Lab 6: Non-Linearity and its effects in communication systems

EE340: Prelab Reading material for Experiment 6

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Non-Linear Systems

- Linear Systems: Satisfy superposition principle
- However, any practical system is non-linear (amount of non-linearity may vary)
- Non-linearity results in generation of "new frequency components" i.e. frequency components that are not there at the input of the system.
- Memory-less non-linearity can be modeled as:

$$y(t) = a_1x(t) + a_2x^2(t) + a_3x^3(t) + a_4x^4(t)...$$

 Memory-less means present output depends only on the present input (also see Appendix – last slide)

Effects of Non-Linearity

Consider a simplified non-linear system described by

$$y(t) = a_1x(t) + a_2x^2(t) + a_3x^3(t)$$

For $x(t) = A\cos(\omega t)$,

$$y(t) = \frac{1}{2}a_2A^2 + (a_1 + \frac{3}{4}a_3A^2)A\cos(\omega t) + \frac{1}{2}a_2A^2\cos(2\omega t) + \frac{1}{4}a_3A^3\cos(3\omega t)$$

Important observations:

Second order non-linearity (a₂ coefficient) :

$$\frac{1}{2}a_2A^2(1+\cos(2\omega t))$$

Adds DC $+ 2^{nd}$ harmonic

Third order non-linearity (a₃ coefficient):

$$(a_1 + \frac{3}{4}a_3A^2)Acos(\omega t) + \frac{1}{4}a_3A^3cos(3\omega t)$$
 Gain: $(a_1 + \frac{3}{4}a_3A^2)$

Adds 3rd harmonic

Gain becomes input amplitude (A) dependent. Also, a_3 is generally negative => gain compression with increasing A

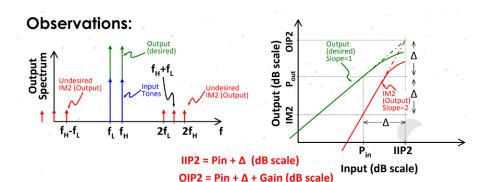
Consider a non-linear system described by

$$y(t) = a_1x(t) + a_2x^2(t)$$

For $x(t) = A(\cos\omega_1 t + \cos\omega_2 t)$,

$$y(t) = a_2 A^2 + a_1 A \left(\cos(\omega_1 t) + \cos(\omega_2 t)\right) + a_2 A^2 \left(\frac{\cos(2\omega_1 t) + \cos(2\omega_2 t)}{2} + \cos((\omega_1 - \omega_2)t) + \cos((\omega_1 + \omega_2)t)\right)$$

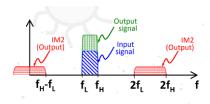
The undesired spectral components generated due to the second order non- linearity coefficent a_2 at frequencies $0,2\omega_1,2\omega_2$, $(\omega_1-\omega_2)$ and $(\omega_1+\omega_2)$ are called IM2 (Inter-Modulation products due to 2^{nd} order non-linearity) components.



where

- 2nd-order intercept point (IP2) is where the asymptotes for the 2nd-order intermodulation product and the fundamental cross.
- IIP2 is the input power and OIP2 is the output power corresponding to the intercept point.
- Pin is the given input signal's power.

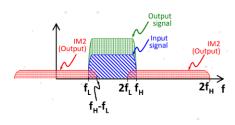
More Observations:



(a) Sub-Octave

Sub-Octave: $f_H < 2f_L$ (i.e. BW $< f_L$)

-> No in-band IM2 distortion out-of-band IM2 components, can easily be filtered out -> DC components can sometimes cause amplifier saturation



(b) Multi-Octave

Multi-Octave: $f_H > 2f_L$ (i.e. BW $> f_L$)

- -> In-band IM2 distortion present can't be filtered out
- -> DC components may cause amplifier saturation

Third Order Non-Linearity

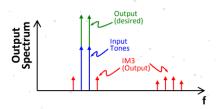
Consider a non-linear system described by

$$y(t) = a_1 x(t) + a_3 x^3(t); \Rightarrow \text{For } x(t) = A \cos(\omega_1 t) + A \cos(\omega_2 t):$$

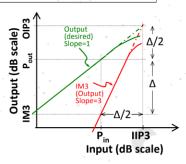
$$y(t) = A \left(a_1 + \frac{9a_3 A^2}{4} \right) \left(\cos(\omega_1 t) + \cos(\omega_2 t) \right) + \frac{1}{4} a_3 A^3 \left(\cos(3\omega_1 t) + \cos(3\omega_2 t) \right)$$

$$+ \frac{3}{4} a_3 A^3 \left[\cos((2\omega_1 - \omega_2)t) + \cos((2\omega_1 + \omega_2)t) + \cos((2\omega_2 - \omega_1)t) + \cos((2\omega_2 + \omega_1)t) \right]$$

Observations:

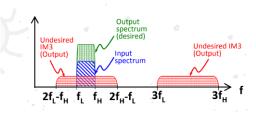


Generates in-band/adjacent band, out-of-band components, but no DC



IIP3 = Pin +
$$\Delta/2$$
 (dB scale)
OIP3 = Pin + $\Delta/2$ + Gain (dB scale)

Third Order Non-Linearity



- The figure above shows the undesired spectrum generated by 3^{rd} order non-linearity (i.e. due to non-zero a_3 coefficient).
- The undesired spectrum generated is called IM3 component, i.e.
 Inter-Modulation products due to 3rd order non-linearity component.
- Due to 3rd or odd order non-linearities (unlike 2nd or even order non-linearities), part of the spectrum is in-band and hence CANNOT be removed by filtering even for narrow-band inputs.
- Therefore, effects of 3rd (or odd) order non-linearities are more difficult to remove in general (than of even order non-linearities).

Calculation Of Intercept Points

For a two-tone source, the general nth-order intercept point is given by

$$IP_n = P_{in} + \frac{P_{in} - P_{IM}}{n - 1} \tag{1}$$

where

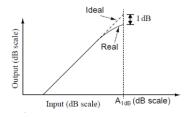
- IP_n is the nth-order intercept point
- P_{in} is the power level of the input tone
- P_{IM} is the power level of the nth-order intermodulation distortion (IMD) product (created by the two tones)
- All the power levels are measured in dBm

For the calculation of IIPn and OIPn, refer to the sections till 4.3 in Calculations of intercept points

Compression Point and Jamming

1-dB compression point: Amplitude (A_{-1dB}) at which gain decreases by 1-dB (without interferer) because a_3 is "almost always" negative.

$$20\log[rac{(a_1+rac{3}{4}a_3A_{-1dB}^2)A_{-1dB}}{a_1A_{-1dB}}]=-1dB$$
 i.e. $A_{-1dB}pprox 0.40\sqrt{rac{|a_1|}{|a_3|}}$



Compression point in $dB = 20 \log(A_{-1dB}) = IIP3(\text{in } dB) - 9.6dB$

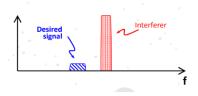
where

$$\begin{split} \textit{IIP3}(\text{in dB}) &= 20\log(\sqrt{\frac{4|a_1|}{3|a_3|}})\\ \textit{OIP3}(\text{in dB}) &= \textit{IIP3}(\text{in dB}) + 20\log(|a_1|) \end{split}$$

Jamming / Blocking / Desensitization

For $x(t) = Acos(\omega t) + Bcos(\omega_1 t)$, where $Acos(\omega t)$ is the desired signal and $Bcos(\omega_1 t)$ is the interferer,

$$y(t)=(a_1+\frac{3}{4}a_3A^2+\frac{3}{2}a_3B^2)Acos(\omega t)+$$
 other terms



- Therefore, if interferer amplitude B >> A, the receiver is jammed
- The transmitter can jam the receiver if they are operating concurrently, for example in full duplex systems (and isolation is poor)

APPENDIX: Real Systems are not memory-less or linear: Non-linear dynamical behaviour

Transfer function of a dynamic non-linear system

- Very complex, commonly expressed as the Volterra series

$$y(t) = a_0 + \sum_{n=1}^{\infty} \frac{1}{n!} \int_{0}^{\infty} \dots \int_{0}^{\infty} a_n(\tau_1, \tau_2, \dots, \tau_n) x(t - \tau_1) x(t - \tau_2) \dots x(t - \tau_n) d\tau_1 d\tau_1 \dots d\tau_n$$

 a_n is called the n^{th} order Volterra kernel.

Therefore, a 2nd order dynamic non-linear system can be modeled as

$$y(t) = a_0 + \int_0^\infty a_1(\tau_1)x(t-\tau_1)d\tau_1 + \frac{1}{2}\int_0^\infty \int_0^\infty a_2(\tau_1,\tau_2)x(t-\tau_1)x(t-\tau_2)d\tau_1d\tau_2$$

√ Other References: Reference link