

DEPARTMENT OF ELECTRONIC AND TELECOMMUNICATION
UNIVERSITY OF MORATUWA

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The Analog-Piano

Team : Dream Epic

S.Sanjith	190562G
T.Sajeepan	190539T
K.G.C.P.Sandaruwan	190557V
G.S.M.U.K.Samarakoon	190543B

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Our sincere thanks to Mr.Bhanuka Silva.

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All the circuit virtual simulation circuits and results can be found [here](#).

Abstract

The electronic pianos available in the markets are using a pre-recorded audio of the sound to generate the tones. The task of this project is explore the possible analog designs to synthesize a tone. In this report, we have discussed our views and experiences on a stable design for synthesizing middle octave c-Note. An audio amplifier design that improvises the generated sound quality and capable of driving mid-power speakers is included in parallel at each stage.

1 Introduction

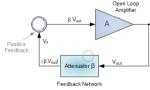
Music is one of the key things to please people and it's based on musical notes. It is so wonderful to observe such notes can be generated by combining electrical signals.

In this device sound of the middle octave, C is mimicked by synthesizing signals. For this purpose, four wien-bridge oscillators have been used to generate sinusoidal waveforms relevant to the major harmonics of the C note. Then these signals are added by a scaling adder and amplified using a Class AB amplifier. A speaker(8Ω preferred) ranges around 3W could be used with the pinout to observe the sound output.

The volume of the speaker and the noise level can be adjusted as the user desires. A complete electronic piano can be implemented by combining such modules and changing the essentials accordingly to generate different notes. The following report will elaborate on the experiences and ideas behind the design process.

2 Theory

2.1 Oscillator



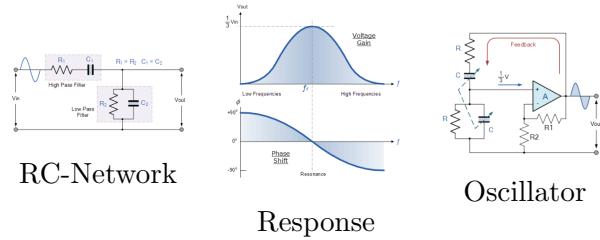
An oscillator is an amplifier that uses positive feedback that generates an output frequency without the use of an externally applied input signal. Once the oscillation is started, the parameters A and β are aligned to maintain a unity gain at the required frequency in order to keep the oscillation indefinitely stable.

Wein-Bridge Oscillator

The Wien Bridge Oscillator uses a feedback circuit consisting of a series RC node cascaded with a parallel RC of the same component values producing a phase delay or phase advance circuit depending upon the frequency. Effectively they act as a second-order frequency dependant Band-Pass-Filter with a high Q factor at the selected frequency $f_r = \frac{1}{2\pi RC}$. This RC network is connected in the positive feed-back

path of the amplifier and has zero phase shift at just one frequency.

Other part of the feedback signal is connected to the inverting input terminal(negative feed-back) via resistor divider network of $R_1 & R_2$. Then at the selected resonant frequency(f_r), the voltages applied to the inverting and non-inverting inputs will be equal and "in-phase". So the positive feedback will cancel out the negative feedback signal causing the circuit to oscillate.



Starting and Damping Oscillation

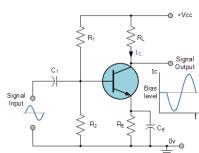
By controlling the negative feedback ratio($\frac{R_2}{R_1+R_2}$) of the oscillator we can start and damp the oscillation as required. To start oscillation, we need to slightly reduce the negative feedback($< \frac{1}{3}$). This will give rise to a resultant signal on the amplifier input side which is get amplified and fed back recursively turns out to drive oscillation.

Keeping the feedback ratio slightly more ($> \frac{1}{3}$) will give rise to a resultant negative input which is get added adversely with output resulting in damping of the oscillation. By fine-tuning the ratio in a very elegant manner, it is possible to control the damping time constant.

2.2 Amplifier

Driving a high-power (3W) speaker draws a high amount of current from the circuit. These current ranges are very much higher than the maximum supply available from op-amps and other low power components used in generating the wave patterns. So it is crucial to maintain an amplifier boundary between low power noisy signal to high power driving signal free of noise. In the following context, we will discuss the theories behind our amplifier design in detail.

Class-A



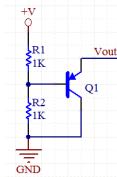
These are the simplest configuration among other families. It uses a single-ended transistor for its output stage with the resistive load connected directly to the Collector terminal. When the transistor switches “ON” it sinks the output current through the Collector resulting in an inevitable voltage drop across the Emitter resistance thereby limiting the negative output capability.

The current handling capability of such an amplifier family can be increased drastically by replacing the output transistor with the structure of **Darlington pair**. These devices provide high input impedance.

amplifiers, these circuits allow the use of compact heat sinks during the operation.

Variable Zerner Diode

This variable Zener diode circuit acts like a Zener diode with a breakdown voltage adjustable in a vast domain. This is achieved by driving a BJT in the active region and controlling the base current.



The current through the voltage divider $R_1 \& R_2$ must be higher compared to the base current.

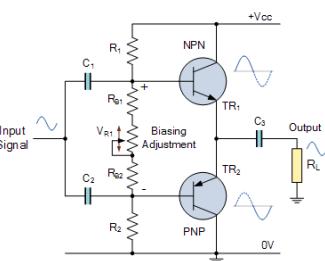
Class-B

Class B Amplifiers are biased to only conduct half of the input signal. Using 2 such amplifiers arranged in a “Push-Pull” configuration, and combining the output signal, the full waveform can be obtained.

As the quiescent current for this amplifier is 0, there is little or no DC, therefore much less power dissipation. However, there is a slight waveform distortion due to the bias voltage requirement of the transistor known as cross-over distortion.

Class-AB

Class AB amplifiers overcome the distortion issue of class B amplifiers by permanently bringing the two transistors just into the active region. This reduces the efficiency, but results in an undistorted the waveform in the output.



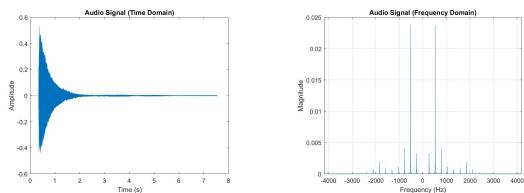
As the power dissipation due to the DC component is much less than class A am-

3 Methodology

3.1 Preliminary Analysis

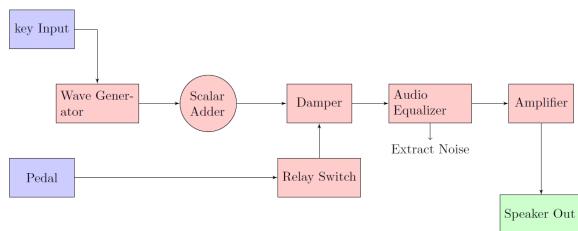
At an earlier stage of the project, it is planned to build an octave piano with twelve notes including minor keys. At that stage, we analyzed the frequency spectrum of each note and found out it is possible to produce a majority feeling of sound with only four harmonics to a given note.

After synthesizing all the keynotes from its harmonics using Matlab, we moved to circuit development. At this stage, it is decided to stimulate only one note from the piano because the generation of notes is modularizable. For this purpose, the C-wave have chosen which is in the middle of the spectrum.



3.2 Circuit Design

The key components of the circuit are illustrated below in the block diagram. Before moving to the prototype all the circuits are simulated using NI Multisim. Working simulation models of all the circuits can be found in the git-repository.



Block Diagram of the Circuit

3.2.1 Wave Generator

Square wave generation of half the frequency together with a bandpass active filter is considered in the first stage of the circuit development. Need for achieving a larger Q factor for

the filter as the number of harmonics increases, lift the choice to not-feasible.

Moving towards a stable solution brought the Wien bridge oscillator into play. These oscillators have the flexibility over frequency choice ($\frac{1}{2\pi RC}$) making them the most suitable option to be used with modularizable piano.

3.2.2 Key and Pedal

After a clear analysis of the waveform using Matlab, it is expected to achieve an exponential decay in the waveform once the oscillation is triggered. Looking at the discharging behavior of the capacitor initially it is decided to engage a capacitor together with an analog multiplier to form an envelope around wave output.

Due to the power inefficiency of the design and difficulty in finding good quality multipliers, the design moved to engage tuning of negative feedback of oscillator to achieve necessary output. This is further utilized to mimic the damping pedal of the piano by controlling the elongation of the signal-out of each oscillator.

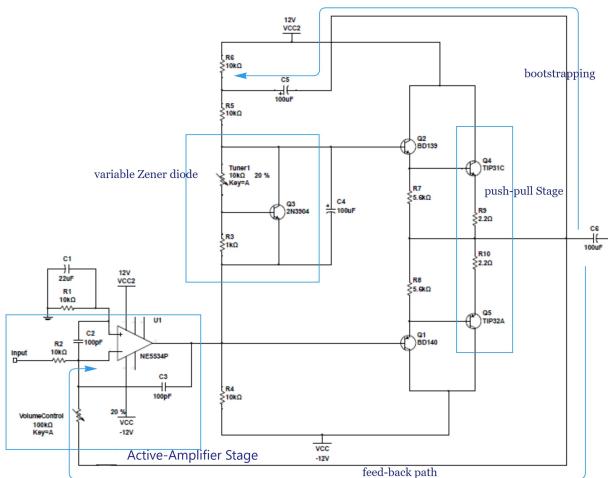
3.2.3 Scalar Adder

Direct connection between outputs of oscillators even after scaling leads to interference in the signal generation stage of the oscillator. In contrast, using a scaling adder we can provide a low impedance output path while scaling the inputs as specified.

3.2.4 Amplifier

At earlier stages, the amplifier was implemented in class-A configuration. The requirement for lower output resistance of the bias path leads to high power dissipation in the signal-free state. This made such a model not practical without huge heatsinks at the cost of low power efficiency.

Active Amplifier Stage: In the first part of the amplifier design an op-amp is used in the inverting configuration. The feedback path is connected to the end of the overall circuit to ensure enough current supply available in the output.



The op-amp NE5534 was chosen for the purpose according to its key characteristics such as high unity-gain bandwidth(10MHz), very low harmonic distortion,high common mode rejection ratio(100dB). The capacitance values of C2 and C3 are chosen to allow only higher frequencies ($> 20\text{kHz}$) to pass through. These are utilized in a manner to remove high-frequency noises from the wave-form.

Push-Pull Stage: Considering the requirement of high power gain it is decided to engage Darlington pairs for this purpose. These components failed in the long run due to the inability of compensating for high power dissipation. Considering this, the design moved to engage two coupled BJTs to allow the choices for transistors to be used in the high current path. The similar pairs TIP31C and TIP32C were chosen after considering their high power compensation capability(around 40W).

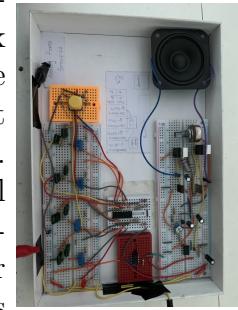
Bias: Due to the requirement for a sudden supply of high current on the keypress, the signal gets noisy when we drive the speaker without any bias. In earlier stages, a few diodes are used to bias the circuit which failed to get rid of the noise. As the next step, we used Zener diodes that provide the capability to choose higher bias voltage. This results in the low efficiency of the circuit. After considering all the methods it is decided to implement the variable Zener diode which has the flexibility over varying bias voltage in a wider range. This provides control over two extremities, effeciency

and quality of the output.

Bootstrapping: The capacitor C5 gets charged to the pre-decided bias voltage. By maintaining the circuit time constant very large ($t = R5 \parallel R6 \star C5 > 0.5S$) the overall bias voltage of the circuit is maintained at a constant value through-out the signal time.

3.3 Prototype Design

At earlier stages, a virtual prototype was developed using Multisim(see Appendix A), and many of the tests were carried out on this program itself. Afterward, the model is moved to the breadboard in a modular manner and the outputs at each stage were tested independently.



As the final step of implementation, PCB for the physical prototype was designed using Altium (see Appendix B for layout). This was then screen printed and the relevant components soldered to the PCB. Finally, heatsinks were mounted accordingly to ensure safer operation.

3.4 Components

Wave Generator

The resistance and capacitance values corresponding to the filter circuit of each frequency in the oscillator are indicated below in the table. The normalized content ratio and resistance used in the input path of the scalar adder are also appended together.

f (Hz)	Oscillator		Scaling	
	R(kΩ)	C(nF)	η	R(kΩ)
281	5.67		0.1386	3.03
537	2.96		1	420
791	2.01	100	0.168	2.5
1087	1.44		0.051	8.33

Easily available 4-quad op-amp LM341 was chosen for oscillators. This allowed having a compact design in prototyping. UA751 op-amp is used in the scalar adder stage and 220Ω is used as feedback resistance to ensure the addition of all four waves sits in the supply range.

Amplifier

The following list of elements is used in the amplifier stage to allow only the frequency in the audible range to pass through and to withstand high power dissipation.

- | | | |
|----------------------|---------------|---|
| | $22\mu F$ | 1 |
| 1. Capacitors : | $100\mu F$ | 1 |
| | $100pF$ | 2 |
| | $10k\Omega$ | 5 |
| 2. Resistors : | $1k\Omega$ | 1 |
| | $5.6k\Omega$ | 2 |
| 3. Presets : | $10k\Omega$ | 1 |
| | $100k\Omega$ | 1 |
| 4. Power Resistors : | 2.2Ω | 2 |
| | 2N3904 | 1 |
| 5. Transistors : | TIP31C,TIP32C | 1 |
| | BD139,BD140 | 1 |
| 6. Op-Amp : | NE5534P | 1 |

4 Results

The evaluation of the model happened in three stages. The first part completely relied on simulation results. The second was the physical simulation of separate modules independently on the breadboard. Finally, the complete prototype was built and tested.

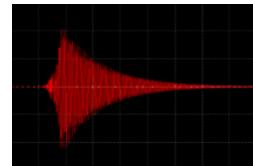
The requirements that needed to be met, and the method utilized to test whether they have been met are as follows:

Design Requirement	Target Value	Testing Method
Spectrum	Specified Amplitude Ratios	
Wave pattern	Exponential-Decay	Stimulation
Power Efficiency	75%	
Speakers	$4\Omega-16\Omega$ & 1W-5W	Prototype
Quality & Loudness	40dB-75dB	Stimulation/ Prototype
Datasheet	parameters	

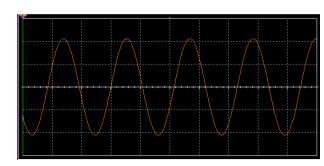
4.1 Simulation

Wave Generator

The outputs of oscillators are very stable although a slight variation in the frequencies(± 3) was observed. The following figures illustrate the observed decay pattern and stable waveform from an oscillator.

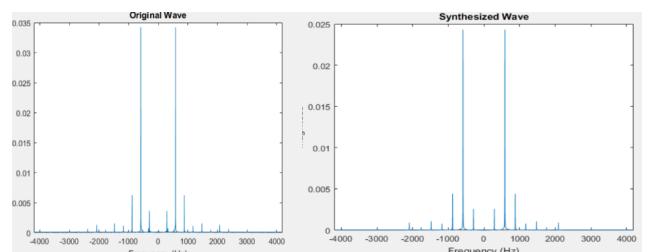


Envelope Pattern



Wave Pattern

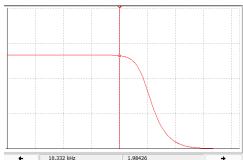
The output of the scalar adder looked similar to the original waveform and the spectrums were closely matched. Somehow at the simulation stage, sound outputs failed to match. Expected and observed wave characteristics as follows:



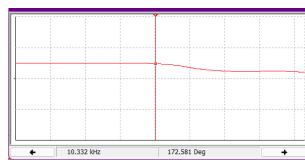
These stages are operated at low power and the oscillations are normally in a damped state. This allows keeping the overall output of the wave generator to be in a normally-off state which is crucial for power efficiency.

Amplifier

Although the wave synthesis process is limited to frequencies lower than 5kHz, it is initially planned to implement an amplifier that has a constant gain throughout the full audible range(up to 20kHz). From the observations, the model was limited to 12kHz which is expected due to imperfections in transistor behaviors.



Voltage Gain



Phase

From the simulation, it was confirmed that the feedback resistance gives linear control over the gain of the amplifier.

1. Input Resistance : 28.2kΩ

The input resistance was determined by using the multimeter tool to measure the current drawn from the source and dividing the source voltage by the measured value.

2. Output Impedance : 1.9Ω

The output impedance was calculated by using voltmeter tool and constant current source. The input was short-circuited and constant current source applied in the output. Then the voltmeter reading in the current source was measured.

$$R_{out} = \frac{V_{read}}{I_{source}}$$

3. Bandwidth : 200Hz-12kHz

Bandwidth was determined using the bode-plot of the amplifier. The region where gain stays constant is only considered.

4. Gain(8Ω) : 50dB-70dB

The gain was determined using the wattmeter

tool between the input source and speaker input.

5. Power Efficiency : 69%

$$\eta = \frac{P_L}{P_S} \times 100\%$$

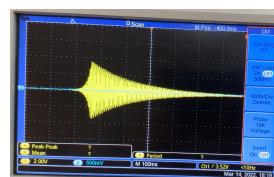
6. Safety Measurements :

The maximum current path was observed to conduct 600mA in the worst case. This was considered in the maximum power calculations and component selections.

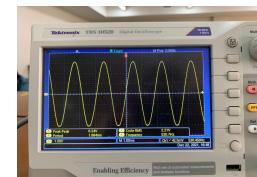
4.2 Circuit Blocks

Wave Generator

Noise-free stable wave pattern is observed at each oscillator. The measured frequencies vary in the range of 10Hz as expected due to the imperfection in resistance selection. Although the wave pattern observed had clipping effect it was observed that they could be eliminated by fine-tuning.



Envelope Pattern



Wave Pattern

Amplifier

The parameters measured were varied with simulation results.

1. Input Resistance : 43MΩ

The input impedance was determined by using a digital multimeter to measure the current being drawn from the input for an audio input of 0.1mA (peak to peak), with the output open-circuited.

2. Output Impedance : 10Ω

Output impedance was measured using the voltmeter, from the open circuit reading in the output terminal (V_O) and the reading in the 8Ω load (V_L).

$$R_{out} = R_L \times \frac{V_L}{V_O}$$

3. Bandwidth : 200Hz-12kHz

Bandwidth was determined using bode-plot of the amplifier. The region where gain stays constant was only considered.

4. Power Efficiency : 63%

Efficiency was determined by inspecting the supply and speaker inputs.

5. Maximum Current : 0.4mA

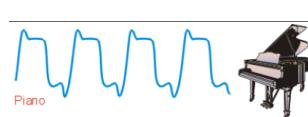
The performance of the amplifier with song output from a mobile phone is also inspected at this stage. The results are as follows.



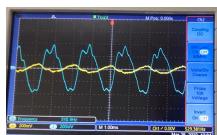
Song Wave : Input - Yellow & Output - Blue

4.3 Integrated-Circuit

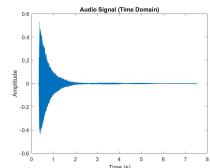
The wave generator is cascaded with the amplifier to create the final prototype of the design. The sound output of the completed circuit was observed very familiarly with the c-wave of the piano. The waveforms of the original wave and finely tuned wave output are as follows:



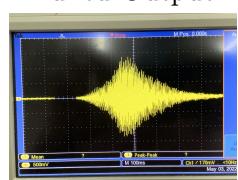
Original Wave



Tuned Output



Original Envelope



Observation

Although a small elongation was observed at

the start of oscillation this could also be controlled by parallel resistance that is responsible for the start of the oscillation. We suspected this behavior is due to an increase in impedance imposed by tracks.

5 Conclusion

We were able to complete the project within the given period. However, some of the design parameters could not be fully met.

The phases of each harmonics couldn't be able to control rather than fine-tuning the oscillator gains. The amplifier design does not meet the expected efficiency and bandwidth range. While it meets the lower cutoff requirement, the upper cutoff is lower than(12kHz) expectation(20kHz). The best-achieved envelope pattern had elongation in the beginning. The final prototype on the PCB couldn't be able to complete due to the poor quality of the tracks.

Discussion

- Although the wave generator did a fine job with synthesizing c-wave, too many tuning parameters and complexity in combining oscillators make it hard to achieve such a feasible end-product as complete piano with this strategy.
- There is a large amount of heat dissipated by the TIP transistors. Heat sinks attached to them failed to compensate for enough heat in the longer run. Thermal run-away behavior was observed which hindered circuit performance with time.
- The values obtained by the virtual simulation did not agree with the values obtained through the physical prototype. However, the specification sheet has been based on the prototype values. Therefore, the specification sheet will be an accurate representation of the performance.

References

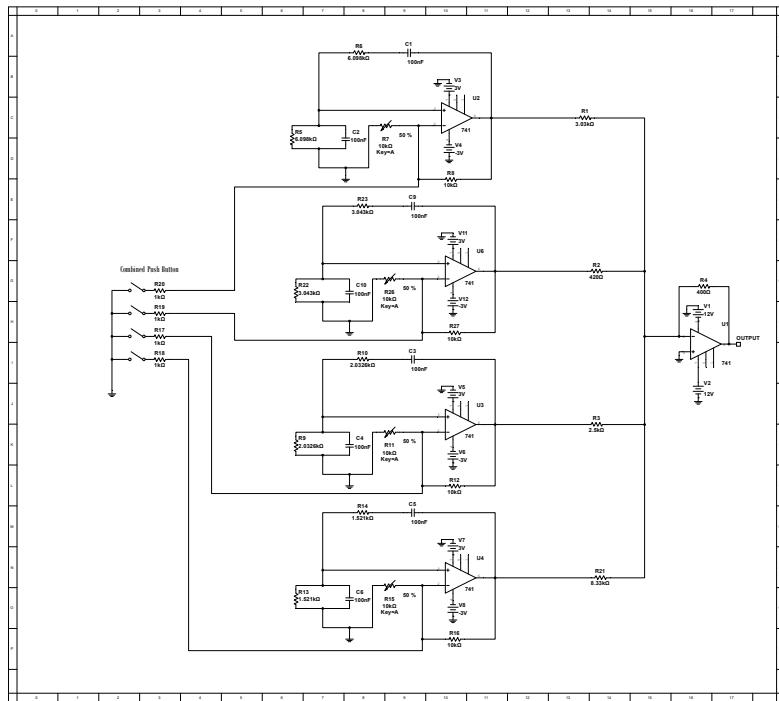
1. Synthesis of Musical Notes and Instrument Sounds with Sinusoids
2. Feasibility about synthesizing sound with analog circuitry
3. Original Sounds of Piano
4. Wave, Sound, and Music
5. Weinbridge-Oscillator
6. Alternative sine wave generators
7. Mathematics behind wave manipulation
8. How to Design and Build an Analog Synthesizer from Scratch

Contribution

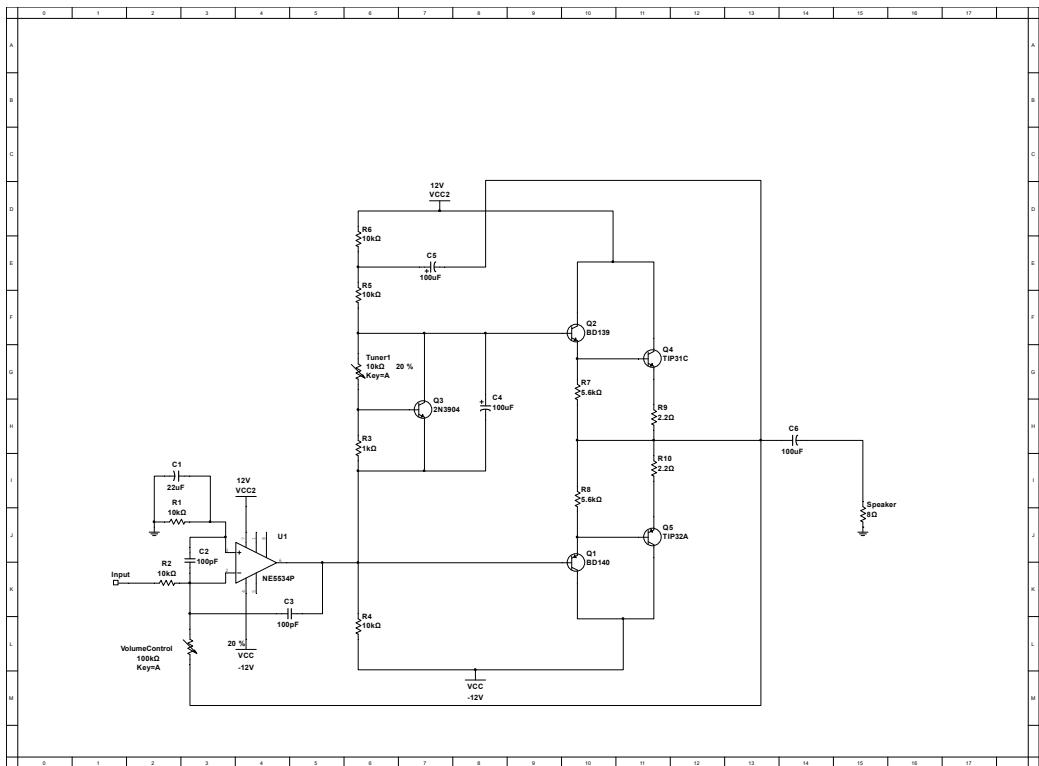
ID NO	Member	Contribution
190562G	S.Sanjith	Damper Design, Improvisation of Amplifier Design, Routing of PCBs, Data Sheet Design
190557V	K.G.C.P.Sandaruwan	Oscillator Design, Scalar Adder Design Oscillator Schematic Design
190539T	T.Sajeepan	Analyzation of Original Wave, Amplifier Design(basic), Amplifier schematic design
190543B	G.S.M.U.K.Samarakoon	Contribution to Amplifier Design

A Circuit Design

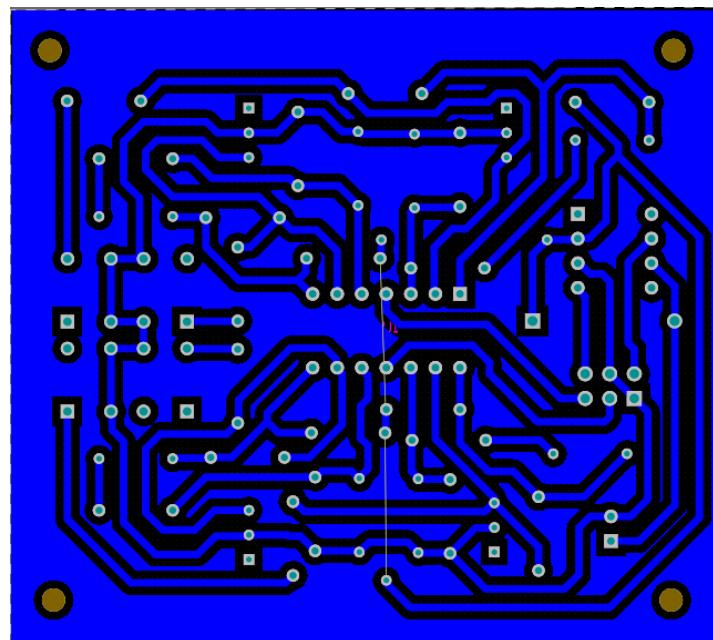
Wave Generator



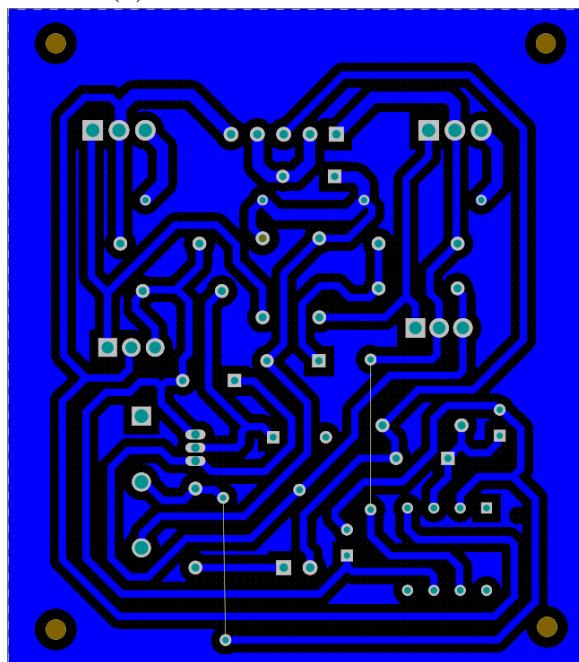
Amplifier



B Layout



(a) **PCB-I** : Wave Generator



(b) **PCB-II** : Amplifier

C Datasheet

The datasheet of the model is as follows...



The Analog Piano

1 Overview

The device is a sound synthesizer that mimics the sound of c-wave similar to that of a piano, on keypress. A speaker(8Ω preferred) ranges around 3W can be used with the pinout to observe the sound output. The volume of the speaker and the noise level can be adjusted according to user interest. The components in the device can be adjusted according to one's interest to mimic a complete piano by implementing many such modules. The amplifier alone can be used to drive small speakers from the low power signal output of simple devices such as mobile phones.



2 Description

As illustrated in the block diagram below the device consist of four oscillators which are fired by a push button. These oscillators mimic the first four harmonics which are strong enough to model the c-keynote. The triggered signals get added and scaled accordingly through a scalar adder. The output is filtered and amplified before reaching the speaker. Damping time of the wave can be controlled via the damping mechanism attached through a variable resistor with each oscillator. These can be used to mimic the functionality of the damping pedal by increasing their values.

The preset in the amplifier block is allowed to tune by the user to get a noise-free output. For longer usage, it is recommended to keep the preset at a lower value which affects the power efficiency of the circuit. It is expected to use the device not more than fifteen minutes continuously which may harm the operation of the amplifier. Heat sinks used in the amplifier can reach up to 100°C . It is not advisable to touch them during the continuous operation of the synthesizer.

The maximum current drawn by the oscillator and scalar adder is less than 5mA. Due to such a lower requirement, it is omitted in the technical specifications.

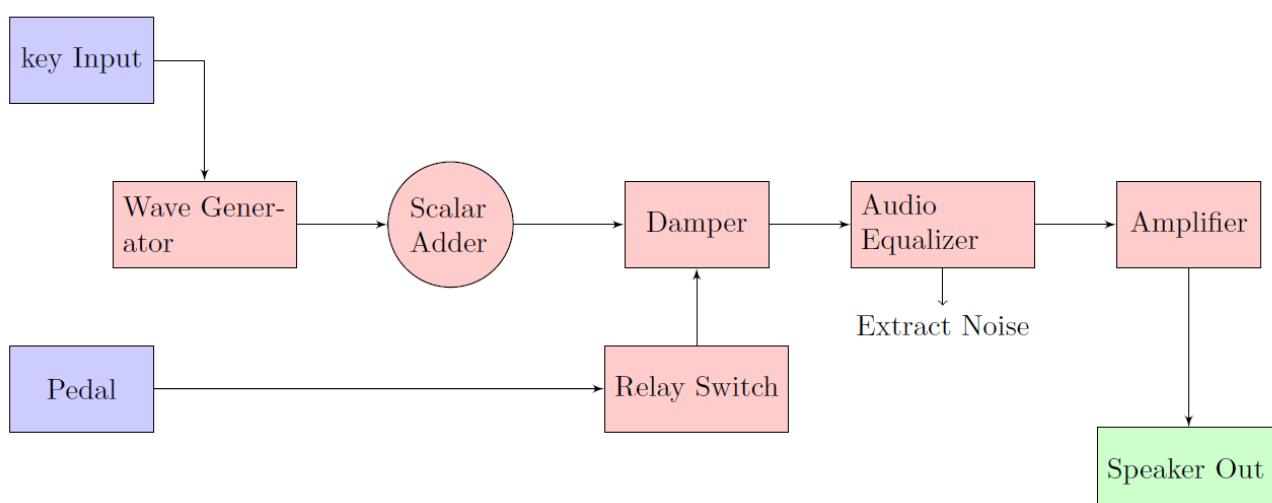


Figure 1: Circuit Block Diagram

3 Technical specification

Specifications are indicated for each module even though its pin-out of the device is narrower. This is done in the belief of allowing the users to make use of this to combine such modules in the creation of complete piano.

Oscillators

Operational Voltage(V)	Operational Frequencies(Hz)	Decaying Control Range(ms)	Output Impedance($k\Omega$)
3-6	281±3	300±100	2.49
	537±3	300±120	0.44
	790±5	300±150	2.37
	1100±5	300±200	7.43

Scalar Adder

Operational Voltage(V)	Allowed Frequency Range(Hz)	Recommended Resistance Range($k\Omega$)	Output Impedance($k\Omega$)
9-12	20-20000	0.5-50	4.53

Amplifier

	Unit	Value
Operational Voltage	V	9-12
Current Requirements	A	0.08-0.5
Input Impedance(Ac)	$M\Omega$	43±5
Output Impedance(Ac)	Ω	10 ± 5
Operational Frequency Range	Hz	200-12000
Volume Control Range	dB	20-70
Achievable Power Efficiency		63%

4 Pinout

PCB-I : Wave Generator

Pin	Signal
P1	
1	Ground
2	Power Supply +10.5±1.5
3	Power Supply -4±1
4	Ground
5	Power Supply +4±1
6	Power Supply -10.5±1.5
P2	
1	Signal Out
2	Ground

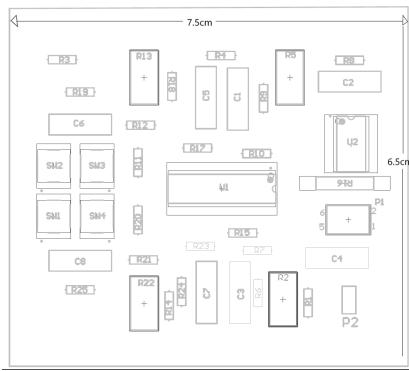
PCB-II : Amplifier

Pin	Signal
P1	
1	Signal In
2	Ground
P2	
1	Power Supply +10.5±1.5
2	Audio Out
3	Ground
4	Audio Out
5	Power Supply -10.5±1.5

5 Fine-Tuning

- Wave Generator :** The resistance values of multi-turn presets R5, R13, R22, and R2 can be adjusted to achieve different damping time constant of the output wave. These are corresponding to frequencies 1100Hz, 790Hz, 537Hz, and 281Hz respectively. Users also have the flexibility to change R8, R17, R23, and R15 in an inversely proportional manner to vary the proportional constants of those frequencies on the final wave output.
- Amplifier :** The resistance value of the preset RP can be adjusted according to the power required to achieve different audio levels in the speaker output. Keeping the resistance values around $2K\Omega$ is recommended for longer usage.

6 Measurements



PCB-I : Wave Generator

