

# Progress Report

## Lifting Linearization of a UAV

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  - Results
- 2 LQR Controller Design
  - Results
- 3 Taylor Linearization
  - LQR controller
  - Servo controller

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$$\begin{aligned}
 \dot{\mathbf{p}} &= \mathbf{v} \\
 \dot{\mathbf{v}} &= \mathbf{r}_z(\mathbf{e})T + \mathbf{g} \\
 \begin{bmatrix} \dot{\boldsymbol{\epsilon}} \\ \dot{\eta} \end{bmatrix} &= \frac{1}{2} \mathbf{J}^E \boldsymbol{\omega} = \frac{1}{2} \begin{bmatrix} \eta \mathbf{I} - \boldsymbol{\epsilon}^\times \\ -\boldsymbol{\epsilon}^T \end{bmatrix} \boldsymbol{\omega}, \\
 \dot{\boldsymbol{\omega}} &= \mathbf{w}_1 \\
 \dot{T} &= w_2
 \end{aligned} \tag{1}$$

$$\mathbf{r}_z(\mathbf{e}) = \mathbf{R}(\mathbf{e}) \begin{bmatrix} 0 \\ 0 \\ 1 \end{bmatrix} = \begin{bmatrix} 2(\epsilon_1\epsilon_3 + \epsilon_2\eta) \\ 2(\epsilon_2\epsilon_3 - \epsilon_1\eta) \\ 1 + 2(-\epsilon_1^2 - \epsilon_2^2) \end{bmatrix}, \boldsymbol{\epsilon}^\times = \begin{bmatrix} 0 & -\epsilon_3 & \epsilon_2 \\ \epsilon_3 & 0 & -\epsilon_1 \\ -\epsilon_2 & \epsilon_1 & 0 \end{bmatrix}, \mathbf{I} = \begin{bmatrix} 1 & 0 & 0 \\ 0 & 1 & 0 \\ 0 & 0 & 1 \end{bmatrix}. \tag{2}$$

- States:  $\mathbf{x} = [\mathbf{p}^T \quad \mathbf{v}^T \quad \boldsymbol{\epsilon}^T \quad \eta \quad \boldsymbol{\omega}^T \quad T]^T_{14 \times 1}$
- Inputs:  $\mathbf{w} = [\mathbf{w}_1^T \quad w_2]^T_{4 \times 1}$
- $\dot{\mathbf{p}}, \dot{\mathbf{v}}, \boldsymbol{\omega}, \mathbf{g}$  are measured in Global Frame.
- $T$  is measured in Body Fixed Frame.

$$\dot{\mathbf{x}} = \begin{pmatrix} \dot{p}_1 \\ \dot{p}_2 \\ \dot{p}_3 \\ \dot{v}_1 \\ \dot{v}_2 \\ \dot{v}_3 \\ \dot{\epsilon}_1 \\ \dot{\epsilon}_2 \\ \dot{\epsilon}_3 \\ \dot{\eta} \\ \dot{\omega}_1 \\ \dot{\omega}_2 \\ \dot{\omega}_3 \\ \dot{T} \end{pmatrix} = \begin{pmatrix} v_1 \\ v_2 \\ v_3 \\ T(2\epsilon_1\epsilon_3 + 2\epsilon_2\eta) \\ T(2\epsilon_2\epsilon_3 - 2\epsilon_1\eta) \\ 9.81 - T(2\epsilon_1^2 + 2\epsilon_2^2 - 1) \\ \frac{\epsilon_3\omega_2}{2} - \frac{\epsilon_2\omega_3}{2} + \frac{\eta\omega_1}{2} \\ \frac{\epsilon_1\omega_3}{2} - \frac{\epsilon_3\omega_1}{2} + \frac{\eta\omega_2}{2} \\ \frac{\epsilon_2\omega_1}{2} - \frac{\epsilon_1\omega_2}{2} + \frac{\eta\omega_3}{2} \\ -\frac{\epsilon_1\omega_1}{2} - \frac{\epsilon_2\omega_2}{2} - \frac{\epsilon_3\omega_3}{2} \\ w_{1,1} \\ w_{1,2} \\ w_{1,3} \\ w_2 \end{pmatrix} = \begin{pmatrix} v_1 \\ v_2 \\ v_3 \\ 2\eta_1 + 2\eta_2 \\ 2\eta_3 - 2\eta_4 \\ T - \eta_6 - 2\eta_5 \\ \eta_7 - \eta_8 + \eta_9 \\ \eta_{10} - \eta_{11} + \eta_{12} \\ \eta_{13} - \eta_{14} + \eta_{15} \\ -\eta_{16} - \eta_{17} - \eta_{18} \\ w_{1,1} \\ w_{1,2} \\ w_{1,3} \\ w_2 \end{pmatrix} \quad (3)$$

$$\begin{pmatrix} T\epsilon_1\epsilon_3 \\ T\epsilon_2\eta \\ T\epsilon_2\epsilon_3 \\ T\epsilon_1\eta \\ T\epsilon_12 \\ 2T\epsilon_2^2 + g \\ \frac{\epsilon_3\omega_2}{2} \\ \frac{\epsilon_2\omega_3}{2} \\ \frac{\eta\omega_1}{2} \\ \frac{\epsilon_1\omega_3}{2} \\ \frac{\epsilon_3\omega_1}{2} \\ \frac{\eta\omega_2}{2} \\ \frac{\epsilon_2\omega_1}{2} \\ \frac{\epsilon_1\omega_2}{2} \\ \frac{\eta\omega_3}{2} \\ \frac{\epsilon_1\omega_1}{2} \\ \frac{\epsilon_2\omega_2}{2} \\ \frac{\epsilon_3\omega_3}{2} \end{pmatrix} = \begin{pmatrix} \eta_1 \\ \eta_2 \\ \eta_3 \\ \eta_4 \\ \eta_5 \\ \eta_6 \\ \eta_7 \\ \eta_8 \\ \eta_9 \\ \eta_{10} \\ \eta_{11} \\ \eta_{12} \\ \eta_{13} \\ \eta_{14} \\ \eta_{15} \\ \eta_{16} \\ \eta_{17} \\ \eta_{18} \end{pmatrix}$$

(4)

$$\begin{pmatrix} \epsilon_1^2 \\ \epsilon_2^2 \\ \epsilon_3^2 \\ \omega_1^2 \\ \omega_2^2 \\ \omega_3^2 \end{pmatrix} = \begin{pmatrix} \gamma_1 \\ \gamma_2 \\ \gamma_3 \\ \gamma_4 \\ \gamma_5 \\ \gamma_6 \end{pmatrix}$$

(5)

$$\epsilon = [0, 0, \sin(5)]$$

$$\eta = \cos(5)$$

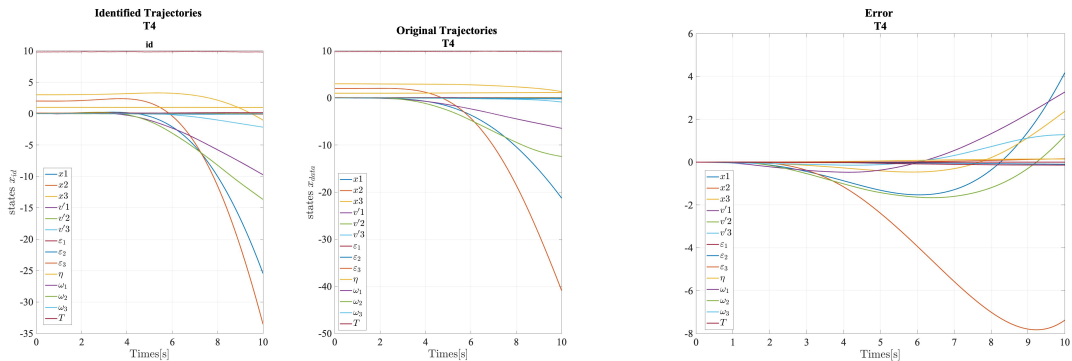


Figure: Linearized vs Real System

$$\epsilon = [0, 0, \sin(10)]$$

$$\eta = \cos(10)$$

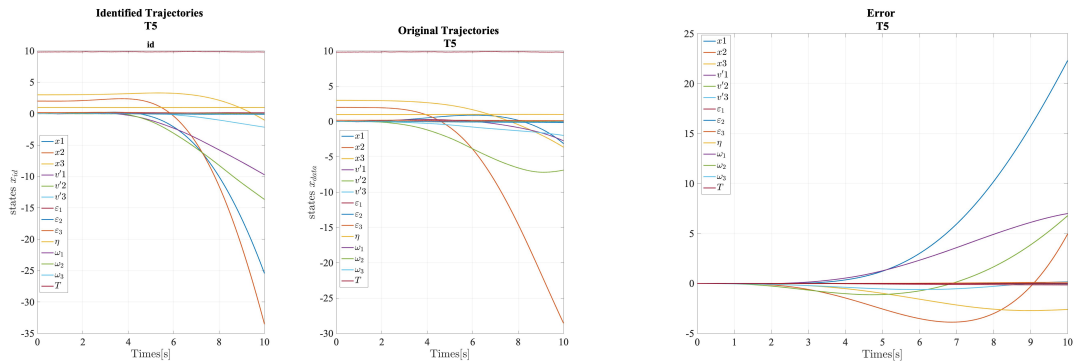


Figure: Linearized vs Real System



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*%% Controller Settings*

$Q_x = 2.3e3 \cdot [1; 1; 1];$

$Q_v = 1e3 \cdot [5; 5; 5];$

$Q_e = .5e3 \cdot [1; 1; 1; 2];$

$Q_{\omega} = 200 \cdot [10; 10; 10];$

$Q_{dfl} = \text{diag}([Q_x; Q_v; Q_e; Q_{\omega}]);$

$R = 1000 \cdot \text{diag}([1; 1; 1; 1]);$

$C_z = [\text{eye}(13, 13), \text{zeros}(13, 25)];$

$K = \text{lqr}(A, B, C_z' \cdot Q_{dfl} \cdot C_z, R);$

## Initial State

- Position:  $p_0 = [0 \ 2 \ 3]^T$
- Velocity:  $v_0 = [0 \ 0 \ 0]^T$
- Orientation:  $\epsilon_0 = [0 \ 0 \ \sin 10]^T, \eta_0 = \cos 10$
- Angular Velocity:  $\omega_0 = [0 \ 0 \ 0]^T$
- Thrust:  $T_0 = 9.81$

## Desired State

- Position:  $p = [0 \ 0 \ 0]^T$
- Velocity:  $v = [0 \ 0 \ 0]^T$
- Orientation:  $\epsilon = [0 \ 0 \ 0]^T, \eta = 1$
- Angular Velocity:  $\omega = [0 \ 0 \ 0]^T$
- Thrust:  $T = 9.81$

# Position and Velocity

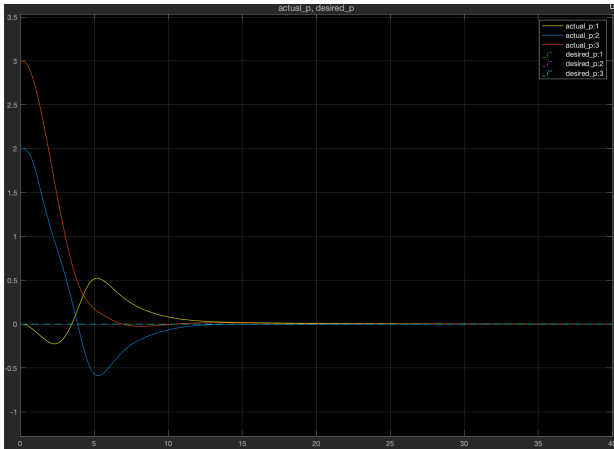


Figure: Position plot

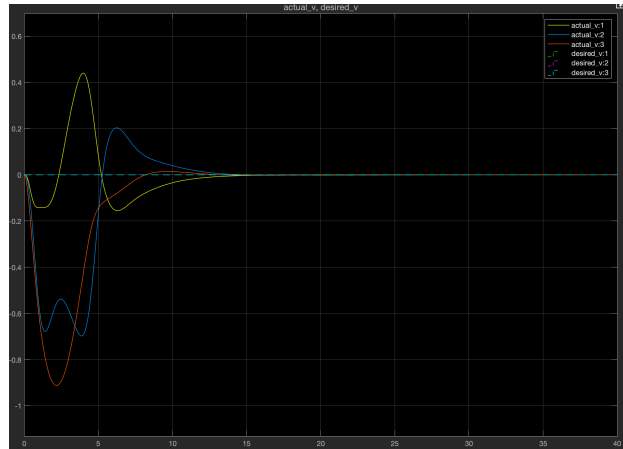


Figure: Velocity plot

# Euler Parameters

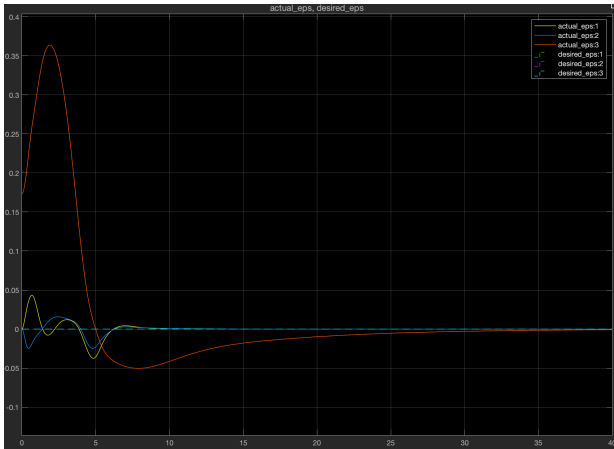


Figure: Epsilon plot



Figure: eta plot

# Angular Velocity and Inputs

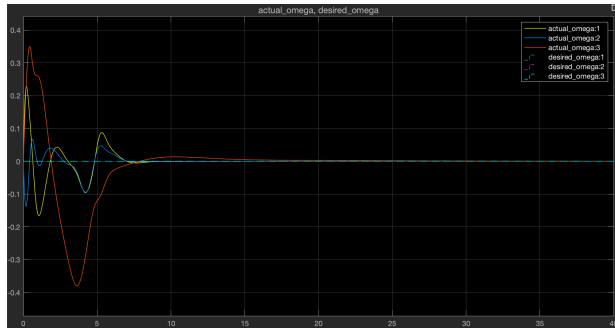


Figure: Angular Velocity plot

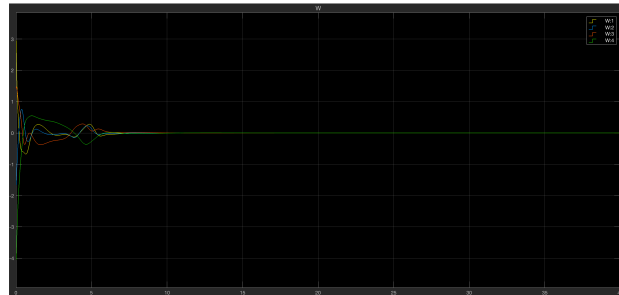


Figure: Inputs plot

# Auxiliary Parameters

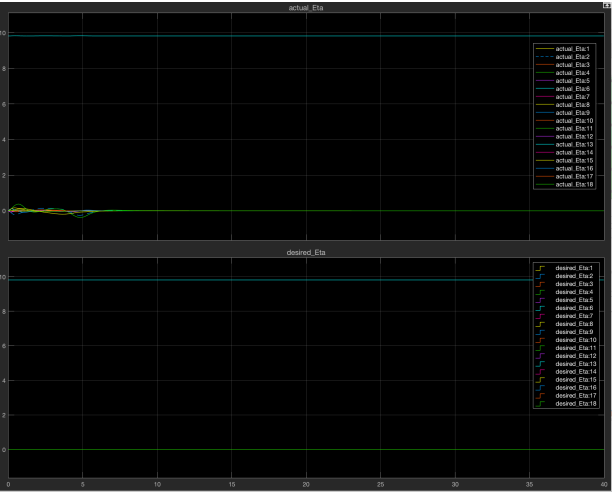


Figure: Etas plot

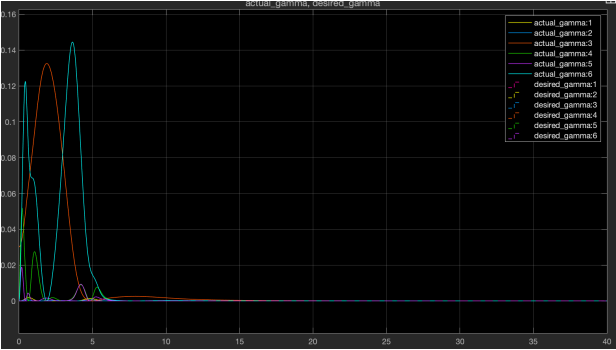


Figure: Gamma plot

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$$\dot{\mathbf{x}} = \begin{pmatrix} \dot{p}_1 \\ \dot{p}_2 \\ \dot{p}_3 \\ \dot{v}_1 \\ \dot{v}_2 \\ \dot{v}_3 \\ \dot{\epsilon}_1 \\ \dot{\epsilon}_2 \\ \dot{\epsilon}_3 \\ \dot{\eta} \\ \dot{\omega}_1 \\ \dot{\omega}_2 \\ \dot{\omega}_3 \\ \dot{T} \end{pmatrix} = \begin{pmatrix} v_1 \\ v_2 \\ v_3 \\ T(2\epsilon_1\epsilon_3 + 2\epsilon_2\eta) \\ T(2\epsilon_2\epsilon_3 - 2\epsilon_1\eta) \\ 9.81 - T(2\epsilon_1^2 + 2\epsilon_2^2 - 1) \\ \frac{\epsilon_3\omega_2}{2} - \frac{\epsilon_2\omega_3}{2} + \frac{\eta\omega_1}{2} \\ \frac{\epsilon_1\omega_3}{2} - \frac{\epsilon_3\omega_1}{2} + \frac{\eta\omega_2}{2} \\ \frac{\epsilon_2\omega_1}{2} - \frac{\epsilon_1\omega_2}{2} + \frac{\eta\omega_3}{2} \\ -\frac{\epsilon_1\omega_1}{2} - \frac{\epsilon_2\omega_2}{2} - \frac{\epsilon_3\omega_3}{2} \\ w_{1,1} \\ w_{1,2} \\ w_{1,3} \\ w_2 \end{pmatrix} = \begin{pmatrix} 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \end{pmatrix}$$

this equilibrium state is reach when  $\mathbf{x} = [0 \ 0 \ 0 \ 0 \ 0 \ 0 \ 0 \ 0 \ 0 \ 0 \ 1 \ 0 \ 0 \ 0 \ 9.81]^T_{14 \times 1}$  So this model can be Linearized in the neighborhood

Linearization of dynamic equation as  $\dot{x} = Ax + Bu$ , where

$$\begin{aligned} A(x, u) &= \frac{\partial}{\partial x} f(x, u) \\ B(x, u) &= \frac{\partial}{\partial u} f(x, u) \end{aligned} \quad (6)$$

$$A = \begin{pmatrix} 0 & 0 & 0 & 1 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 1 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 1 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 2 T \epsilon_3 & 2 T \eta & 2 T \epsilon_1 & 2 T \epsilon_2 & 0 & 0 & 0 & 2 \epsilon_1 \epsilon_3 + 2 \epsilon_2 \eta \\ 0 & 0 & 0 & 0 & 0 & 0 & -2 T \eta & 2 T \epsilon_3 & 2 T \epsilon_2 & -2 T \epsilon_1 & 0 & 0 & 0 & 2 \epsilon_2 \epsilon_3 - 2 \epsilon_1 \eta \\ 0 & 0 & 0 & 0 & 0 & 0 & -4 T \epsilon_1 & -4 T \epsilon_2 & 0 & 0 & 0 & 0 & 0 & -2 \epsilon_1^2 - 2 \epsilon_2^2 + 1 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 & -\frac{\omega_3}{2} & \frac{\omega_2}{2} & \frac{\omega_1}{2} & \frac{\eta}{2} & \frac{\epsilon_3}{2} & -\frac{\epsilon_2}{2} & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & \frac{\omega_3}{2} & 0 & -\frac{\omega_1}{2} & \frac{\omega_2}{2} & -\frac{\epsilon_3}{2} & \frac{\eta}{2} & \frac{\epsilon_1}{2} & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & -\frac{\omega_2}{2} & \frac{\omega_1}{2} & 0 & \frac{\omega_3}{2} & \frac{\epsilon_2}{2} & -\frac{\epsilon_1}{2} & \frac{\eta}{2} & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & -\frac{\omega_1}{2} & -\frac{\omega_2}{2} & -\frac{\omega_3}{2} & 0 & -\frac{\epsilon_1}{2} & -\frac{\epsilon_2}{2} & -\frac{\epsilon_3}{2} & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \end{pmatrix}$$

$$B = \begin{pmatrix} 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 \\ 1 & 0 & 0 & 0 \\ 0 & 1 & 0 & 0 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{pmatrix}$$

The rank of the controllability matrix is smaller than the number of states, so I had to remove the uncontrollable states. In this case, only one state was removed,  $\eta$

Constant disturbance ( $F_{dis} = [2.50, 1.25, 2.00]^T$ ) was added to the translational dynamics ( $\dot{\mathbf{v}}$ ). The following figures show the outputs:

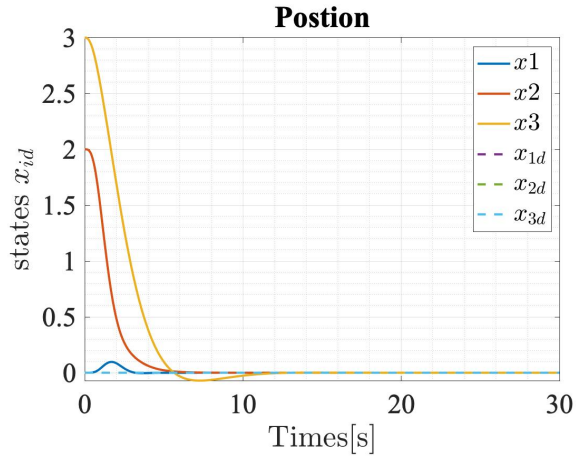


Figure: Postion without disturbance

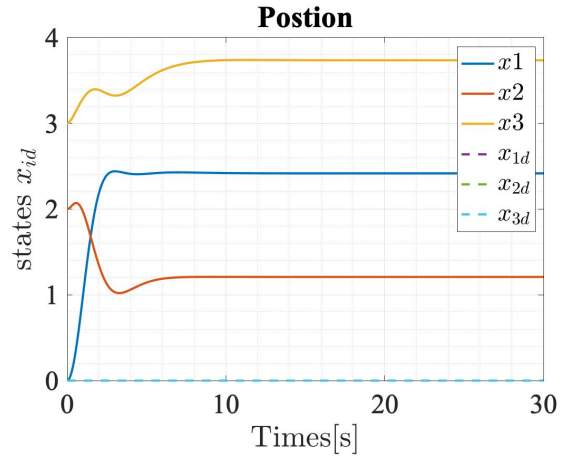


Figure: Postion with disturbance

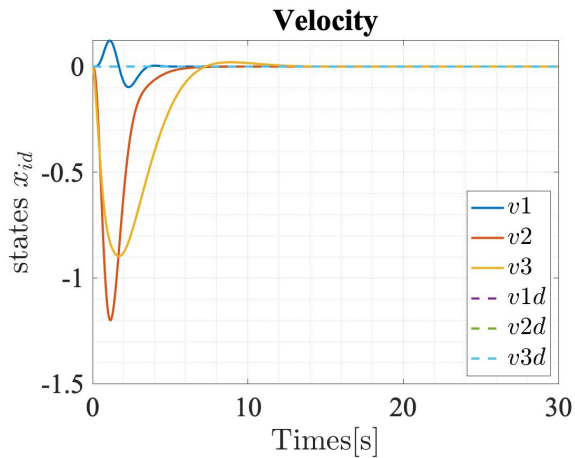


Figure: Velocity without disturbance

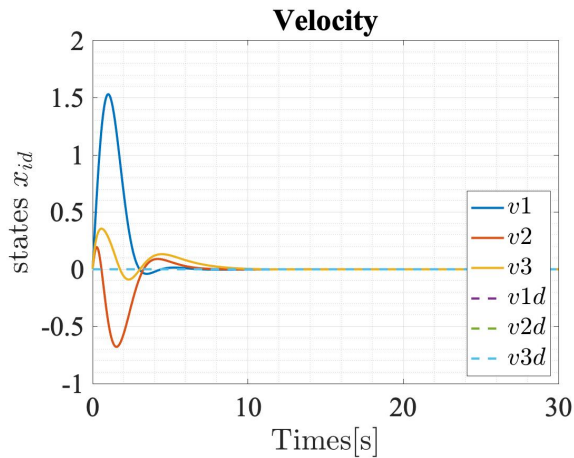


Figure: Velocity with disturbance

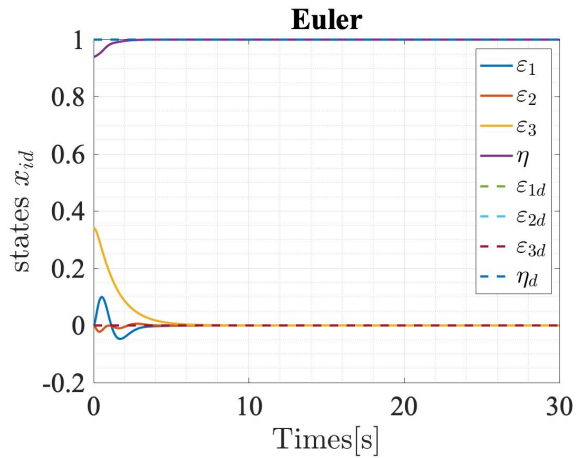


Figure: Euler without disturbance

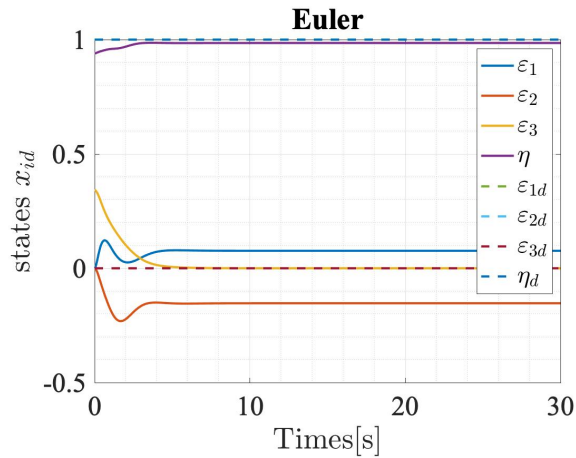


Figure: Euler with disturbance



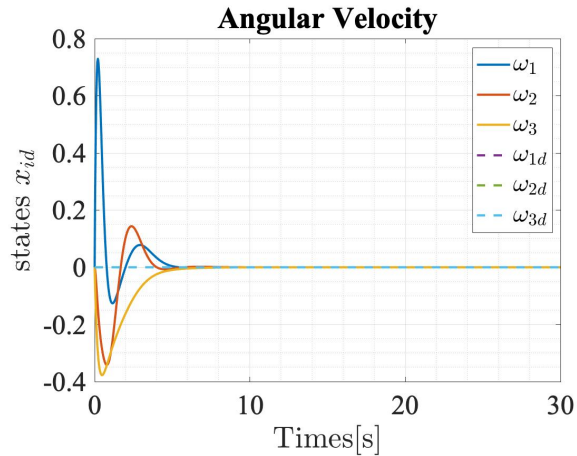


Figure: Angular Velocity without disturbance

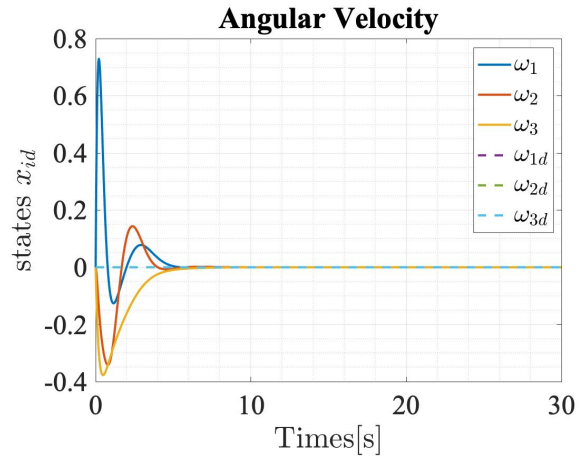


Figure: Angular Velocity with disturbance

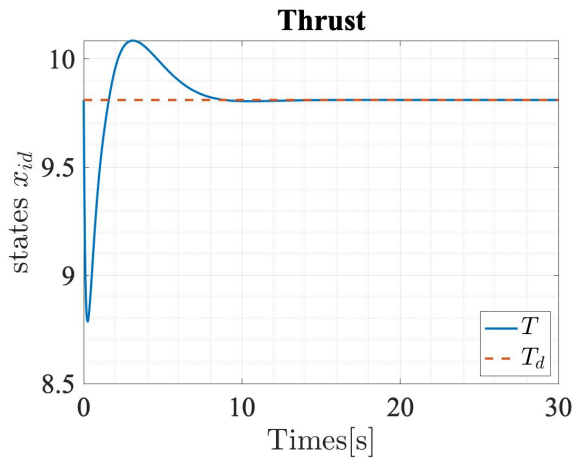


Figure: Thrust without disturbance

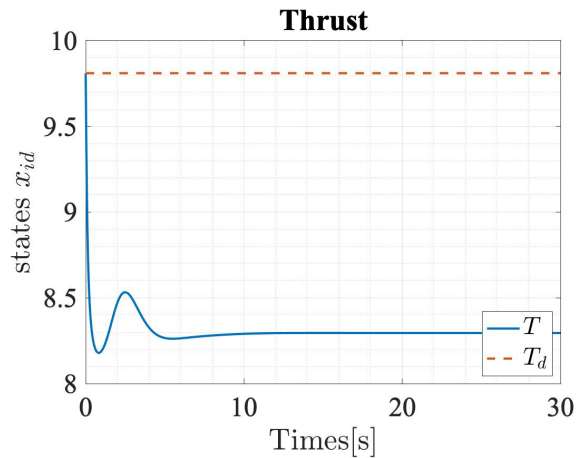


Figure: Thrust with disturbance

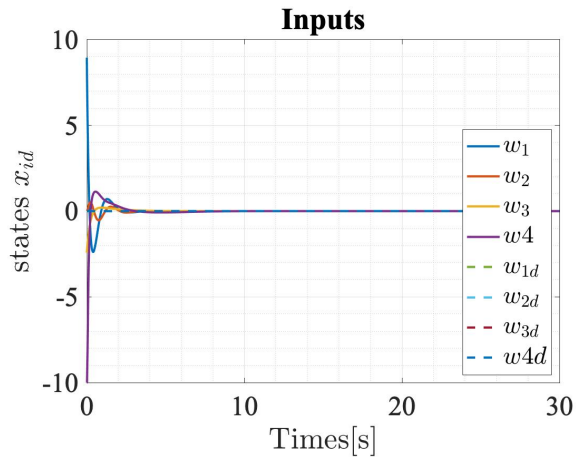


Figure: Inputs without disturbance

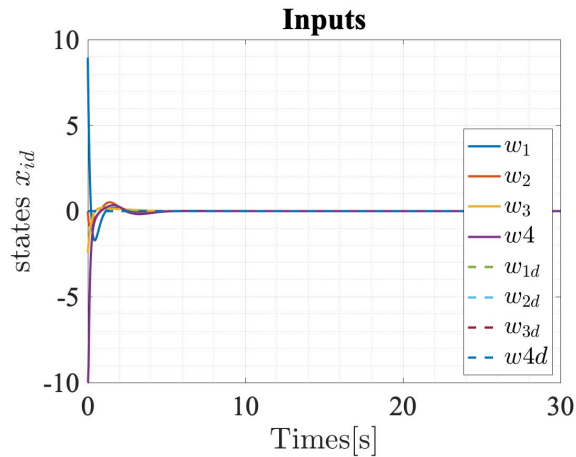


Figure: Inputs with disturbance

Constant disturbance ( $F_{dis} = [2.50, 1.25, 2.00]^T$ ) was added to the translational dynamics ( $\dot{\mathbf{v}}$ ). The following figures show the outputs:

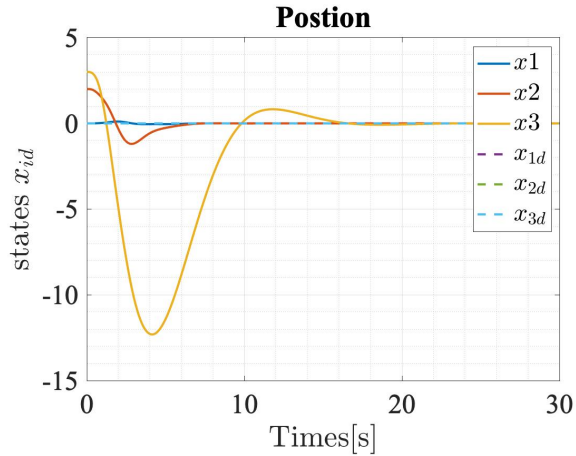


Figure: Position without disturbance

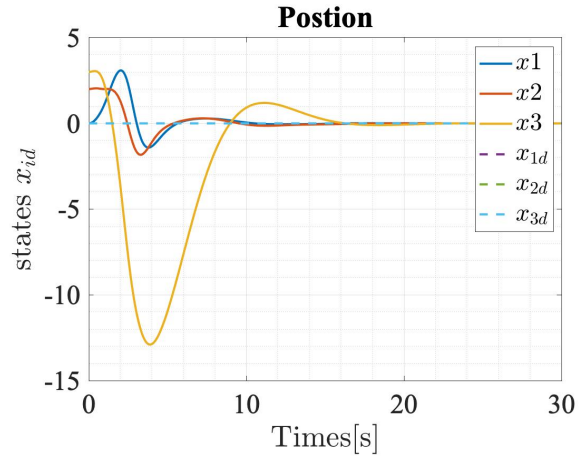


Figure: Position with disturbance

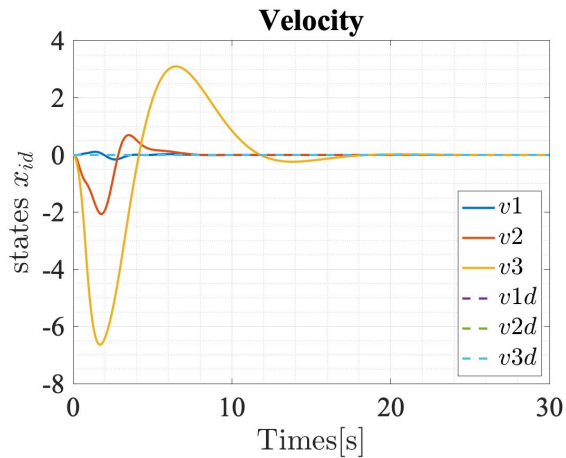


Figure: Velocity without disturbance

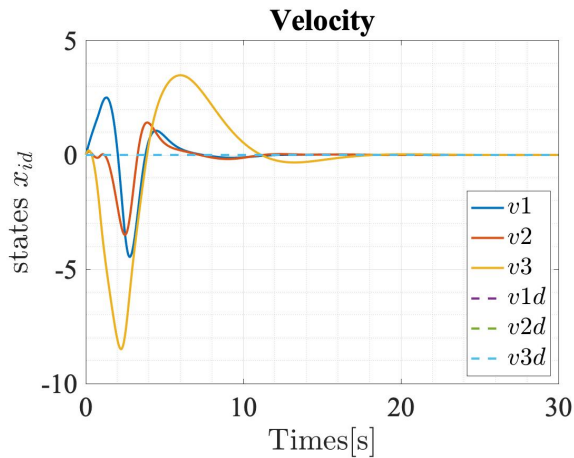


Figure: Velocity with disturbance

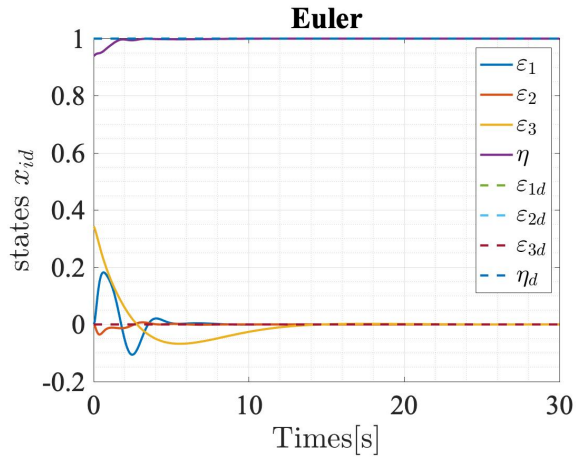


Figure: Euler without disturbance

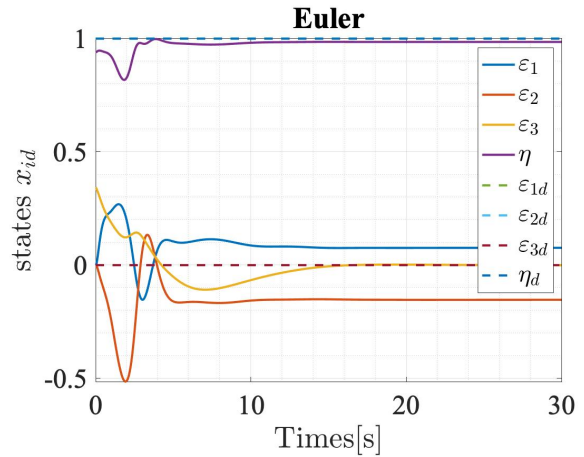


Figure: Euler with disturbance

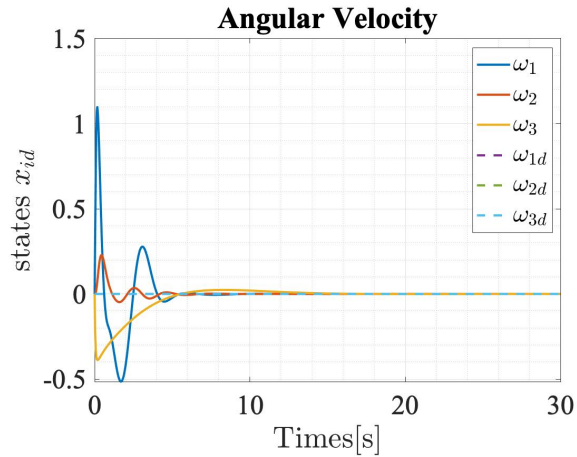


Figure: Angular Velocity without disturbance

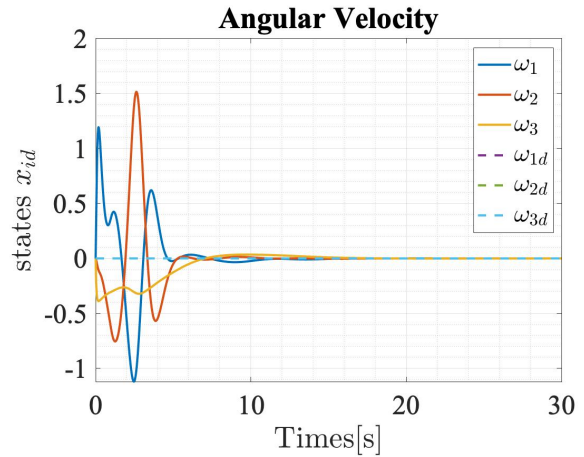


Figure: Angular Velocity with disturbance



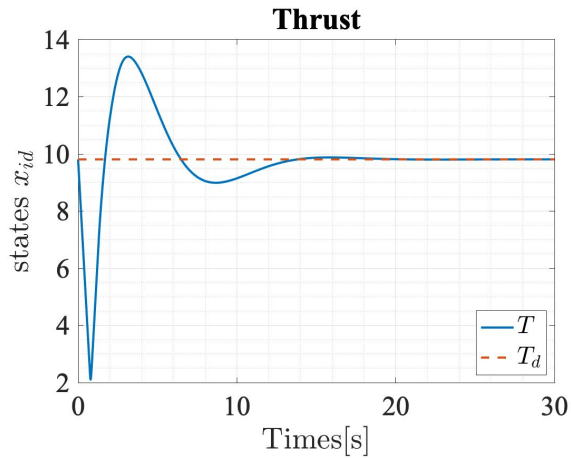


Figure: Thrust without disturbance

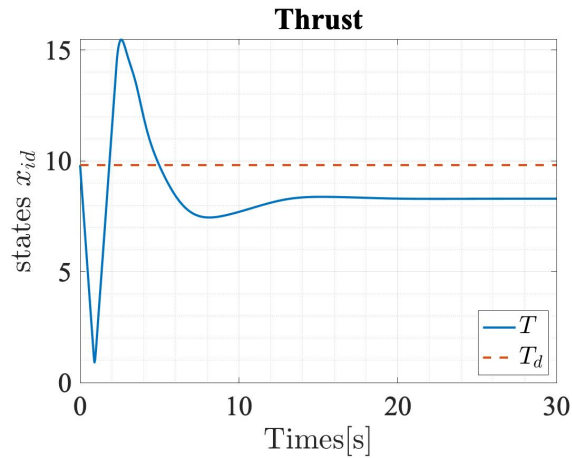


Figure: Thrust with disturbance

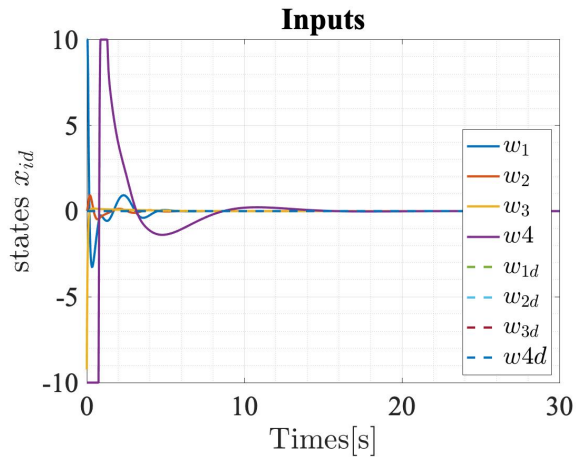


Figure: Inputs without disturbance

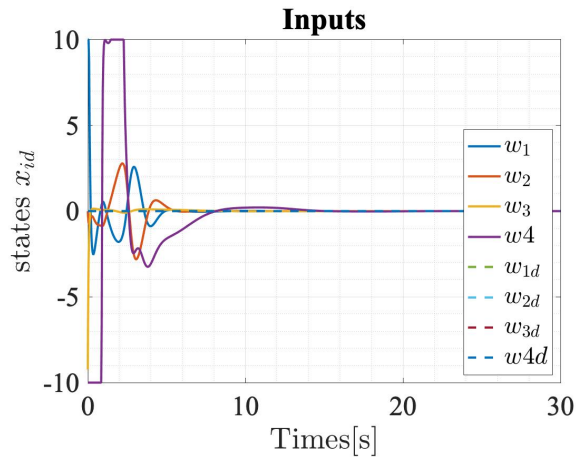


Figure: Inputs with disturbance