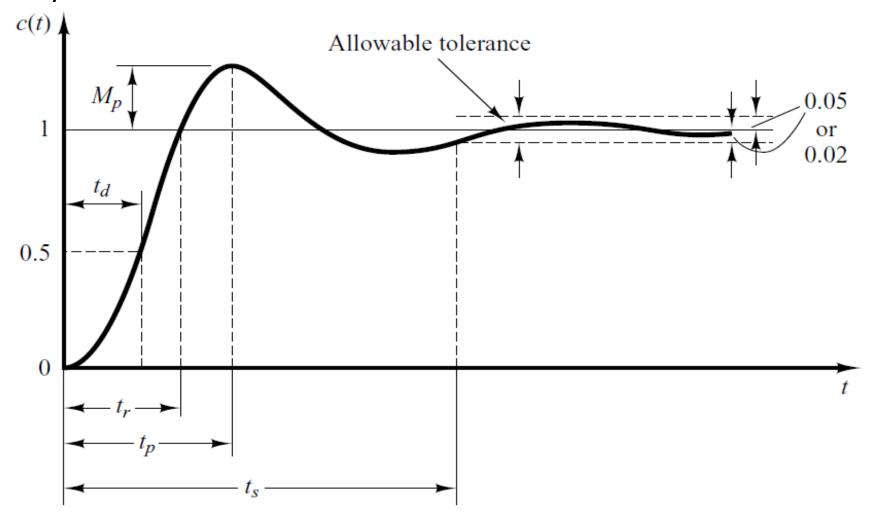
Time Domain Specifications of Underdamped system



Rise Time (t_r)

Response of Second Order System for under damped Case

$$C(t) = 1 - \frac{e^{-\xi \omega_n t}}{\sqrt{(1-\xi^2)}} \sin(\omega_d t + \theta)$$

At t =
$$t_r$$
, $C(t_r) = 1$

$$\Rightarrow C(t_r) = 1 - \frac{e^{-\xi \omega_n t_r}}{\sqrt{(1-\xi^2)}} \sin(\omega_d t_r + \theta) = 1$$

$$\Rightarrow -\frac{e^{-\xi\omega_n t_r}}{\sqrt{(1-\xi^2)}}\sin(\omega_d t_r + \theta) = 0$$

Rise Time (t_r)

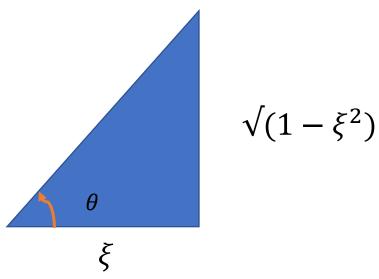
Since
$$\frac{e^{-\xi\omega_n t_r}}{\sqrt{(1-\xi^2)}} \neq 0$$

$$\Rightarrow \sin(\omega_d t_r + \theta) = 0$$

$$\Rightarrow \omega_d t_r + \theta = \pi$$

$$\rightarrow \omega_d \iota_r + \sigma - \pi$$

$$\xi$$
 => $t_r = \frac{\pi - \theta}{\omega_d}$ where $\theta = tan^{-1} \frac{\sqrt{(1 - \xi^2)}}{\xi}$ and $\omega_d = \omega_n \sqrt{(1 - \xi^2)}$



Peak Time (t_p)

Response of Second Order System for under damped Case

$$C(t) = 1 - \frac{e^{-\xi \omega_n t}}{\sqrt{(1-\xi^2)}} \sin(\omega_d t + \theta)$$

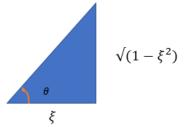
To get the Peak value,
$$\frac{d\mathbf{q}(t)}{dt} | t = t_p = 0$$

$$\frac{d\mathbf{C}(\mathsf{t})}{dt} = \frac{-e^{-\xi\omega_n t}}{\sqrt{(1-\xi^2)}} \left(-\xi\omega_n\right) \sin(\omega_d \mathsf{t} + \theta) + \frac{-e^{-\xi\omega_n t}}{\sqrt{(1-\xi^2)}} \left(\omega_d\right) \sin(\omega_d \mathsf{t} + \theta)$$

Peak Time (t_p)

$$\frac{d\mathbf{q}(t)}{dt} = \frac{-e^{-\xi\omega_n t}}{\sqrt{(1-\xi^2)}} \left(-\xi\omega_n\right) \sin(\omega_d t + \theta) + \frac{-e^{-\xi\omega_n t}}{\sqrt{(1-\xi^2)}} \left(\omega_d\right) \sin(\omega_d t + \theta)$$

Put
$$\omega_d$$
= $\omega_n \sqrt{(1-\xi^2)}$



$$\Rightarrow \frac{d\mathbf{q}(t)}{dt} = \frac{\omega_n e^{-\xi \omega_n t}}{\sqrt{(1-\xi^2)}} [(\xi) \sin(\omega_d t + \theta) - \sqrt{(1-\xi^2)} \sin(\omega_d t + \theta)]$$

$$\Rightarrow \frac{d\mathbf{q}(t)}{dt} = \frac{\omega_n e^{-\xi \omega_n t}}{\sqrt{(1-\xi^2)}} \left[\cos(\theta) \sin(\omega_d t + \theta) - \sin(\theta) \sin(\omega_d t + \theta) \right]$$

Peak Time (t_p)

$$\Rightarrow \frac{d\mathbf{c}(t)}{dt} = \frac{\omega_n e^{-\xi \omega_n t}}{\sqrt{(1-\xi^2)}} \left[\sin(\omega_d t + \theta - \theta) \right] = \frac{\omega_n e^{-\xi \omega_n t}}{\sqrt{(1-\xi^2)}} \sin(\omega_d t)$$

$$\frac{d\mathbf{q}(\mathbf{t})}{dt} \mid \mathbf{t} = \boldsymbol{t_p} = 0$$
Since $\frac{\omega_n e^{-\xi \omega_n t_p}}{\sqrt{(1-\xi^2)}} \neq 0 \implies \sin(\omega_d \, \boldsymbol{t_p}) = 0$

$$\Rightarrow \omega_d \ t_p = \pi$$
 $\Rightarrow t_p = \frac{\pi}{\omega_d} = \frac{\pi}{\omega_n \sqrt{(1-\xi^2)}}$

% Peak Overshoot (%
$$M_p$$
) = $\frac{c(t_p)-c(x)}{c(x)}$ * 100

From Response of Second Order System for under damped Case

$$C(t) = 1 - \frac{e^{-\xi\omega_n t}}{\sqrt{(1-\xi^2)}} \sin(\omega_d t + \theta)$$

$$=> C(\boldsymbol{t_p}) = 1 - \frac{e^{-\xi \omega_n t_p}}{\sqrt{(1-\xi^2)}} \sin(\omega_d \boldsymbol{t_p} + \theta)$$

Since
$$t_p = \frac{\pi}{\omega_d} = \frac{\pi}{\omega_n \sqrt{(1-\xi^2)}}$$

$$\Rightarrow C(t_p) = 1 - \frac{e^{-\xi \omega_n \frac{\pi}{\omega_n \sqrt{(1-\xi^2)}}}}{\sqrt{(1-\xi^2)}} \sin(\omega_d \frac{\pi}{\omega_d} + \theta)$$

$$C(\boldsymbol{t_p}) = 1 - \frac{e^{-\xi \frac{\pi}{\sqrt{(1-\xi^2)}}}}{\sqrt{(1-\xi^2)}} \sin(\pi + \theta)$$

But $\sin(\pi + \theta) = -\sin(\theta)$

$$C(t_p) = 1 + \frac{e^{-\xi \frac{\pi}{\sqrt{(1-\xi^2)}}}}{\sqrt{(1-\xi^2)}} \sin(\theta)$$

$$C(t_p) = 1 + \frac{e^{-\xi \frac{\pi}{\sqrt{(1-\xi^2)}}}}{\sqrt{(1-\xi^2)}} \sqrt{(1-\xi^2)}$$

$$C(\boldsymbol{t_p}) = 1 + e^{-\xi \frac{\pi}{\sqrt{(1-\xi^2)}}}$$
 And $C(\infty) = 1 - \frac{e^{-\xi \omega_n \infty}}{\sqrt{(1-\xi^2)}} \sin(\omega_d \propto + \theta) = 1 - 0 = 1$

% Peak Overshoot (%
$$M_p$$
) = $\frac{c(t_p)-c(x)}{c(x)}$ * 100

$$=\frac{1+e^{-\xi\frac{\pi}{\sqrt{(1-\xi^2)}}}-1}{1}*100$$

$$\% M_p = e^{-\xi \frac{\pi}{\sqrt{(1-\xi^2)}}} * 100$$

Settling Time (t_s)

The response of the second order system has two components

- 1. Decaying Exponential Component, $\frac{e^{-\xi \omega_n t}}{\sqrt{(1-\xi^2)}}$
- 2. Sinusoidal component, $sin(\omega_d t + \theta)$

For 2 % tolerance error band at t =
$$t_s$$
 , $\frac{e^{-\xi \omega_n t_s}}{\sqrt{(1-\xi^2)}}$ = 0.02

For Least Values of ξ , Denominator = 1

$$=>e^{-\xi\omega_n t_s}=0.02$$
 $=>-\xi\omega_n t_s=\ln(0.02)=-4$

Settling Time (t_s)

$$\Rightarrow -\xi \omega_n t_s = -4$$

$$\Rightarrow t_s = \frac{4}{\xi \omega_n}$$

Similarly for 5% error,

$$e^{-\xi \omega_n t_s} = 0.05$$
 => $-\xi \omega_n t_s = \ln(0.05) = -3$

$$\Rightarrow t_s = \frac{3}{\xi \omega_n}$$

Summary of Time Domain Specifications

Rise Time

$$t_r = \frac{\pi - \theta}{\omega_d} = \frac{\pi - \theta}{\omega_n \sqrt{1 - \zeta^2}}$$

Peak Time

$$t_p = \frac{\pi}{\omega_d} = \frac{\pi}{\omega_n \sqrt{1 - \zeta^2}}$$

Settling Time (2%)

$$t_s = 4T = \frac{4}{\zeta \omega_n}$$

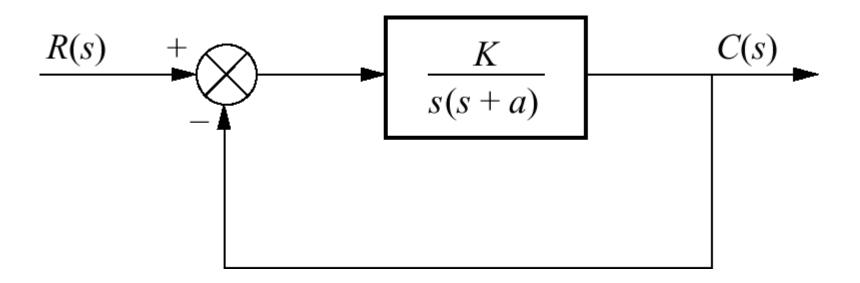
$$t_s = 3T = \frac{3}{\zeta \omega_n}$$

Settling Time (4%)

Maximum Overshoot

$$M_p = e^{-\frac{\pi \zeta}{\sqrt{1-\zeta^2}}} \times 100$$

Second-order feedback control system



The closed loop transfer function is
$$T(s) = \frac{K}{s^2 + as + K}$$

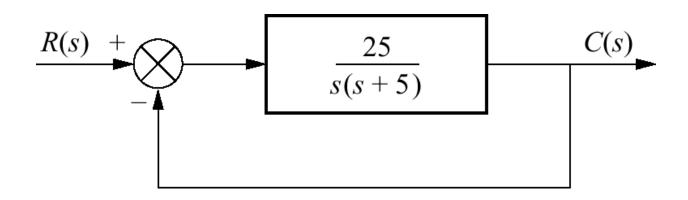
Note K is the amplifier gain, As K varies, the poles move through the three ranges of operations OD, CD, and UD

0<K<a²/4 system is over damped

 $K = a^2/4$ system is critically damped

 $K > a^2/4$ system is under damped

Finding transient response Example



Problem: For the system shown, find peak time, percent overshot, and settling time.

Solution: The closed loop transfer function is $T(s) = \frac{\Box 25}{\Box c}$

 $s^2 + 5s + 25$

And

$$\omega_n = \sqrt{25} = 5$$
 $2\xi\omega_n = 5$ so $\xi = 0.5$

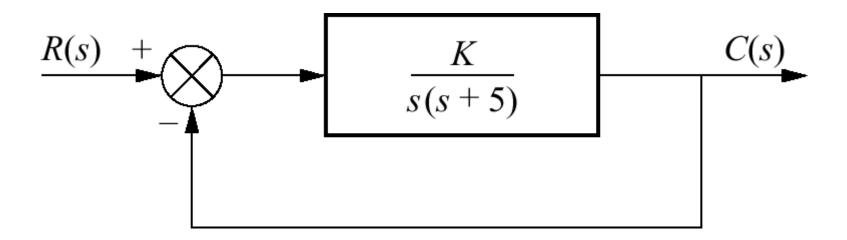
using values for ξ and ω_n and equation in chapter 4 we find

$$T_{p} = \frac{\Box \pi}{\omega_{n}} \sqrt{1 - \xi^{2}}$$
 sec

$$\% OS = e^{-\xi \pi / \sqrt{1 - \xi^{2}}} X \ 100 = 16.303$$

$$T_{s} = \frac{4}{\xi \omega_{n}} = 1.6$$
 sec
CIET- EE 311- LINEAR CONTROL SYSTEMS

Gain design for transient response Example



Problem: Design the value of gain K, so that the system will respond with a 10% overshot. $T(s) = \frac{\Box K}{s^2 + 5s + K}$

Solution: The closed loop transfer function is

$$\omega_n = \sqrt{K}$$
 and $2\xi\omega_n = 5$ thus $\xi = \frac{5}{2\sqrt{K}}$

For 10% OS we find $\xi = 0.591$

We substitute this value in previous equation to find K = 17.9

A unity feedback system has

$$G(s) = \frac{16}{s(s+5)}$$

If a step input is given calculate

- 1. Damping Ratio
- 2. Overshoot
- 3. Settling Time

Solution:
$$G(s) = \frac{16}{s(s+5)}$$
 $H(s) = 1$

Determine the closed loop transfer function

$$\frac{C(s)}{R(s)} = \frac{G}{1+GH} = \frac{\frac{16}{s(s+5)}}{1+\frac{16}{s(s+5)}} = \frac{\frac{16}{s^2+5s+16}}{s^2+5s+16}$$

Compare closed loop TF with standard form of second order system

$$\frac{\omega_{n}^{2}}{s^{2} + 2\xi\omega_{n}s + \omega_{n}^{2}} = \frac{16}{s^{2} + 5s + 16}$$

Compare denominators of both

Natural Frequency;

$$\omega_n^2 = 16$$

∴
$$\omega_n = 4 \ rad / sec$$

Damping Ratio;

$$2ξω ns = 5s$$

$$\therefore \xi = \frac{5}{2 \times \omega_n} = \frac{5}{2 \times 4} = 0.625$$

Settling Time;

$$T_s = \frac{4}{\xi \omega_n} = \frac{4}{(0.625) \times (4)} = 1.6 \text{ sec}$$

cont.....

Overshoot

$$\% M \qquad p = e^{-\left\{\frac{\xi\pi}{\sqrt{1-\xi}}\right\}_{1-\xi}^{2}} \times 100$$

%
$$M$$
 $p = e^{-\left\{\frac{(0.625)\pi}{\sqrt{1-(0.625)^2}}\right\}} \times 100$

$$\% M_p = 8.08\%$$

A unity feedback system has

$$G(s) = \frac{100}{s(s+5)}$$

If it is subjected to unit step input determine;

- 1. Damped frequency of oscillations
- 2. Time for first overshoot
- 3. Settling Time
- 4. Maximum Peak Overshoot



$$G(s) = \frac{100}{s(s+5)}$$

$$H(s)=1$$

Determine the closed loop transfer function

$$\frac{C(s)}{R(s)} = \frac{G}{1+GH} = \frac{\frac{100}{s(s+5)}}{1+\frac{100}{s(s+5)}} = \frac{100}{s^2 + 5s + 100}$$

Compare closed loop TF with standard form of second order system

$$\frac{\omega_n^2}{s^2 + 2\xi \omega_n s + \omega_n^2} = \frac{100}{s^2 + 5s + 100}$$

Compare denominators of both

Natural Frequency;

$$\omega_n^2 = 100$$

∴
$$\omega_n = 10 \text{ rad / sec}$$

cont.....

Damping Ratio;

$$2\xi\omega \, ns = 5s \qquad \qquad \therefore \xi = \frac{5}{2 \times \omega \, n} = \frac{5}{2 \times 10} = 0.25$$

Damped frequency of oscillations;

$$\omega_d = \omega_n \sqrt{1 - \xi^2}$$
 : $\omega_d = 10\sqrt{1 - (0.25)^2} = 9.68 \ rad \ / \sec$

Time for first overshoot (Peak Time);

$$T_p = \frac{\underline{\pi}}{\omega_d} = \frac{\underline{\pi}}{9.68} = 0.324 \text{ sec}$$

Settling Time;

$$T_s = 4T = \frac{4}{\xi \omega_n} = \frac{4}{(0.25) \times (10)} = 1.6$$
 sec

cont.....

Maximum Peak Overshoot

$$\% M \qquad p = e^{-\left\{\frac{\xi\pi}{\sqrt{1-\xi}}\right\}_{1-\xi}^{2}} \times 100$$

$$\% M \qquad p = e^{-\left\{\frac{(0.25)\pi}{\sqrt{1-(0.25)^2}}\right\}} \times 100$$

$$\% M_p = 44.48\%$$

For the unity feedback control system having open loop transfer function

$$G(s) = \frac{10}{s(s+4)}$$

Determine;

- 1. Delay Time
- 2. Rise Time
- 3. Peak Time
- 4. Settling Time
- 5. Maximum Peak Overshoot

$$G(s) = \frac{10}{s(s+4)}$$

$$H(s)=1$$

Determine the closed loop transfer function

$$\frac{C(s)}{R(s)} = \frac{G}{1+GH} = \frac{\frac{10}{s(s+4)}}{1+\frac{10}{s(s+4)}} = \frac{10}{s^2 + 4s + 10}$$

Compare closed loop TF with standard form of second order system

$$\frac{\omega_n^2}{s^2 + 2\xi \omega_n s + \omega_n^2} = \frac{10}{s^2 + 4s + 10}$$

Compare denominators of both

Natural Frequency;

$$\omega_n^2 = 10$$

∴
$$\omega_n = 3.16 \quad rad \mid sec$$

Damping Ratio;

$$2ξω ns = 4s$$

$$\therefore \xi = \frac{4}{2 \times \omega_n} = \frac{4}{2 \times 3.16} = 0.633$$

Damped frequency of oscillations;

$$\omega_d = \omega_n \sqrt{1 - \xi^2}$$

$$\therefore \omega_d = 3.16\sqrt{1 - (0.633)^2} = 2.44 \ rad \ / \sec$$

Delay Time;

$$T_d = \frac{1+0.7\xi}{\Omega_n} = \frac{1+0.7(0.633)}{3.16} = 0.457$$
 sec

cont.....

Rise Time;

$$\beta = \tan^{-1} \frac{\sqrt{1-\xi^{-2}}}{\xi} = \tan^{-1} \frac{\sqrt{1-(0.633)}}{(0.633)} = 0.885$$
 rad

$$T_r = \frac{\pi - \beta}{\omega_d} = \frac{\pi - 0.885}{(0.244)} = 0.92$$
 sec

Peak Time;

$$T_p = \frac{\pi}{\omega_d} = \frac{\pi}{2.44} = 1.273$$
 sec

Settling Time;

$$T_s = 4T = \frac{4}{\xi \omega_n} = \frac{4}{(0.633) \times (3.16)} = 1.997$$
 sec

cont.....

Maximum Peak Overshoot

$$\% M \qquad p = e^{-\left\{\frac{\xi\pi}{\sqrt{1-\xi}}\right\}} \times 100$$

$$\% M \qquad p = e^{-\left\{\frac{-(0.633)\pi}{\sqrt{1-(0.633)^2}}\right\}} \times 100$$

$$\% M_p = 7.66\%$$

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A second order servo system has a unity feedback,

$$G(s) = \frac{500}{s(s+15)}$$

Determine;

- 1. Delay Time
- 2. Rise Time
- 3. Peak Time
- 4. Settling Time
- 5. Maximum Peak Overshoot

$$G(s) = \frac{500}{s(s+15)}$$

$$H(s)=1$$

Determine the closed loop transfer function

$$\frac{C(s)}{R(s)} = \frac{G}{1+GH} = \frac{\frac{500}{s(s+15)}}{1+\frac{500}{s(s+15)}} = \frac{500}{s^2 + 15s + 500}$$

Compare closed loop TF with standard form of second order system

$$\frac{\omega_n^2}{s^2 + 2\xi \omega_n s + \omega_n^2} = \frac{500}{s^2 + 15s + 500}$$

By comparing denominators of both

Natural Frequency;

$$\omega_{n}^{2} = 500$$

∴
$$\omega_n = 22.36 \quad rad / sec$$

cont.....

Damping Ratio;

$$2ξω ns = 15s$$

$$\therefore \xi = \frac{15}{2 \times \omega_n} = \frac{15}{2 \times 22.36} = 0.335$$

Damped frequency of oscillations;

$$\omega_d = \omega_n \sqrt{1 - \xi^2}$$

$$\therefore \omega_d = 22.36\sqrt{1 - (0.335)^2} = 21.06 \ rad \ / \sec$$

Delay Time;

$$T_d = \frac{1+0.7\xi}{\omega_n} = \frac{1+0.7(0.335)}{22.36} = 0.055 \text{ sec}$$

cont.....

Rise Time;

$$\beta = \tan^{-1} \frac{\sqrt{1-\xi^{2}}}{\xi} = \tan^{-1} \frac{\sqrt{1-(0.335)}^{2}}{(0.335)} = 1.229 \text{ rad}$$

$$T_r = \frac{\pi - \beta}{\omega_d} = \frac{\pi - 1.229}{(21.06)} = 0.091$$
 sec

Peak Time;

$$T_p = \frac{\pi}{\omega_d} = \frac{\pi}{21.06} = 32.73 \text{ sec}$$

Settling Time;

$$T_s = 4T = \frac{4}{\xi \omega_n} = \frac{4}{(0.335) \times (22.36)} = 0.534$$
 sec

cont.....

Maximum Peak Overshoot

$$\% M \qquad p = e^{-\left\{\frac{\xi\pi}{\sqrt{1-\xi}}\right\}_{1-\xi}^{2}} \times 100$$

%
$$M$$
 $p = e^{-\left\{\frac{(0.335)\pi}{\sqrt{1-(0.335)^2}}\right\}} \times 100$

$$\% M_p = 32.75\%$$

The open loop transfer function of a unity feedback system is,

$$G(s) = \frac{4}{s(s+1)}$$

Determine;

- 1. Delay Time
- 2. Rise Time
- 3. Peak Time
- 4. Settling Time
- 5. Maximum Peak Overshoot

$$G(s) = \frac{4}{s(s+1)}$$

$$H(s)=1$$

Determine the closed loop transfer function

$$\frac{C(s)}{R(s)} = \frac{G}{1+GH} = \frac{\frac{4}{s(s+1)}}{1+\frac{4}{s(s+1)}} = \frac{4}{s^2+s+4}$$

Compare closed loop TF with standard form of second order system

$$\frac{\omega_n^2}{s^2 + 2\xi\omega_n s + \omega_n^2} = \frac{4}{s^2 + s + 4}$$

By comparing denominators of both

Natural Frequency;

$$\omega_n^2 = 4$$
 $\therefore \omega_n = 2 \ rad \ / \sec$

Damping Ratio;

$$2\xi\omega \, ns = s \qquad \qquad \therefore \xi = \frac{1}{2 \times \omega \, n} = \frac{1}{2 \times 2} = 0.25$$

Damped frequency of oscillations;

$$\omega_d = \omega_n \sqrt{1 - \xi^2}$$
 $\therefore \omega_d = 2\sqrt{1 - (0.25)^2} = 1.936 \ rad \ / \sec$

Delay Time;

$$T_d = \frac{1+0.7\xi}{\omega_n} = \frac{1+0.7(0.25)}{2} = 0.587 \text{ sec}$$

cont.....

Rise Time;

$$\beta = \tan^{-1}$$
 $\frac{\sqrt{1-\xi^{2}}}{\xi} = \tan^{-1}$ $\frac{\sqrt{1-(0.25)}^{2}}{(0.25)} = 1.310$ rad

$$T_r = \frac{\pi - \beta}{\omega_d} = \frac{\pi - 1.310}{(1.936)} = 0.945$$
 sec

Peak Time;

$$T_p = \frac{\pi}{\omega_d} = \frac{\pi}{1.936} = 1.622 \text{ sec}$$

Settling Time;

$$T_s = 4T = \frac{4}{\xi \omega_n} = \frac{4}{(0.25) \times (2)} = 8 \sec$$

cont.....

Maximum Peak Overshoot

$$\% M \qquad p = e^{-\left\{\frac{\xi\pi}{\sqrt{1-\xi}}\right\}_{1-\xi}^{2}} \times 100$$

$$\% M \qquad p = e^{-\left\{\frac{-(0.25)\pi}{\sqrt{1-(0.25)^2}}\right\}} \times 100$$

$$\% M_p = 43.26\%$$

The open loop transfer function of a unity feedback system is,

$$G(s) = \frac{25}{s(s+5)}$$

Determine;

- 1. Delay Time
- 2. Rise Time
- 3. Peak Time
- 4. Settling Time
- 5. Maximum Peak Overshoot

$$G(s) = \frac{25}{s(s+5)}$$

$$H(s)=1$$

Determine the closed loop transfer function

$$\frac{C(s)}{R(s)} = \frac{G}{1+GH} = \frac{\frac{25}{s(s+5)}}{1+\frac{25}{s(s+5)}} = \frac{25}{s^2 + 5s + 25}$$

Compare closed loop TF with standard form of second order system

$$\frac{\omega_n^2}{s^2 + 2\xi \omega_n s + \omega_n^2} = \frac{25}{s^2 + 5s + 25}$$

By comparing denominators of both

Natural Frequency;

$$\omega_n^2 = 25$$
 $\therefore \omega_n = 5 \quad rad \mid sec$

Damping Ratio;

$$2ξω ns = 5s$$

$$\therefore \xi = \frac{5}{2 \times \omega_n} = \frac{5}{2 \times 5} = 0.5$$

Damped frequency of oscillations;

$$\omega_d = \omega_n \sqrt{1 - \xi^2}$$

$$\therefore \omega_d = 5\sqrt{1 - (0.5)^2} = 4.33 \ rad \ / \sec$$

Delay Time;

$$T_d = \frac{1+0.7\xi}{\omega_n} = \frac{1+0.7(0.5)}{5} = 0.27 \text{ sec}$$

cont.....

Rise Time;

$$\beta = \tan^{-1} \frac{\sqrt{1-\xi^2}}{\xi} = \tan^{-1} \left[\frac{\sqrt{(0.5)}}{(0.5)} \right]^{-2} = 1.24 \text{ rad}$$

$$T_r = \frac{\pi - \beta}{\omega_d} = \frac{\pi - 1.04}{(4.330)} = 0.485$$
 sec

Peak Time;

$$T_p = \frac{\pi}{\omega_d} = \frac{\pi}{4.330} = 0.725 \quad \text{sec}$$

Settling Time;

$$T_s = 4T = \frac{4}{\xi \omega_n} = \frac{4}{(0.5) \times (5)} = 1.6$$
 sec

cont.....

Maximum Peak Overshoot

%
$$M$$

$$p = e^{-\frac{\xi \pi}{\sqrt{1-\xi^2}}} \times 100$$

$$\% M \qquad p = e^{-\left\{\frac{-(0.5)\pi}{\sqrt{1-(0.5)^2}}\right\}} \times 100$$

$$\% M_p = 16.30\%$$

The closed loop transfer function of a unity feedback system is,

$$\frac{C(s)}{R(s)} = \frac{10}{s^2 + 4s + 5}$$

Determine;

- 1. Delay Time
- 2. Rise Time
- 3. Peak Time
- 4. Settling Time
- 5. Maximum Peak Overshoot

Solution:

The given closed loop transfer function is,

$$\frac{C(s)}{R(s)} = \frac{10}{s^2 + 4s + 5}$$

Compare closed loop TF with standard form of second order system

$$\frac{\omega^{n^2}}{s^2 + 2\xi \omega_{n}s + \omega^{n^2}} = \frac{10}{s^2 + 4s + 5}$$

By comparing denominators of both

Natural Frequency;

$$\omega_n^2 = 5$$
 $\therefore \omega_n = 2.23$ rad / sec

Damping Ratio;

$$2\xi\omega ns = 4s$$

$$\therefore \xi = \frac{4}{2 \times \omega_n} = \frac{4}{2 \times 2.23} = 0.896$$

Damped frequency of oscillations;

$$\omega_d = \omega_n \sqrt{1 - \xi^2}$$

$$\therefore \omega_d = 2.23\sqrt{1 - (0.896)^2} = 0.99 \ rad \ / \sec$$

Delay Time;

$$T_d = \frac{1+0.7\xi}{\omega_n} = \frac{1+0.7(0.896)}{2.23} = 0.72 \text{ sec}$$

cont.....

Rise Time;

$$\beta = \tan^{-1} \frac{\sqrt{1-\xi^{2}}}{\xi} = \tan^{-1} \left[\frac{\sqrt{(0.896)}}{(0.896)} \right]^{2} = 0.46 \text{ rad}$$

$$T_r = \frac{\pi - \beta}{\omega_d} = \frac{\pi - 0.46}{(0.99)} = 2.70$$
 sec

Peak Time;

$$T_p = \frac{\pi}{\omega_d} = \frac{\pi}{0.99} = 2.1515 \text{ sec}$$

Settling Time;

$$T_s = 4T = \frac{4}{\xi \omega_n} = \frac{4}{(0.896) \times (2.23)} = 2.00$$
 sec

cont.....

Maximum Peak Overshoot

$$\% M \qquad p = e^{-\left\{\frac{\xi\pi}{\sqrt{1-\xi}}\right\}} \times 100$$

$$\% M \qquad p = e^{-\left\{\frac{-(0.896)\pi}{\sqrt{1-(0.896)^2}}\right\}} \times 100$$

$$\% M_p = 0.17\%$$

The closed loop transfer function of a unity feedback system is,

$$\frac{C(s)}{R(s)} = \frac{100}{s^2 + 15s + 100}$$

Determine;

- 1. Delay Time
- 2. Rise Time
- 3. Peak Time
- 4. Settling Time
- 5. Maximum Peak Overshoot

Solution:

The given closed loop transfer function is,

$$\frac{C(s)}{R(s)} = \frac{100}{s^2 + 15s + 100}$$

Compare closed loop TF with standard form of second order system

$$\frac{\omega_n^2}{s^2 + 2\xi \omega_n s + \omega_n^2} = \frac{100}{s^2 + 15s + 100}$$

By comparing denominators of both

Natural Frequency;

$$\omega_n^2 = 100$$
 $\therefore \omega_n = 10 \quad rad \mid sec$

Damping Ratio;

$$2\xi\omega \, _{n}s = 15s$$
 $\therefore \xi = \frac{15}{2 \times \omega _{n}} = \frac{15}{2 \times 10} = 0.75$

Damped frequency of oscillations;

$$\omega_d = \omega_n \sqrt{1 - \xi^2}$$
 $\therefore \omega_d = 10\sqrt{1 - (0.75)^2} = 6.61 \ rad \ / \sec$

Delay Time;

$$T_d = \frac{1+0.7\xi}{\omega_n} = \frac{1+0.7(0.75)}{10} = 0.135 \text{ sec}$$

cont.....

Rise Time;

$$\beta = \tan^{-1} \frac{\sqrt{1-\xi^{2}}}{\xi} = \tan^{-1} \left[\frac{\sqrt{(0.75)}}{(0.75)} \right]^{2} = 0.722 \text{ rad}$$

$$T_r = \frac{\pi - \beta}{\omega_d} = \frac{\pi - 0.722}{(6.61)} = 0.365$$
 sec

Peak Time;

$$T_p = \frac{\underline{\pi}}{\omega_d} = \frac{\underline{\pi}}{6.61} = 0.474 \text{ sec}$$

Settling Time;

$$T_s = 4T = \frac{4}{\xi \omega_n} = \frac{4}{(0.75) \times (10)} = 0.533$$
 sec

cont.....

Maximum Peak Overshoot

$$\% M \qquad p = e^{-\left\{\frac{\xi\pi}{\sqrt{1-\xi}}\right\}_{1-\xi}^{2}} \times 100$$

$$\% M \qquad p = e^{-\left\{\frac{-(0.75)\pi}{\sqrt{1-(0.75)^2}}\right\}} \times 100$$

$$\% M_p = 2.83\%$$

The closed loop transfer functions of certain second order unity feedback control system is,

$$\frac{C(s)}{R(s)} = \frac{8}{s^2 + 3s + 8}$$

Determine the type of damping in the system.

Solution:

The given closed loop transfer function is,

$$\frac{C(s)}{R(s)} = \frac{8}{s^2 + 3s + 8}$$

Compare closed loop TF with standard form of second order system

$$\frac{\omega_n^2}{s^2 + 2\xi \omega_n s + \omega_n^2} = \frac{8}{s^2 + 3s + 8}$$

By comparing denominators of both

Natural Frequency;
$$\omega_n^2 = 8$$

$$\therefore \omega_n = 2.82 \quad rad \mid sec$$

Damping Ratio;
$$2\xi\omega ns = 3s$$
 $\therefore \xi = \frac{3}{2\times\omega n} = \frac{3}{2\times2.82} = 0.53$

Since $\xi < 1$, it is an underdamped system.

The closed loop transfer functions of certain second order unity feedback control system is,

$$\frac{C(s)}{R(s)} = \frac{2}{s^2 + 4s + 2}$$

Determine the type of damping in the system.

Solution:

The given closed loop transfer function is,

$$\frac{C(s)}{R(s)} = \frac{2}{s^2 + 4s + 2}$$

Compare closed loop TF with standard form of second order system

$$\frac{\omega^{2}}{s^{2} + 2\xi \omega_{n}s + \omega^{2}} = \frac{2}{s^{2} + 4s + 2}$$

By comparing denominators of both

$$\omega_n^2 = 2$$

Natural Frequency;
$$\omega_n^2 = 2$$
 $\therefore \omega_n = 1.414$ rad / sec

$$2\xi\omega$$
 $ns=4s$

$$2\xi\omega \, ns = 4s$$
 $\therefore \xi = \frac{4}{2 \times \omega \, n} = \frac{4}{2 \times 1.414} = 1.41$

Since $\xi > 1$, it is an overdamped system.

The closed loop transfer functions of certain second order unity feedback control system is,

$$\frac{C(s)}{R(s)} = \frac{2}{s^2 + 2s + 1}$$

Determine the type of damping in the system.

Solution:

The given closed loop transfer function is,

$$\frac{C(s)}{R(s)} = \frac{2}{s^2 + 2s + 1}$$

Compare closed loop TF with standard form of second order system

$$\frac{\omega^{2}}{s^{2} + 2\xi \omega ns + \omega^{2}} = \frac{2}{s^{2} + 2s + 1}$$

By comparing denominators of both

$$\omega_n^2 = 1$$

Natural Frequency;
$$\omega_n^2 = 1$$
 $\therefore \omega_n = 1$ rad / sec

$$2\xi\omega \, _{n}s=2s$$

$$2\xi\omega_n s = 2s \qquad \therefore \xi = \frac{2}{2\times\omega_n} = \frac{2}{2\times1} = 1$$

Since $\xi = 1$, it is an critically damped system.

The closed loop transfer functions of certain second order unity feedback control system is,

$$\frac{C(s)}{R(s)} = \frac{2}{s^2 + 4}$$

Determine the type of damping in the system.

Solution:

The given closed loop transfer function is,

$$\frac{C(s)}{R(s)} = \frac{2}{s^2 + 4}$$

Compare closed loop TF with standard form of second order system

$$\frac{\omega_n^2}{s^2 + 2\xi \omega_n s + \omega_n^2} = \frac{2}{s^2 + 4}$$

By comparing denominators of both

$$\omega_n^2 = 4$$

Natural Frequency;
$$\omega_n^2 = 4$$
 $\therefore \omega_n = 2 \ rad \ / sec$

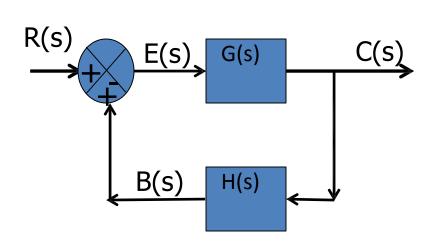
$$2\xi\omega \, ns = 0$$
 $\therefore \xi = 0$

$$\therefore \xi = 0$$

Since $\xi = 0$, it is an undamped system.

Derivation of Steady State Error

The steady state response is important to judge the accuracy of the output. The difference between the steady state response and desired reference gives the steady state error.



For given figure,

$$E(s) = R(s) - B(s)$$

But

$$B(s) = C(s).H(s)$$

E(s) =
$$R(s) - C(s)$$
.H(s)
But
 $C(s) = G(s)$.E(s)
 $E(s) = R(s) - G(s)$.E(s).H(s)
 $R(s) = E(s) + G(s)$.E(s).H(s)
 $R(s) = E(s)\{1 + G(s)$.H(s)\}
 $E(s) = \frac{R(s)}{1 \pm G(s)}$.H(s)

Derivation of Steady State Error

In time domain,

$$e(t) = L^{-1} E(s)$$

and is the expression of error valid for all time. Steady state error is defined as,

$$e_{ss}(t) = \lim_{t \to \infty} e(t)$$

From the final value theorem in Laplace transform,

$$e_{ss}(t) = \lim_{s \to 0} sE(s)$$

Steady state error,

$$e_{ss}(t) = \lim_{s \to 0} sE(s)$$

$$e_{ss}(t) = \lim_{s\to 0} \frac{sR(s)}{1+G(s) H(s)}$$

Steady state error for step input:

A step input of magnitude A is applied,

$$r(t) = A. u(t)$$
 $t>0$
= 0 $t<0$

Taking Laplace transform,

$$R(s) = L\{r(t)\} = L\{A\} = \frac{A}{s}$$

Steady state error,

$$e_{ss}(t) = \lim_{s\to 0} \frac{sR(s)}{1+G(s) H(s)}$$

Steady state error for step input:

$$e_{ss}(t) = \lim_{s \to 0} \frac{\frac{A}{s}}{1 + G(s) H(s)}$$

$$e_{ss}(t) = \lim_{s \to 0} \frac{A}{1 + G(s) H(s)}$$

$$e_{ss}(t) = \frac{A}{1 + \lim_{s \to 0} G(s) H(s)}$$

$$e_{ss}(t) = \frac{A}{1 + K_p}$$

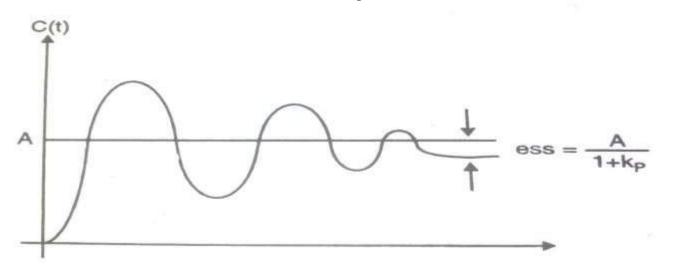
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Steady state error for step input:

The position error constant Kp of a system is defined as,

$$K_p = \lim_{s \to 0} G(s). H(s)$$

When a step input of magnitude A is given, in response to this gives $e_{ss}(t) = \frac{A}{1 + K_p}$ steady state error



*Kp depends
on type of
system

Steady state error for ramp input:

A ramp input of slope A is applied,

$$r(t) = A.t$$
 $t>0$ $t<0$

Taking Laplace transform,

$$R(s) = L\{r(t)\} = L\{At\} = \frac{A}{s^2}$$

Steady state error,

$$e_{ss}(t) = \lim_{s\to 0} \frac{sR(s)}{1+G(s) H(s)}$$

Steady state error for ramp input:

$$e_{ss}(t) = \lim_{s \to 0} \frac{s \frac{A}{s^2}}{1 + G(s) H(s)}$$

$$e_{ss}(t) = \lim_{s \to 0} \frac{\frac{A}{s}}{1 + G(s) H(s)}$$

$$e_{ss}(t) = \lim_{s\to 0} \frac{A}{s + sG(s)H(s)}$$

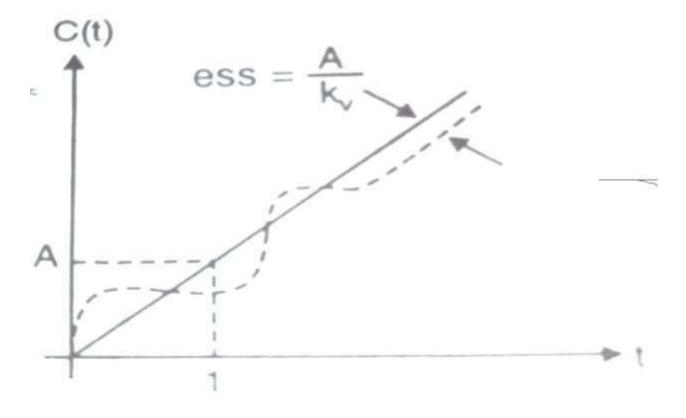
$$e_{ss}(t) = \frac{A}{0 + \lim_{s \to 0} sG(s) H(s)}$$

$$e_{ss}(t) = \frac{\underline{A}}{K_{v}}$$

Steady state error for ramp input:

The velocity error constant Kv of a system is defined as,

$$K_v = \lim_{s\to 0} sG(s). H(s)$$



Steady state error for parabolic input:

A parabolic input of slope coefficient A/2 is applied,

Taking Laplace transform,

$$R(s) = L\{r(t)\} = L\{\frac{A}{2} t^2\} = \frac{A}{s^3}$$

Steady state error,

$$e_{ss}(t) = \lim_{s \to 0} \frac{sR(s)}{1 + G(s) H(s)}$$

Steady state error for parabolic input:

$$e_{ss}(t) = \lim_{s \to 0} \frac{s \frac{A}{s^3}}{1 + G(s) H(s)}$$

$$e_{ss}(t) = \lim_{s \to 0} \frac{\frac{A}{s^2}}{1 + G(s) \text{ H(s)}}$$

$$e_{ss}(t) = \lim_{s \to 0} \frac{A}{s^2 + s^2 G(s) H(s)}$$

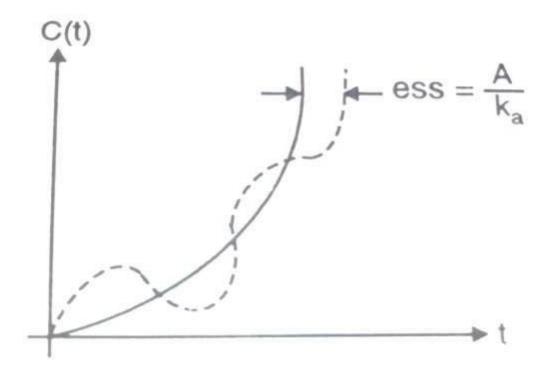
$$e_{ss}(t) = \frac{A}{0 + \lim_{s \to 0} s^2 G(s) H(s)}$$

$$e_{ss}(t) = \frac{A}{K_a}$$

Steady state error for parabolic input:

The acceleration error constant Ka of a system is defined as,

$$K_a = \lim_{s\to 0} s^2 G(s)$$
. H(s)



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Steady state error and Standard Signals

Summary:

Sr. No.	Input Signal	Steady State Error	Constant	Constant Expression
1	Step Input	$e_{ss}(t) = \frac{A}{1 + K_p}$	Position Error Constant	$K_p = \lim_{s \to 0} G(s).H(s)$
2	Ramp Input	$e_{ss}(t) = \frac{A}{K^{v}}$	Velocity Error Constant	$K_{v} = \lim_{s \to 0} sG(s).H(s)$
3	Parabolic Input	$e_{ss}(t) = \frac{A}{K_a}$	Acceleration Error Constant	$K_a = \lim_{s \to 0} s^2 G(s). H(s)$

Relation between steady state error and Type of system

The type of system means the number of poles G(s)H(s) at s=0. Consider the general form,

$$G(s). H(s) = \frac{K (1 + T_{1}s)(1 + T_{2}s)....(1 + T_{m}s)}{s^{n} (1 + T_{a}s)(1 + T_{b}s)....(1 + T_{n}s)}$$

Here there are n poles at s=0. Hence the type of system is n.

For type zero system, n=0

$$G(s).H(s) = \frac{K(1+T_1s)(1+T_2s)....(1+T_ms)}{(1+T_as)(1+T_bs)....(1+T_ns)}$$

The position error constant is given by,

$$K_p = \lim_{s\to 0} G(s). H(s)$$

$$K_p = \lim_{s \to 0} \frac{K(1 + T_1 s)(1 + T_2 s)....(1 + T_m s)}{(1 + T_a s)(1 + T_b s)....(1 + T_n s)}$$

$$K_p = \frac{K (1 + T_10)(1 + T_20)....(1 + T_m 0)}{(1 + T_a0)(1 + T_b0)....(1 + T_n 0)}$$

$$K_p = \frac{K(1)(1)....(1)}{(1)(1)...(1)}$$

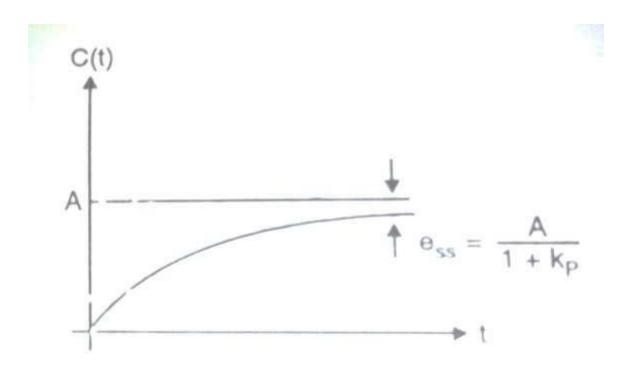
$$K_p = K$$

$$e_{ss}(t) = \frac{A}{1 + K_p}$$

$$e_{ss}(t) = \frac{A}{1+K}$$

$$e_{ss}(t) = \frac{A}{1+K}$$

A type zero system has a finite steady state error to a step input,



For type one system, n=1

$$G(s).H(s) = \frac{K(1+T_1s)(1+T_2s)....(1+T_ms)}{s(1+T_as)(1+T_bs)....(1+T_ns)}$$

The position error constant is given by,

$$K_p = \lim_{s\to 0} G(s). H(s)$$

$$K_p = \lim_{s \to 0} \frac{K(1 + \text{T 1 S})(1 + \text{T 2 S})....(1 + \text{TmS})}{\text{S}(1 + \text{T a S})(1 + \text{T b S})....(1 + \text{TnS})}$$

$$K_p = \frac{K(1 + T_10)(1 + T_20)....(1 + T_m 0)}{0(1 + T_a0)(1 + T_b0)....(1 + T_n 0)}$$

$$K_p = \frac{K(1)(1)....(1)}{0}$$

$$K_p = \infty$$

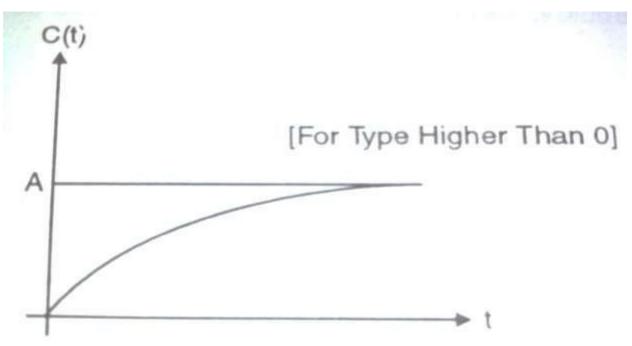
$$e_{ss}(t) = \frac{A}{1 + K_p}$$

$$e_{ss}(t) = \frac{A}{1+\infty}$$

$$e_{ss}(t) = 0$$

$$e^{ss}(t) = 0$$

A type one system has a zero steady state error to a step input,



For type two system, n=2

$$G(s). H(s) = \frac{K (1 + T_{1}s)(1 + T_{2}s)....(1 + T_{m}s)}{s^{2} (1 + T_{a}s)(1 + T_{b}s)....(1 + T_{n}s)}$$

The position error constant is given by,

$$K_p = \lim_{s \to 0} G(s). H(s)$$

$$K_p = \lim_{s \to 0} \frac{K (1 + T_{1S})(1 + T_{2S})....(1 + T_{mS})}{s^2 (1 + T_{aS})(1 + T_{bS})....(1 + T_{nS})}$$

$$K_p = \frac{K (1 + T_1 0)(1 + T_2 0)....(1 + T_m 0)}{0(1 + T_a 0)(1 + T_b 0)...(1 + T_n 0)}$$

$$K_p = \frac{K(1)(1)....(1)}{0}$$

$$K_p = \infty$$

$$e_{ss}(t) = \frac{A}{1 + K_p}$$

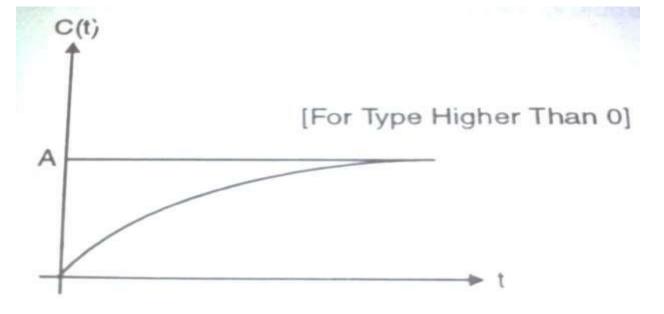
$$e_{ss}(t) = \frac{A}{1+\infty}$$

$$e_{ss}(t) = 0$$

$$ess(t) = 0$$

A type two system has a zero steady state error to a step

input,



It is clear that all higher type systems except type zero have zero steady state error.

For type zero system, n=0

$$G(s).H(s) = \frac{K(1+T_1s)(1+T_2s)....(1+T_ms)}{(1+T_as)(1+T_bs)....(1+T_ns)}$$

The velocity error constant is given by,

$$K_v = \lim_{s\to 0} sG(s). H(s)$$

$$K_{v} = \lim_{s \to 0} s \left\{ \frac{K(1 + T_{1}s)(1 + T_{2}s)....(1 + T_{m}s)}{(1 + T_{a}s)(1 + T_{b}s)....(1 + T_{n}s)} \right\}$$

$$K_{\nu} = 0 \times \{ \frac{K (1 + T_{1} s)(1 + T_{2} s)....(1 + T_{m} s)}{(1 + T_{a} s)(1 + T_{b} s)....(1 + T_{n} s)} \}$$

$$K_{v}=0$$

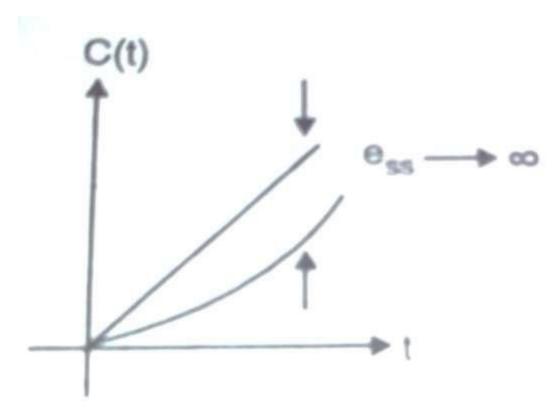
$$e_{ss}(t) = \frac{A}{K_{v}}$$

$$e_{ss}(t) = \frac{A}{0}$$

$$e_{ss}(t) = \infty$$

$$e_{ss}(t) = \infty$$

The error increase continuously hence type zero system fails to track a ramp input successfully.



For type one system, n=1

$$G(s).H(s) = \frac{K(1+T_1s)(1+T_2s)....(1+T_ms)}{s(1+T_as)(1+T_bs)....(1+T_ns)}$$

The velocity error constant is given by,

$$K_{\nu} = \lim_{s \to 0} sG(s). H(s)$$

$$K_{v} = \lim_{s \to 0} s \left\{ \frac{K (1 + T_{1}s)(1 + T_{2}s)....(1 + T_{m}s)}{s(1 + T_{a}s)(1 + T_{b}s)....(1 + T_{n}s)} \right\}$$

$$K_{\nu} = \frac{K (1 + T_{10})(1 + T_{20}).....(1 + T_{m0})}{(1 + T_{a0})(1 + T_{b0}).....(1 + T_{n0})}$$

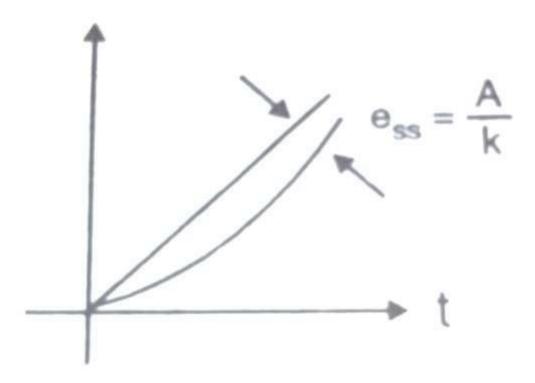
$$K_{v} = K$$

$$e_{ss}(t) = \frac{A}{K_v}$$

$$e_{ss}(t) = \frac{A}{K}$$

$$e_{ss}(t) = \frac{A}{K}$$

This indicates finite steady state error for type one system for ramp input



For type two system, n=2

$$G(s). H(s) = \frac{K (1 + T_1 s)(1 + T_2 s)....(1 + T_m s)}{s^2 (1 + T_a s)(1 + T_b s)....(1 + T_n s)}$$

The velocity error constant is given by,

$$K_{v} = \lim_{s \to 0} sG(s). H(s)$$

$$K_{v} = \lim_{s \to 0} s \left\{ \frac{K (1 + T_{1} s)(1 + T_{2} s)....(1 + T_{m} s)}{s^{2} (1 + T_{a} s)(1 + T_{b} s)....(1 + T_{n} s)} \right\}$$

$$K_{v} = \frac{K (1 + T_{1}s)(1 + T_{2}s)....(1 + T_{m}s)}{s(1 + T_{a}s)(1 + T_{b}s)....(1 + T_{n}s)}$$

$$K_{v}=\infty$$

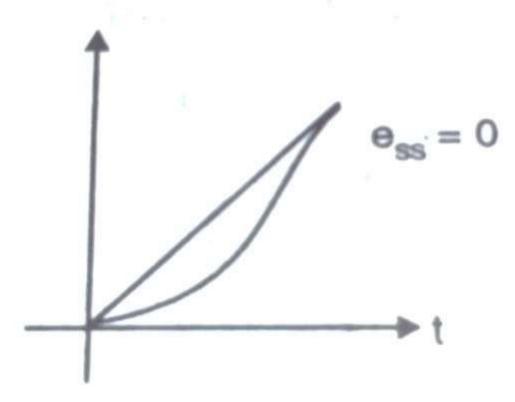
$$e_{ss}(t) = \frac{\underline{A}}{K_v}$$

$$e_{ss}(t) = \frac{A}{\infty}$$

$$e_{ss}(t) = 0$$

$$ess(t) = 0$$

There is no steady state error for a ramp input for type two system



Steady state error for Parabolic input for Type 0 system

For type zero system, n=0

$$G(s).H(s) = \frac{K(1+T_1s)(1+T_2s)....(1+T_ms)}{(1+T_as)(1+T_bs)....(1+T_ns)}$$

The acceleration error constant is given by,

$$K_a = \lim_{s\to 0} s^2 G(s)$$
. H(s)

$$K_a = \lim_{s \to 0} s^2 \left\{ \frac{K (1 + T_1 s)(1 + T_2 s)....(1 + T_m s)}{(1 + T_a s)(1 + T_b s)....(1 + T_n s)} \right\}$$

$$K_a = 0 \times \left\{ \begin{array}{l} \frac{K(1 + T_1 s)(1 + T_2 s)....(1 + T_m s)}{(1 + T_a s)(1 + T_b s)...(1 + T_n s)} \right\} \end{array}$$

Steady state error for Parabolic input for Type 0 system

$$K_a = 0$$

$$e_{ss}(t) = \frac{A}{K_a}$$

$$e_{ss}(t) = \frac{A}{0}$$

$$e_{ss}(t) = \infty$$

Steady state error for Parabolic input for Type 0 system

$$e_{ss}(t) = \infty$$

There is infinite steady state error indicating failure to track a parabolic input in type zero system

Steady state error for Parabolic input for Type 1 system

For type one system, n=1

$$G(s).H(s) = \frac{K(1+T_1s)(1+T_2s)....(1+T_ms)}{s(1+T_as)(1+T_bs)....(1+T_ns)}$$

The acceleration error constant is given by,

$$K_a = \lim_{s\to 0} s^2 G(s)$$
. H(s)

$$K_a = \lim_{s \to 0} s^2 \left\{ \frac{K (1 + T_1 s)(1 + T_2 s)....(1 + T_m s)}{s(1 + T_a s)(1 + T_b s)....(1 + T_n s)} \right\}$$

$$K_a = 0 \times \left\{ \begin{array}{l} \frac{K(1 + T_1 s)(1 + T_2 s)....(1 + T_m s)}{(1 + T_a s)(1 + T_b s)...(1 + T_n s)} \right\} \end{array}$$

Steady state error for Parabolic input for Type 1 system

$$K_a = 0$$

$$e_{ss}(t) = \frac{A}{K_a}$$

$$e_{ss}(t) = \frac{A}{0}$$

$$e_{ss}(t) = \infty$$

Steady state error for Parabolic input for Type 1 system

$$e_{ss}(t) = \infty$$

There is infinite steady state error indicating failure to track a parabolic input in type one system

Steady state error for Parabolic input for Type 2 system

For type two system, n=2

G(s). H(s) =
$$\frac{K(1+T_1s)(1+T_2s)....(1+T_ms)}{s^2(1+T_as)(1+T_bs)...(1+T_ns)}$$

The acceleration error constant is given by,

$$K_a = \lim_{s\to 0} s^2 G(s)$$
. H(s)

$$K_a = \lim_{s \to 0} s^2 \left\{ \frac{K (1 + T_{1S})(1 + T_{2S})....(1 + T_{mS})}{s^2 (1 + T_{aS})(1 + T_{bS})....(1 + T_{nS})} \right\}$$

$$K_a = \left\{ \begin{array}{l} \frac{K(1+T_1s)(1+T_2s)....(1+T_ms)}{(1+T_as)(1+T_bs)} \right\} \end{array}$$

Steady state error for Parabolic input for Type 2 system

$$K_a = K$$

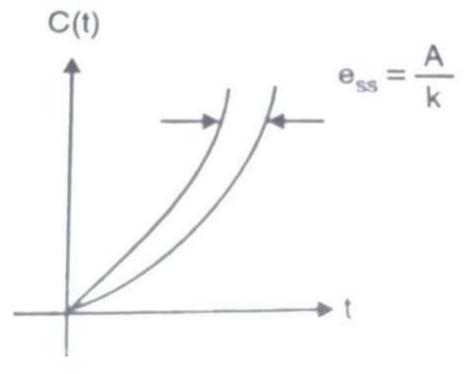
$$e_{ss}(t) = \frac{A}{K_a}$$

$$e_{ss}(t) = \frac{A}{K}$$

Steady state error for Parabolic input for Type 2 system

$$e_{ss}(t) = \frac{A}{K}$$

There is finite steady state error for type two system



Relation between steady state error and Type of system

Summary:

Sr. No.	Type of System	Step Input		Ramp Input		Parabolic Input	
		K _P	e _{ss}	K _V	e _{ss}	K _a	e _{ss}
1	Zero	K	$\frac{A}{1+K}$	0	∞	0	∞
2	One	∞	0	K	<u>A</u> K	0	∞
3	Two	∞	0	∞	0	K	<u>A</u> K

Example

The control system having unity feedback has,

$$G(s) = \frac{20}{s(1+4s)(1+s)}$$

Determine

1. Different static error coefficients.

2. Steady State error if input
$$r(t) = 2 + 4t + \frac{t^2}{2}$$

Solution:

Position error constant,

$$K_p = \lim_{s \to 0} G(s)H(s)$$

$$K_p = \lim_{s \to 0} \frac{20}{s(1+4s)(1+s)}$$

$$K_p = \frac{20}{0(1+4s)(1+s)}$$

$$K_p = \infty$$

Example

Velocity error constant,

$$K_{v} = \lim_{s \to 0} sG(s)H(s)$$

$$K_v = \lim_{s \to 0} s[\frac{20}{s(1+4s)(1+s)}]$$

$$K_{v} = \frac{20}{(1+4s)(1+s)}$$

$$K_{v} = 20$$

Acceleration error constant,

$$K_a = \lim_{s \to 0} s^2 G(s) H(s)$$

$$K_a = \lim_{s \to 0} s^2 \left[\frac{20}{s(1+4s)(1+s)} \right]$$

$$K_a = 0[\frac{20}{s(1+4s)(1+s)}]$$

$$K_a = 0$$

Example

Steady state error, for
$$r(t) = 2 + 4t + \frac{t^2}{2}$$

$$R(s) = L\{r(t)\}$$
 = $\frac{2}{s} + \frac{4}{s^2} + \frac{1}{s^3}$

$$e_{ss} = \lim_{s \to 0} \frac{sR(s)}{1 + G(s)H(s)}$$

$$e_{ss} = \lim_{s \to 0} \frac{s\left[\frac{2}{s} + \frac{4}{s^{2}} + \frac{1}{s}\right]}{1 + \frac{20}{s(1+4s)(1+s)}}$$

$$e_{SS} = \infty$$

Example

The control system having unity feedback has,

$$G(s) = \frac{50(s+5)}{s^2}$$

Determine

1. Different static error coefficients.

Solution:

Position error constant,

$$K_p = \lim_{s \to 0} G(s)H(s)$$

$$K_p = \lim_{s \to 0} \frac{50(s+5)}{s^2}$$

$$K_p = \frac{50(s+5)}{(0)^2}$$

$$K_p = \infty$$

Velocity error constant,

$$K_{v} = \lim_{s \to 0} sG(s)H(s)$$

$$K_{\nu} = \lim_{s \to 0} s\left[\frac{50(s+5)}{s^2}\right]$$

$$K_{v} = \lim_{s \to 0} \frac{50(s+5)}{s}$$

$$K_{\nu} = \frac{50(s+5)}{0}$$

$$K_v = \infty$$

Acceleration error constant,

$$K_a = \lim_{s \to 0} s^2 G(s) H(s)$$

$$K_a = \lim_{s \to 0} s^2 \left[\frac{50(s+5)}{s^2} \right]$$

$$K_a = \lim_{s \to 0} 50(s+5)$$

$$K_a = 250$$

The control system having,

$$G(s) = \frac{20}{s(s^2 + 2s + 5)} \qquad H(s) = \frac{10}{(s + 4)}$$

Determine

Different static error coefficients.

2. Steady State error if input
$$r(t) = 5 + 10t + \frac{t^2}{2}$$

Solution:

Position error constant,

$$K_p = \lim_{s \to 0} G(s) H(s)$$

$$K_p = \lim_{s \to 0} \frac{20}{s(s^2 + 2s + 5)} \times \frac{10}{(s + 4)}$$

$$K_p = \infty$$

Velocity error constant,

$$K_{v} = \lim_{s \to 0} sG(s)H(s)$$

$$K_{v} = \lim_{s \to 0} s[\frac{20}{s(s^{2} + 2s + 5)} \times \frac{10}{(s+4)}]$$

$$K_{v} = \frac{200}{20}$$

$$K_{v} = 10$$

Acceleration error constant,

$$K_a = \lim_{s \to 0} s^2 G(s) H(s)$$

$$K_a = \lim_{s \to 0} s^2 \left[\frac{20}{s(s^2 + 2s + 5)} \times \frac{10}{(s+4)} \right]$$

$$K_a = 0[\frac{20}{(s^2 + 2s + 5)} \times \frac{10}{(s+4)}]$$

$$K_a = 0$$

Steady state error, for
$$r(t) = 5 + 10t + \frac{t^2}{2}$$

$$R(s) = L\{r(t)\}$$
 = $\frac{5}{s} + \frac{10}{s^2} + \frac{1}{s^3}$

Steady state error is given by,

$$e_{ss} = \lim_{s \to 0} \frac{sR(s)}{1 + G(s)H(s)}$$

$$e_{ss} = \lim_{s \to 0} \frac{s \left[\frac{5}{s} + \frac{10}{s^2} + \frac{1}{s} \right]}{1 + \left[\frac{20}{s(s^2 + 2s + 5)} \times \frac{10}{(s + 4)} \right]}$$

$$e_{ss} = \infty$$

The control system having unity feedback has,

$$G(s) = \frac{20(1+s)}{s^2(2+s)(4+s)}$$

Determine

1. Different static error coefficients.

2. Steady State error if input r(t) = 40 + 2t + 5t

Solution:

Position error constant,

$$K_p = \lim_{s \to 0} G(s) H(s)$$

$$K_p = \lim_{s \to 0} \frac{20(1+s)}{s^2 (2+s)(4+s)}$$

$$K_p = \frac{20(1+s)}{0^2(2+s)(4+s)}$$

$$K_p = \infty$$

Velocity error constant,

$$K_{v} = \lim_{s \to 0} sG(s)H(s)$$

$$K_v = \lim_{s \to 0} s[\frac{20(1+s)}{s^2(2+s)(4+s)}]$$

$$K_{\nu} = \lim_{s \to 0} \frac{20(1+s)}{s(2+s)(4+s)}$$

$$K_{v} = \infty$$

Acceleration error constant,

$$K_a = \lim_{s \to 0} s^2 G(s) H(s)$$

$$K_a = \lim_{s \to 0} s^2 \left[\frac{20(1+s)}{s^2 (2+s)(4+s)} \right]$$

$$K_a = \lim_{s \to 0} \frac{20(1+s)}{(2+s)(4+s)}$$

$$K_a = \frac{5}{2}$$

Steady state error, for $r(t) = 40 + 2t + 5t^2$

$$R(s) = L\{r(t)\}$$
 = $\frac{40}{s} + \frac{2}{s^2} + \frac{10}{s^3}$

Steady state error is given by,

$$e_{SS} = \lim_{s \to 0} \frac{sR(s)}{1 + G(s)H(s)}$$

$$e_{ss} = \lim_{s \to 0} \frac{s \left[\frac{40}{s} + \frac{2}{s^2} + \frac{10}{s^3} \right]}{1 + \frac{20(1+s)}{s^2 (2+s)(4+s)}}$$

$$e_{ss}=4$$

The control system having unity feedback has,

$$G(s) = \frac{20(s+1)}{s(s+2)(s^2+2s+2)}$$

Determine

- 1. Different static error coefficients.
- 2. Steady State error if input r(t) = 10 + 20t

Solution:

Position error constant,

$$K_p = \lim_{s \to 0} G(s) H(s)$$

$$K_p = \lim_{s \to 0} \frac{20(s+1)}{s(s+2)(s^2+2s+2)}$$

$$K_p = \frac{20(s+1)}{0(s+2)(s^2+2s+2)}$$

$$K_p = \infty$$

Velocity error constant,

$$K_{v} = \lim_{s \to 0} sG(s)H(s)$$

$$K_v = \lim_{s \to 0} s[\frac{20(s+1)}{s(s+2)(s^2+2s+2)}]$$

$$K_v = \lim_{s \to 0} \frac{20(s+1)}{(s+2)(s^2+2s+2)}$$

$$K_{v} = 5$$

Acceleration error constant,

$$K_a = \lim_{s \to 0} s^2 G(s) H(s)$$

$$K_a = \lim_{s \to 0} s^2 \left[\frac{20(s+1)}{s(s+2)(s^2+2s+2)} \right]$$

$$K_a = \lim_{s \to 0} s[\frac{20(s+1)}{(s+2)(s^2+2s+2)}]$$

$$K_a = 0$$

The control system having unity feedback has,

$$G(s) = \frac{20(s+4)}{s(s+2)(s^2+2s+2)}$$

Determine

- Different static error coefficients.
- 2. Steady State error if input $r(t) = 6t + \frac{3}{2}t^2$

Solution:

Position error constant,

$$K_p = \lim_{s \to 0} G(s) H(s)$$

$$K_p = \lim_{s \to 0} \frac{20(s+4)}{s(s+2)(s^2+2s+2)}$$

$$K_p = \frac{20(s+4)}{0(s+2)(s^2 + 2s + 2)}$$

$$K_p = \infty$$

Velocity error constant,

$$K_{v} = \lim_{s \to 0} sG(s)H(s)$$

$$K_v = \lim_{s \to 0} s[\frac{20(s+4)}{s(s+2)(s^2+2s+2)}]$$

$$K_{v} = \lim_{s \to 0} \frac{20(s+4)}{(s+2)(s^{2}+2s+2)}$$

$$K_v = 20$$

Acceleration error constant,

$$K_a = \lim_{s \to 0} s^2 G(s) H(s)$$

$$K_a = \lim_{s \to 0} s^2 \left[\frac{20(s+4)}{s(s+2)(s^2+2s+2)} \right]$$

$$K_a = \lim_{s \to 0} s[\frac{20(s+4)}{(s+2)(s^2+2s+2)}]$$

$$K_a = 0$$

Steady state error, for $r(t) = 6t + \frac{3}{2}t^2$

$$r(t) = 6t + \frac{3}{2}t^2$$

$$R(s) = L\{r(t)\} = \frac{\underline{6}}{s^2} + \frac{\underline{3}}{s^3}$$

Steady state error is given by,

$$e_{SS} = \lim_{s \to 0} \frac{sR(s)}{1 + G(s)H(s)}$$

$$e_{ss} = \lim_{s \to 0} \frac{s \left[\frac{6}{s^2} + \frac{3}{s^3}\right]}{1 + \frac{20(s+4)}{s(s+2)(s^2 + 2s+2)}}$$

$$e_{SS} = \infty$$

The open loop transfer function of servo system with unity feedback is,

$$G(s) = \frac{10}{s(0.1s+1)}$$

Determine

- 1. Different static error coefficients.
- 2. Steady State error if input $r(t) = a_0 + a_1 t + \frac{a_2}{2}t^2$

Solution:

Position error constant,

$$K_p = \lim_{s \to 0} G(s)H(s)$$

$$K_p = \lim_{s \to 0} \frac{10}{s(0.1s+1)}$$

$$K_p = \frac{10}{0(0.1s + 1)}$$

$$K_p = \infty$$

Velocity error constant,

$$K_{v} = \lim_{s \to 0} sG(s)H(s)$$

$$K_{v} = \lim_{s \to 0} s[\frac{10}{s(0.1s+1)}]$$

$$K_{v} = \lim_{s \to 0} \frac{10}{(0.1s+1)}$$

$$K_{v} = 10$$

Acceleration error constant,

$$K_a = \lim_{s \to 0} s^2 G(s) H(s)$$

$$K_a = \lim_{s \to 0} \quad s^2 \left[\frac{10}{s(0.1s+1)} \right]$$

$$K_a = \lim_{s \to 0} s[\frac{10}{(0.1s+1)}]$$

$$K_a = 0$$

Steady state error, for
$$r(t) = a_0 + a_1 t + \frac{a_2}{2} t^2$$

$$R(s) = L\{r(t)\}$$
 = $\frac{a_0}{s} + \frac{a_1}{s^2} + \frac{a_2}{s^3}$

Steady state error is given by,

$$e_{ss} = \lim_{s \to 0} \frac{sR(s)}{1 + G(s)H(s)}$$

$$e_{SS} = \lim_{s \to 0} \frac{\underbrace{s \left[\frac{a_0}{+} + \frac{a_1}{s^2} \right]}_{s \to 0} \underbrace{\frac{a_2}{s^2}}_{s \to 0}}_{1 + \frac{10}{s(0.1s+1)}}$$

$$e_{ss} = \infty$$

The open loop transfer function of servo system with unity feedback is,

$$G(s) = \frac{10}{s^2(1+s)}$$

Determine

- 1. Different static error coefficients.
- 2. Steady State error if input $r(t) = a_0 + a_1t + a_2t^2$

Solution:

Position error constant,

$$K_p = \lim_{s \to 0} G(s) H(s)$$

$$K_p = \lim_{s \to 0} \frac{10}{s^2 (1+s)}$$

$$K_p = \frac{10}{0^2(1+s)}$$

$$K_p = \infty$$

Velocity error constant,

$$K_{v} = \lim_{s \to 0} sG(s)H(s)$$

$$K_{v} = \lim_{s \to 0} \quad s\left[\frac{10}{s^{2}}\right]$$

$$K_{v} = \lim_{s \to 0} \left[\frac{10}{s(1+s)} \right]$$

$$K_{v} = \infty$$

Acceleration error constant,

$$K_a = \lim_{s \to 0} s^2 G(s) H(s)$$

$$K_a = \lim_{s \to 0} s^2 \left[\frac{10}{s^2(1+s)} \right]$$

$$K_a = \lim_{s \to 0} \left[\frac{10}{(1+s)} \right]$$

$$K_a = 10$$

Steady state error, for $r(t) = a_0 + a_1t + a_2t^2$

$$r(t) = a_0 + a_1 t + a_2 t^2$$

$$R(s) = L\{r(t)\} \qquad \qquad = \frac{\underline{a_0}}{s} + \frac{\underline{a_1}}{s^2} + \frac{\underline{2a_2}}{s^3}$$

Steady state error is given by,

$$e_{ss} = \lim_{s \to 0} \frac{sR(s)}{1 + G(s)H(s)}$$

$$e_{ss} = \lim_{s \to 0} \frac{s \left[\frac{a_0}{s} + \frac{a_1}{s} + \frac{2a_2}{s} \right]}{1 + \frac{10}{s^2 (1+s)}}$$

$$e_{ss} = \frac{a_2}{5}$$

A unity feedback system is characterized by the open loop transfer function is,

$$G(s) = \frac{1}{s(0.5s+1)(0.2s+1)}$$

Determine steady state errors for unit step input, unit ramp input and unit acceleration input.

Solution:

Position error constant,

$$K_p = \lim_{s \to 0} G(s) H(s)$$

$$K_p = \lim_{s \to 0} \frac{1}{s(0.5s + 1)(0.2s + 1)}$$

$$K_p = \infty$$

Steady state error for unit step input is given by,

$$e_{ss}(t) = \frac{1}{1 + K_p}$$

$$e_{ss}(t) = \frac{1}{1+\infty}$$

$$e_{ss}(t) = 0$$

Velocity error constant,

$$K_{v} = \lim_{s \to 0} sG(s)H(s)$$

$$K_v = \lim_{s \to 0} s[\frac{1}{s(0.5s+1)(0.2s+1)}]$$

$$K_{v} = 1$$

Steady state error for unit ramp input is given by,

$$e_{ss}(t) = \frac{1}{K_v}$$

$$e_{ss}(t) = \frac{1}{1}$$

$$e_{ss}(t) = 1$$

Acceleration error constant, $K_a = \lim_{s \to 0} s^2 G(s) H(s)$

$$K_a = \lim_{s \to 0} s^2 \left[\frac{1}{s(0.5s+1)(0.2s+1)} \right]$$

$$K_a = 0$$

Steady state error for unit parabolic input is given by,

$$e_{ss}(t) = \frac{1}{K_a}$$

$$e_{ss}(t) = \frac{1}{0}$$

$$e_{ss}(t) = \infty$$