# Introduction to SFG

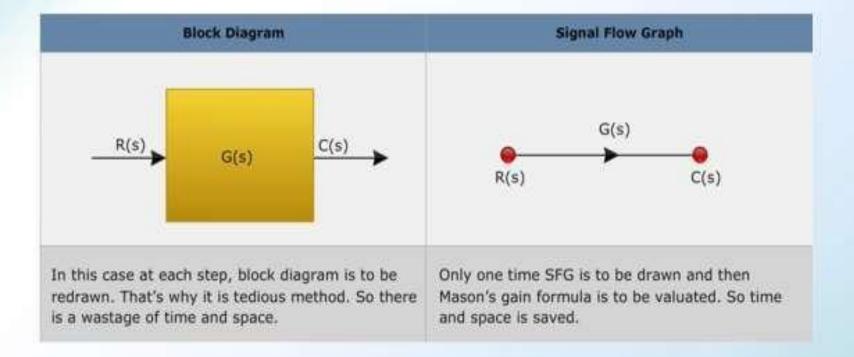
Alternative method to block diagram representation, developed by Samuel Jefferson Mason.

Advantage: the availability of a flow graph gain formula, also called Mason's gain formula.

A signal-flow graph consists of a network in which nodes are connected by directed branches.

It depicts the flow of signals from one point of a system to another and gives the relationships among the signals.

#### Comparison of BD and SFG



# Fundamentals of Signal Flow Graphs

Consider a simple equation below and draw its signal flow graph:

$$y = ax$$

The signal flow graph of the equation is shown below;

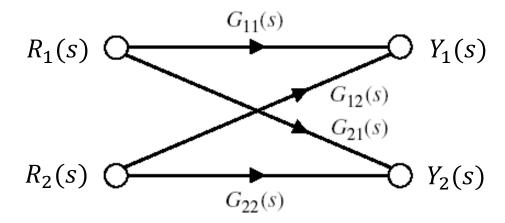


- Every variable in a signal flow graph is represented by a Node.
- Every transmission function in a signal flow graph is represented by a Branch.
- Branches are always unidirectional.
- The arrow in the branch denotes the direction of the signal flow.

# **Signal-Flow Graph Models**

$$Y_1(s) = G_{11}(s) \cdot R_1(s) + G_{12}(s) \cdot R_2(s)$$

$$Y_2(s) = G_{21}(s) \cdot R_1(s) + G_{22}(s) \cdot R_2(s)$$



### Signal-Flow Graph Models

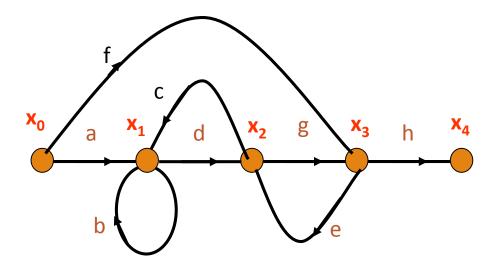
 $x_0$  is input and  $x_4$  is output

$$x_1 = ax_0 + bx_1 + cx_2$$

$$x_2 = dx_1 + ex_3$$

$$x_3 = fx_0 + gx_2$$

$$x_4 = hx_3$$



# Terminologies

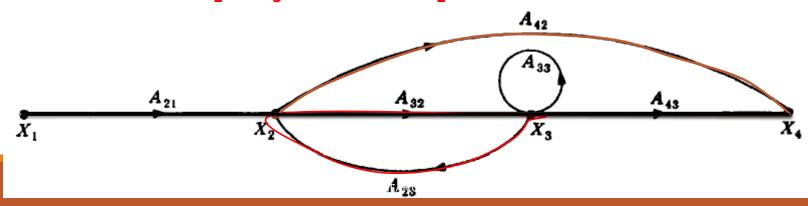
- An input node or source contain only the outgoing branches. i.e.,  $X_1$
- An output node or sink contain only the incoming branches. i.e.,  $X_{\Delta}$
- A path is a continuous, unidirectional succession of branches along which no node is passed more than ones. i.e.,

$$X_1$$
 to  $X_2$  to  $X_3$  to  $X_4$   $X_1$  to  $X_2$  to  $X_4$ 

$$X_1$$
 to  $X_2$  to  $X_4$ 

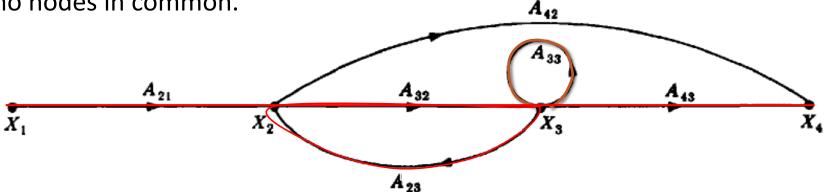
$$X_2$$
 to  $X_3$  to  $X_4$ 

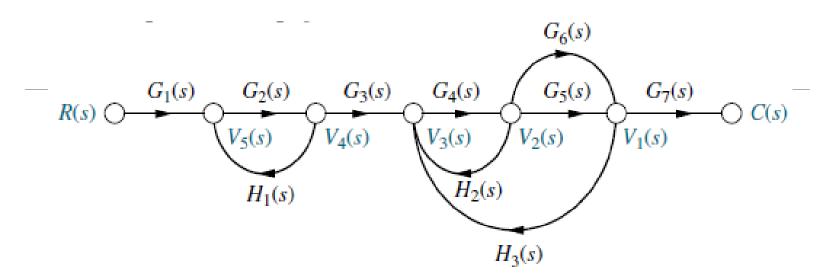
- A forward path is a path from the input node to the output node. i.e.,  $X_1$  to  $X_2$  to  $X_3$  to  $X_4$ , and  $X_1$  to  $X_2$  to  $X_4$ , are forward paths.
- A feedback path or feedback loop is a path which originates and terminates on the same node. i.e.;  $X_2$  to  $X_3$  and back to  $X_2$  is a feedback path.



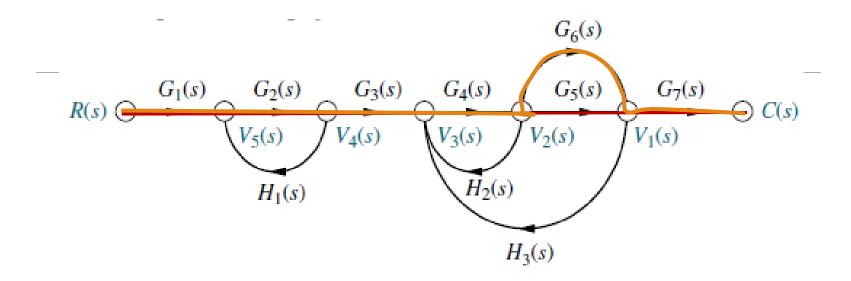
# Terminologies

- A self-loop is a feedback loop consisting of a single branch. i.e.;  $A_{33}$  is a self loop.
- The gain of a branch is the transmission function of that branch.
- The path gain is the product of branch gains encountered in traversing a path. i.e. the gain of forwards path  $X_1$  to  $X_2$  to  $X_3$  to  $X_4$  is  $A_{21}A_{32}A_{43}$
- The loop gain is the product of the branch gains of the loop. i.e., the loop gain of the feedback loop from  $X_2$  to  $X_3$  and back to  $X_2$  is  $A_{32}A_{23}$ .
- Two loops, paths, or loop and a path are said to be non-touching if they have no nodes in common.





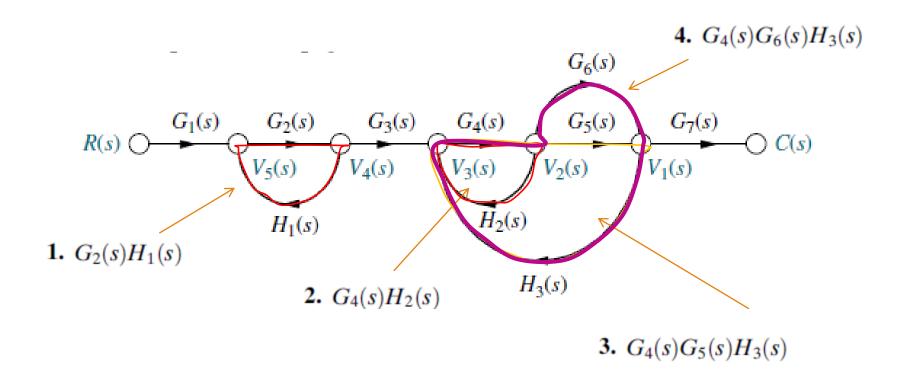
- a) Input node.
- b) Output node.
- c) Forward paths.
- d) Feedback paths (loops).
- e) Determine the loop gains of the feedback loops.
- f) Determine the path gains of the forward paths.
- g) Non-touching loops

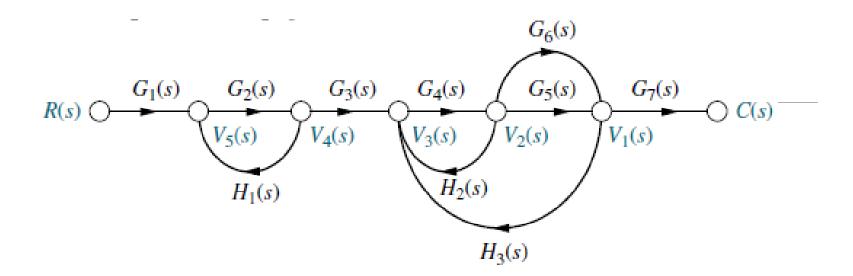


There are two forward path gains;

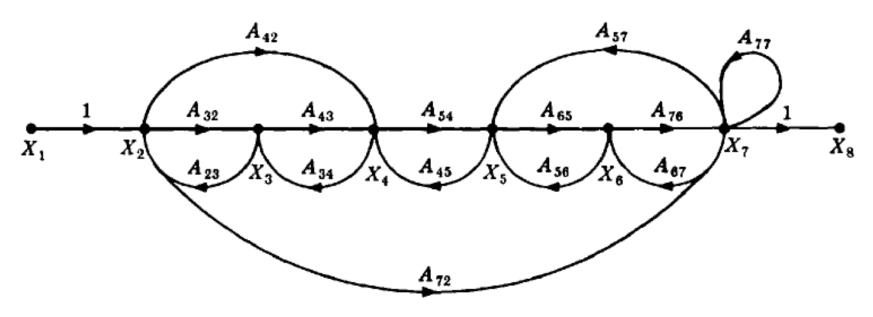
- **1.**  $G_1(s)G_2(s)G_3(s)G_4(s)G_5(s)G_7(s)$
- **2.**  $G_1(s)G_2(s)G_3(s)G_4(s)G_6(s)G_7(s)$

#### There are four loops



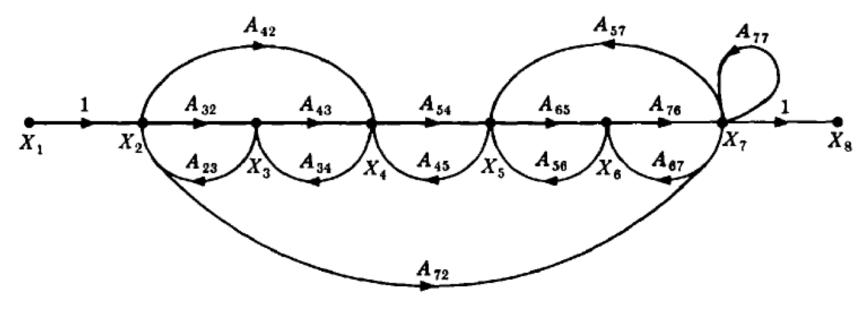


- Nontouching loop gains;
  - **1.**  $[G_2(s)H_1(s)][G_4(s)H_2(s)]$
- **2.**  $[G_2(s)H_1(s)][G_4(s)G_5(s)H_3(s)]$
- **3.**  $[G_2(s)H_1(s)][G_4(s)G_6(s)H_3(s)]$



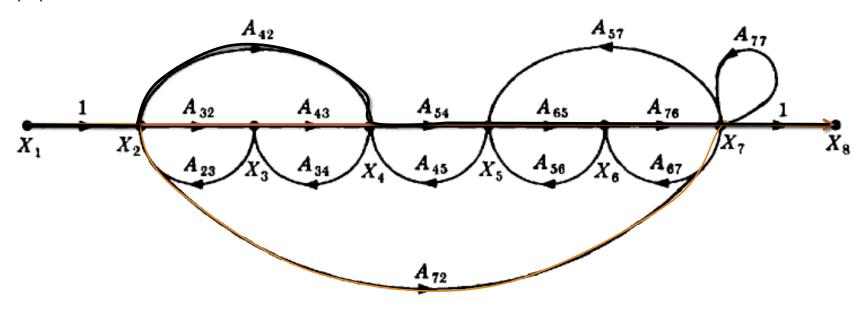
- a) Input node.
- b) Output node.
- c) Forward paths.
- d) Feedback paths.
- e) Self loop.
- f) Determine the loop gains of the feedback loops.
- g) Determine the path gains of the forward paths.

### Input and output Nodes



- a) Input node  $X_1$
- b) Output node  $X_8$

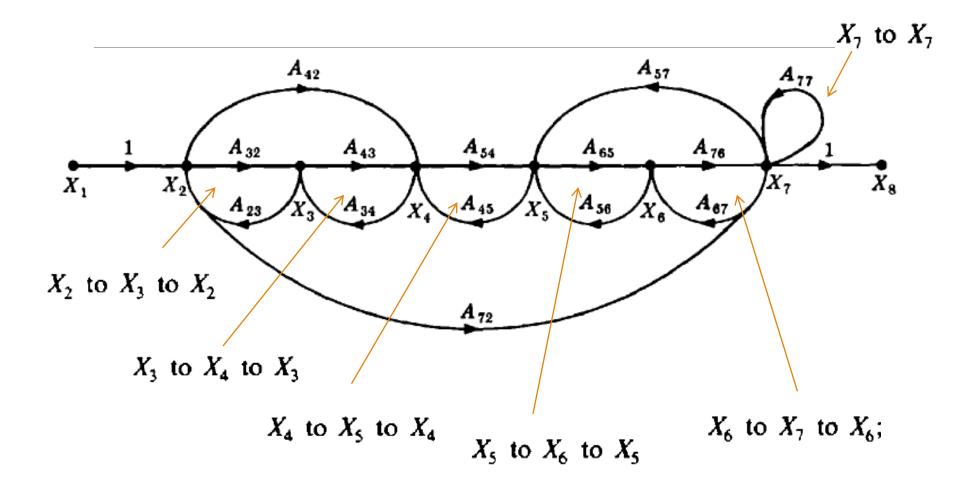
### (c) Forward Paths

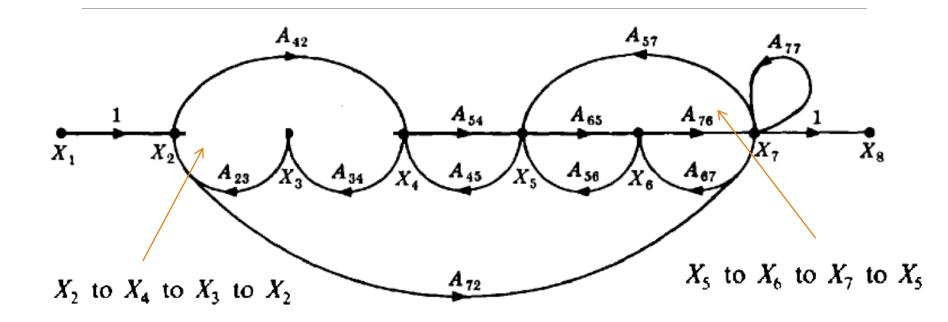


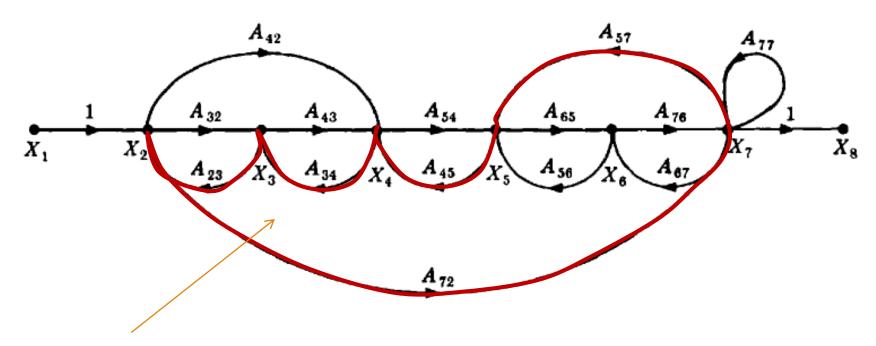
 $X_1$  to  $X_2$  to  $X_3$  to  $X_4$  to  $X_5$  to  $X_6$  to  $X_7$  to  $X_8$ 

 $X_1$  to  $X_2$  to  $X_7$  to  $X_8$ 

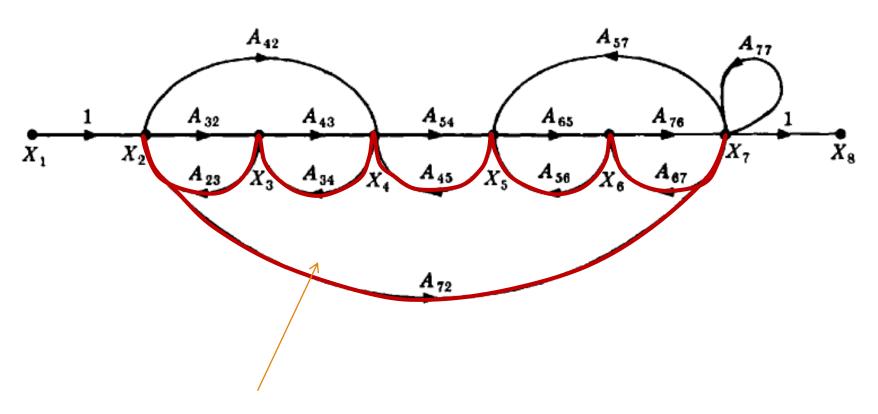
 $X_1$  to  $X_2$  to  $X_4$  to  $X_5$  to  $X_6$  to  $X_7$  to  $X_8$ 





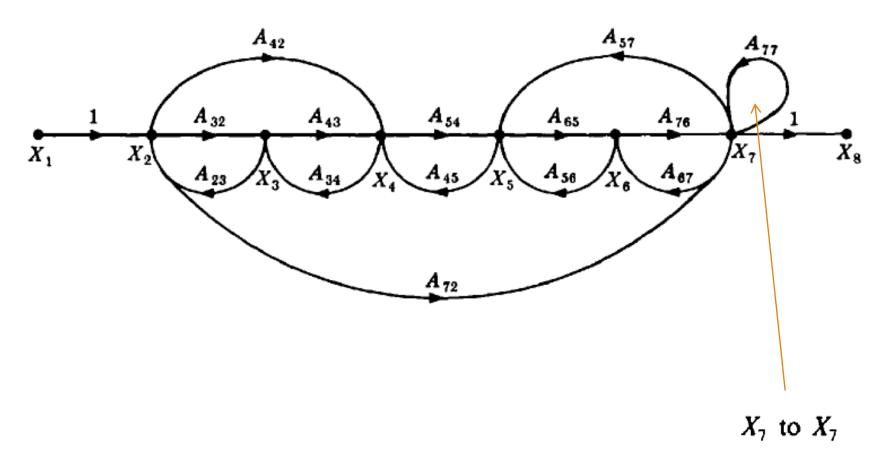


 $X_2$  to  $X_7$  to  $X_5$  to  $X_4$  to  $X_3$  to  $X_2$ 

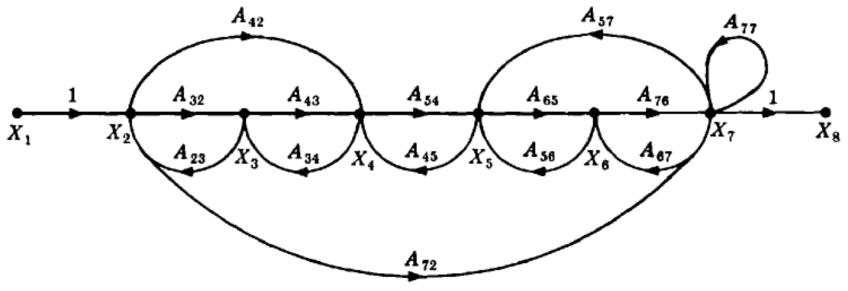


 $X_2$  to  $X_7$  to  $X_6$  to  $X_5$  to  $X_4$  to  $X_3$  to  $X_2$ 

### (e) Self Loop(s)



#### (f) Loop Gains of the Feedback Loops



$$A_{32}A_{23}$$
  $A_{76}A_{67}$ ;

$$A_{43}A_{34}$$
:  $A_{65}A_{76}A_{57}$ :

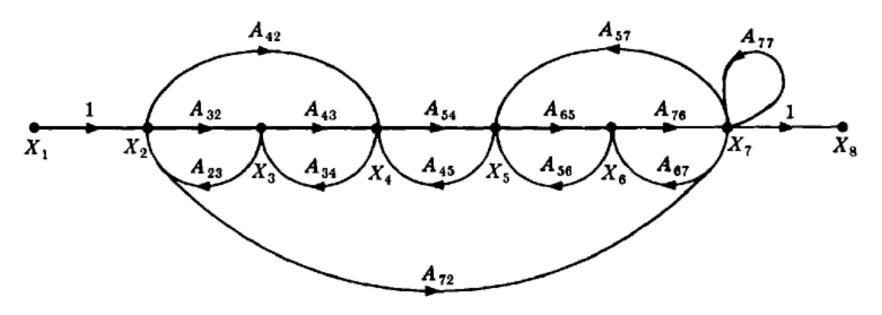
$$A_{54}A_{45}$$
:  $A_{77}$ 

$$A_{65}A_{56}$$
  $A_{42}A_{34}A_{23}$ 

$$A_{72}A_{57}A_{45}A_{34}A_{23};$$

$$A_{72}A_{67}A_{56}A_{45}A_{34}A_{23}$$

### (g) Path Gains of the Forward Paths



$$A_{32}A_{43}A_{54}A_{65}A_{76}$$

 $A_{72}$ 

$$A_{42}A_{54}A_{65}A_{76}$$

# Mason's Rule (Mason, 1953)

- The block diagram reduction technique requires successive application of fundamental relationships in order to arrive at the system transfer function.
- On the other hand, Mason's rule for reducing a signal-flow graph to a single transfer function requires the application of one formula.
- The formula was derived by S. J. Mason when he related the signal-flow graph to the simultaneous equations that can be written from the graph.

# Mason's Rule:

The transfer function, C(s)/R(s), of a system represented by a signal-flow graph is;

$$\frac{C(s)}{R(s)} = \frac{\sum_{i=1}^{n} P_i \Delta_i}{\Delta}$$

Where

n = number of forward paths.

 $P_i$  = the  $i^{th}$  forward-path gain.

 $\Delta$  = Determinant of the system

 $\Delta_i$  = Determinant of the  $i^{th}$  forward path

•  $\Delta$  is called the signal flow graph determinant or characteristic function. Since  $\Delta$ =0 is the system characteristic equation.

# Mason's Rule:

$$\frac{C(s)}{R(s)} = \frac{\sum_{i=1}^{n} P_i \Delta_i}{\Delta}$$

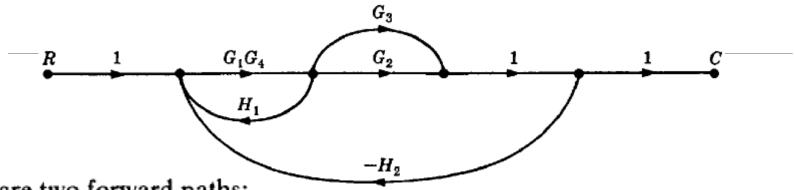
 $\Delta$  = 1- (sum of all individual loop gains) + (sum of the products of the gains of all possible two loops that do not touch each other) – (sum of the products of the gains of all possible three loops that do not touch each other) + ... and so forth with sums of higher number of non-touching loop gains

 $\Delta_i$  = value of  $\Delta$  for the part of the block diagram that does not touch the i-th forward path ( $\Delta_i$  = 1 if there are no non-touching loops to the i-th path.)

## Systematic approach

- 1. Calculate forward path gain  $P_i$  for each forward path i.
- 2. Calculate all loop transfer functions
- 3. Consider non-touching loops 2 at a time
- 4. Consider non-touching loops 3 at a time
- 5. Calculate  $\Delta$  from steps 2,3,4 and 5
- 6. Calculate  $\Delta_i$  as portion of  $\Delta$  not touching forward path i

Example#1: Apply Mason's Rule to calculate the transfer function of the system represented by following Signal Flow Graph



There are two forward paths:

$$P_1 = G_1 G_2 G_4$$
  $P_2 = G_1 G_3 G_4$ 

$$P_2 = G_1 G_3 G_4$$

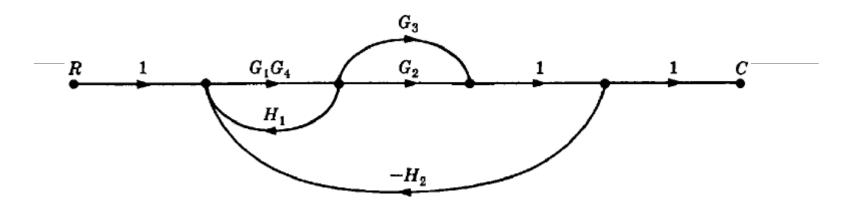
Therefore,

$$\frac{C}{R} = \frac{P_1 \Delta_1 + P_2 \Delta_2}{\Delta}$$

There are three feedback loops

$$L_1 = G_1G_4H_1$$
,  $L_2 = -G_1G_2G_4H_2$ ,  $L_3 = -G_1G_3G_4H_2$ 

Example#1: Apply Mason's Rule to calculate the transfer function of the system represented by following Signal Flow Graph



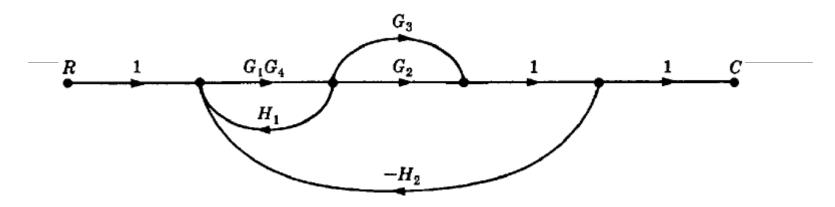
#### There are no non-touching loops, therefore

 $\Delta$  = 1- (sum of all individual loop gains)

$$\Delta = 1 - (L_1 + L_2 + L_3)$$

$$\Delta = 1 - (G_1 G_4 H_1 - G_1 G_2 G_4 H_2 - G_1 G_3 G_4 H_2)$$

Example#1: Apply Mason's Rule to calculate the transfer function of the system represented by following Signal Flow Graph



#### Eliminate forward path-1

$$\Delta_1$$
 = 1- (sum of all individual loop gains)+...

$$\Delta_1 = 1$$

#### **Eliminate forward path-2**

$$\Delta_2$$
 = 1- (sum of all individual loop gains)+...

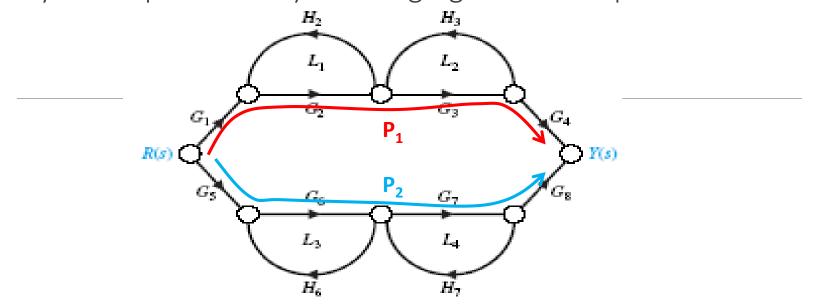
$$\Delta_2 = 1$$

### Example#1: Continue

$$\frac{C}{R} = \frac{P_1 \Delta_1 + P_2 \Delta_2}{\Delta} = \frac{G_1 G_2 G_4 + G_1 G_3 G_4}{1 - G_1 G_4 H_1 + G_1 G_2 G_4 H_2 + G_1 G_3 G_4 H_2}$$

$$= \frac{G_1 G_4 (G_2 + G_3)}{1 - G_1 G_4 H_1 + G_1 G_2 G_4 H_2 + G_1 G_3 G_4 H_2}$$

Example#2: Apply Mason's Rule to calculate the transfer function of the system represented by following Signal Flow Graph



1. Calculate forward path gains for each forward path.

$$P_1 = G_1G_2G_3G_4$$
 (path 1) and  $P_2 = G_5G_6G_7G_8$  (path 2)

2. Calculate all loop gains.

$$L_1 = G_2 H_2$$
,  $L_2 = H_3 G_3$ ,  $L_3 = G_6 H_6$ ,  $L_4 = G_7 H_7$ 

3. Consider two non-touching loops.

$$L_1L_3$$
  $L_1L_4$   $L_2L_4$ 

# Example#2: continue

- Consider three non-touching loops.
   None.
- 5. Calculate  $\Delta$  from steps 2,3,4.

$$\Delta = 1 - (L_1 + L_2 + L_3 + L_4) + (L_1 L_3 + L_1 L_4 + L_2 L_3 + L_2 L_4)$$

$$\Delta = 1 - (G_2 H_2 + H_3 G_3 + G_6 H_6 + G_7 H_7) +$$

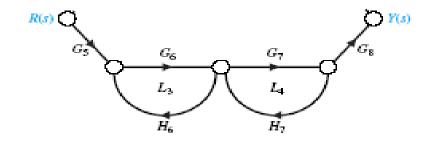
$$(G_2 H_2 G_6 H_6 + G_2 H_2 G_7 H_7 + H_3 G_3 G_6 H_6 + H_3 G_3 G_7 H_7)$$

# Example#2: continue

#### Eliminate forward path-1

$$\Delta_1 = 1 - (L_3 + L_4)$$

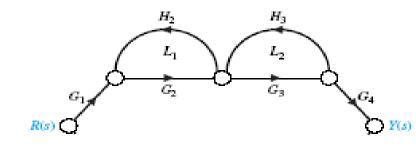
$$\Delta_1 = 1 - (G_6 H_6 + G_7 H_7)$$



#### Eliminate forward path-2

$$\Delta_2 = 1 - (L_1 + L_2)$$

$$\Delta_2 = 1 - (G_2 H_2 + G_3 H_3)$$



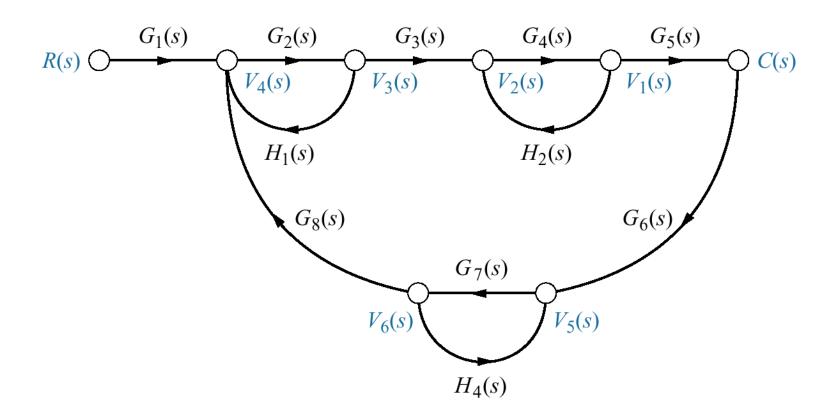
# Example#2: continue

$$\frac{Y(s)}{R(s)} = \frac{P_1 \Delta_1 + P_2 \Delta_2}{\Delta}$$

$$\frac{Y(s)}{R(s)} = \frac{G_1G_2G_3G_4\left[1 - \left(G_6H_6 + G_7H_7\right)\right] + G_5G_6G_7G_8\left[1 - \left(G_2H_2 + G_3H_3\right)\right]}{1 - \left(G_2H_2 + H_3G_3 + G_6H_6 + G_7H_7\right) + \left(G_2H_2G_6H_6 + G_2H_2G_7H_7 + H_3G_3G_6H_6 + H_3G_3G_7H_7\right)}$$

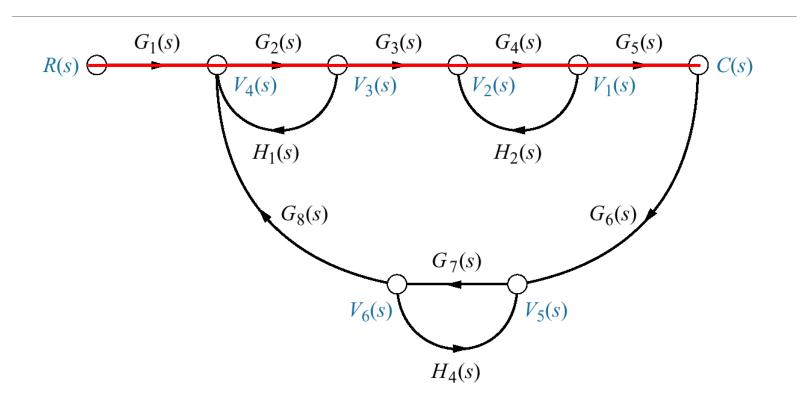
# Example#3

Find the transfer function, C(s)/R(s), for the signal-flow graph in figure below.



# Example#3

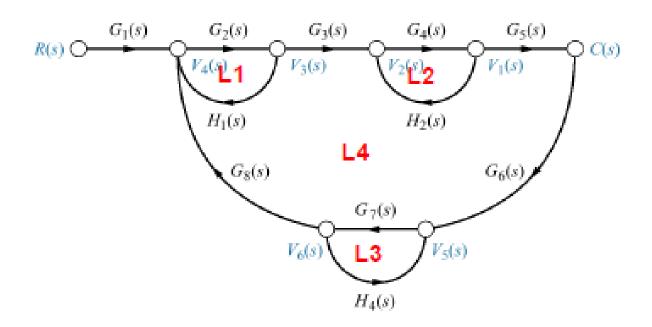
There is only one forward Path.



$$P_1 = G_1(s)G_2(s)G_3(s)G_4(s)G_5(s)$$

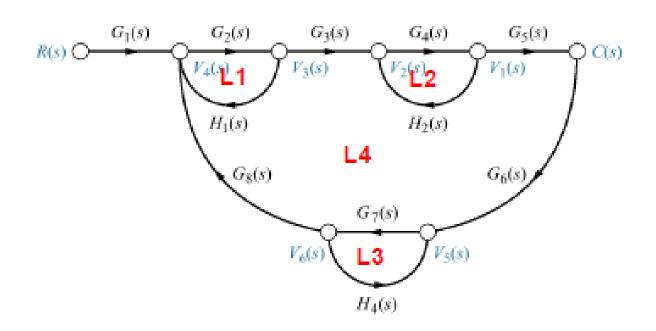
# Example#3

There are four feedback loops.



- L1.  $G_2(s)H_1(s)$  L3.  $G_7(s)H_4(s)$
- L2.  $G_4(s)H_2(s)$
- L4.  $G_2(s)G_3(s)G_4(s)G_5(s)G_6(s)G_7(s)G_8(s)$

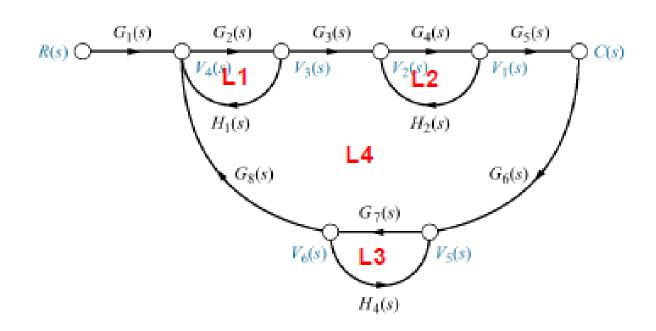
Non-touching loops taken two at a time.



L1 and L2:  $G_2(s)H_1(s)G_4(s)H_2(s)$  L2 and L3:  $G_4(s)H_2(s)G_7(s)H_4(s)$ 

L1 and L3:  $G_2(s)H_1(s)G_7(s)H_4(s)$ 

Non-touching loops taken three at a time.

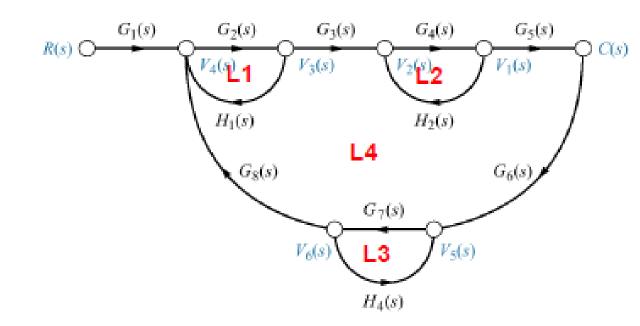


L1, L2, L3: 
$$G_2(s)H_1(s)G_4(s)H_2(s)G_7(s)H_4(s)$$

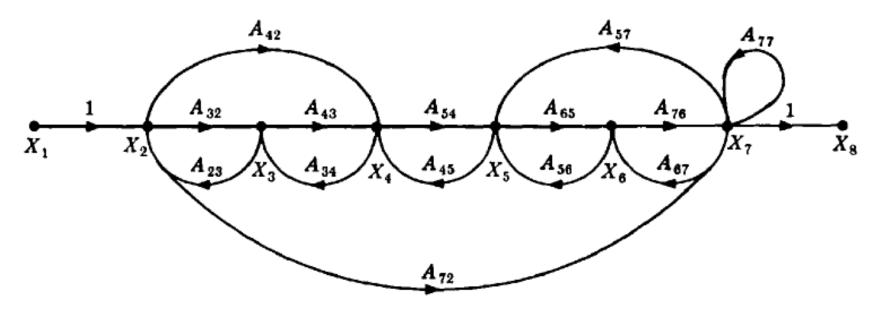
$$\begin{split} &\Delta = 1 - [G_2(s)H_1(s) + G_4(s)H_2(s) \\ &+ G_7(s)H_4(s) + G_2(s)G_3(s)G_4(s)G_5(s)G_6(s)G_7(s)G_8(s)] \\ &+ [G_2(s)H_1(s)G_4(s)H_2(s) + G_2(s)H_1(s)G_7(s)H_4(s) \\ &+ G_4(s)H_2(s)G_7(s)H_4(s)] \\ &- [G_2(s)H_1(s)G_4(s)H_2(s)G_7(s)H_4(s)] \end{split}$$

#### Eliminate forward path-1

$$\Delta_1 = 1 - G_7(s)H_4(s)$$



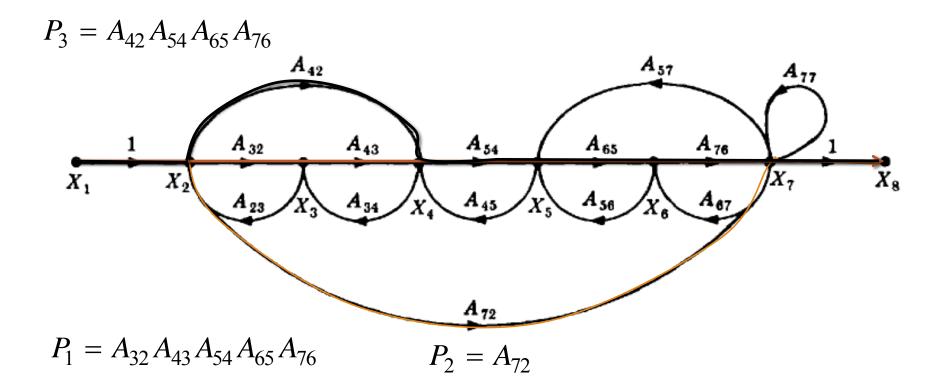
Example#4: Apply Mason's Rule to calculate the transfer function of the system represented by following Signal Flow Graph



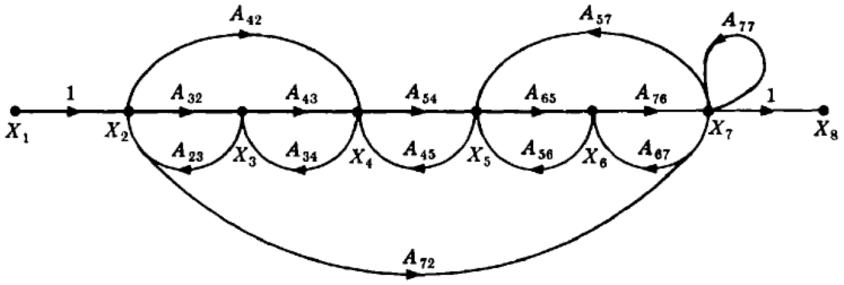
There are three forward paths, therefore n=3.

$$\frac{C(s)}{R(s)} = \frac{\sum_{i=1}^{3} P_i \Delta_i}{\Delta} = \frac{P_1 \Delta_1 + P_2 \Delta_2 + P_3 \Delta_3}{\Delta}$$

## Example#4: Forward Paths



### Example#4: Loop Gains of the Feedback Loops



$$L_1 = A_{32}A_{23}$$

$$L_2 = A_{43}A_{34}$$

$$L_3 = A_{54} A_{45}$$

$$L_4 = A_{65} A_{56}$$

$$L_5 = A_{76}A_{67}$$

$$L_6 = A_{77}$$

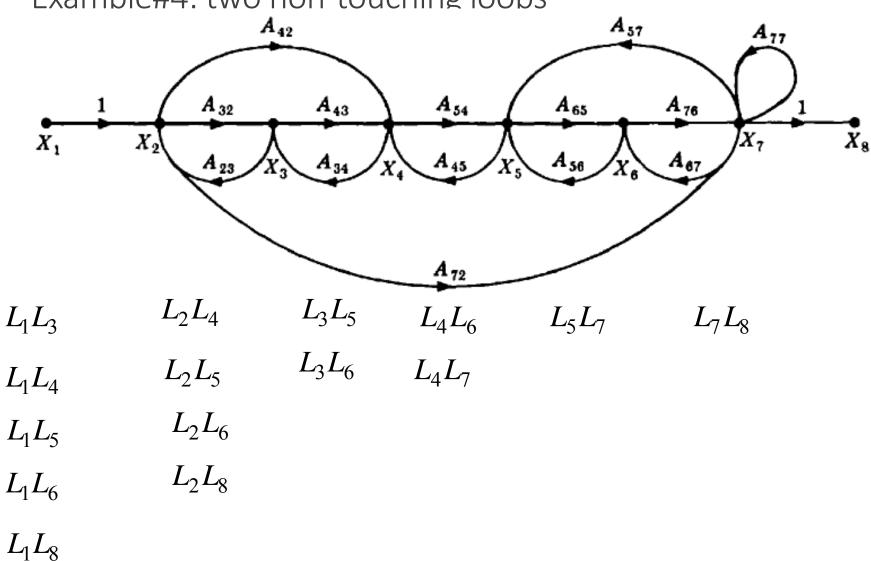
$$L_7 = A_{42} A_{34} A_{23}$$

$$L_8 = A_{65} A_{76} A_{67}$$

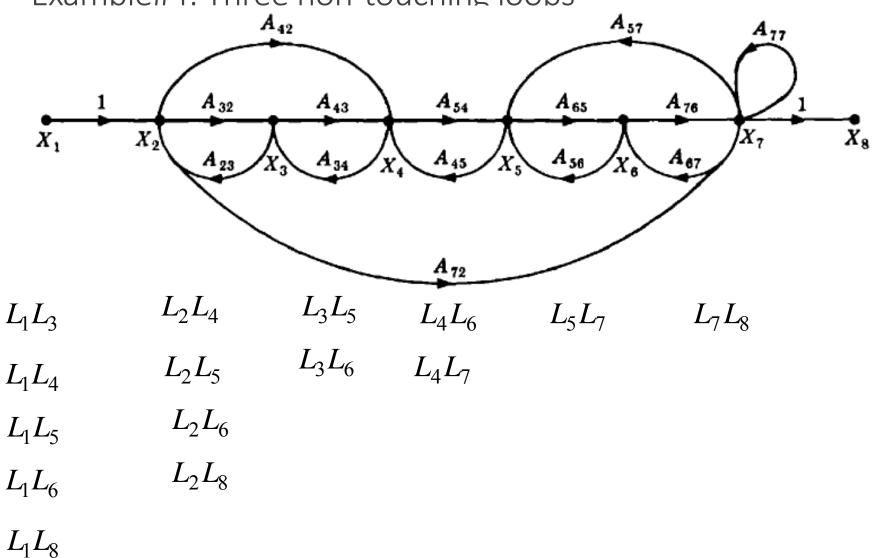
$$L_9 = A_{72} A_{57} A_{45} A_{34} A_{23}$$

$$L_{10} = A_{72} A_{67} A_{56} A_{45} A_{34} A_{23}$$





Example#4: Three non-touching loops



### Rules for Drawing of SFG from Block Diagram

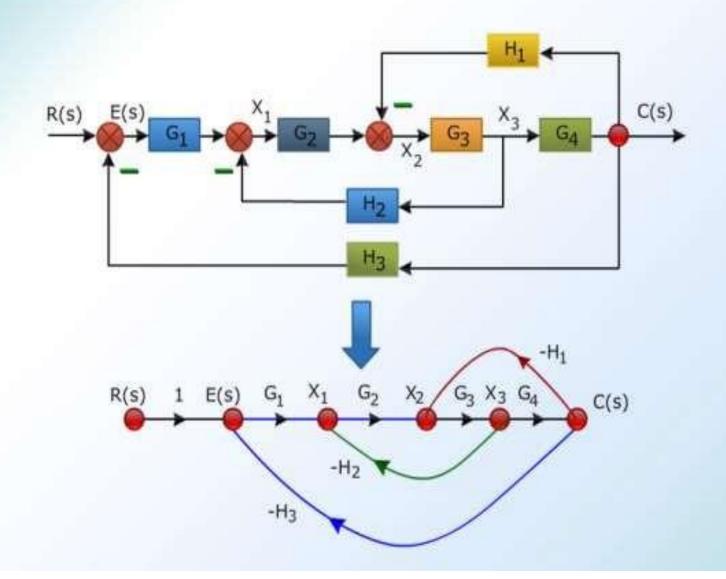
- All variables, summing points and take off points are represented by nodes
- If a summing point is placed before a take off point then the summing point and take off point shall be represented by a single node
- If a summing point is placed after a take off point then the summing point and take off point shall be represented by separate nodes connected by a branch having transmittance unity

### Converting Block Diagram to Signal-Flow Graph

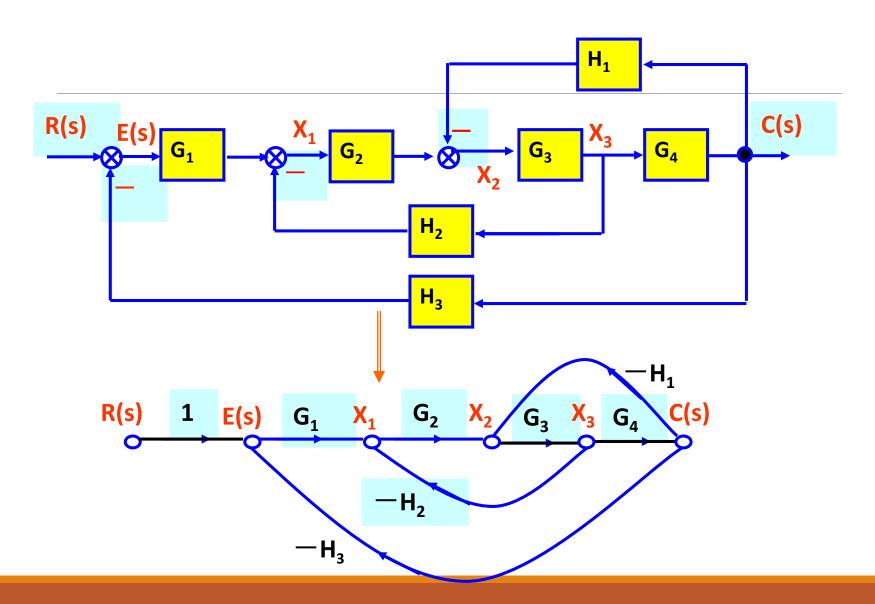
#### Procedure

- Assume nodes at input, output, at every summing point, at every branch point and in between cascaded blocks
- Draw the nodes separately as small circles and number the circles in the order 1, 2, 3.... or name them in terms of variables names
- From the block diagram find the gain between each node in the main forward path
- Connect all the corresponding circles by straight line and mark gain between the nodes
- Draw the feed forward paths between various nodes and mark the gain of feed forward path along with sign
- Draw the feedback paths between various nodes and mark the gain of feedback paths along with sign

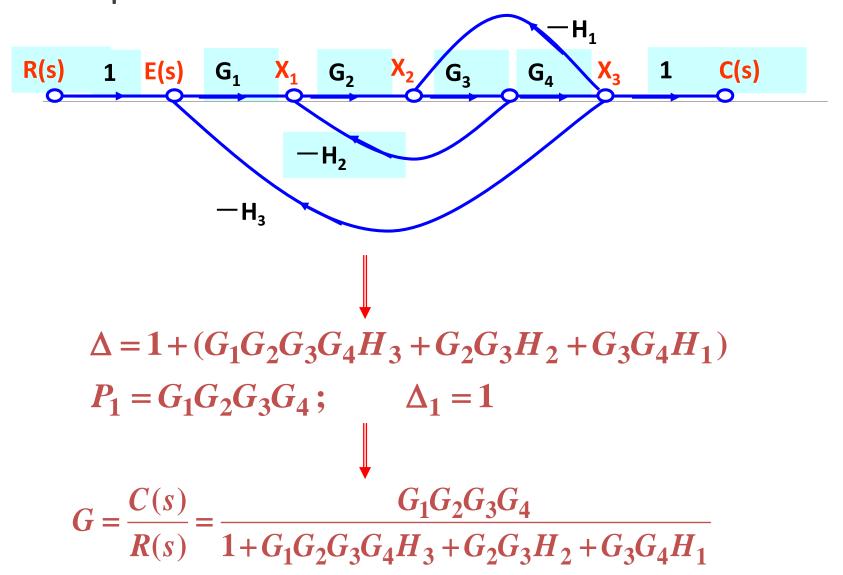
### From Block Diagram to Signal-flow Graph Models

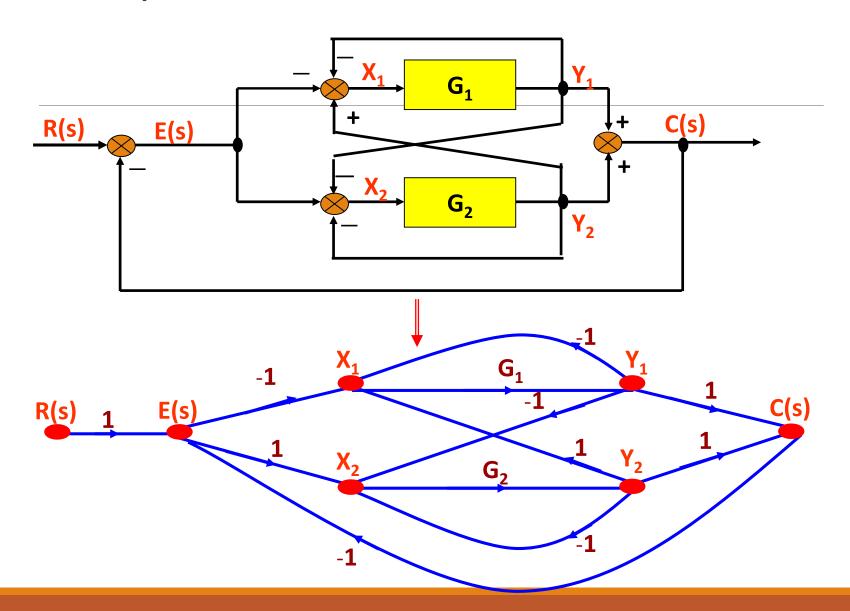


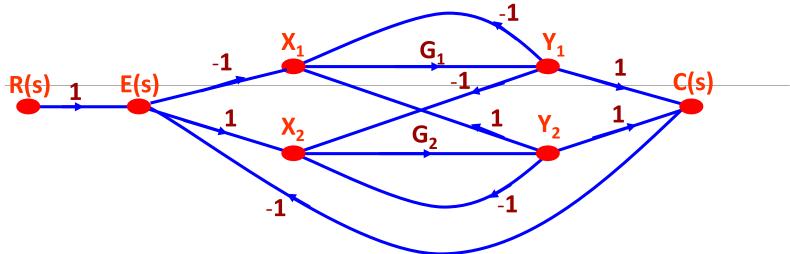
# From Block Diagram to Signal-Flow Graph Models Example#5



# From Block Diagram to Signal-Flow Graph Models Example#5





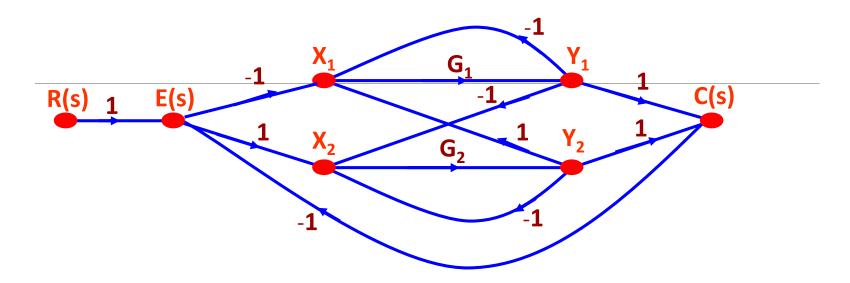


### 7 loops:

$$[G_1 \cdot (-1)]; \quad [G_2 \cdot (-1)]; \quad [G_1 \cdot (-1) \cdot G_2 \cdot 1]; \quad [(-1) \cdot G_1 \cdot 1 \cdot (-1)];$$
$$[(-1) \cdot G_1 \cdot (-1) \cdot G_2 \cdot 1 \cdot (-1)]; \quad [1 \cdot G_2 \cdot 1 \cdot (-1)]; \quad [1 \cdot G_2 \cdot 1 \cdot G_1 \cdot 1 \cdot (-1)].$$

## 3 '2 non-touching loops':

$$[G_1 \cdot (-1)] \cdot [G_2 \cdot (-1)];$$
  $[(-1) \cdot G_1 \cdot 1 \cdot (-1)] \cdot [G_2 \cdot (-1)];$   $[1 \cdot G_2 \cdot 1 \cdot (-1)] \cdot [G_1 \cdot (-1)].$ 



Then: 
$$\Delta = 1 + 2G_2 + 4G_1G_2$$

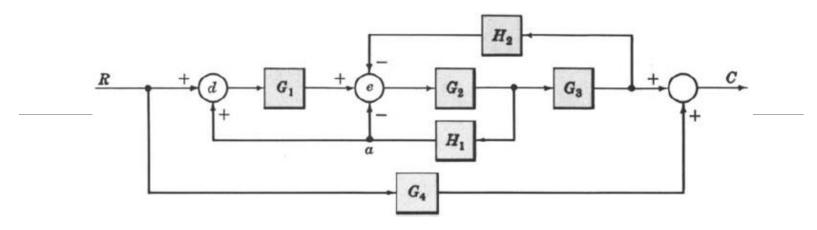
$$p_1 = (-1) \cdot G_1 \cdot 1$$
  $\Delta_1 = 1 + G_2$   
 $p_2 = (-1) \cdot G_1 \cdot (-1) \cdot G_2 \cdot 1$   $\Delta_2 = 1$   
 $p_3 = 1 \cdot G_2 \cdot 1$   $\Delta_3 = 1 + G_1$   
 $p_4 = 1 \cdot G_2 \cdot 1 \cdot G_1 \cdot 1$   $\Delta_4 = 1$ 

### We have

$$\frac{C(s)}{R(s)} = \frac{\sum p_k \Delta_k}{\Delta}$$

$$= \frac{G_2 - G_1 + 2G_1G_2}{1 + 2G_2 + 4G_1G_2}$$

**Example-7:** Determine the transfer function C/R for the block diagram below by signal flow graph techniques.



- The signal flow graph of the above block diagram is shown below.
- There are two forward paths. The path gains are

$$P_1 = G_1 G_2 G_3$$
 and  $P_2 = G_4$ 

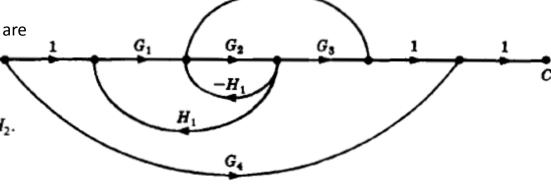
The three feedback loop gains are

$$P_{11} = -G_2H_1, P_{21} = G_1G_2H_1, P_{31} = -G_2G_3H_2.$$

No loops are non-touching, hence

$$\Delta = 1 - (P_{11} + P_{21} + P_{31})$$

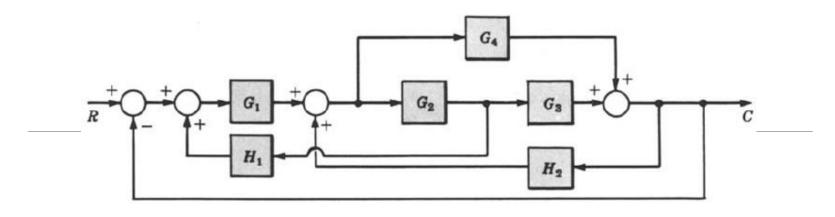
- Because the loops touch the nodes of P1, hence Δ<sub>1</sub> = 1
- Since no loops touch the nodes of P2, therefore  $\Delta_2 = \Delta$ .



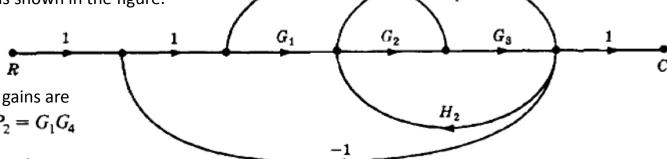
Hence the control ratio T = C/R is

$$T = \frac{P_1 \Delta_1 + P_2 \Delta_2}{\Delta} = \frac{G_1 G_2 G_3 + G_4 + G_2 G_4 H_1 - G_1 G_2 G_4 H_1 + G_2 G_3 G_4 H_2}{1 + G_2 H_1 - G_1 G_2 H_1 + G_2 G_3 H_2}$$

**Example-6**: Find the control ratio C/R for the system given below.



The signal flow graph is shown in the figure.



- The two forward path gains are  $P_1 = G_1 G_2 G_3$  and  $P_2 = G_1 G_4$
- The five feedback loop gains are  $P_{11} = G_1 G_2 H_1, P_{21} = G_2 G_3 H_2, P_{31} = -G_1 G_2 G_3,$  $P_{41} = G_4 H_2$ , and  $P_{51} = -G_1 G_4$ .
- All feedback loops touches the two forward
- paths, hence  $\Delta_1 = \Delta_2 = 1$

$$\frac{C}{R} = \frac{P_1 \Delta_1 + P_2 \Delta_2}{\Delta} = \frac{G_1 G_2 G_3 + G_1 G_4}{1 + G_1 G_2 G_3 - G_1 G_2 H_1 - G_2 G_3 H_2 - G_4 H_2 + G_1 G_4}$$

There are no non-touching loops, hence

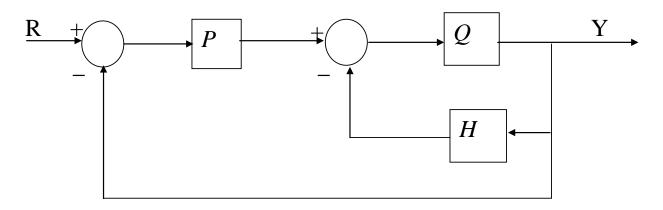
 $\Delta = 1 - (P_{11} + P_{21} + P_{31} + P_{41} + P_{51})$ 

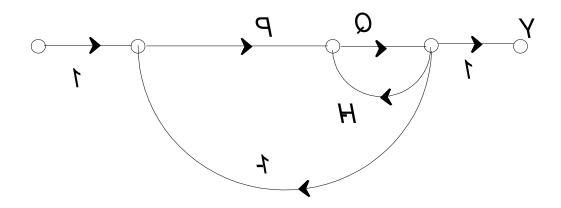
 $= 1 + G_1 G_2 G_3 - G_1 G_2 H_1 - G_2 G_3 H_2 - G_4 H_2 + G_1 G_4$ 

Hence the control ratio T =

### Example:

Determine the transfer function of Y(s)/R(s) the following block diagram.





$$L_1 = -Q.H$$
 and  $L_2 = -P.Q.1$ .

$$\sum L_i = L_1 + L_2 = -Q.H - P.Q.$$

$$\sum L_i L_j = 0$$
 etc.

$$\Delta = 1 - \sum L_i + \sum L_i L_j + \sum L_i L_j L_k - \dots = 1 + Q.H + P.Q$$

$$P_1 = 1.P.Q.1$$
,

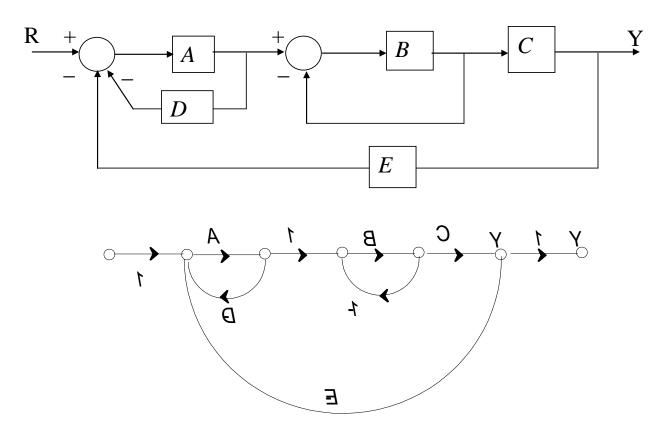
$$\Delta_1 = 1$$
.

Transfer function

$$\frac{Y}{R} = \frac{P.Q}{1 + Q.H + P.Q}$$

#### Example:

Determine Y(s)/R(s).



$$L_1 = -A.D$$
,  $L_2 = -1.B$  and  $L_3 = -A.1.B.C.E$ 

$$\sum L_i = L_1 + L_2 + L_3 = -A.D - B - A.B.C.E$$

$$\sum L_i L_j = L_1.L_2 = -A.D. - B = A.D.B$$

$$\sum L_i L_j L_k = 0$$

$$\Delta = I - \sum L_i + \sum L_i L_j + \sum L_i L_j L_k - \dots$$

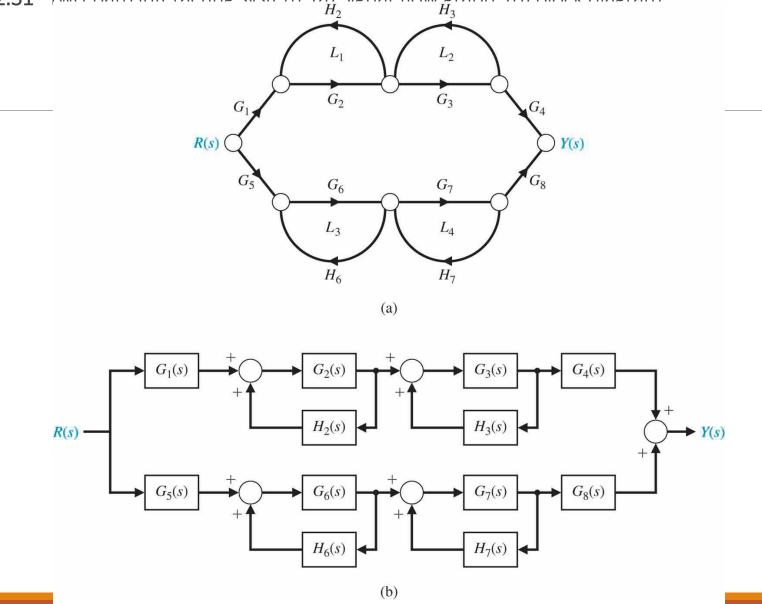
$$= I - [-AD - B - ABCE] + ADB$$

$$= I + AD + B + ABCE + ADB$$

$$\Delta_1 = 1$$

$$\frac{Y(S)}{R(s)} = \frac{ABC}{1 + AD + B + ABCE + ADB}$$

Figure 2.31 Two-nath interacting system (a) Signal-flow granh (h) Rlock diagram  $H_2$ 



$$P_1 = G_1 G_2 G_3 G_4$$
 (path 1)

$$P_2 = G_5 G_6 G_7 G_8$$
 (path 2)

There are four self loops:

$$L_1 = G_2H_2$$
,  $L_2 = H_3G_3$ ,  $L_3 = G_6H_6$ , and  $L_4 = G_7H_7$ 

Loops L<sub>1</sub> and L<sub>2</sub> do not touch L<sub>3</sub> and L<sub>4</sub>, 
$$\Delta = I - (L_1 + L_2 + L_3 + L_4) + (L_1 L_3 + L_1 L_4 + L_2 L_3 + L_2 L_4)$$

$$L_1 = L_2 = 0$$

Removing loops that touch path  $\stackrel{1}{\Delta}_I \stackrel{1}{=} I - (L_3 + L_4)$ 

$$L_3 = L_4 = 0$$

Removing loops that touch path 2,  $\Delta_2 = I - (L_1 + L_2)$ 

$$\frac{Y(s)}{R(s)} = \frac{P_1 \Delta_1 + P_2 \Delta_2}{\Delta}$$

$$= \frac{G_1 G_2 G_3 G_4 (1 - L_3 - L_4) + G_5 G_6 G_7 G_8 (1 - L_1 - L_2)}{1 - L_1 - L_2 - L_3 - L_4 + L_1 L_3 + L_1 L_4 + L_2 L_3 + L_2 L_4}$$

Using the block diagram,

$$Y_{I}(s) = G_{I}(s) \left[ \frac{G_{2}(s)}{1 - G_{2}(s)H_{2}(s)} \right] \left[ \frac{G_{3}(s)}{1 - G_{3}(s)H_{3}(s)} \right] G_{4}(s)R(s)$$

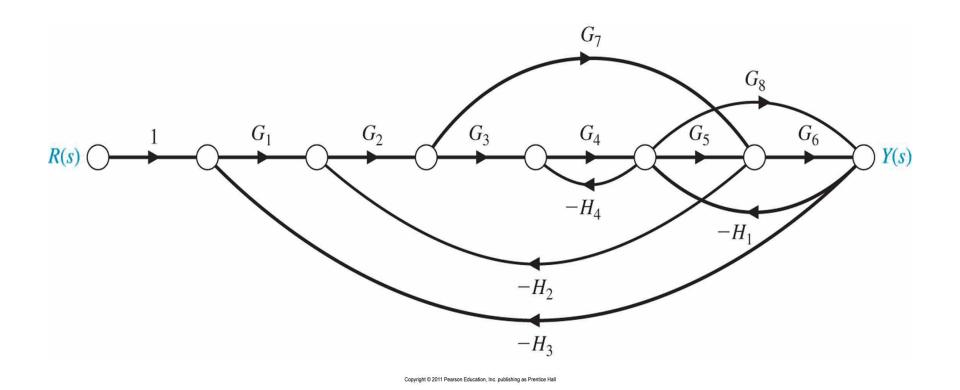
$$= \left[ \frac{G_{I}(s)G_{2}(s)G_{3}(s)G_{4}(s)}{\left(1 - G_{2}(s)H_{2}(s)\right)\left(1 - G_{3}(s)H_{3}(s)\right)} \right] R(s)$$

$$Y_{2}(s) = G_{5}(s) \left[ \frac{G_{6}(s)}{1 - G_{6}(s)H_{6}(s)} \right] \left[ \frac{G_{7}(s)}{1 - G_{7}(s)H_{7}(s)} \right] G_{8}(s)R(s)$$

$$= \left[ \frac{G_{5}(s)G_{6}(s)G_{7}(s)G_{8}(s)}{\left(1 - G_{6}(s)H_{6}(s)\right)\left(1 - G_{7}(s)H_{7}(s)\right)} \right] R(s)$$

$$Y(s) = Y_{1}(s) + Y_{2}(s) = \begin{bmatrix} G_{1}(s)G_{2}(s)G_{3}(s)G_{4}(s) \\ \hline (1 - G_{2}(s)H_{2}(s))(1 - G_{3}(s)H_{3}(s)) \\ + \dfrac{G_{5}(s)G_{6}(s)G_{7}(s)G_{8}(s)}{(1 - G_{6}(s)H_{6}(s))(1 - G_{7}(s)H_{7}(s))} \end{bmatrix} R(s)$$

Figure Multiple-loop system.



Find the paths,

$$P_{1} = G_{1}G_{2}G_{3}G_{4}G_{5}G_{6},$$

$$P_{2} = G_{1}G_{2}G_{7}G_{6},$$

$$P_{3} = G_{1}G_{2}G_{3}G_{4}G_{8}$$

Find the feedback loops:

$$\begin{split} L_1 &= -G_2 G_3 G_4 G_5 H_2, \ L_2 = -G_5 G_6 H_1, \ L_3 = -G_8 H_1, \ L_4 = -G_7 H_2 G_2, \\ L_5 &= -G_4 H_4, \ L_6 = -G_1 G_2 G_3 G_4 G_5 G_6 H_3, \ L_7 = -G_1 G_2 G_7 G_6 H_3, \\ L_8 &= -G_1 G_2 G_3 G_4 G_8 H_3 \end{split}$$

Loop  $L_5$  does not touch  $L_4$  or  $L_7$ , and loop  $L_3$  does not touch  $L_4$ 

$$\Delta = I - (L_1 + L_2 + L_3 + L_4 + L_5 + L_6 + L_7 + L_8) + (L_5 L_7 + L_5 L_4 + L_3 L_4)$$

$$\Delta_1 = \Delta_3 = 1$$
 and  $\Delta_2 = 1 - L_5 = 1 + G_4 H_4$ 

$$\frac{Y(s)}{R(s)} = \frac{P_1 + P_2 \Delta_2 + P_3}{\Delta}$$