

Liquid scintillator tiles

Alberto Belloni^{a,*}, Mahnegar Amouzegar^a, Burak Bilki^f, Jeff Calderon^a, Pawel De Barbaro^g, Sarah C. Eno^a, Kenichi Hatakeyama^e, James Hirschauer^d, Geng-Yuan Jeng^a, Joseph Pastika^e, Kevin Pedro^d, Joshua Samuel^a, Elmer Sharp^c, Young Ho Shin^a, Emrah Tiras^e, Dmitry Vishnevskiy^g, Zishuo Yang^a, Yao Yao^a, Sung Woo Youn^b

^a*Dept. Physics, U. Maryland, College Park MD 30742 USA*

^b*Institute for Basic Science, Center for Axion and Precision Physics Research, IBS Center for Axion and Precision Physics Research Room 4315, Department of Physics, Natural Science Building (E6-2), KAIST, 291 Daehak-ro, Yuseong-gu, Daejeon 305-701, South Korea*

^c*Elmer Sharp Engineering, 7007 Leesville Blvd. Springfield, VA 22151*

^d*Fermi National Accelerator Laboratory, Batavia, IL, USA*

^e*Baylor University, Waco, Texas, USA*

^f*The University of Iowa, Iowa City, IA, USA*

^g*The University of Rochester, Rochester, NY, USA*

Abstract

Future experiments in high energy and nuclear physics may require large, inexpensive calorimeters that can continue to operate after receiving doses of 50 Mrad or more. The light output of liquid scintillators suffers little degradation under irradiation. However, many challenges exist before liquids can be used in sampling calorimetry, especially regarding developing a packaging that has sufficient efficiency and uniformity of light collection, as well as suitable mechanical properties. We present the results of a study of a scintillator tile based on EJ-309 liquid scintillator using cosmic rays and test beam on the light collection efficiency and uniformity. and some preliminary results on radiation hardness.

Keywords: organic scintillator, liquid scintillator, radiation hardness, calorimetry

*Corresponding author

Email address: abelloni@umd.edu (Alberto Belloni)

1. Introduction

Sampling calorimeters using plastic scintillator tiles with wavelength-shifting (WLS) fibers as their active element, such as the CDF plug calorimeter [1] and the CMS Barrel [2] and Endcap [3] hadron calorimeters, are popular due to their low cost and ease of construction. Plastic scintillator is available commercially from companies such as St. Gobain and Eljen Technology. When irradiated, however, the performance of plastic scintillator and WLS fibers deteriorates; light self-absorption (yellowing) increases and light output decreases. The resulting loss of light output has been studied using irradiations from electron linacs and ^{60}Co sources [4, 5]. Generally, the light output decreases exponentially with dose, with an decay constant on the order of ten Mrad. Future high energy and nuclear experiments, however, may have to operate in environments that will deliver doses of many tens of Mrad. Previous studies of liquid scintillator have shown little decrease of light output with dose [6, 7, 8]. However, there are challenges regarding the design of a package with sufficient light output and uniformity, as well as adequate mechanical properties. In this paper, we present the design and optimization of a liquid scintillator tile for uniformity of light output and discuss some remaining challenges regarding other mechanical properties that remain. An earlier liquid tile design by another group is described in [9].

2. Tile design

Our tile is based on EJ-309 scintillator, from Eljen Technology, which uses naphthalene as the substrate with wavelength shifting additives. EJ-309 has a light output that is 75% of anthracene, a wavelength of maximum emission of 424 nm, a volumetric thermal expansion coefficient of 0.1%/C, a refractive index of 1.57, and a flash point of 144° C. It is classified as a Class IIIB combustible liquid. The high flash point is important for its suitability for a collider environment.

The design of a tile to hold the liquid needs to consider light collection efficiency, light collection uniformity, and cost. The container should not leak, and there should not be interactions between the container and its contents that degrade the light output over time or compromise the integrity of the container. Figure 1 shows the mechanical construction of our prototype. The case is made of aluminum. Two transparent quartz support tubes run through the liquid and can hold either a WLS fiber or liquid wavelength shifter. When a WLS fiber was used, the end of the fiber not connected to the photodetector was coated with Al to increase the light output unless otherwise noted. The support tube is sealed to the case with a Viton fluoroelastomer o-ring¹. The thicknesses of the top and bottom Aluminum plates are 0.5 mm. The total internal volume is 88 mm x 88 mm x 4 mm. The inner surface of the container is a lapped and polished Al-6016-T6 (as suggested by Eljen), available from McMaster Carr. The material comes with a plastic coating that can be used to maintain its mirror quality during the machining process and then is removed before the welding step. The liquid was transferred into the container in an inert atmosphere, as contamination with Oxygen decreases the light output.

Several variations on this design were constructed. For the default design, the thickness of the liquid is 4 mm. A version with a 6 mm thickness was also made. The default support tubes (“quartz1”), from Atlantic International, were quartz with an inner diameter of 1.3 mm and were used with Kuraray Y-11 fiber (doping of 200 ppm), double-clad. The index of refraction was measured at the Quattrone Nanofabrication Facility at the University of Pennsylvania to be 1.600. As an alternative, two types of Quartz tubes filled with liquid wavelength shifter (capillaries) were also used. One set (“quartz2”), of ordinary quartz, had an outer diameter of 2 mm, an inner diameter of 1 mm, and a measured index of refraction of 1.548. Another (“quartz3”) used special radiation-resistant quartz and had an outer diameter of 1 mm and an inner diameter of 0.4 mm. Its index was not measured. These dimension are not optimal in any sense for this

¹EJ-309 interactions with common o-ring materials such as neoprene or buna-N

design, but funding was not available to allow the construction of a more suitable liquid capillary with radiation hard quartz. The liquid wavelength shifter was a prototype material from Eljen, and is not yet a commercial item. The liquid wavelength shifter has an emission maximum from between 481 and 492 nm and a decay time between 2 and 8 ns. The solvent was the same as that used for EJ-309.

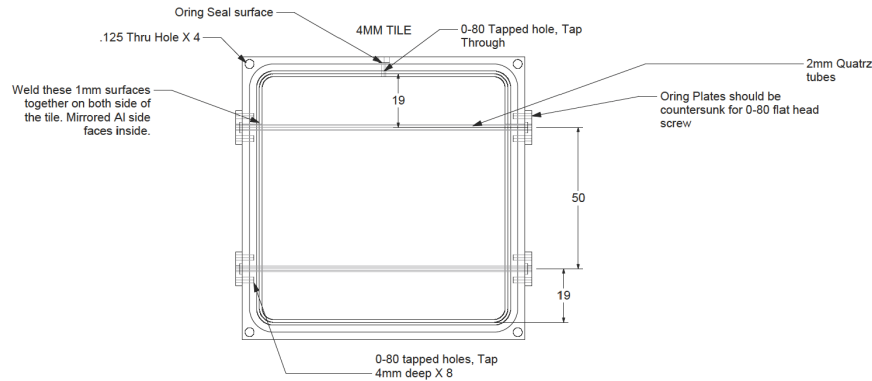


Figure 1: Mechanical design of a liquid scintillator tile. Units are [mm].

In what follows, the results shown are for the mirrored tile with 4 mm thick-
65 ness, the quartz1 support tubes, and a 0.9 mm diameter Y-11 WLS fiber, unless
otherwise stated.

3. Light yield and uniformity as measured in test beam

The light yield and uniformity of the tiles was measured in the H2 test beam facility at CERN using 120 GeV muons. The trigger required coincidence of two out of four plastic scintillator hodoscopes. The effective beam cross sectional area, after trigger requirements, was $14 \times 14 \text{ cm}^2$. The positions of the muons were measured with four wire chambers. The position obtained from the counter closest to the prototype was used. We also required the signal in each wire chamber be consistent with that of a single muon, and that the difference

75 in positions in sequential chambers be consistent within uncertainties. As many groups were using the same test beam, there was material upstream of our counters. For some runs, several steel blocks were used to support experiments upstream of our counters. Because the muons were high energy, the probability of a muon-induced shower was non-negligible. (This was verified later at a test
80 beam at FNAL that had a cleaner beam line, by varying the material in front of the tile and through simulations with varying amounts of material.) We present here the results from the runs and tiles with the smallest upstream material.

The WLS fiber was connected to a clear fiber using a connector designed at FNAL. The clear fiber was lead away from the beam line. The light output
85 was measured using a Hamamatsu R7600U-200-M4 photomultiplier tube and a custom ASIC that integrates and digitizes the resulting charge, called the “QIE” [10]. The photomultiplier has a peak quantum efficiency of 40% at a wavelength of 400 nm and produces a clear single photo-electron (pe) peak. The integrated charge is digitized every 25 ns. Ten digitizations were recorded
90 per muon trigger. The sum of the signal in four consecutive time samples was used.

The average number of pe’s produced per minimum ionizing particle (mip) was estimated by doing a Gaussian fit to the peak centered on the pedestal. The mean number of pe’s was calculated using the fraction of events in this
95 peak, assuming a Poisson distribution. The nominal tile produced 1.7 pe’s per mip. A plastic tile (SCSN-81 with Y-11 fiber) with dimensions 10 cm x 10 cm x 3.7 mm tested at the same time gave 1.8 pe/MIP. The results have a systematic uncertainty related to the handling of the events with showering muons. We evaluate this uncertainty by looking at the results after truncating the distri-
100 bution at around 25 pe’s (2000 adc counts). The results were stable to within 5%. In addition, runs taken with varying amounts of material in front of our detector (up to 20 cm of steel) resulted in a 15% variation in light yield. We therefore take a 16% uncertainty due to upstream material.

The uniformity of the light collection was also studied at the CERN test
105 beam. Figure 2 shows the fraction of events with at least 1 pe versus the impact

position of the mip along the axis parallel to the support tubes (left) and perpendicular to the support tubes (right). As expected, there is little dependence on the coordinate parallel to the support tubes. The light yield does depend on the perpendicular distance. The light collection efficiency is maximum for muons near the WLS fiber and is approximately 20% lower for muons in the center or edges of the tile. For most hadron calorimetry applications, we verified through simulation that this degree of non-uniformity would not adversely affect jet resolutions.

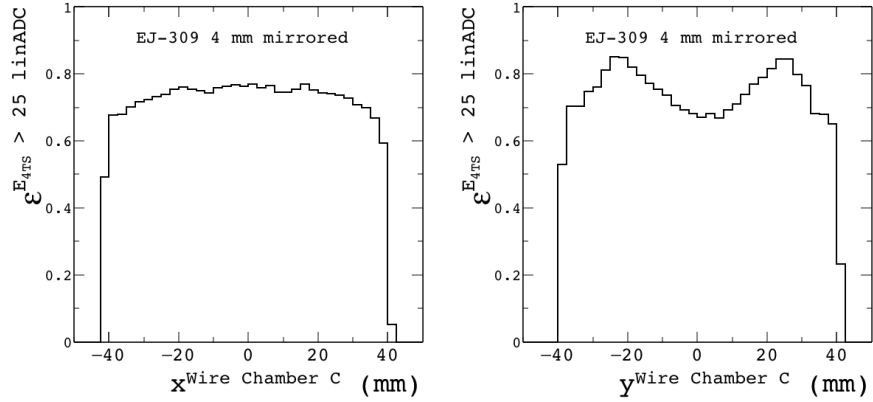


Figure 2: For the nominal liquid tile, fraction of mips with at least one pe as a function of the impact position of the mip along the axis parallel to the support tubes (left) and perpendicular to the support tubes (right).

4. Light yield dependence on tile parameters

The dependence of the light yield on variations in the design parameters was studied using cosmic ray data taken at the University of Maryland. Scintillator-based counters above and below the tile were used for triggers. The tile light output was measured using a Hamamatsu R7600U-200-M4 photomultiplier tube. Fibers were connected to the tube using optical glue. Data was collected with a Tektronix MSO 5204 oscilloscope. No attempt was made to select minimum ionizing muons. The muons thus are low energy and will produce more light

than those studied at the CERN test beam.

We found an average of 2.88 ± 0.05 pe for the nominal tile. A similar tile but without the mirroring yielded 1.98 ± 0.03 pe, a reduction of a factor of 1.45.

125 A tile with a 6 mm thickness of liquid, non-mirrored, yielded 2.61 ± 0.05 pe, an increase over the 4 mm non-mirrored tile of a factor of 1.32. Figure 3 shows the collected charge (arbitrary units) for the three different configurations.

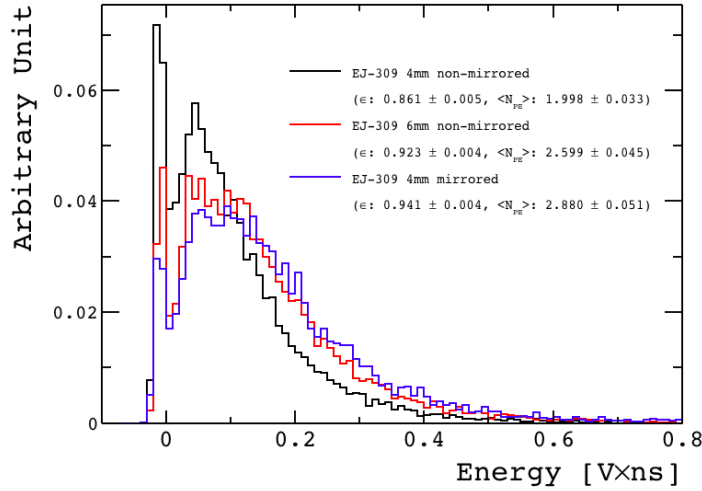


Figure 3: Comparison between the light output (arbitrary unit) of liquid scintillator tiles with different thickness and different treatment of the aluminum surface in contact with the liquid scintillator. The light is readout with the same 0.9 mm (O.D.) Y11 plastic WLS fiber. The three distributions are normalized to the same area of 1.

The light yield was also studied using a capillary, filled with liquid WLS, instead of a quartz tube containing plastic WLS, since plastic WLS is susceptible
130 to radiation damage (the “quartz2” configuration). The capture efficiency of the WLS for the two different configurations depends crucially on the index of the surrounding media. For the WLS fiber, there is an air gap with an index of 1. For the capillary, the liquid WLS is instead bordered by quartz, with an index of 1.6. The plastic and liquid WLS have very similar indices of refraction. In
135 both cases, the shifted light propagates in the WLS, but the capture efficiency is

higher for the lower index air. Figure 4 shows the charge collected (in arbitrary units) from cosmic muons for the two different configurations. The fraction of events in the pedestal, which is the Gaussian-shaped peak at low charge, can be used to calculate the fraction of muons producing at least one pe (light collection efficiency) and the mean number of pe's per muon. The light collection efficiency is 92% for the plastic WLS and 45% for the liquid. The light yield for the liquid is half that of the plastic. The light collection efficiency with the liquid could be improved if lower index quartz could be found.

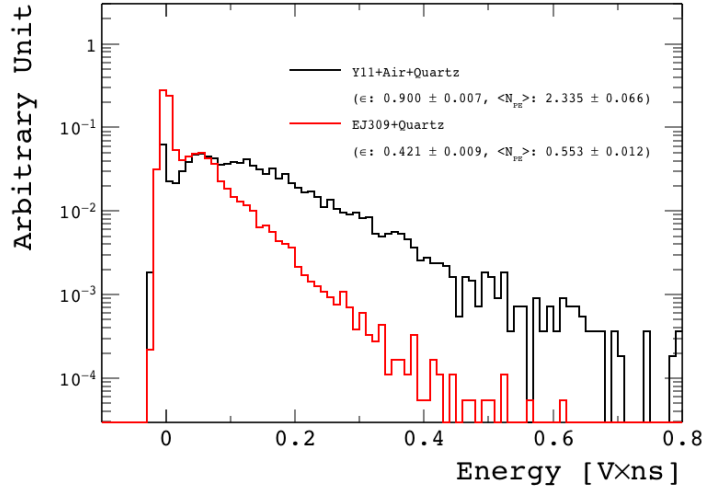


Figure 4: Comparison between the light output of a liquid scintillator tile equipped with a plastic WLS fiber, and a capillary filled with liquid WLS. The two distributions are normalized to have the same area of 1.

Finally, we tested the performance of the same tile, 4 mm-thick, with a mirrored aluminum surface, and the quartz2 configuration, as a function of the thickness of the readout plastic WLS fiber. We tested three plastic fibers, with a thickness of 0.5 mm, 0.9 mm, and 1 mm. The higher the fiber thickness, the higher the efficiency and light output, as shown in Figure 5.

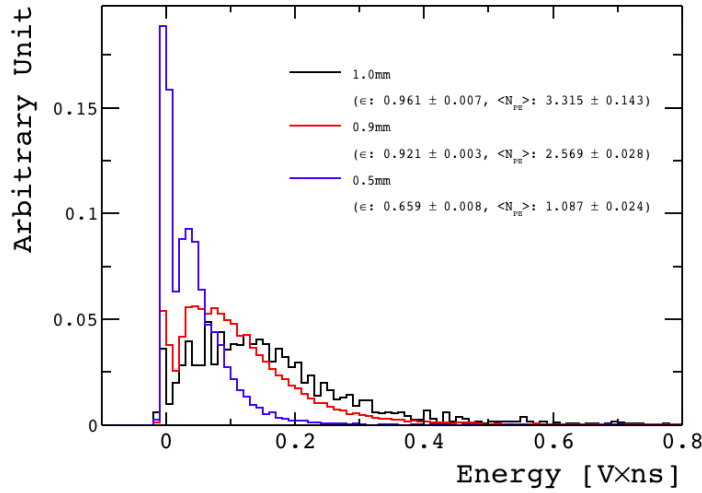


Figure 5: Comparison between the light output of liquid scintillator tiles readout with plastic WLS fibers with different thickness. The three distributions are normalized to have the same area of 1.

5. Radiation hardness tests

150 Several different tests were made using irradiations with a ^{60}Co source at the University of Maryland.

A dark-glass vial containing 125 ml of liquid scintillator was irradiated with γ -rays to a dose of 50 Mrad, at a dose rate of 1 Mrad/hr. Figure 6 compares the integrated charge (arbitrary units) from the same tile when filled with unirradiated liquid and irradiated liquid. The efficiency and light output from the two measurements are consistent within the uncertainty, indicating that light
155 output of the EJ-309 is radiation-tolerant to γ -ray irradiations.

We also irradiated a tile with the “quartz3” readout configuration at an irradiation facility at Goddard Space Flight Center, to a dose of 30 Mrad at a dose rate of 3 krad/minute. Some bulging of the container indicated that
160 outgassing of the EJ-309 may pose challenges for containers. We intend to report measurements of the outgassing in a future paper.

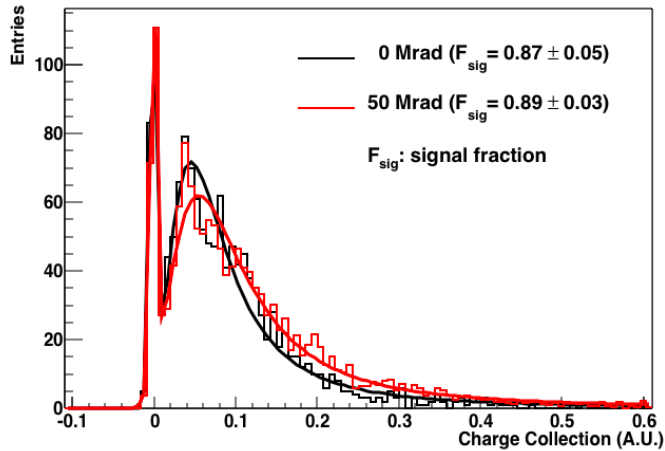


Figure 6: Comparison between the light output of a liquid scintillator tile filled with unirradiated (black) and irradiated (red) liquid scintillator. The two distributions are normalized to have the same number of events in the pedestal.

6. Comparison with simulation, and optimization

We use the GEANT4 [11] package to simulate the optics of our tile. GEANT4's
 165 optical package includes simulations of refraction, reflection, wave length shift-
 ing, and light attenuation. A variety of options for the reflection are available.
 We used the “Specular Spike” option for the Al and an absorption length of
 2 m for the EJ-309. When simulating the WLS fiber, an air gap was included
 between the fiber cladding and the support tube, while no such gap exists for
 170 the simulation of the capillary. An index of refraction of 1.57 is used for the
 EJ-309. The index for sapphire used was 1.77. For quartz, values between 1.46
 and 1.55 were used. Photons are generated at random positions inside the liquid
 volume, with a spectrum corresponding to the emission spectrum of EJ-309.

As shown in Figure 7 left, we find the simulation reproduces the light col-
 175 lection non-uniformity when a reflectivity of 0.9 is used for the mirrored Al.

We find that the light collection efficiency is a strong function of the reflec-
 tivity of the Al (Figure 7 right).

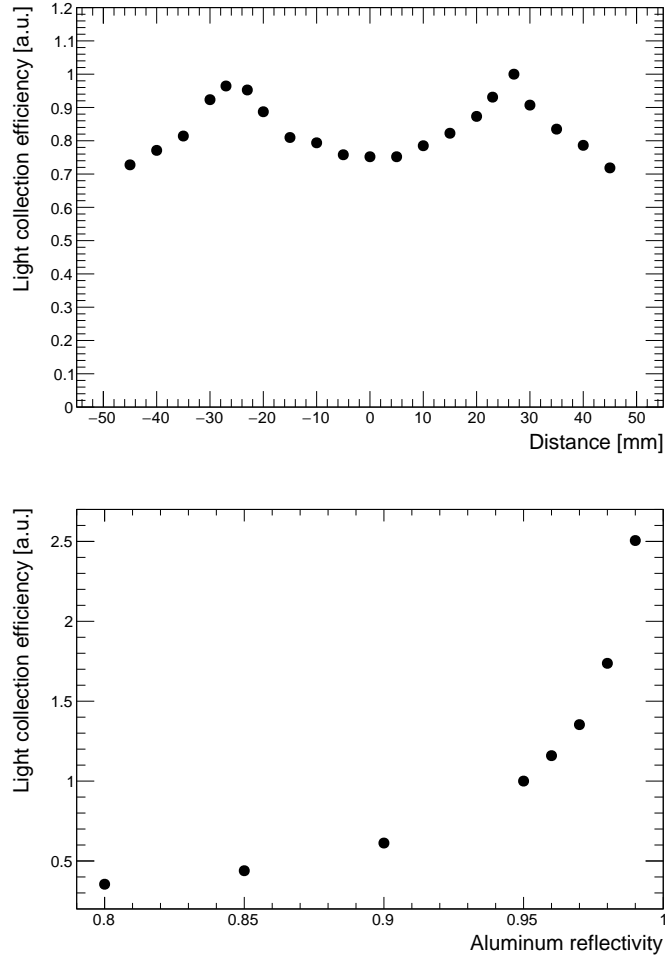


Figure 7: (left) Ratio of light yield to maximum light yield from simulated tile as a function of the distance perpendicular to the support tubes, normalized to the efficiency at the position of the support tubes. (right) Light collection efficiency vs Aluminum reflectivity, normalized to a reflectivity of 0.95.

We find the best light collection comes when the support tube has the lowest possible index of refraction for liquid WLS. The opposite is true for a fiber with an air gap (and plastic WLS). For a 1 mm diameter for the WLS, the light collection efficiency increases by a factor of 3.57 going from an index of 1.55 to

1.46 for liquids. Presumably this difference would decrease as the reflectivity of the Al increases. For a fiber with an air gap, the efficiency decreases by a factor of 1.42 going from an index of 1.77 to 1.46.

185 7. Conclusions

We presented results for a liquid scintillating tile using WLS fiber readout. For our nominal design, 1.7 ± 0.2 pe's were produced for minimum ionizing particles with a 20% nonuniformity. While the light collection efficiency was adequate for calorimetry, and while the light output of EJ-309 showed little signs
190 of degradation, outgassing needs to be measured and the results considered for future tile designs.

8. Acknowledgments

The authors would like to thank Randy Ruchti of Notre Dame for providing the capillaries and both Randy and Chuck Hurlbut of Eljen Technologies for
195 advice in general on liquids and Yasar Onel's group at the University of Iowa for help with the test beam, and Victor Guarino of Argonne National Laboratory for help with preliminary mechanical designs. We would like to thank Eric Johnston from the Quattrone Nanofabrication Facility at the University of Pennsylvania for measuring the indices of refraction of our support tubes. The
200 authors would like to thank the University of Maryland's Nuclear Reactor and Radiation Facilities group for assistance with the irradiations. We would like to thank the University of Maryland FabLab for help with fiber sputtering. We would also like to thank the staff at the irradiation facility at Goddard Space Flight center. This work was supported in part by U.S. Department of Energy
205 Grant DESC0010072.

References

- [1] S. Aota *et al.*, A scintillating tile/fiber system for the cdf plug upgrade em calorimeter, Nuclear Instruments and Methods in

- Physics Research Section A: Accelerators, Spectrometers, Detectors and Associated Equipment 352 (3) (1995) 557 – 568.
 210 [http://dx.doi.org/http://dx.doi.org/10.1016/0168-9002\(95\)90005-5](http://dx.doi.org/http://dx.doi.org/10.1016/0168-9002(95)90005-5)
[doi:http://dx.doi.org/10.1016/0168-9002\(95\)90005-5](http://dx.doi.org/http://dx.doi.org/10.1016/0168-9002(95)90005-5).
- [2] S. Abdullin *et al.*, Design, performance, and calibration of cms hadron-barrel calorimeter wedges, The European Physical Journal C 55 (1) (2008)
 215 159–171. doi:10.1140/epjc/s10052-008-0573-y.
- [3] The CMS hadron calorimeter project: Technical Design Report, Technical Design Report CMS, CERN, Geneva, 1997.
- [4] V. Hagopian, I. Daly, Radiation damage of fibers, AIP Conference Proceedings 450 (1) (1998) 53–61. doi:http://dx.doi.org/10.1063/1.56958.
- 220 [5] A. Byon-Wagner, Radiation hardness test programs for the {SDC} calorimeter, Radiation Physics and Chemistry 41 (12) (1993) 263 – 271. [http://dx.doi.org/http://dx.doi.org/10.1016/0969-806X\(93\)90064-2](http://dx.doi.org/http://dx.doi.org/10.1016/0969-806X(93)90064-2)
[doi:http://dx.doi.org/10.1016/0969-806X\(93\)90064-2](http://dx.doi.org/http://dx.doi.org/10.1016/0969-806X(93)90064-2).
- 225 [6] C. Zorn, S. Majewski, R. Wojcik, C. Hurlbut, W. Moser, Preliminary study of radiation damage in liquid scintillators, Nuclear Science, IEEE Transactions on 37 (2) (1990) 487–491. doi:10.1109/23.106666.
- [7] J. Klein, J. Gresset, F. Heisel, G. Laustriat, Effets des rayonnements-sur les caracteristiques des scintillateurs organiques, The International Journal of Applied Radiation and Isotopes 18 (6) (1967) 399 –
 230 406. [http://dx.doi.org/http://dx.doi.org/10.1016/0020-708X\(67\)90143-3](http://dx.doi.org/http://dx.doi.org/10.1016/0020-708X(67)90143-3)
[doi:http://dx.doi.org/10.1016/0020-708X\(67\)90143-3](http://dx.doi.org/http://dx.doi.org/10.1016/0020-708X(67)90143-3).
- [8] I. Berlman, The effect of massive Co⁶⁰ doses on the light output of a scintillator solution, Radiological Physics Division Semiannula Report for July through December 1957.
- 235 [9] J. Marchant, B. Baumbaugh, L. Ciastko, B. Dolezal, A. Heering, C. Hurlbut, M. McKenna, T. Pearson, R. Ruchti, A. Williams, Liquid-based scin-

tillators for particle physics, in: Nuclear Science Symposium Conference Record (NSS/MIC), 2010 IEEE, 2010, pp. 10–13. doi:10.1109/NSSMIC.2010.5873708.

- 240 [10] T. Shaw, A. Baumbaugh, A. Boubekur, J. Elias, J. Hoff, S. Holm, S. Los, C. Rivetta, A. Ronzhin, J. Whitmore, T. Zimmerman, R. Yarema, Front end readout electronics for the cms hadron calorimeter, in: Nuclear Science Symposium Conference Record, 2002 IEEE, Vol. 1, 2002, pp. 194–197 vol.1. doi:10.1109/NSSMIC.2002.1239297.
- 245 [11] S. Agostinelli, et al., Geant4a simulation toolkit, Nuclear Instruments and Methods in Physics Research Section A: Accelerators, Spectrometers, Detectors and Associated Equipment 506 (3) (2003) 250 – 303. [http://dx.doi.org/http://dx.doi.org/10.1016/S0168-9002\(03\)01368-8](http://dx.doi.org/http://dx.doi.org/10.1016/S0168-9002(03)01368-8) doi: [http://dx.doi.org/10.1016/S0168-9002\(03\)01368-8](http://dx.doi.org/10.1016/S0168-9002(03)01368-8).