

# pypbomb: A Python package with tools for the design of detonation tubes

Mick Carter<sup>1</sup> and David Blunck<sup>1</sup>

<sup>1</sup> School of Mechanical, Industrial, and Manufacturing Engineering, Oregon State University, Corvallis, OR, USA

DOI: [10.21105/joss.03176](https://doi.org/10.21105/joss.03176)

## Software

- [Review](#) ↗
- [Repository](#) ↗
- [Archive](#) ↗

Editor: [Pending Editor](#) ↗

Submitted: 11 April 2021

Published: 16 April 2021

## License

Authors of papers retain copyright and release the work under a Creative Commons Attribution 4.0 International License ([CC BY 4.0](#)).

## Statement of need

A detonation is supersonic combustion in which a reaction front is coupled with a pressure shock front ([Lee, 2008](#)). Adiabatic heating from the shock front helps to sustain the combustion, which in turn accelerates the shock front and allows it to propagate supersonically. Because the products of a detonation are at a higher pressure than the reactants, thermodynamic cycles using detonations, such as the Humphrey cycle, have the potential for higher thermodynamic efficiency than deflagration-based cycles, such as the Brayton cycle ([Coleman, 2001](#)). However, knowledge of a reactant mixture's characteristic detonation structure is needed in order to make practical use of it with detonation-based cycles.

The behavior of a detonation can be investigated either via simulation or physical experimentation. Given that detonation is an inherently three-dimensional process ([Ciccarelli & Dorofeev, 2008](#); [Lee, 2008](#)), accurate simulations can be computationally expensive ([Kessler et al., 2010](#)), requiring runs on the order of days to months for a single 2-D simulation depending on the hardware involved ([Kessler et al., 2011](#); [Radulescu et al., 2007](#)). Alternatively, a detonation tube is often used to experimentally study the behavior of detonations. In a detonation tube, data for a given set of initial conditions can be collected anywhere from multiple times per second (e.g. in a pulse detonation engine) to multiple times per hour (e.g. in a closed-end detonation tube).

The design of a detonation tube requires many considerations, including estimation of the required length for deflagration-to-detonation transition (DDT), tube material and size selection (including the effects of transient pressures), fastener failure calculations (including bolt pull-out), flange class selection, viewing window sizing (if optical access is required), and prediction of safe operating conditions (including accounting for detonation reflection in the case of a closed-end tube). All of this is specific to the mixture being detonated, therefore it is important to be able to quickly re-perform the analysis for new reactant mixtures. The tools within pypbomb provide a first-order analysis meant to serve as the basis for the previously detailed analysis.

## Summary

pypbomb contains a series of tools that can be used to iterate on initial design parameters and obtain an estimate for the operational envelope of a closed-end detonation tube. This package is not meant to replace the design process entirely, but rather to provide an initial design of a detonation tube through a series of simplified analyses. A conservative safety factor is recommended given the dynamic nature of detonations, as well as a more in-depth analysis of the tube's individual components; the analysis in this package assumes steady state propagation at equilibrium conditions and does not account for transient effects other than

41 through a dynamic load factor. The first iteration of this package was written during the  
42 design of a detonation tube that has been used to measure cell sizes of gaseous detonations,  
43 and will be used in the near future for the study of detonations in two-phase mixtures.

44 `pybomb.Tube` allows the user to quickly iterate on the design of the piping portion of a  
45 detonation tube and determine its safe operational limits. Nominal Pipe Size (NPS) lookups  
46 are included, allowing the user to quickly assess different tube geometries. Once the tube  
47 geometry is determined, the stress limits of the pipe material are used to evaluate the maximum  
48 allowable static pressure within the tube. For convenience, maximum allowable stress values  
49 of stainless steels are available as a function of temperature ([American Society of Mechanical  
50 Engineers, 2007](#)). Alternative allowable stress values, such as those calculated using the ASME  
51 Boiler and Pressure Vessel code, may also be manually supplied by the user. However, it is  
52 important to keep in mind that no code currently exists for the design of detonation tubes  
53 (because of the dynamic transient pressures they experience as well as with their experimental  
54 nature), and any estimate using existing code should be accompanied by a more in-depth  
55 evaluation and/or a large safety factor. Once the user has determined the allowable stress, it  
56 is used to calculate the maximum operating pressure of the tube ([Megyesy, 2001](#)). Accounting  
57 for the tube geometry and predicted mixture detonation behavior, a dynamic load factor is  
58 calculated and applied ([Shepherd, 2009](#)). The dynamic load factor is used to adjust the  
59 static pressure limit to account for the tube's response to the transient pressure caused by  
60 the detonation wave. The maximum initial reactant pressure is then iteratively determined  
61 for a given tube geometry, reactant mixture, and initial temperature using the maximum  
62 operating pressure. Detonation wave speeds and reflection properties for the desired reactant  
63 mixture are calculated using selected functions adapted from the shock and detonation toolbox  
64 (SDToolbox) ([Browne et al., 2019](#)). The curve fitting portion of the wave speed estimation  
65 in SDToolbox has been parallelized in order to speed up computation.

66 Once the operational limits of a tube are determined, flanges can be sized. `pybomb.Fl`  
67 `ange` looks up the minimum necessary flange class based on the maximum tube pressure  
68 and temperature based on the standards set forth in ASME B16.5-2003 ([American Society  
69 of Mechanical Engineers, 2004](#)). Although they are used here to provide an estimate of  
70 minimum flange class, ASME codes do not account for impulsive loads such as those caused  
71 by detonations. Therefore further analysis should be conducted on a per-flange basis, using  
72 the recommended flange size as an initial design.

73 A successful detonation tube design must account for the deflagration-to-detonation transition  
74 (DDT). DDT is usually achieved using a series of blockages, which causes the combustion  
75 wave to undergo local accelerations, thereby aiding in the DDT process ([Ciccarelli & Dorofeev,  
76 2008](#)). The blockages must be properly sized, and must continue for a minimum (mixture  
77 specific) distance in order to maximize the probability of a successful transition to detonation.  
78 To this end, `pybomb.DDT` contains tools for Shchelkin spiral blockage ratio and diameter  
79 calculations, and allows the user to estimate the necessary DDT run-up length for a desired  
80 mixture using Cantera ([Ciccarelli & Dorofeev, 2008](#); [Goodwin et al., 2018](#)).

81 Finally, `pybomb` provides some tools to facilitate the inclusion of optical access in the deto-  
82 nation tube. Historically, the structure of detonations have typically been studied using soot  
83 covered foils inserted along the wall or end-cap of detonation tubes ([Lee, 2008](#)). More re-  
84 cently, however, researchers have begun using high speed photography to study detonation  
85 waves, including PLIF and focusing schlieren methods ([Mével et al., 2015](#); [Pintgen & Shep-  
86 herd, 2003](#); [Radulescu et al., 2007](#); [Rankin, 2016](#); [Stevens et al., 2015](#)). In some cases, soot  
87 foil and schlieren techniques have been used simultaneously ([Kellenberger & Ciccarelli, 2017](#)).  
88 If optical access is desired, window thickness and factor of safety calculations can be quickly  
89 performed for clamped rectangular windows using `pybomb.Window` ([Crystran LTD, 2014](#)).  
90 These calculations do not account for loads applied to the window due to contact with the  
91 detonation tube or window retainers; it is critical that windows be isolated from contact with  
92 any hard surfaces. In our tube this was accomplished using rubber gaskets on the faces of the  
93 windows as well as around the periphery. In addition to window calculations, `pybomb.Bolt`

allows the user to estimate bolt stress areas and safety factors in order to keep the windows intact and prevent bolts from pulling out of the tube (Oberg, 2000).

## Acknowledgements

This work is supported by the Office of Naval Research, contract N000141612429. The authors would like to thank the Detonation Group at the Air Force Research Laboratory for providing access to a detonation tube, as well as for their invaluable input and technical advice. Additionally, the authors would like to thank Kyle Niemeyer for his instruction and encouragement in the area of open-source software development for engineering research. Finally, this package and the research that it precedes are enabled by the resources made available to the public by Joseph Shepherd's [Explosion Dynamics Laboratory](#) at Caltech; a debt of gratitude is owed to everyone who has contributed to that group, and insightful comments about this manuscript by Dr. Shepherd are gratefully acknowledged.

## References

- American Society of Mechanical Engineers. (2007). *ASME B31.1-2007 power piping*. American Society of Mechanical Engineers.
- American Society of Mechanical Engineers. (2004). *ASME B16.5-2003 pipe flanges and flanged fittings: NPS 1/2 through NPS 24 metric/inch standard*. American Society of Mechanical Engineers.
- Browne, S., Ziegler, J., Bitter, N., Schmidt, B., Lawson, J., & Shepherd, J. E. (2019). *SDToolbox numerical tools for shock and detonation wave modeling*. Explosion Dynamics Laboratory. <https://shepherd.caltech.edu/EDL/PublicResources/sdt/>
- Ciccarelli, G., & Dorofeev, S. (2008). Flame acceleration and transition to detonation in ducts. *Progress in Energy and Combustion Science*, 34(4), 499–550. <https://doi.org/10.1016/j.pecs.2007.11.002>
- Coleman, M. L. (2001). *Overview of Pulse Detonation Propulsion Technology*. Chemical Propulsion Information Agency. <http://www.dtic.mil/dtic/tr/fulltext/u2/a390257.pdf>
- Crystran LTD. (2014, October). *The design of pressure windows*. <https://www.crystran.co.uk/userfiles/files/design-of-pressure-windows.pdf>
- Goodwin, D. G., Speth, R. L., Moffat, H. K., & Weber, B. W. (2018). *Cantera: An Object-oriented Software Toolkit for Chemical Kinetics, Thermodynamics, and Transport Processes* (Version 2.4.0). Zenodo. <https://doi.org/10.5281/zenodo.1174508>
- Kellenberger, M., & Ciccarelli, G. (2017). Simultaneous schlieren photography and soot foil in the study of detonation phenomena. *Experiments in Fluids*, 58(10), 1–13. <https://doi.org/10.1007/s00348-017-2420-0>
- Kessler, D. A., Gamezo, V. N., & Oran, E. S. (2010). Simulations of flame acceleration and deflagration-to-detonation transitions in methane – air systems. *Combustion and Flame*, 157(11), 2063–2077. <https://doi.org/10.1016/j.combustflame.2010.04.011>
- Kessler, D. A., Gamezo, V. N., & Oran, E. S. (2011). Multilevel detonation cell structures in methane-air mixtures. *Proceedings of the Combustion Institute*, 33(2), 2211–2218. <https://doi.org/10.1016/j.proci.2010.07.071>
- Lee, J. H. S. (2008). *The Detonation Phenomenon*. Cambridge University Press. <https://doi.org/10.2514/1.43659>

- 136 Megyesy, E. F. (2001). *Pressure vessel handbook* (p. 14). PV Publishing, Inc.
- 137 Mével, R., Davidenko, D., Lafosse, F., Chaumeix, N., Dupré, G., Paillard, C.-É., & Shepherd,  
138 J. E. (2015). Detonation in hydrogen–nitrous oxide–diluent mixtures: An experimental  
139 and numerical study. *Combustion and Flame*, 162(5), 1638–1649. <https://doi.org/10.1016/j.combustflame.2014.11.026>
- 140
- 141 Oberg, E. (2000). *Machinery's handbook* (26th ed.). Industrial Press.
- 142 Pintgen, F., & Shepherd, J. E. (2003). Simultaneous Soot Foil and PLIF Imaging of  
143 Propagating Detonations. *19th International Colloquium on the Dynamics of Explosions  
144 and Reactive Systems*, 1–4. [https://shepherd.caltech.edu/EDL/publications/reprints/ICDERS03soot\\_revised.pdf](https://shepherd.caltech.edu/EDL/publications/reprints/ICDERS03soot_revised.pdf)
- 145
- 146 Radulescu, M. I., Sharpe, G. J., Law, C. K., & Lee, J. H. S. (2007). The hydrodynamic  
147 structure of unstable cellular detonations. *Journal of Fluid Mechanics*, 580(2007), 31.  
148 <https://doi.org/10.1017/S0022112007005046>
- 149 Rankin, B. A. (2016). *Evaluation of Mixing Processes in a Non-Premixed Rotating Detonation Engine Using Acetone PLIF Imaging*. January, 1–12. <https://doi.org/10.2514/6.2016-1198>
- 150
- 151
- 152 Shepherd, J. E. (2009). Structural Response of Piping to Internal Gas Detonation. *Journal  
153 of Pressure Vessel Technology*, 131(3), 031204. <https://doi.org/10.1115/1.3089497>
- 154 Stevens, C. A., Hoke, J., & Schauer, F. (2015, January). Optical Measurement of Detonation  
155 with a Focusing Schlieren Technique. *53rd AIAA Aerospace Sciences Meeting*. <https://doi.org/10.2514/6.2015-1350>
- 156