

$$A_s = \frac{1000 \times \text{Area of 1 bar}}{\text{Spacing}}$$

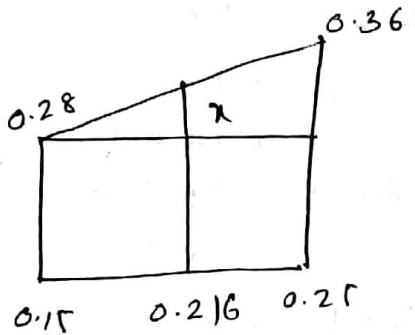
Shorter direction

$$= \frac{1000 \times \pi/4 \times 10^2}{250}$$

$$= 314.159 \text{ mm}^2$$

$$\frac{100 A_s}{bd} = \frac{100 \times 314.159}{1000 \times 145}$$

$$= 0.216$$



$$\frac{0.25 - 0.15}{0.216 - 0.15} = \frac{0.36 - 0.28}{x}$$

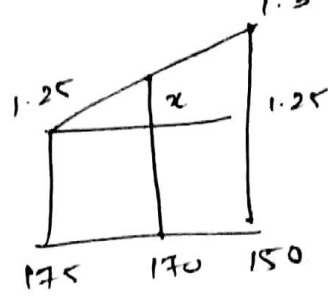
$$x = 0.0528$$

$$T_c = 0.28 + 0.0528$$

$$T_c = 0.3328$$

From cl. 40.2.1.1 of

$$D = 170$$



$$\frac{175 - 150}{175 - 170} = \frac{1.3 - 1.25}{x}$$

$$x = 0.01$$

$$k = 1.26$$

$$k T_c = 0.4193$$

$$T_v < k T_c$$

Slab is safe in shear.

Step 7: Check for development length.

[cl. 26.2]

$$L_d = \frac{\phi \sigma_s}{4 T_b d}$$

$$= \frac{10 \times 0.87 \times 415}{4 \times 1.2}$$

$$= 752.187 \text{ mm}$$

Q: Design a RCC roofing slab over a room $4\text{m} \times 5\text{m}$ the slab is simply supported on all 4 edges with corners held down. The superimposed load is 2 kN/m^2 and floor finish is

Use M15 concrete
Fe 415 steel

Given:-

$$L = 5m$$

$$l = 4m$$

$$f_{ck} = 15 \text{ N/mm}^2$$

$$f_y = 415 \text{ N/mm}^2$$

$$L.L = 2 \text{ kN/m}^2 \quad \begin{matrix} \text{? doubt} \\ \text{for an area} \end{matrix}$$

$$= 2 \times 1 \text{ kN/m} \quad \left[\begin{matrix} \text{breadth} \\ \text{if unit} \\ \text{is m} \end{matrix} \right]$$

STEP 1: CHECK FOR ONE WAY OR TWO WAY SLAB.

$$\frac{L}{l} = \frac{5}{4} = 1.25 < 2$$

\therefore It is a 2 way slab.

STEP 2: COMPUTATION OF SLAB DIMENSION

$$\frac{l}{d} = 20 \times M.F \quad \begin{matrix} \% \text{ tensile} \\ \text{reinforcement} \end{matrix}$$

$$\text{Assume } \alpha = 0.35\%$$

$$M.F = 1.4$$

\therefore from fig 4. of IS 456:2000

$$M.F = 1.4$$

$$\frac{l}{d} = 20 \times 1.4$$

$$\frac{4000}{d} = 20 \times 1.4$$

$$d = 142.857$$

Assume a clear cover of 20mm and diameter of 10mm

$$\begin{aligned} D &= d + c + \phi/2 \\ &= 142.85 + 20 + 10/2 \\ &= 167.85 \approx 170 \end{aligned}$$

$$\begin{aligned} d &= D - c - \phi/2 \\ &= 170 - 20 - 10/2 \\ &= 145 \end{aligned}$$

Assume width $b = 1m$

Effective span in one direction
 $l + d$

$$\begin{aligned} l + d &= 4000 + 145 \\ &= 4145 \text{ mm} \end{aligned}$$

Effective span in other direction

$$\begin{aligned} l + d &= 5000 + 145 \\ &= 5145 \text{ mm} \end{aligned}$$

STEP 3:

COMPUTATIONS OF LOADS AND BENDING MOMENT

$$L.L = 2 \text{ kN/m}$$

$$\begin{aligned} D.L &= 0.17 \times 1 \times 25 \\ &= 4.25 \text{ kN/m} \end{aligned}$$

$$\begin{aligned} F.L &= 0.5 \text{ kN/m}^2 \\ &= 0.5 \text{ kN/m} \end{aligned}$$

$$\begin{aligned} \text{Total load} \\ &= 6.75 \text{ kN/m} \end{aligned}$$

$$\frac{l_y}{l_x} = \frac{5.145}{4.145} = 1.24 \approx 1.25$$

From table 22.6

$$\begin{aligned} \alpha_x &= \frac{0.072 + 0.079}{2} \\ &= 0.0755 \end{aligned}$$

(From table for all edges discontinuous)

$$\alpha_y = 0.056$$

Annex D

D-1.1.

$$M_x = \alpha_x w l_x^2$$

$$= 0.0755 \times 6.75 \times 4.145^2$$

$$= 8.755 \text{ kNm}$$

$$M_{ux} = 8.755 \times 1.5 = 13.1325 \text{ kNm}$$

$$M_y = \alpha_y w l_y^2$$

$$= 0.056 \times 6.75 \times 4.145^2$$

$$= 6.494 \text{ kNm}$$

$$M_{uy} = 9.741 \text{ kNm}$$

Effective depth required =

$$M_u = 0.36 \frac{f_{ck} b d^2}{d} \left(1 - 0.42 \frac{f_{ck} b d^2}{d} \right)$$

Highest $b d^2 f_{ck}$

$$13.134 \times 10^6 = 0.36 \times 0.48 \left[1 - 0.42 \times 0.48 \right] \times 1000 \times d^2 \times 15$$

$$d = 79.66 \text{ mm}$$

required

$$d_{req} < d_{provided}$$

Hence safe

STEP 4: COMPUTATION OF REINFORCEMENT

Shorter direction

$$M_u = 0.87 f_y A_{st} d \left(1 - \frac{A_{st} f_y}{b d f_{ck}} \right)$$

$$13.134 = 0.87 \times 415 \times A_{st} \times 145 \left(1 - \frac{A_{st} \times 415}{1000 \times 145 \times 15} \right)$$

$$9.508 \times 10^{-4} = A_{st} - A_{st}^2 \times 1.908 \times 10^{-4}$$

$$A_{st} = 264.124$$

A_{st}

$$= 1000 \times \frac{\pi}{4} \times 10^2$$

$$264.124$$

$$= 297.35 \approx 290 \text{ mm}$$

Longer direction: $d = 145 - 10 = 135$

$$9.741 \times 10^6 = 0.87 \times 415 \times A_{st} \times 135 \left(1 - \frac{A_{st} \times 415}{1000 \times 135 \times 15} \right)$$

$$199.8 \times 10^{-4} = A_{st} - A_{st}^2 \times 2.049 \times 10^{-4}$$

$$A_{st} = 208.7$$

Spacing = 1000 Area of 1 bar

A_{st}

$$= \frac{1000 \times \frac{\pi}{4} \times 10^2}{208.7}$$

$$= 376.3 \approx 390 \text{ mm}$$

max

STEP 5: TORSIONAL REINFORCEMENT

As the corners are held on all the 4 corners are provided with torsion reinforcement

Size of torsion mesh

$$\text{Size} = \frac{l_x}{5} \times \frac{l_y}{5}$$

$$\frac{4.145}{5} = 0.83$$

$$s_{12} = 0.829m \times 0.829m$$

At each corner 2 meshes
one @ the top and one @
the bottom are provided.

$$\text{Area of tension steel} =$$

$$= \frac{3}{4} A_{stx}$$

$$= \frac{3}{4} \times 264.124$$

$$= 198.09 \text{ mm}^2$$

provide 10mm ϕ bars at
spacing

$$= \frac{1000 \times \text{Area of 1 bar}}{A_{st}}$$

$$= \frac{1000 \times \frac{\pi}{4} \times 10^2}{198.09}$$

$$= 396 \approx 300$$

STEP 6: CHECK FOR SHEAR