

$$\frac{l}{d} = 20 \times M.F$$

Assume % tensile reinforcement = 0.85%

∴ From fig 4 of IS 456:2000
M.F = 1.4

$$\frac{l}{d} = 20 \times 1.4$$

$$\frac{4000}{d} = 20 \times 1.4$$

$$\therefore d = \underline{\underline{142.85}}$$

Assume a clear cover of 20 mm ϕ of
bar 10 mm

$$D = d + C + \frac{10}{2}$$

$$= 142.85 + 20 + 5$$

$$= \underline{\underline{167.85 \text{ mm}}} \approx \underline{\underline{170 \text{ mm}}}$$

$$\therefore d = \underline{\underline{145}}$$

Assume $b = 1 \text{ m}$

Eff. span of slab = $l + b$

$$\text{Eff. span in one dir}^n = 4000 + 145$$

$$= \underline{\underline{4145 \text{ mm}}}$$

$$\text{Eff. span in other dir}^n = 5000 + 145$$

$$= \underline{\underline{5145 \text{ mm}}}$$

Step 3 Computatn of loads & B.M.

∴ Hence safe

$$\text{Development length} = \frac{\phi \sigma_c}{4 \tau_{bd}} = \frac{10 \times 0.87 \times 415}{4 \times 1.2} \\ = 752.187 \text{ mm}$$

Q. Design RCC Roofing slab over a room $4\text{m} \times 5\text{m}$.
The slab is simply supported on all four edges with corners held-down. The super imposed load is 2 kN/m^2 & floor finish is 0.5 kN/m^2 .
Use M15 concrete & Fe 415 steel.

Q. Given

$$L = 5\text{ m}$$

$$l = 4\text{ m}$$

$$f_{ck} = 15\text{ N/mm}^2$$

$$f_y = 415\text{ N/mm}^2$$

$$LL = 2\text{ kN/m}^2$$

nt - 1 and
area

Step 1 Check for one way or 2 way slab

$$\frac{L}{l} = \frac{5}{4} = 1.25 < 2$$

∴ It is a 2-way slab

Q.2 Computation of slab dimension

$$q_L = 2 \text{ KN/m}$$

$$q_L = 0.17 \times 1 \times 25$$

$$= 4.25 \text{ KN/m}$$

$$q_L = 0.5 \text{ KN/m}^2$$

$$= 0.5 \text{ KN/m}$$

$$\text{Total load} = 6.75 \text{ KN/m}$$

$$\frac{l_y}{l_x} = \frac{5.145}{4.145} = 1.241$$

From table 26, for all edges discontinuous

$$\alpha_x = \frac{0.072 + 0.079}{2}$$

$$= 0.0755$$

$$\alpha_y = 0.056$$

$$M_x = \alpha_x W l_x^2$$

$$= 0.0755 \times 6.75 \times 4.145^2$$

$$= 8.7558 \text{ KNm}$$

$$M_{ax} = 8.7558 \times 1.5 = 13.134 \text{ KNm}$$

$$M_y = \alpha_y W l_y^2$$

$$= 0.056 \times 6.75 \times 5.145^2$$

$$= 6.4944 \text{ KNm}$$

$$M_{ay} = 6.4944 \times 1.5$$

$$= 9.741 \text{ KNm}$$

$$\text{depth required} = 0.36 \times \frac{M_{max}}{f} \left(\frac{1 + \frac{M_{max}}{M_y}}{2} \right) \frac{W}{b}$$

$$13.134 \times 10^5 = 0.36 \times 0.48 \left(1 - 0.42 \times 0.48\right) \times 1000 \times d^2 \times 15$$

$$d_{\text{req}} = 79.6 \text{ mm (min)}$$

$d_{\text{req}} < d_{\text{provided}}$, hence safe.



Step 4: Computation of reinforcement

$$M_u = 0.87 f_y A_{st} d \left(1 - \frac{A_{st} f_y}{b d f_{ck}}\right)$$

$$13.134 \times 10^5 = 0.87 \times 415 \times A_{st} \times 145 \left(1 - \frac{A_{st} \times 415}{1000 \times 145 \times 15}\right)$$

$$250.877 = A_{st} - 1.909 A_{st}^2$$

$$1.909 A_{st}^2 - A_{st} + 250.877 = 0$$

$$A_{st} = 264.124$$

$$\text{Spacing} = \frac{1000 \times \text{Area of one bar}}{A_{st}}$$

$$= \frac{1000 \times \frac{\pi}{4} \times 10^2}{264.124} = 297 \approx 290 \text{ mm}$$

ii) longer dirⁿ



$$\begin{aligned} \text{Eff. depth} &= 145 - 10 \\ &= 135 \text{ mm} \end{aligned}$$

$$M_{uy} = 0.87 f_y A_{st} d \left(1 - \frac{A_{st} f_y}{b d f_{ck}}\right)$$

$$9.74 \times 10^6 = 0.87 \times 415 \times A_{st} \times 135 \left(1 - \frac{A_{st} \times 415}{1000 \times 135 \times 15}\right)$$

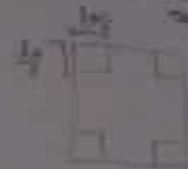
$$199.828 = A_{st} - 2.049 \times 10^{-4} A_{st}^2$$

$$2.049 \times 10^{-4} A_{st}^2 - A_{st} + 199.828 = 0$$

$$A_{st} = 208.757 \text{ mm}^2$$

$$\begin{aligned} \text{spacing} &= \frac{1000 \times \text{Area of one bar}}{A_{st}} \\ &= \frac{1000 \times \frac{\pi}{4} \times 10^2}{208.757} = 376.22 \approx 300 \text{ mm} \end{aligned}$$

Step 5 Torsional reinforcement



As the corners are held down, all the four corners are held down with torsional reinforcement provided

$$\text{size of torsional mesh} = \frac{l_x}{5} \times \frac{l_x}{5}$$

$$= \frac{4.145}{5} \times \frac{4.145}{5}$$

$$= 0.829 \times 0.829 \text{ m}$$

At each corner two meshes one at top & one at bottom are provided

$$\begin{aligned} \text{Area of torsional steel} &= \frac{3}{4} A_{stx} \\ &= \frac{3}{4} \times 264.124 \\ &= 198.09 \text{ mm}^2 \end{aligned}$$

Provide 10mm ϕ bars at spacing

$$\begin{aligned} &= \frac{1000 \times \frac{\pi}{4} \times 10^2}{198.09} = 396.48 \\ &\approx 300 \text{ mm} \end{aligned}$$

Check for shear

Q: Determine the mom. of resistance of a T-beam with following data
 $b_f = 740 \text{ mm}$, $d = 400 \text{ mm}$, $b_w = 240 \text{ mm}$,
 $A_{st} = 5, 20 \text{ mm } \phi$ Fe 250, $D_f = 100 \text{ mm}$, M15 concrete is used.

Sol: $D_f = 100 \text{ mm}$

$$\frac{x_u}{d} = \frac{0.87 f_y A_{st}}{0.36 f_{ck} b_f x_{u, \text{max}} d}$$
$$= \frac{0.87 \times 250 \times 5 \times \frac{\pi}{4} \times 20^2}{0.36 \times 15 \times 740 \times 400}$$
$$= 0.2137$$

$$x_u = 0.2137 \times 400$$
$$= 85.48 \approx 85.5 \text{ mm}$$
$$85.5 < 100$$



$$x_u < D_f$$

N.A lies inside flange. It behaves as rectangular section.

$$\frac{x_{u, \max}}{d} = 0.53$$

$$\frac{x_u}{d} < \frac{x_{u, \max}}{d}$$

It is under reinforced section.

From Cl. 1.1.6 of IS 456: 2000

$$M_u = 0.87 f_y A_{st} d \left[1 - \frac{A_{st} f_y}{bd f_{ck}} \right]$$

$$= 0.87 \times 250 \times 5 \times 20^2 \times \frac{\pi}{4} \times 400 \left[1 - \frac{1570 \times 250}{740 \times 400 \times 15} \right]$$

$$= 1245 \text{ KNm}$$