



Individual Pitch Control

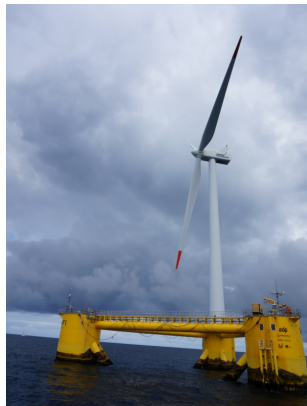
Prof. Dr.-Ing. David Schlipf

16.09.2024

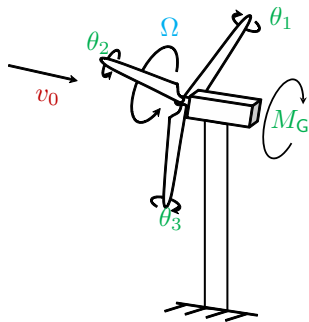
Lecture #9
Controller Design for Wind
Turbines and Wind Farms

Schedule

- 02.09. 1 Controller Design Objectives and Modeling
- 03.09. 2 Baseline Generator Torque Controller
- 04.09. 3 Collective Pitch Controller
- 05.09. 4 Filter Design
- 06.09. 7 Wind Field Generation
- 09.09. 10 Lidar-Assisted Control I
- 10.09. 11 Lidar-Assisted Control II
- 11.09. 5 Tower Damper
- 12.09. 6 Advanced Torque Controller
- 12.09. 8 Steady State Calculations
- 16.09. 9 Individual Pitch Control**
- 17.09. 12 Wind Farm Effects
- 18.09. 13 Wind Farm Control
- 19.09. 14 Floating Wind Control I
- 20.09. 15 Floating Wind Control II



Individual Pitch Control and Other Concepts



Motivation

- ▶ a wind field is more complex than only rotor-effective wind speed v_0
- ▶ the size of modern wind turbines increase more and more
- ▶ modern wind turbines have more and more sensors available

Objectives

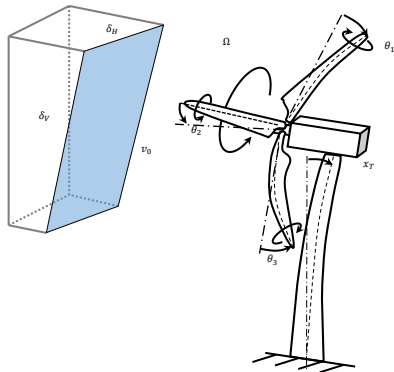
- ▶ Why could it be useful to control each blade individually and how to do it?
- ▶ What other control concepts are applied in wind energy?

Content

1. Individual Pitch Control
2. Other Concepts
3. Conclusion and Learning Objectives



Individual Pitch Control



Main Idea

- ▶ modern wind turbines (WT) have three independent pitch actuators
- ▶ reducing asymmetrical aerodynamic loads from rotor-effective shears δ_H , δ_V , which are responsible for a significant contribution to fatigue loads
- ▶ adjustment of pitch θ_1 , θ_2 , and θ_3
- ▶ reduction of rotor yaw and pitch moment by introducing two control loops:
 - ▶ horizontal (H)
 - ▶ vertical (V)
- ▶ also reduction of 1P blade bending

Coleman Transformation

$$\underbrace{\begin{bmatrix} M_V \\ M_H \end{bmatrix}}_{\text{fixed}} = \underbrace{\frac{2}{3} \begin{bmatrix} \cos(\psi_1) & \cos(\psi_2) & \cos(\psi_3) \\ \sin(\psi_1) & \sin(\psi_2) & \sin(\psi_3) \end{bmatrix}}_{T_c} \underbrace{\begin{bmatrix} M_1 \\ M_2 \\ M_3 \end{bmatrix}}_{\text{rotating}}$$

$$\text{with } \psi_2 = \psi_1 + \frac{2\pi}{3} \quad \text{and } \psi_3 = \psi_1 + \frac{4\pi}{3}$$

$$\underbrace{\begin{bmatrix} \theta_1 \\ \theta_2 \\ \theta_3 \end{bmatrix}}_{\text{rotating}} = \underbrace{\begin{bmatrix} \cos(\psi_1) & \sin(\psi_1) \\ \cos(\psi_2) & \sin(\psi_2) \\ \cos(\psi_3) & \sin(\psi_3) \end{bmatrix}}_{T_c^{-1}} \underbrace{\begin{bmatrix} \theta_V \\ \theta_H \end{bmatrix}}_{\text{fixed}}$$

Coleman Transformation

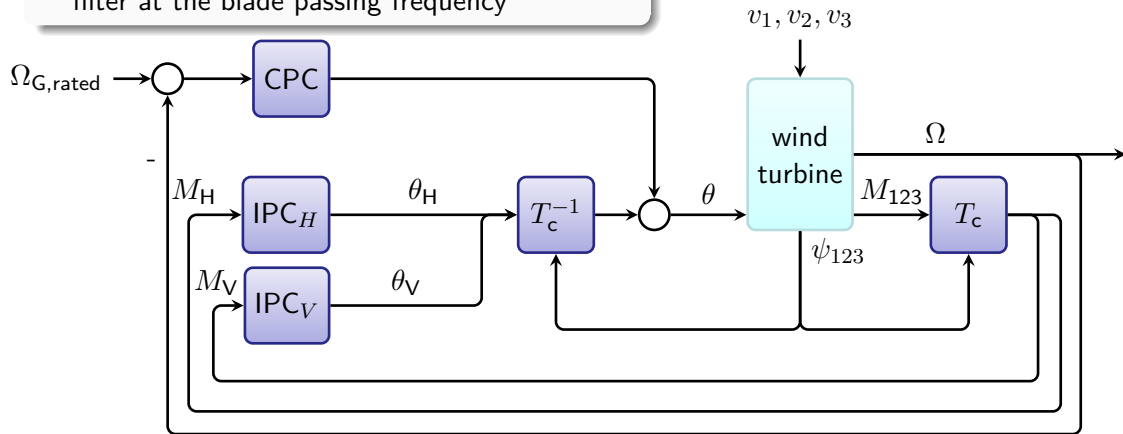
- ▶ transforms the load from the rotating axes to the non-rotating (fixed) axes
- ▶ from 3 blade root bending moments to 2 rotor moments
- ▶ rotor azimuth ψ as input
- ▶ based on Park's transformation [1] for three-phase electrical machines

Inverse Coleman Transformation

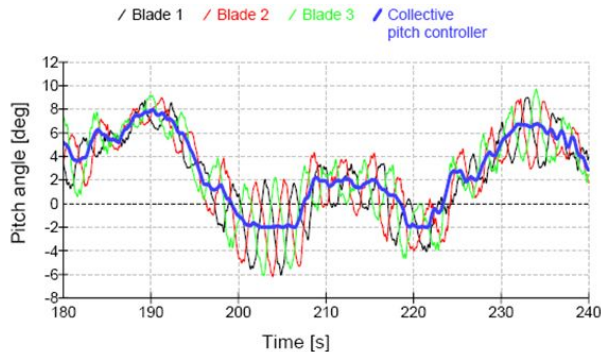
from horizontal and vertical pitch angle to 3 individual blade pitch angle

Implementation

- ▶ two independent and identical SISO controllers
- ▶ low bandwidth PI controllers with a notch filter at the blade passing frequency



Pitch Action

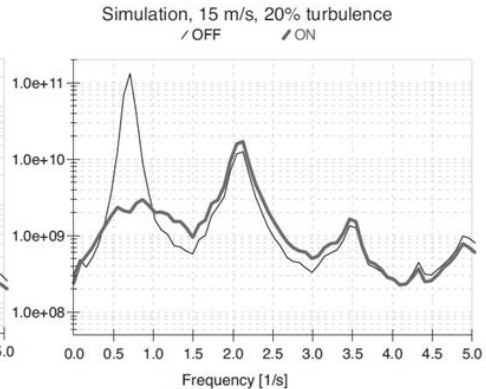
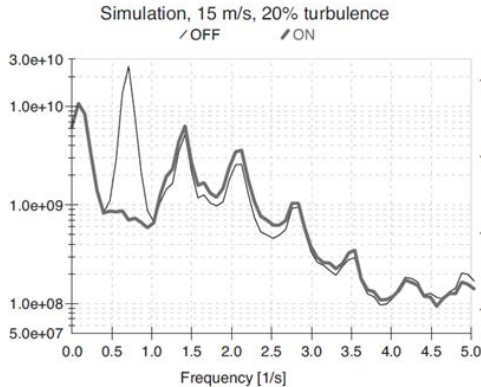


Resulting blade pitch signals

- ▶ three near-sinusoidal individual pitch demands around the collective pitch signal
- ▶ frequency: 1P
- ▶ phase-shifted by $2\pi/3$
- ▶ significantly increased pitch activity

[2].

Effect in Rotating Frame



[3]

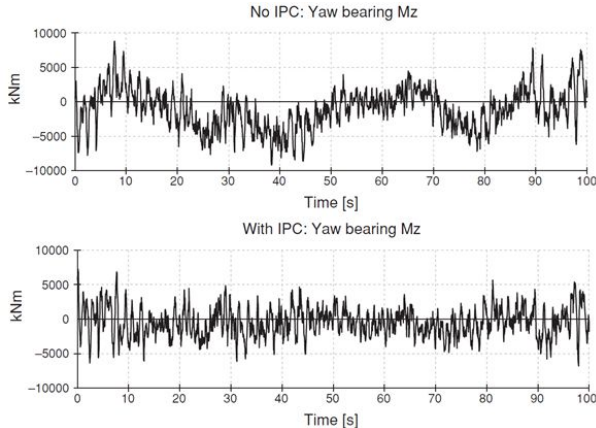
Reduction of 1P in ...

- ▶ blade root out of plane moment (left)
- ▶ rotating shaft bending moment (right)

Fatigue load reduction

- ▶ ~ 20 % for blade root out of plane moment
- ▶ 30-40 % for rotating shaft bending moment

Effect in Fixed Frame



Time series of yaw bearing moment:

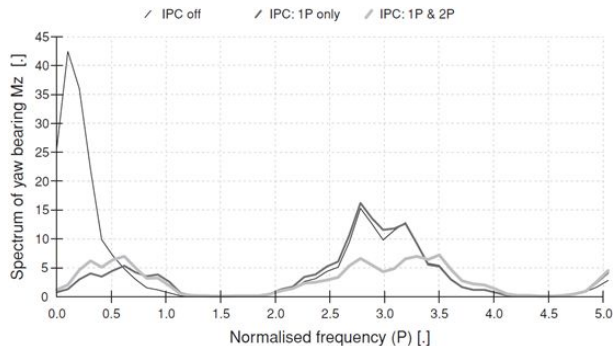
- ▶ IPC reduces the low frequency variation of the nacelle yawing moment
- ▶ this results in peak load reduction
- ▶ can be used to assist yaw control
- ▶ nacelle pitching moment is reduced in a very similar way

[3]

Second-harmonic IPC

Second-harmonic IPC

- ▶ dominant source of fatigue loading for a three-bladed WT on the non-rotating components is at 3P
- ▶ these loads can be reduced with 2P IPC
- ▶ achieved in exactly the same way as 1P IPC but sine and cosine arguments in Coleman Transformation multiplied by 2
- ▶ results in 2P pitch action

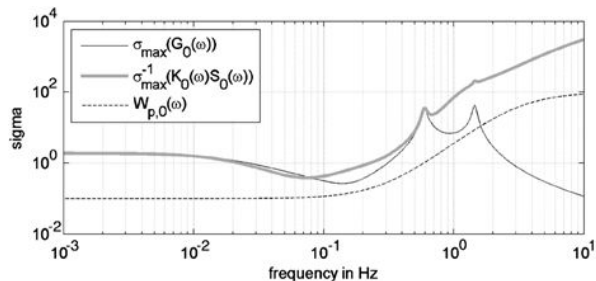


[3]

Design

Alternative Controllers

- ▶ the two H/V loops are not completely decoupled
- ▶ but they are nearly linear
- ▶ typical application for robust multivariable controllers like:
 - ▶ LQG [2]
 - ▶ H_∞ [4]
 - ▶ ℓ_1 -Optimal [5]



Plot of pitch angle weighting function $W_{p,0}$; comparison with inverted maximum singular value of control sensitivity function K_0S_0 and maximum singular value of nominal plant G_0 for designing an H_∞ controller [from 4]

[4]

Sensors

Further remarks:

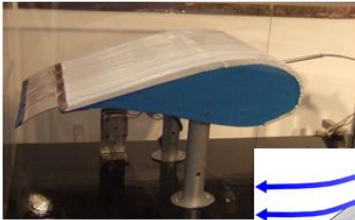
- ▶ IPC requires a reliable sensor system
 - ▶ strain gauges are not reliable over 20 years
 - ▶ strain sensors based on fibre Bragg gratings are promising
- ▶ alternative sensor positions in the nacelle are imaginable
- ▶ IPC is phased out below rated
- ▶ IPC could also be used to generate a yaw moment and support the yaw actuator



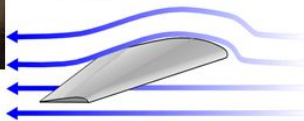
Temperature compensated fiber optic strain sensor „fos4Strain expert“ from fos4X

[fos4X]

Smart Rotors I



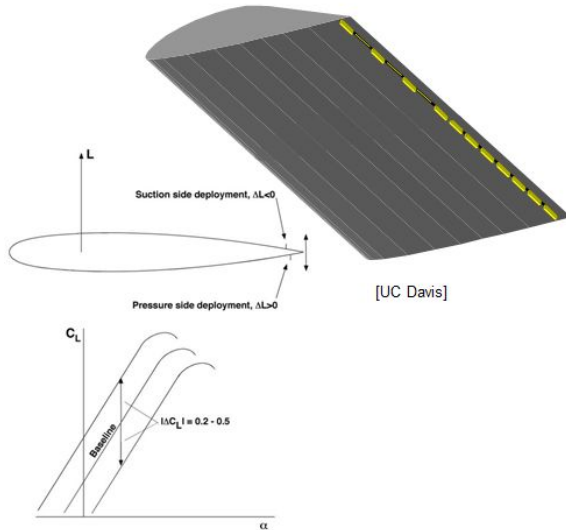
[DTU/RISOE]



Deformable Trailing Geometries:

- ▶ flaps are added to the trailing edge of the rotor blade (c.f. air planes)
- ▶ advantages: reduces extreme loads, less pitch activity, better exploitation of gusts
- ▶ disadvantages: high maintenance and service demands
- ▶ complex distributed control algorithms needed

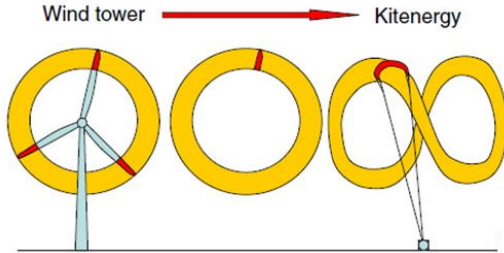
Smart Rotors II



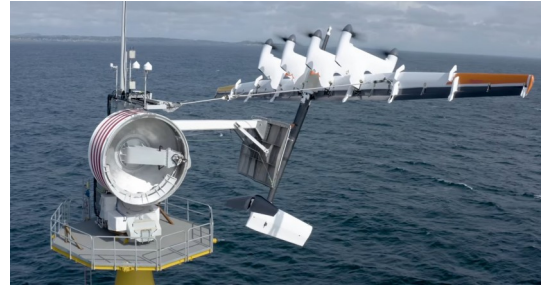
Microtabs:

- ▶ extendable Gurney-flaps are added to the trailing edge of the rotor blade (only on/off)
- ▶ advantages: reduces loads, low own consumption
- ▶ disadvantages: maintenance and service demands
- ▶ complex distributed control algorithms needed

Airborne Wind



[6],[youtube-AirborneWindEnergy]



[Makani]

- ▶ wind speed increases with height, but classical tower based WTs are limited in their height
- ▶ a flying wind energy converter gets rid of the massive structures of a classical WT
- ▶ benefits: much lighter, cheaper and more flexible systems
- ▶ types: energy generation on ground (kites) or on wings
- ▶ challenges: control, air traffic safety

Conclusion

- ▶ Why could it be useful to control each blade individually?

Asymmetric loads can be reduced!

- ▶ two independent and identical SISO controller loops
- ▶ based on direct measurement of the blade root bending moments
- ▶ Coleman Transformation to go from rotating frame to fixed frame and vice versa
- ▶ typical application for robust multivariable controllers (H_∞ , LQG controllers, ...)

- ▶ What other control concepts are applied in wind energy?

A lot of innovative concepts are developed and tested in research!

- ▶ Smart Rotors with additional actuator to influence the blade aerodynamics
- ▶ Flying Wind Energy Converters to overcome the limited structural height of WTs

Quick check on learning objectives

After this lectures you should be able to...

- ▶ describe the control loop of individual pitch control.
- ▶ describe the Coleman transformation.
- ▶ describe the effect of individual pitch control.
- ▶ describe how we can measure blade loads.
- ▶ describe how smart rotor and kites work and why they are promising technologies.

References

- [1] R. H. Park. “Two-reaction theory of synchronous machines generalized method of analysis-part I”. In: *Transactions of the American Institute of Electrical Engineers* 48 (3 1929), pp. 716–727. DOI: 10.1109/T-AIEE.1929.5055275.
- [2] E. A. Bossanyi. “Individual Blade Pitch Control for Load Reduction”. In: *Wind Energy* 6 (2 2003), pp. 119–128. DOI: 10.1002/we.76.
- [3] T. Burton, N. Jenkins, D. Sharpe, and E. Bossanyi. *Wind Energy Handbook*. New York, USA: John Wiley & Sons, 2011.
- [4] M. Geyler and P. Caselitz. “Robust Multivariable Pitch Control Design for Load Reduction on Large Wind Turbines”. In: *ASME Journal of Solar Energy Engineering* 130 (2008). DOI: 10.1115/1.2931510.
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- [6] L. Fagiano, M. Milanese, and D. Piga. “Optimization of airborne wind energy generators”. In: *International Journal of Robust and Nonlinear Control* 22 (18 2012), pp. 2055–2083. DOI: 10.1002/rnc.1808.

Please let me know if you have further questions!

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