 & 0 & 0 \\ 0 & 0 & 0 & -1 & 1 & -1 \end{bmatrix}$$

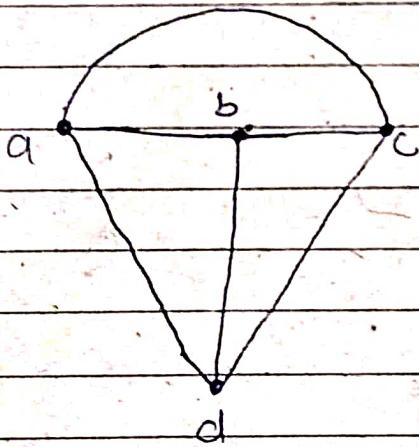


$$[A]^T [V_{node}] = [V_{branch}]$$

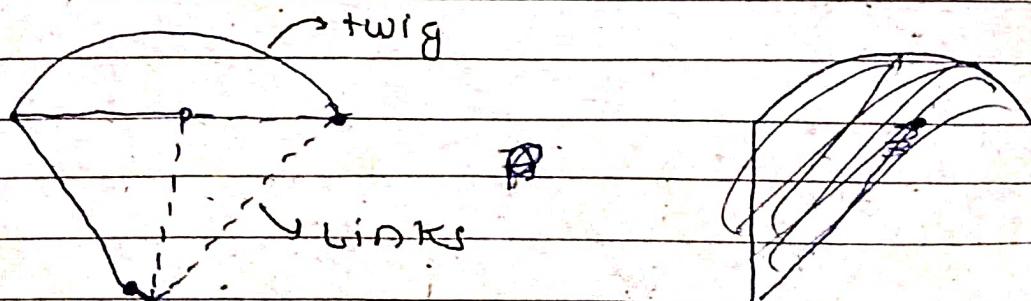
$$\begin{vmatrix} 1 & -1 & 0 & 0 \\ 1 & 0 & -1 & 0 \\ 0 & 1 & -1 & 0 \\ 0 & 0 & 1 & -1 \\ 0 & -1 & 0 & 1 \\ 1 & 0 & 0 & -1 \end{vmatrix} \begin{bmatrix} V_a \\ V_b \\ V_c \\ V_d \end{bmatrix} = \begin{bmatrix} V_{b1} \\ V_{b2} \\ V_{b3} \\ V_{b4} \\ V_{b5} \\ V_{b6} \end{bmatrix}$$

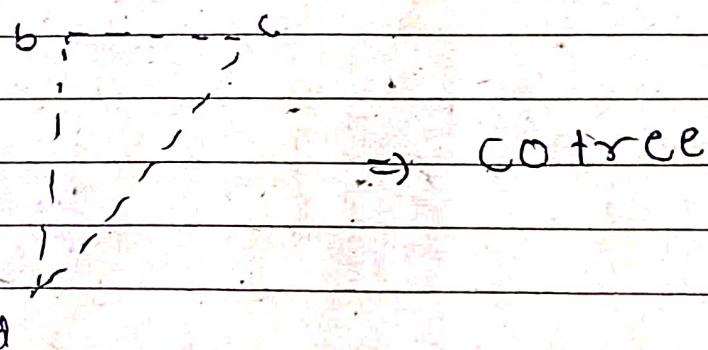
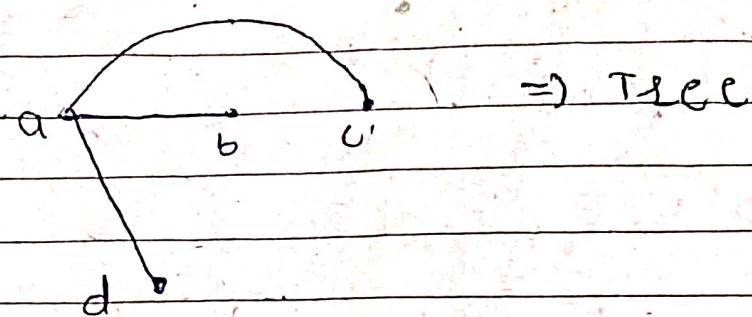
AFTER SOLVING THIS WE GET ALL KVL EQUATION'S

\* Tree and co-tree :-

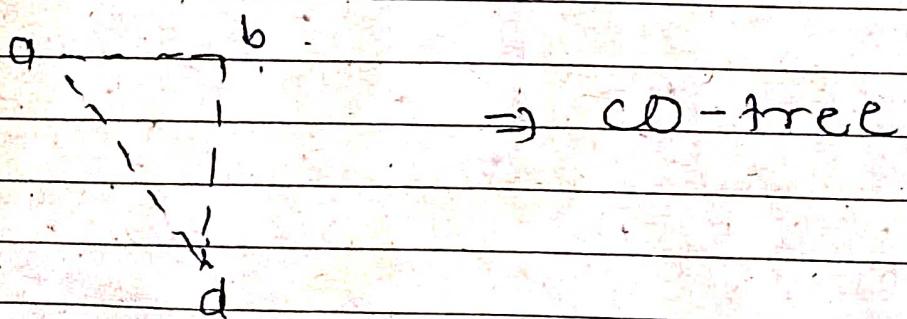
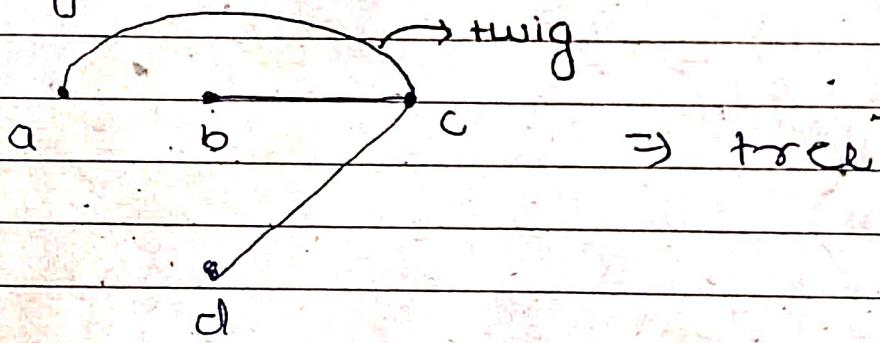


→ while making tree we have to remember that loop should not be made.





② Another ~~possible~~ possible combination  
of tree & co-tree are



$$\text{no. of possible tree} = \det \{ [A] * [A]^T \}$$

$$\begin{array}{|c c|} \hline
 \begin{matrix} 1 & 1 & 0 & 0 & 0 & 1 \\ -1 & 0 & 1 & 0 & -1 & 0 \\ 0 & -1 & -1 & 1 & 0 & 0 \\ -1 & 0 & 0 & 0 & -1 & -1 \end{matrix} & \begin{matrix} 1 & -1 & 0 & 0 \\ 1 & 0 & -1 & 0 \\ 0 & 1 & -1 & 0 \\ 0 & 0 & 1 & -1 \\ 0 & -1 & 0 & 1 \\ 1 & 0 & 0 & -1 \end{matrix} \\ \hline
 4 \times 6 & 6 \times 4 \\ \hline
 \end{array}$$

$$\Rightarrow \begin{bmatrix} 3 & -1 & -1 & -1 \\ -1 & 3 & -1 & -1 \\ -1 & -1 & 3 & -1 \\ -1 & -1 & -1 & 3 \end{bmatrix}$$

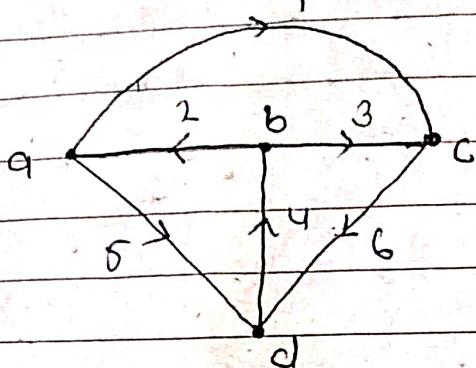
After considering reduce incidence matrix  
we get  $3 \times 3$  matrix

$$\begin{bmatrix} 3 & -1 & -1 \\ -1 & 3 & -1 \\ -1 & -1 & 3 \end{bmatrix}$$

$$\Rightarrow 3(9-1) + 1(-3-1) - 1(1+3)$$

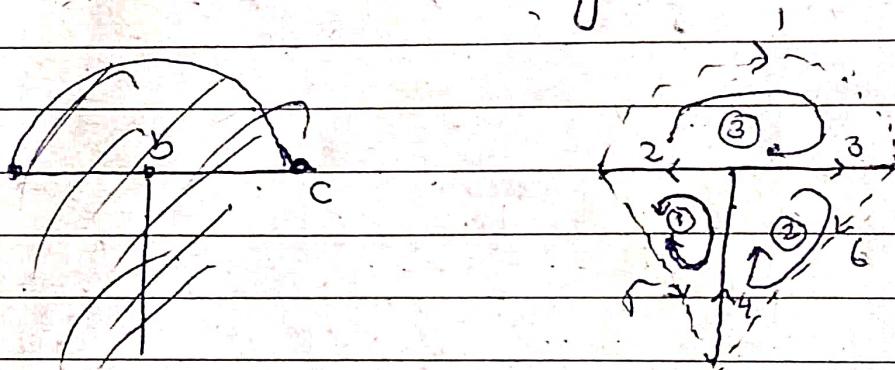
$\Rightarrow 16 \rightarrow$  ~~16~~ possible tree will form

## Tie-set Matrix



law :-

→ we have to consider only ~~those~~<sup>those</sup> loop  
that has 1 link & 2 twig



branch →

loop ↓	1	2	3	4	5	6
1	0	1	0	1	1	0
2	0	0	1	1	0	1
3	1	1	-	0	0	0

→ Tie set matrix

- Jis loop ko dekh raha hai then us loop ke branch ko consider karege baaki sab zero din
- If current ka same as the loop din the take 1 otherwise 0

\* KVL in tie set matrix

in loop 1

$$V_4 + V_2 + V_5 = 0$$

in loop 2

$$V_3 + V_6 + V_4 = 0$$

in loop 3

$$V_1 - V_3 + V_2 = 0$$

then  $[A_T] [V_b] = 0$

$$\begin{bmatrix} 0 & 1 & 0 & 1 & 1 & 0 \\ 0 & 0 & 1 & 1 & 0 & 1 \\ 1 & 1 & -1 & 0 & 0 & 0 \end{bmatrix} \begin{bmatrix} V_1 \\ V_2 \\ V_3 \\ V_4 \\ V_5 \\ V_6 \end{bmatrix} = 0$$

after solving this we get all KVL eqns.

\* KCL in Tie Set

$i_b, i_L$

$$i_1 = i_{L2}, \quad i_2 = i_{L1} + i_{L3}$$

$$i_3 = i_{L2} - i_{L3}, \quad i_4 = i_{L4} + i_{L2}$$

$$i_5 = i_{L1}, \quad i_{L6} = i_{L2}$$

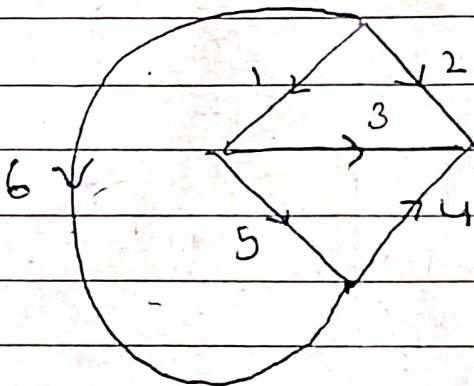
then,

$$[i_b] = [A_T]^T [i_L]$$

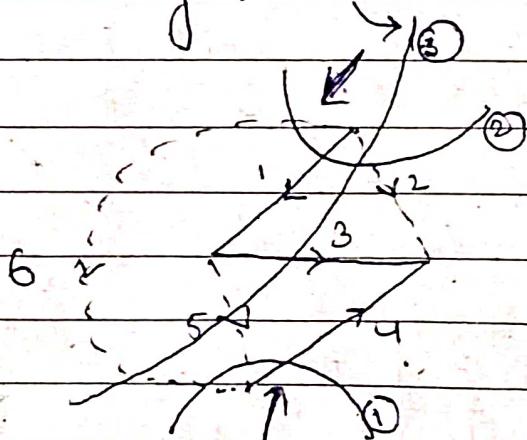
$$\begin{vmatrix} 1 & 0 & 1 \\ 1 & 0 & 1 \\ 0 & 1 & -1 \\ 1 & 1 & 0 \\ 1 & 0 & 0 \\ 0 & 1 & 0 \end{vmatrix} \begin{bmatrix} i_1 \\ i_2 \\ i_3 \\ i_4 \\ i_5 \\ i_6 \end{bmatrix} = \begin{bmatrix} i_1 \\ i_2 \\ i_3 \\ i_4 \\ i_5 \\ i_6 \end{bmatrix}$$

After solving this we get all the eqns

\* Cut set matrix :



→ cut those branches that include only one twig and at least 2 link



→ Cut set Jitni branches KO cut kar rahe hai sirf unhi branches Pe value assign hogi baaki sab zero

→ cut dair ki dair twig ke dair ko dekh ke assign karenge



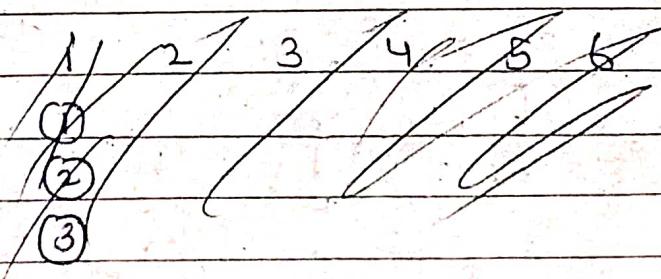
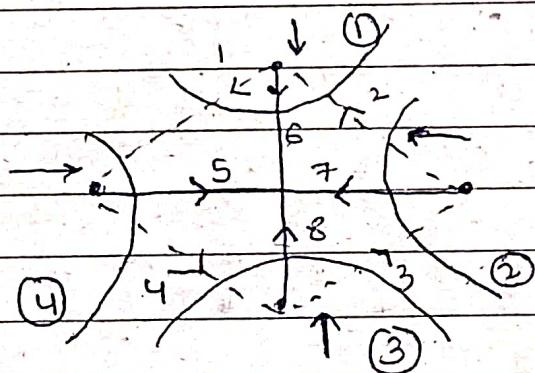
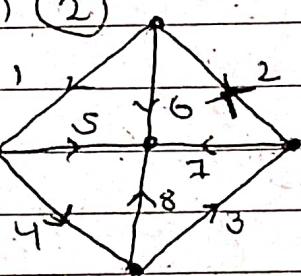
→ Cut set ke dir me current hoga to (+1) assign karenge otherwise (-1)

bland →

cutset ↓	1	2	3	4	5	6	
(1)	0	0	0	1	-1	-1	
(2)	1	1	0	0	0	1	
(3)	0	1	1	0	1	1	

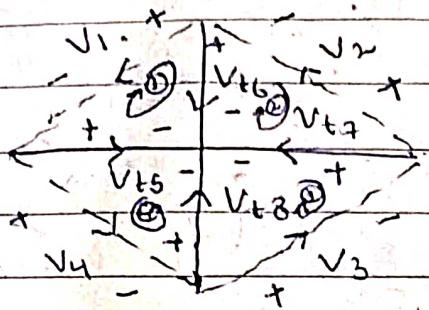
← cutset matrix

Illustration (2)



	1	2	3	4	5	6	7	8
(1)	1	-1	0	0	0	1	0	0
(2)	0	1	-1	0	0	0	1	0
(3)	0	0	1	-1	0	0	0	1
(4)	-1	0	0	1	1	0	0	0

KVL in cut set matrix



In loop ①

$$-v_1 - v_{t5} + v_{t6} = 0$$

$$v_1 = -v_{t5} + v_{t6} \quad \text{--- } ①$$

In loop ②

$$v_2 = -v_{t6} + v_{t7} \quad \text{--- } ②$$

In loop 3

$$v_3 = -v_{t7} + v_{t8} \quad \text{--- } ③$$

In loop 4

$$v_4 = -v_{t8} + v_{t5} \quad \text{--- } ④$$

In general

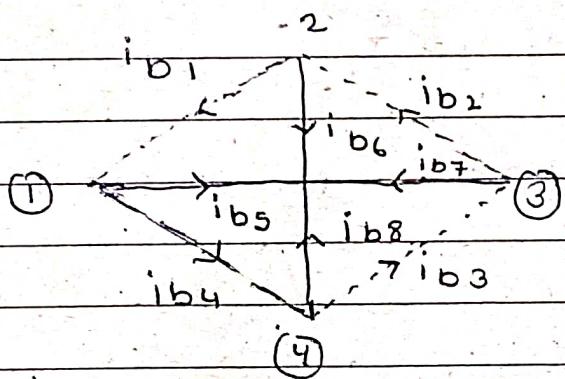
$$v_b = [0_t]^T [v_t]$$

t: twig  
b: branch

$$\left[ \begin{array}{cccc} -1 & 1 & 0 & 0 \\ 0 & -1 & 1 & 0 \\ 0 & 0 & -1 & 1 \\ 1 & 0 & 0 & -1 \\ 1 & 0 & 0 & 0 \\ 0 & 1 & 0 & 0 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{array} \right] \left[ \begin{array}{c} V_{t6} \\ V_{t6} \\ V_{t7} \\ V_{t8} \\ V_0 \end{array} \right]$$

After solving this we get all KVL eqns

KCL in cut set matrix :-



at node ①

$$ib_1 = ib_u + ib_s$$

at node ②

$$ib_2 = ib_i + ib_6$$

at node ③

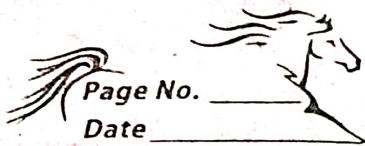
$$ib_3 = ib_7 + ib_8$$

at node ④

$$ib_4 = ib_8 + ib_3$$

(D) General

$$[\alpha][i_b] = 0$$



$$\begin{bmatrix} -1 & 0 & 0 & 1 & 1 & 0 & 0 & 0 \\ 1 & -1 & 0 & 0 & 0 & 1 & 0 & 0 \\ 0 & 1 & -1 & 0 & 0 & 0 & 1 & 0 \\ 0 & 0 & 1 & -1 & 0 & 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} i_b_1 \\ i_b_2 \\ i_b_3 \\ i_b_4 \\ i_b_5 \\ i_b_6 \\ i_b_7 \\ i_b_8 \end{bmatrix} = 0$$



## \* Network synthesis :

- There is no unique soln
- For passive elements only

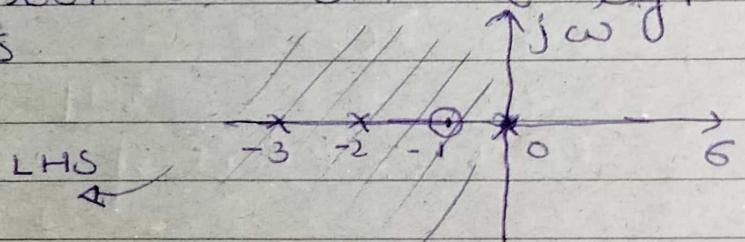
## Hurwitz polynomial :

$$H(s) = \frac{N(s)}{D(s)} = \frac{s+1}{s(s+2)(s+3)}$$

When  $H(s)$  become zero then that value of  $s$  gives zeros here only one zero exist  $(s = -1)$

when  $H(s)$  become infinite then that value of  $s$  gives poles here 3 poles exist  $s=0, s=-2, s=-3$

→ For a system to become stable then all system must lie on the left side of HSC y axis



→ For a complicated expression of  $H(s)$  Hurwitz gives the idea of that system is stable or not.

Q:- check whether polynomial is Hurwitz?

$$(a) P(s) = s^3 + 2s^2 + 4s + 2$$

SOL even part of  $P(s)$   
odd " " "

$$m(s) = 2s^2 + 2$$

$$n(s) = s^3 + 4s$$

$$\alpha(s) = \frac{m(s)}{n(s)} \text{ or } \frac{n(s)}{m(s)}$$

→ we take that part of  $P(s)$  as numerator which have highest degree

$$\alpha(s) = \frac{s^3 + 4s}{2s^2 + 2}$$

By continued fraction expansion

$$2s^2 + 2 \left[ \begin{matrix} s^3 + 4s \\ s^3 + s \end{matrix} \right] \left( \frac{s}{2} \right)$$

$$3s \left[ \begin{matrix} 2s^2 + 2 \\ 2s^2 \end{matrix} \right] \left( \frac{2s}{3} \right)$$

$$2 \left[ \begin{matrix} 3s \\ 3s \end{matrix} \right] \left( \frac{3s}{2} \right)$$

all quotient terms are +ve so  $P(s)$  is Hurwitz

$$(b) P(s) = s^4 + s^3 + 4s^2 + 2s + 3$$

$$\underline{\underline{SOL}} \quad m(s) = s^4 + 4s^2 + 3$$

$$n(s) = s^3 + 2s$$



$$Q(s) = \frac{m(s)}{n(s)} = \frac{s^4 + 4s^2 + 3}{s^3 + 2s}$$

$$\begin{array}{r} s^3 + 2s \sqrt{s^4 + 4s^2 + 3} |(s) \\ \underline{-} \quad s^4 + 2s^2 \cancel{+ 3s^2} \\ \hline \end{array}$$

$$\begin{array}{r} 2s^2 + 3 \sqrt{s^3 + 2s} |(s) \\ \underline{-} \quad s^3 + 3s \\ \hline -s^2 \end{array}$$

$$\frac{1}{2}s \sqrt{2s^3 + 3} |(s)$$

$$\frac{3\sqrt{\frac{1}{2}s}}{0} |(s)$$

all quotients are +ve then  
it is Hurwitz polynomial

$$(c) P(s) = s^5 + 2s^3 + 3$$

SOL As all even part are missing thus  
it satisfy Hurwitz polynomial property

$$P(s) = s^5 + 2s^3 + 3s = N(s)$$

$$\frac{dP(s)}{ds} = 5s^4 + 6s^2 + 3 = M(s)$$

$$Q(s) = \frac{N(s)}{M(s)} = \frac{s^5 + 2s^3 + 3s}{5s^4 + 6s^2 + 3}$$

## Positive Real Function (PRF)

$$P(s) = Z(s) = \frac{P(s)}{Q(s)} = \frac{a_n s^n + a_{n-1} s^{n-1} + \dots + a_1 s + a_0}{b_m s^m + b_{m-1} s^{m-1} + \dots + b_1 s + b_0}$$

$$\begin{matrix} P(s) \\ Q(s) \end{matrix} \quad \begin{matrix} m_1, n_1 \\ m_2, n_2 \end{matrix}$$

if,  $(m_1 m_2 - n_1 n_2) \Big|_{s=j\omega} \geq 0.$

If this condition satisfy then it is PRF.

Q:- check whether  $F(s) = \frac{s+2}{s+4}$  is the real function?

Sol Given  $F(s) = \frac{s+2}{s+4}$

$$\therefore |m_1 m_2 - n_1 n_2| \Big|_{s=j\omega} \geq 0$$

$$m_1 = 2, \quad m_2 = 4 \\ n_1 = 5, \quad n_2 = 5$$

$$8 - 5^2 \Big|_{s=j\omega} \geq 0$$

$$= 8 - (j\omega)^2 \Rightarrow (8 + \omega^2 > 0)$$

thus it is PRF



$$(b) F(s) = \frac{s^2 + 7s + 12}{s^3 + 9s^2 + 20s + 12}$$

SOL  $m_1 = s^2 + 12$ ,  $m_2 = 9s^2 + 12$   
 $n_1 = 7s$ ,  $n_2 = s^3 + 20s$

$$\therefore m_1m_2 - n_1n_2 \geq 0 \quad |_{s=j\omega}$$

$$\begin{aligned} & (s^2 + 12)(9s^2 + 12) - 7s(s^3 + 20s) \\ &= (9s^4 + 12s^2 + 108s^2 + 144) - 7s^4 - 140s^2 \\ &\quad 2s^4 + 120s^2 - 140s + 144 \\ & 2(j\omega)^4 - 20(j\omega)^2 + 144, \text{ put } s=j\omega \\ & (2\omega^4 + 20\omega^2 + 144 \geq 0) \end{aligned}$$

as it is greater than zero thus it is PRR

$$(c) F(s) = \frac{s^2 + 9}{s^3 + s} \quad s^2 + 9 = 0$$

modifying

$$F(s) = \frac{(s+j3)(s-j3)}{s(s^2+1)} \quad s^2 = -9 \quad s = \pm j3$$

$$= \frac{(s+j3)(s-j3)}{s(s+j)(s-j)} \quad \text{Find residues}$$

thus By Partial fraction

$$\frac{(s+j3)(s-j3)}{s(s+j)(s-j)} = \frac{A}{s} + \frac{B}{s+j} + \frac{B^*}{s-j}$$

$$A|_{s=0} = \frac{(s+j3)(s-j3)}{(s+j)(s-j)} = \frac{3j \times -3j}{j \times -j} = 9$$

$$B|_{s=-j} = \frac{(s+j3)(s-j3)}{s(s-j)} = \frac{(-j+j3)(-j-j3)}{-j} = -4$$

$$B^*|_{s=j} = \frac{(s+j3)(s-j3)}{s \times (s+j)} = \frac{(j+j3)(j-j3)}{j(j+j)} = -4$$

The residue  $B$  &  $B^*$  are real, but not positive  
so the  $F(s)$  is not PRF

### Network synthesis

Q:- Synthesize the impedance function

$$(a) Z(s) = \frac{2s^3 + 7s}{s^3 + 3}$$

$$\underline{\underline{Z(s)}} = \frac{s^2 + 3}{s^3 + 3} \left[ \frac{2s^3 + 7s}{2s^3 + 6s} \right] \xrightarrow{s} \frac{2s + \frac{s}{s}}{s^3 + 3}$$

$$Z(s) = Z_1(s) + Z_2(s)$$

$$Z_1(s) = 2s \quad , \quad Z_2(s) = \frac{s}{s^3 + 3} = Y_2(s) = \frac{1}{s^3 + 3}$$

$$Y_2(s) = s + \frac{3}{s} \Rightarrow Y_2(s) = Y_3(s) + Y_4(s)$$

$$\Rightarrow Z(s) = 2s + \frac{1}{Y_2(s)}$$

$$= 2s + \frac{1}{Y_3(s) + Y_4(s)}$$

$$= 2s + \frac{1}{(s+3/s)}$$

$$\text{Series } \left. \begin{array}{l} R \\ C \rightarrow \frac{1}{SC} \\ L \rightarrow SL \end{array} \right\} \text{parallel}$$

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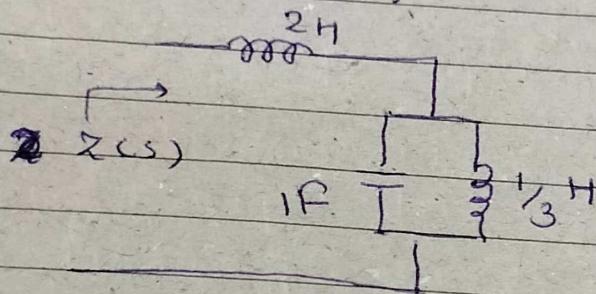


$$Y_3(s) = s = sc \Rightarrow c = 1$$

$$Y_4(s) = \frac{3}{s} = \frac{1}{s^6} \Rightarrow L = \frac{1}{3} H$$

$$z(s) = 2s \rightarrow l = 2H$$

CKT LOOK like



$$(b) Z(s) = \frac{8s^3 + 4s^2 + 4s + 1}{8s^3 + 4s}$$

$$\underline{\text{SOL}} \quad 8s^3 + 4s^2 + 4s + 1 \quad | \quad 1$$

$$8s^3 + 4s^2 + 4s + 1$$

$$-\underline{8s^3 + 4s}$$

$$-\underline{\underline{4s^2 + 1}}$$

$$1 + \frac{4s^2 + 1}{8s^3 + 4s}$$

$$x_1(s) \quad \Downarrow$$

$$z_2(s)$$

$$Z(s) = R_1(s) + Z_2(s)$$

$$Z(s) = \frac{1}{\chi_2(s)} = \frac{8s^3 + 4s}{4s^2 + 1}$$

$$4s^2 + 1, \overline{[8s^8 + 4s]} \underline{8s^3 + 2s}$$

$$Y_2(s) = \frac{2s + 2s}{4s^2 + 1}$$

$$= \frac{2s + 2}{(4s^2 + 1)s}$$



$$Z(s) = Y_1(s) + \frac{1}{Y_2(s)} = Z_1(s) + \frac{1}{Y_3(s) + Y_4(s)}$$

$$\Rightarrow 1 + \frac{1}{2s+2} \quad \Rightarrow Y_4(s) = \frac{2}{4s+1}$$

$$Y_4(s) = \frac{4s+1}{2}$$

$$Z_4(s) = 2s + \frac{1}{2s} = \frac{1}{Y_4(s)}$$

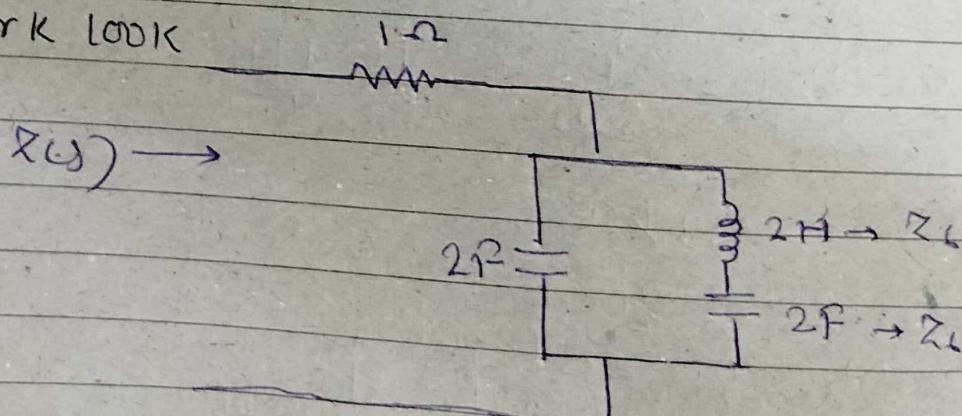
$$Z(s) = Z_1(s) + \frac{1}{Y_3(s) + \frac{1}{Z_4(s)}}$$

$$Z_1(s) = 1 \\ (R = 1 \Omega)$$

$$Y_3(s) = 2s = Cs \quad (C = 2F)$$

$$Z_5 = 2s, \quad (L = 2H) \\ Z_6 = \frac{1}{2s}, \quad (C = 2F)$$

Network look like,



$$(C) Z(s) = \frac{s^2 + 3s + 12}{s(s+4)}$$

Q1  $s^2 + 4s \quad s^2 + 3s + 12 \quad (+1)$

$$s^2 + 4s$$

$$-s + 12$$

as it become ve HWS  
we stop here & do

$$\begin{array}{r} s^2 + 4s \\ \times s^2 + 3s + 12 \\ \hline s^2 \end{array}$$

$$\Rightarrow \frac{3}{s} + \frac{s^2}{s^2 + 4s}$$

$\downarrow$   
 $Z(s)$

$$Z(s) = Z_1(s) + Z_2(s)$$

$$Z(s) = \frac{3}{s} + \frac{s}{s+4}$$

$$Y_2(s) = Z_2(s) = \frac{s+4}{s}$$

$$Z(s) = Z_1(s) + \frac{1}{Y_3(s) + Y_4(s)}$$

$$\begin{matrix} 1+4 \\ \downarrow \\ Y_3 \end{matrix} \quad \begin{matrix} \downarrow \\ Y_4 \end{matrix}$$

NOW,

$$Z_1(s) = \frac{3}{s} \quad C = \frac{1}{3} R$$

$$Y_3(s) = 1, \quad R = 1 \Omega$$

$$Y_4(s) = \frac{4}{s} = \frac{1}{sL} = L = \frac{1}{4} H$$

