

$$4 \times 1.2$$

$$= \frac{25 \times 0.87 \times 415}{4 \times 1.2}$$

$$= 1880.46 \text{ mm}$$

$$= 1880.46 \text{ mm}$$

$$BM = \frac{wl^2}{8}$$

$$= \frac{40 \times 5^2}{8}$$

$$= 125$$

$$M_u = 125 \times 1.5$$

$$= 187.5$$

Q: Design a RC beam of rectangular section using the following data

effective span = 5m

width of beam = 250mm

Overall depth D = 500mm

Service load including

DL and LL = 40 kN/m

Effective cover = 50mm

Material M20 concrete

Fe 415 Steel.



STEP 1 COMPUTATION OF BEAM DIMENSION

$$l_{eff} = 5m$$

$$D = 500mm$$

$$\frac{l}{d} = 12$$

or

$$D - \text{eff cover} = d$$

$$d = 500 - 50 = 450$$

$$d' = 50$$

$$b = 250$$

$$f_{ck} = 20 \text{ N/mm}^2$$

$$f_y = 415 \text{ N/mm}^2$$

STEP 3 SINGLE / DOUBLY

$$cl. G. 1.1.6$$

$$M_{u,limit} = 0.36 \frac{x_{u,max}}{d} \left[1 - 0.42 \frac{x_{u,max}}{d} \right] b d^2 f_{ck}$$

$$= 0.36 \times 0.48 \left[1 - 0.42 \times 0.48 \right] \times 250 \times 450^2 \times 20$$

$$= 139688064$$

$$= 139.688 \text{ kNm}$$

$$M_u > M_{u,limit}$$

∴ Doubly reinforced.

SKIP STEP 4

STEP 5 : COMPUTATION OF REINFORCEMENT

$$M_{u,limit} = 0.87 f_y A_{st1} d \left[1 - \frac{A_{st1} f_y}{b d f_{ck}} \right]$$

$$139.688 \times 10^6 = 0.87 \times 415 A_{st1} \times 450$$

$$\left[1 - \frac{A_{st1} \times 415}{250 \times 450 \times 20} \right]$$

$$859.76 = A_{st1} - A_{st1}^2 \times 1.84 \times 10^{-4}$$

$$x = 1070.6, 4364.08$$

$$A_{st1} = 1070.6$$

Annex G.1.2 of 456:2000

$$M_u - M_{u, \text{limit}} = f_{sc} A_{sc} (d - d')$$

$$\text{Strain, } \epsilon_{sc} = 0.0035 \left[\frac{x_{u, \text{max}} - d'}{x_{u, \text{max}}} \right]$$

$$= 0.0035 \left[\frac{0.48d - d'}{0.48d} \right]$$

$$= 0.0035 \left[\frac{0.48 \times 450 - 50}{0.48 \times 450} \right]$$

$$= 2.68 \times 10^{-3}$$

from fig. 3 of SP 16

$$f_{sc} = 350 \text{ N/mm}^2$$

Annex G.1.2 of 456:2000

$$M_u - M_{u, \text{limit}} = f_{sc} A_{sc} (d - d')$$

$$(187.5 - 139.688) \times 10^6 = f_{sc} A_{sc} (450 - 50)$$

$$47.812 \times 10^6 = f_{sc} A_{sc} \times 400$$

$$A_{sc} = \frac{47.812 \times 10^6}{350 \times 400}$$

$$= 341.51 \text{ mm}^2$$

cl. G.1.2 of IS 456:2000

$$A_{st2} = \frac{A_{sc} f_{sc}}{0.87 f_y}$$

$$= \frac{341.51 \times 350}{0.87 \times 415}$$

$$A_{st2} = 331.058 \text{ mm}^2$$

$$A_{st} = A_{st1} + A_{st2}$$

$$= 1070.6 + 331.058$$

$$= 1401.65 \text{ mm}^2$$

Check for ^{tension} reinforcement

from cl. 26.5.1.1 of IS 456:2000

$$\frac{A_{st, \text{min}}}{bd} = \frac{0.85}{f_y}$$

$$A_{st, \text{min}} = \frac{0.85 \times 250 \times 450}{415}$$

$$= 230.42$$

$$A_{st, \text{max}} = 0.04 bD$$

$$= 0.04 \times 250 \times 500$$

$$= 5000$$

$$A_{st, \text{min}} < A_{st} < A_{st, \text{max}}$$

CHECK FOR COMPRESSION REINFORCEMENT

cl. 26.5.1.2

$$A_{sc, \text{max}} = 0.04 bD$$

$$= 5000$$

$A_{sc, \text{min}}$ = shall not be less than 0.2% of bD

$$A_{sc_{min}} = \frac{0.02 \times 250 \times 500}{100}$$

$$= \frac{0.02 \times 250 \times 500}{100}$$

$$= 250$$

$$A_{sc_{min}} < A_{sc} < A_{sc_{max}}$$

No. of bars in tension

$$\frac{A_{st}}{\text{Area of 1 bar}}$$

$$= \frac{1401.65}{\frac{\pi}{4} \times \frac{25^2}{25^2}} = \frac{2.8}{4.446}$$

$$= \text{5 No.} \rightarrow 3 \text{ bars}$$

No. of bars in compression

$$= \frac{A_{sc}}{\text{Area of 1 bar.}}$$

$$= \frac{341.51}{\frac{\pi}{4} \times 16^2} = 1.6$$

$$= 2 \text{ bars}$$

So provide 3 bars of 25mm ϕ on tension side and 2 bars of 16mm ϕ on compression side.

✓ STEP 6 : CHECK FOR SHEAR
(Cl. 40.1 of IS 456:2000)

$$\tau_v = \frac{V_u}{b d}$$

$$V_u = \frac{w l}{2} \times 1.5$$

$$= \frac{40 \times 5}{2} \times 1.5$$

$$= 150 \text{ kN}$$

$$\tau_v = \frac{150 \times 10^3}{250 \times 450}$$

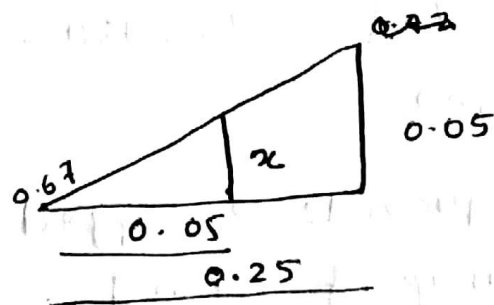
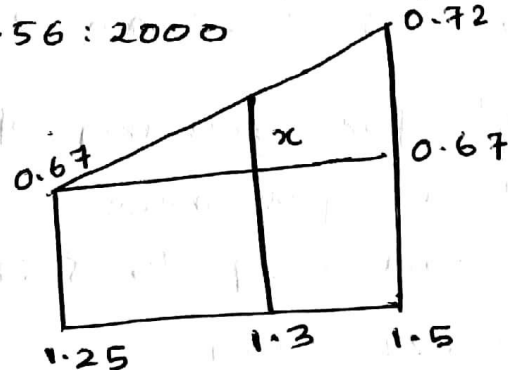
$$= 1.33$$

$$\tau_c \Rightarrow 100 \frac{A_s}{b d} \rightarrow \text{tension}$$

$$= \frac{100 \times 3 \times \frac{\pi}{4} \times 25^2}{250 \times 450}$$

$$= 1.3$$

From table 19 of IS 456:2000



$$\frac{0.05}{x} = \frac{0.25}{0.05} \quad x = 0.01$$

$$\tau_c = 0.67 + 11$$

$$= 0.68 \text{ N/mm}^2$$

$$\tau_{cmax} = 2.8 \text{ N/mm}^2$$

$$\tau_v > \tau_c > \tau_{cmax}$$

Provide design shear reinforcement in the form of vertical stirrups

$$V_{us} = \frac{0.87 f_y A_{sv} d}{S_v}$$

$$V_{us} = V_u - \tau_c b d$$

$$= 150 \times 10^3 - 0.68 \times 250 \times 450$$

$$= 73500 \text{ N}$$

2 legged - $\phi 8 \text{ mm}$

$$73500 = \frac{0.87 \times 415 \times 2 \times \frac{\pi}{4} 8^2 \times 450}{S_v}$$

$$S_v = 222.22 \text{ mm} = 220 \text{ mm}$$

Check for spacing of shear reinforcement

Cl 26.5.1.5 of IS 456:2000

$$(i) \quad 222.22 = 220 \quad 3^\circ$$

$$(ii) \quad 0.75d = 0.75 \times 450 = 337.5$$

$$(iii) \quad 300$$

So provide 2 legged

stirrup of $8 \text{ mm } \phi$ 4°

@ 220 mm c/c

STEP 7 CHECK FOR
DEFLECTION

$$\frac{l}{d} = \frac{5000}{450} = 11.11 < 20$$

\therefore safe

STEP 8 CHECK FOR
DEVELOPMENT LENGTH

Cl. 26.2.1

$$L_d = \frac{\phi \sigma_s}{4 \tau_{bd}}$$

$$= \frac{25 \times 0.87 \times 415}{4 \times 1.2}$$

$$= 1880.46 \text{ mm}$$

23.10.19