1. A digital communication link carries binary-coded words representing samples of an input signal,

$$x(t) = 3\cos 600\pi t + 2\cos 1800\pi t$$

The link is operated at 10,000 bits/s and each input sample is quantized into 1024 different voltage levels.

- i. What is the sampling frequency & folding frequency?
- ii. What is the Nyquist rate for the signal x(t)?
- iii. What are the frequencies in the resulting discrete time signal x[n]?
- iv. What is the resolution Δ ?

Solution: →

As the link is operated at 10,000 bits/s & each input sample is quantized into 1024 different voltage levels the each sampled value is represented by $log_21024 = 10$ bits/sample

i. Then maximum sampling frequency, $F_s = \frac{10,000 \text{ bits/sec}}{10 \text{ bits/sample}} = 1000 \text{ samples/sec}$

Folding frequency (is the maximum frequency that can be represented uniquely by sampled signal), $\frac{F_s}{2} = 500 \ samples/sec$.

ii. $x(t) = 3\cos 600\pi t + 2\cos 1800\pi t$

Here, $F_1 = 300 \text{ Hz}$ and $F_2 = 900 \text{ Hz}$. Thus $F_{max} = 900 \text{ Hz}$.

The Nyquist rate, $F_N = 2F_{max} = 1800 \text{ Hz.}$

iii. For sampling frequency, $F_s = 1000 \text{ Hz}$,

$$x[n] \cong x(nT) = x\left(\frac{n}{F_s}\right) = 3\cos 2\pi \left(\frac{300}{1000}\right)n + 2\cos 2\pi \left(\frac{900}{1000}\right)n$$
$$= 3\cos 2\pi \left(\frac{3}{10}\right)n + 2\cos 2\pi \left(\frac{9}{10}\right)n$$

(Here frequency f2 = 9/10 is greater than $\frac{1}{2}$, so)

$$= 3\cos 2\pi \left(\frac{3}{10}\right)n + 2\cos 2\pi \left(1 - \frac{1}{10}\right)n$$
$$= 3\cos 2\pi \left(\frac{3}{10}\right)n + 2\cos 2\pi \left(\frac{1}{10}\right)n$$
$$\therefore f_1 = \frac{3}{10} \& f_2 = \frac{1}{10}$$

Here both frequencies f_1 and f_2 lies in the interval $-\frac{1}{2} \le f \le \frac{1}{2}$

iv. ADC resolution = 10 bits

Voltage resolution,
$$\Delta = \frac{x_{max} - x_{min}}{L - 1} = \frac{5 - (-5)}{1024 - 1} = 9.76 \text{ mV}.$$

2. Check for linearity, time invariant and stability of following system:

$$y[n] = x[n^2 - 3]u[n] + x[n]u[n]$$

Solution →

For Linearity:

$$y_{1}[n] = x_{1}[n^{2} - 3]u[n] + x_{1}[n]u[n]$$

$$y_{2}[n] = x_{2}[n^{2} - 3]u[n] + x_{2}[n]u[n]$$

$$let x_{3}[n] = a_{1}x_{1}[n] + a_{2}x_{2}[n]$$

$$\therefore y_{3}[n] = x_{3}[n^{2} - 3]u[n] + x_{3}[n]u[n]$$

$$= \{a_{1}x_{1}[n^{2} - 3] + a_{2}x_{2}[n^{2} - 3]\}u[n] + \{a_{1}x_{1}[n] + a_{2}x_{2}[n]\}u[n]$$

$$= a_{1}\{x_{1}[n^{2} - 3]u[n] + x_{1}[n]u[n]\} + a_{2}\{x_{2}[n^{2} - 3]u[n] + x_{2}[n]u[n]\}$$

$$= a_{1}y_{1}[n] + a_{2}y_{2}[n]$$

Since $y_3[n] = a_1y_1[n] + a_2y_2[n]$, the system is linear.

For Time invariant:

Response of delayed input, $y(n,k) = x[n^2-3-k]u[n] + x_1[n-k]u[n]$

Delayed response,
$$y[n-k] = x[(n-k)^2 - 3]u[n-k] + x[n-k]u[n-k]$$

Since $y(n, k) \neq y[n - k]$, the system is time variant.

For Stabilty:

Bounded Input condition: $|x[n]| \le M_x < \infty$

For bounded output,

$$|y[n]| = |x[n^2 - 3]u[n] + x[n]u[n]|$$

 $\leq |x[n^2 - 3]u[n]| + |x[n]u[n]|$
 $\leq M_x + M_x \leq M_y < \infty$

Here, the output is bounded, therefore the system is stable.

3. The impulse response h[n] of an LTI system is known to be zero, except in the interval $N_0 \le n \le N_1$. The input x[n] is known to be zero, except in the interval $N_2 \le n \le N_3$. As a result, the output is constrained to be zero, except in some interval $N_4 \le n \le N_5$. Determine N_4 and N_5 in terms of N_0 , N_1 , N_2 , and N_3 .

Solution: \rightarrow

For an LTI system the output is obtained from the convolution of the input with impulse response of the system:

$$y[n] = \sum_{k=-\infty}^{\infty} h[k]x[n-k]$$

Since $h[n] \neq 0$ for $N_0 \leq n \leq N_1$

$$y[n] = \sum_{k=N_0}^{N_1} h[k]x[n-k]$$

The input $x[n] \neq 0$ for $N_2 \leq n \leq N_3$, so

$$x[n-k] \neq 0$$
 for $N_2 \leq (n-k) \leq N_3$

Note the minimum value of (n - k) is N_2 . Thus the lower bound on n, which occurs for $k = N_0$ is

$$N_4 = N_0 + N_2$$

Using similar argument

$$N_5 = N_1 + N_3 N_0 + N_2 \le n \le N_1 + N_3$$

4. Find the response of the system to the input signal x[n] = u[n] - u[n-5]. The impulse response of the system is given by $x[n] = \alpha^n u[n]$.

Solution: From figure

$$y[n] = 0 \ for \ n < 0$$

$$y[0] = h[k]x[-k] = 1$$

$$y[1] = h[k]x[1 - k] = 1 + \alpha$$

$$y[2] = h[k]x[2 - k] = 1 + \alpha + \alpha^2$$

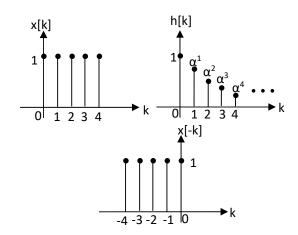
$$y[3] = h[k]x[3 - k] = 1 + \alpha + \alpha^2 + \alpha^3$$

$$y[4] = h[k]x[4 - k] = 1 + \alpha + \alpha^2 + \alpha^3 + \alpha^4$$

$$y[5] = h[k]x[5 - k] = \alpha + \alpha^2 + \alpha^3 + \alpha^4 + \alpha^5$$

$$y[6] = h[k]x[6 - k] = \alpha^2 + \alpha^3 + \alpha^4 + \alpha^5 + \alpha^6$$
And so on..

Therefore,



Nepal Engineering College **Digital Signal Analysis & Processing**

Answer of some selected questions

$$y[n] = \begin{cases} 0, & for \ n < 0 \\ \sum_{k=0}^{n} \alpha^{k}, & 0 \le n \le 4 \\ \sum_{k=0}^{n} \alpha^{k}, & for \ n > 4 \end{cases}$$

5. Find z-transform of $x[n] = a^n(cos\omega_0 n)u[n]$. Solution ->

$$x[n] = a^{n}(cos\omega_{0}n)u[n] = \frac{1}{2}a^{n}e^{j\omega_{0}n}u[n] + \frac{1}{2}a^{n}e^{-j\omega_{0}n}u[n]$$

We can write the above expression as $x[n] = v[n] + v^*[n]$

where
$$v[n] = \frac{1}{2}\alpha^n u[n]$$
 with $\alpha = ae^{j\omega_0}$

The z-transform V(z) of v[n] by linearity and scaling in z-domain properties:

$$V(z) = \frac{1}{2} \cdot \frac{1}{1 - \alpha z^{-1}} = \frac{1}{2} \cdot \frac{1}{1 - a e^{j\omega_0} z^{-1}}, |z| > |\alpha| = a$$

From conjugate of complex sequence property,

$$V^*(z^*) = \frac{1}{2} \cdot \frac{1}{1 - \alpha^* z^{-1}} = \frac{1}{2} \cdot \frac{1}{1 - q e^{-j\omega_0} z^{-1}}, |z| > |\alpha| = a$$

By linearity property of the z-transform, we obtain
$$X(z) = V(z) + V^*(z^*)$$

$$= \frac{1}{2} \left(\frac{1}{1 - ae^{j\omega_0}z^{-1}} + \frac{1}{1 - ae^{-j\omega_0}z^{-1}} \right) = \frac{1 - (acos\omega_0)z^{-1}}{1 - (2acos\omega_0)z^{-1} + a^2z^{-2}} \quad |z| > a$$

- 6. Given the system y[n] = 3y[n-1] 0.1y[n-2] + x[n]
 - a. Find the system function, H(z).
 - b. Is the system IIR or FIR?
 - c. Plot the pole-zero diagram.
 - d. Plot the magnitude response. [PU Fall 2012 5(a)]

Solution: \rightarrow

a. Taking z-transform of both sides, we get

$$Y(z) = 3z^{-1}Y(z) - 0.1z^{-2}Y(z) + X(z)$$

$$=> Y(z)\{1-3z^{-1}+0.1z^{-2}\}=X(z)$$

$$\therefore H(z) = \frac{Y(z)}{X(z)} = \frac{1}{1 - 3z^{-1} + 0.1z^{-2}}$$

This is the required System function of given system.

- b. As the system contains poles the given system is IIR. (If the system contain poles then system is IIR)
- c. Also,

$$H(z) = \frac{1}{1 - 3z^{-1} + 0.1z^{-2}} = \frac{1}{(1 - 2.9663z^{-1})(1 - 0.0337z^{-1})}$$
The system contains poles at $p_1 = 2.966$ and $p_2 = 0.034$, and zeros are at $z_1 = z_2 = 0$, the pole-zero

diagram is shown below:

d. For the frequency response, we will take z

$$\therefore H(e^{j\omega}) = \frac{1}{(1 - 2.9663e^{-j\omega})(1 - 0.0337e^{-j\omega})}$$

Magnitude is given by

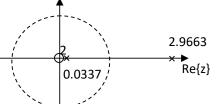


Figure 1: Pole-zero plot

$$|H(e^{j\omega})| = \left| \frac{1}{(1 - 2.9663e^{-j\omega})(1 - 0.0337e^{-j\omega})} \right| = \frac{1}{|1 - 2.9663e^{-j\omega}|(1 - 0.0337e^{-j\omega})|}$$

$$= \frac{1}{\sqrt{(1 - 2.9663\cos\omega)^2 + (2.9663\sin\omega)^2} \cdot \sqrt{(1 - 0.0337\cos\omega)^2 + (0.0337\sin\omega)^2}}$$

For the magnitude response, we can

find the ω Vs. $|H(e^{j\omega})|$ as,

ω	H(e ^{jω})
0	0.5263
$\pi/6$	0.4770
$2\pi/6$	0.3890
$3\pi/6$	0.3193
$4\pi/6$	0.2751
$5\pi/6$	0.2514
π	0.2493

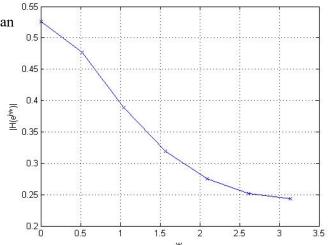


Figure 2: Magnitude Response

7. Determine the inverse z-transform of

$$H(z) = \frac{1 + 2z^{-1} + z^{-2}}{1 + 4z^{-1} + 4z^{-2}}$$

For all possible ROCs. [PU 2009 Spring, 3(a)]

Solution: \rightarrow

We have,

$$H(z) = \frac{1 + 2z^{-1} + z^{-2}}{1 + 4z^{-1} + 4z^{-2}} = \frac{1 + 2z^{-1} + z^{-2}}{(1 + 2z^{-1})^2}$$

$$= \frac{1}{(1 + 2z^{-1})^2} + \frac{2z^{-1}}{(1 + 2z^{-1})^2} + \frac{z^{-2}}{(1 + 2z^{-1})^2}$$

$$= -0.5z \times \frac{-2z^{-1}}{(1 - (-2)z^{-1})^2} + (-1) \times \frac{-2z^{-1}}{(1 - (-2)z^{-1})^2} + (-0.5)z^{-1} \times \frac{-2z^{-1}}{(1 - (-2)z^{-1})^2}$$

The system have poles at $p_1 = -2$ and $p_2 = -2$. Therefore the possible ROCs are |z| > 2 and |z| < 2.

a. For ROC |z| > 2 (Causal Signal)

b. For ROC |z| < 2 (Anticausal signal)

Note: We have used shifting property of z-transform and following z-transform table:

$$na^{n}u[n] \stackrel{z}{\longleftrightarrow} \frac{az^{-1}}{(1-az^{-1})^{2}}, \quad |z| > |a|$$

$$-na^{n}u[-n-1] \stackrel{z}{\longleftrightarrow} \frac{az^{-1}}{(1-az^{-1})^{2}}, \quad |z| < |a|$$

$$property,$$

After using shifting property,

$$(n-k)a^{n-k}u[n-k] \longleftrightarrow z^{-k} \times \frac{az^{-1}}{(1-az^{-1})^2}, \quad |z| > |a|$$
$$-(n-k)a^{n-k}u[-(n-k)-1] \longleftrightarrow z^{-k} \times \frac{az^{-1}}{(1-az^{-1})^2}, \quad |z| < |a|$$

8. If $y[n] = \{1, 1, 2, -1, 3\}$ is output and impulse response is $h[n] = \{1, 2, 3\}$ find discrete-time signal x[n].

Solution: \rightarrow

Taking z-transform,

$$Y(z) = 1 + z^{-1} + 2z^{-2} - z^{-3} + 3z^{-4}$$

$$H(z) = 1 + 2z^{-1} + 3z^{-2}$$

$$\therefore X(z) = \frac{Y(z)}{H(z)} = \frac{1 + z^{-1} + 2z^{-2} - z^{-3} + 3z^{-4}}{1 + 2z^{-1} + 3z^{-2}}$$

By division method:

Therefore X(z) is given by,

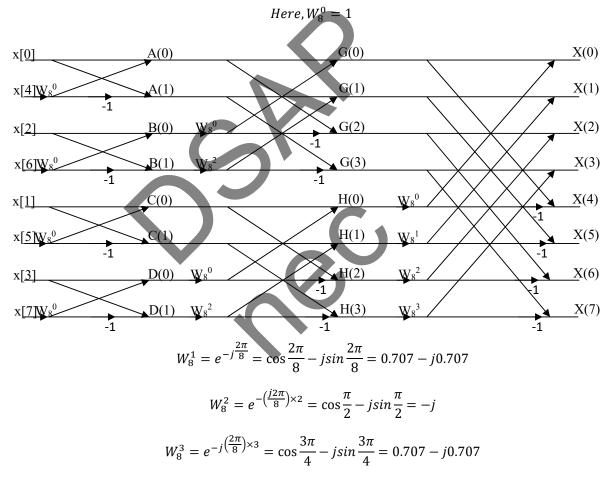
$$X(z) = 1 - z^{-1} + z^{-2}$$

Taking inverse z-transfrom, we get,

$$x[n] = \{1, -1, 1\}.$$

9. Find fft of the signal $x[n] = \{1, 2, 5, 4, -3, 0, 4, 1\}$.

Solution: ->



Output of first Stage:

$$A(0) = x[0] + W_8^0 x[4] = 1 + 1 \times -3 = -2,$$
 $A(1) = x[0] - W_8^0 \cdot x[4] = 1 - 1 \times -3 = 4$

$$B(0) = x[2] + W_8^0 \cdot x[6] = 5 + 1 \times 4 = 9,$$
 $B(1) = x[2] - W_8^0 \cdot x[6] = 5 - 1 \times 4 = 1$

$$C(0) = x[1] + W_8^0 \cdot x[5] = 2 + 1 \times 0 = 2,$$
 $C(1) = x[1] - W_8^0 \cdot x[5] = 2 - 1 \times 0 = 2$

$$D(0) = x[3] + W_8^0 \cdot x[7] = 4 + 1 \times 1 = 5,$$
 $D(1) = x[3] - W_8^0 \cdot x[7] = 4 - 1 \times 1 = 3$

Output of second stage:

$$G(0) = A(0) + W_8^0 \cdot B(0) = -2 + 1 \times 9 = 7,$$
 $H(0) = C(0) + W_8^0 \cdot D(0) = 2 + 1 \times 5 = 7$

$$G(1) = A(1) + W_8^2 \cdot B(1) = 4 + (-j) \times 1 = 4 - j,$$

 $H(1) = C(1) + W_8^2 \cdot D(1) = 2 + (-j) \times 3 = 2 - j3$

$$G(2) = A(0) - W_8^0 \cdot B(0) = -2 - 1 \times 9 = -11$$
, $H(2) = A(0) - W_8^0 \cdot B(0) = 2 - 1 \times 5 = -3$

$$G(3) = A(1) - W_8^2$$
. $B(1) = 4 - (-j) \times 1 = 4 + j$,
 $H(3) = C(1) - W_8^2$. $D(1) = 2 - (-j) \times 3 = 2 + j3$

Output of third stage:

$$X(0) = G(0) + W_8^0 \cdot H(0) = 7 + 1 \times 7 = 14$$

$$X(1) = G(1) + W_8^1 \cdot H(1) = (4 - j) + (0.707 - j0.707) \times (2 - j3) = 3.293 - j4.535$$

$$X(2) = G(2) + W_8^2$$
. $H(2) = -11 + (-j) \times (-3) = -11 + j3$

$$X(3) = G(3) + W_8^2$$
. $H(3) = (4+j) + (-0.707 - j0.707) \times (2+j3) = 4.707 - j2.535$

$$X(4) = G(0) - W_8^0$$
. $H(0) = 7 - 1 \times 7 = 0$

$$X(5) = G(1) - W_8^1 H(1) = (4 - j) - (0.707 - j0.707) \times (2 - j3) = 4.707 + j2.535$$

$$X(6) = G(2) - W_8^2 \cdot H(2) = -11 - (-j) \times (-3) = -11 - j3$$

$$X(7) = G(3) - W_8^2$$
. $H(3) = (4 + j) - (-0.707 - j0.707) \times (2 + j3) = 3.293 + j4.535$

$$\therefore X(k) = \{14, 3.293 - j4.535, -11 + j3, 4.707 - j2.535, 0, 4.707 + j2.535, -11 - j3, 3.293 + j4.535\}$$

10. Draw the lattice structure of the following system:

$$H(z) = \frac{1 + 3z^{-1} + 3z^{-2} + z^{-3}}{2 - 1.8z^{-1} + 1.28z^{-2} - 1.152z^{-3}}.$$
 Is this system stable?

Solution:

Given,
$$H(z) = \frac{C_3(z)}{2A_3(z)} = \frac{1 + 3z^{-1} + 3z^{-2} + z^{-3}}{2(1 - 0.9z^{-1} + 0.64z^{-2} - 0.576z^{-3})}$$

Note: We have to make $\alpha_m(0) = 1$ *for mathematical convenience.*

First consider,
$$A_3(z) = 1 - 0.9z^{-1} + 0.64z^{-2} - 0.576z^{-3}$$

$$B_3(z) = -0.576 + 0.64z^{-1} - 0.9z^{-2} + z^{-3}$$
. (reverse polynomial of $A_3(z)$)

We know,
$$k_m = \alpha_m(m)$$
, therefore $k_3 = -0.576$

Similarly,

$$A_1(z) = \frac{A_2(z) - k_2 B_2(\overline{z})}{(1 - k_2^2)} = 1 - 0.672z^{-1}$$

$$\therefore k_2 = 0.182$$

Now consider the numerator part $C_3(z)$

$$\begin{split} C_3(z) &= c_3(0) + c_3(1)z^{-1} + c_3(2)z^{-2} + c_3(3)z^{-3} = 1 + 3z^{-1} + 3z^{-2} + z^{-3} \\ & \textit{We know}, v_m = c_m(m). \textit{Therefore } v_3 = c_3(3) = 1 \\ & \textit{Now we have, } C_{m-1}(z) = C_m(z) - v_m B_m(z) \\ & \therefore C_2(z) = C_3(z) - v_3 B_3(z) \; (\textit{Note: } B_3(z) \; \textit{is from lattice part}) \\ & C_3(z) = 1 + 3z^{-1} + 3z^{-2} + z^{-3} - 1(-0.576 + 0.64z^{-1} - 0.9z^{-2} + z^{-3}) \\ & = 1.576 + 2.36z^{-1} + 3.9z^{-2} \\ & \therefore v_2 = c_2(2) = 3.9 \end{split}$$

Similarly,
$$C_1(z) = C_2(z) - v_2 B_2(z) = 0.866 + 5.46z^{-1} = > : v_1 = c_1(1) = 5.46z^{-1}$$

And,
$$C_0(z) = C_1(z) - v_1 B_1(z) = 4.535 ==> :: v_0 = c_0(0) = C_0(Z) = 4.535$$

For Stability, $|k_m| < 1$. Therefore the system is stable.

The lattice ladder structure is shown below:

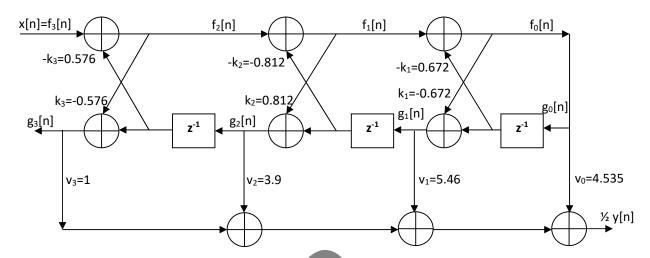


Fig: Lattice-ladder structure of given question.

11. Design an FIR filter with 9 coefficients for the following specifications:

- Passband edge frequency = 0.5 KHz
- Sampling frequency = 2 KHz
- Use suitable window in design.

Solution:

Given,

$$M = 9$$
 $F_c = 0.5 \text{ KHz}$ $F_s = 2 \text{ KHz}$

We know,

$$\omega_c = 2\pi f = 2\pi F_c/F_s = 0.5\pi$$

The desired frequency response is given by

$$H_d(\omega) = \begin{cases} e^{-j\omega\tau} & \text{for } |\omega| \le \omega_c \\ 0 & \text{elsewhere} \end{cases}$$

Taking inverse discrete-time Fourier transform to obtain desired unit sample response, we get,

$$h_d(n) = \frac{1}{2\pi} \int_{-\pi}^{\pi} H_d(\omega) e^{j\omega n} d\omega = \frac{1}{2\pi} \int_{-0.5\pi}^{-0.5\pi} e^{-j\omega \tau} e^{j\omega n} d\omega$$

Solving above equation we get,

$$h_d(n) = \begin{cases} \frac{\sin 0.5\pi (n-\tau)}{\pi (n-\tau)}, & for \ n \neq \tau \\ \frac{1}{2}, & for \ n = \tau \end{cases}$$

We know for symmetric FIR filter, the conditions are

h[n] = h[M - 1 - n] &
$$\tau = \frac{M-1}{2}$$

for M = 9, the value of τ = 4

$$\therefore h_d(n) = \begin{cases} \frac{\sin 0.5\pi (n-4)}{\pi (n-\tau)}, & for \ n \neq 4\\ \frac{1}{2}, & for \ n = 4 \end{cases}$$

As minimum stopband attenuation condition is not given, We can take any window for the design. So, taking Hanning window for our design,

Then the required unit sample is given by,

$$h[n] = h_d[n].w[n]$$

Taking Hanning window in design, the required unit sample of given filter is given in table below:

N	h _d [n]	$w[n] = 0.5 \left(1 - \cos\frac{2\pi n}{M - 1}\right)$	$h[n] = h_d[n].w[n]$
0	0	0	0
1	-0.106	0.146	0.015
2	0	0.5	0
3	0.318	0.854	0.269
4	0.5	1	0.5
5	0.318	0.854	0.269
6	0	0.5	0
7	-0.106	0.146	0.015
8	0	0	0

12. Design an FIR linear phase filter using Kaiser window to meet the following specifications.

$$0.99 \le |H(e^{jw})| \le 1.01, for \ 0 \le |w| \le 0.19\pi$$

 $|H(e^{jw})| \le 0.01, \quad for \ 0.21\pi \le |w| \le \pi$

Solution:

Step I: Given data

The given specifications may be rewritten as under

$$\begin{array}{l} 1\text{--}0.01 \, \leq \, |H(e^{jw})| \, {\leq} 1\text{+-}0.01, \, for \, 0 \, \leq \omega \leq 0.19\pi \\ |\, H(e^{jw})| \, {\leq} 0.01, \, for \, 0.21\pi \, \leq \omega \leq \pi \end{array}$$

On comparing the above given specifications with magnitude response of filter,

$$\delta_1$$
=0.01 δ_2 =0.01

$$\omega_p = 0.19\pi$$
 $\omega_s = 0.21\pi$

$$\Delta \omega = \omega_s - \omega_p = 0.02\pi$$

 δ = minimum of δ_1 and δ_2 = 0.01

Now, A = $-20\log_{10}\delta = 40$

Step 2: To determine cutoff frequency ω_c

Cutoff frequency is given by

$$\omega_c = (\omega_p + \omega_s)/2 = 0.2\pi$$

Step 3: To obtain β and M

Here A = 40, which lies in the range of 21 to 51

Hence, β can be obtained as,

$$\beta = 0.5842(A-21)^{0.4} + 0.07886(A-21) = 3.395$$

and
$$M = \frac{A-8}{2.285\Delta\omega} = 222.88 \cong 223$$

Step 4: To obtain expression of Kaiser window

The window will be defined as under

$$w[n] = \frac{I_0 \left[\beta \left(\sqrt{1 - \left(\left(n - \frac{M}{2}\right) / \frac{M}{2}\right)^2}\right)\right]}{I_0(\beta)} \text{ for } 0 \le n \le M$$

The function $I_0()$ in the above expression may be calculated with the help of following equation

$$I_0(x) = 1 + \sum_{r=1}^{\infty} \left[\frac{(x/2)^r}{r!} \right]^2$$

Since, it is an infinite series, maximum possible terms must be taken to reduce the error.

The ideal desired frequency response is given by

$$H_d(\omega) = \begin{cases} e^{-j\omega\tau\left(\frac{M-1}{2}\right)} & \text{for } |\omega| \le \omega_c \\ 0 & \text{elsewhere} \end{cases}$$

Now, $h_d(n)$ may be obtained by taking inverse Fourier transform of above equation, i.e

$$h_d(n) = \frac{\sin\left[\omega_c\left(n - \frac{M}{2}\right)\right]}{\pi\left(n - \frac{M}{2}\right)}, \text{ for } 0 \le n \le M,$$

Substituting for $\omega_c = 0.2\pi$ and M = 223,

$$h_d(n) = \frac{\sin[0.2\pi(n-111.5)]}{\pi(n-111.5)}, \ for \ 0 \le n \le 223,$$

The unit sample response of FIR filter may be obtained by windowing, i.e.

$$h[n] = h_d[n]\omega[n]$$

$$h(n) = \frac{\sin[0.2\pi(n-111.5)]}{\pi(n-111.5)} \frac{I_0\left[3.395\left(\sqrt{1-\binom{(n-115.5)}{111.5}}\right)^2\right)}{I_0(3.395)}, \ for \ 0 \le n \le 223,$$

This is the required relationship for unit sample response FIR filter using Kaiser Window.

13. Design a lowpass Butterworth filter to meet the following specifications.

Passband gain = 0.89

Passband frequency edge = 30 Hz

Attenuation = 0.20

Stopband edge = 75 Hz

(Use impulse invariance and Bilinear Transformation method to convert the filter from analog to digital).

Solution:→

We have

$$\Omega_p = 2\pi \times 30 = 60\pi \text{ rad/s} \qquad (F_p = 30 \text{ Hz})$$

$$\Omega_{\rm s} = 2\pi \times 75 = 150\pi \text{ rad/s}$$
 (F_s = 75 Hz)

$$\alpha_{\text{max}} = -20\log_{10}(0.89) = 1.0122 \, dB$$

$$\alpha_{min} = -20 \log_{10}(0.20) = 13.9794 \, dB$$

$$\alpha_{min} = -20 \log_{10}(0.20) = 13.9794 \, dB$$

$$\varepsilon^2 = 10^{0.1\alpha_{max}} - 1 = 10^{0.10122} - 1 = 0.2625 \Longrightarrow \varepsilon = 0.5123$$

$$\delta^2 = 10^{0.1\alpha_{min}} - 1 = 10^{1.39794} - 1 = 24 = 0$$

$$\delta^{2} = 10^{0.1\alpha_{min}} - 1 = 10^{1.39794} - 1 = 24 = \gg \delta = 4.899$$

$$\therefore N = \frac{\log_{10}\left(\frac{\delta}{\varepsilon}\right)}{\log_{10}\left(\frac{\Omega_{s}}{\Omega_{p}}\right)} = \frac{\log_{10}\left(\frac{4.899}{0.5123}\right)}{\log_{10}\left(\frac{150\pi}{60\pi}\right)} = \frac{0.9806}{0.3979} = 2.4644$$

Since the number of poles must be an integer, we round up to N = 3.

Matching the frequency response exactly at stopband produces,

$$\Omega_c = \frac{\Omega_s}{\frac{1}{6N}} = \frac{150\pi}{4899\frac{1}{3}} = 277.4632$$

[Note: If we were instead to match the frequency response at passband, we would obtain

$$\Omega_c = \frac{\Omega_p}{\varepsilon^{\frac{1}{N}}} = \frac{60\pi}{0.5123^{\frac{1}{3}}} = 235.5734$$

In principle, any value of the critical frequency that satisfies $\frac{\Omega_p}{\frac{1}{2}} \le \Omega_c \le \frac{\Omega_s}{\frac{1}{2}}$ would be valid.]

For N = 3 and $\Omega_c = 1$ (Normalized Transfer function)

$$H(s) = \frac{1}{(s+1)(s^2+s+1)}$$

(This can be obtained from formula as well as table given)

This transfer function is normalized for $\Omega_c = 1$. However $\Omega_c = 277.46$, we need to denormalize H(s) by $\Omega_c = 277.46$ rad/s

$$H(s)|s = {}^{S}/_{\Omega_{c}} = \frac{\Omega_{c}^{3}}{(s + \Omega_{c})(s^{2} + \Omega_{c}s + \Omega_{c}^{2})} = \frac{2.136 \times 10^{7}}{(s + 277.46)(s^{2} + 277.46s + 76984)}$$

Using Impulse invariance method:

$$H(s) = \frac{2.136 \times 10^7}{(s + 277.46)(s^2 + 277.46s + 76984)} = \frac{A}{s + 277.46} + \frac{Bs + c}{s^2 + 277.46s + 76984}$$

Solving we get,
$$A = 277.46$$
, $B = -277.46$ and $C = 0$.

$$H(s) = \frac{277.46}{s + 277.46} = \frac{277.46s}{s^2 + 277.46} - \frac{277.46s}{s^2 + 2 \times s \times 138.73s + 138.73^2 + 230.29^2}$$

$$= \frac{277.46}{s + 277.46} - \frac{277.46(s + 138.73) - 38492}{(s + 138.73)^2 + 230.29^2}$$

$$= \frac{277.46}{s + 277.46} - \frac{277.46(s + 138.73)}{(s + 138.73)^2 + 230.29^2} + \frac{\frac{38492}{230.29} * 230.29}{(s + 138.73)^2 + 230.29^2}$$

Using mapping method:

$$H(z) = \frac{277.46}{1 - e^{-277.46T}z^{-1}} - 277.46 \times \frac{1 - e^{-138.73T}\cos(230.29T)z^{-1}}{1 - 2e^{-138.73T}\cos(230.29T)z^{-1} + e^{-277.46T}z^{-2}} + 167.14 \times \frac{e^{-138.73T}\sin(230.29T)z^{-1}}{1 - 2e^{-138.73T}\cos(230.29T)z^{-1} + e^{-277.46T}z^{-2}}$$

Analog Domain H(s)	Digital Domain H(z)
1	1
$\overline{s-p_k}$	$\overline{1 - e^{p_k T} z^{-1}}$

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s + a	$1 - e^{-aT}cos(bT)z^{-1}$
$(s+a)^2+b^2$	$1 - 2e^{-aT}cos(bT)z^{-1} + e^{-2aT}z^{-2}$
<i>b</i>	$e^{-aT}sin(bT)z^{-1}$
$(s+a)^2+b^2$	$1 - 2e^{-aT}cos(bT)z^{-1} + e^{-2aT}z^{-2}$

ii. Using Bilinear Transformation Method:

$$s = \frac{2}{T} \left(\frac{1 - z^{-1}}{1 + z^{-1}} \right).$$

$$H(s) = \frac{2.136 \times 10^7}{(s + 277.46)(s^2 + 277.46s + 76984)}$$

$$H(s) = \frac{2.136 \times 10^{7}}{(s + 277.46)(s^{2} + 277.46s + 76984)}$$

$$\therefore H(z) = \frac{2.136 \times 10^{7}}{\left(\frac{2}{T}\left(\frac{1 - z^{-1}}{1 + z^{-1}}\right) + 277.46\right)\left(\left(\frac{2}{T}\left(\frac{1 - z^{-1}}{1 + z^{-1}}\right)\right)^{2} + 277.46\frac{2}{T}\left(\frac{1 - z^{-1}}{1 + z^{-1}}\right) + 76984\right)}$$

Butterworth Polynomials in Factorized form		
Order(n)	$H(s) = H(s) = \frac{1}{A(s)}, Where A(s)$	
1	(s+1)	
2	$(s^2 + 1.4142s + 1)$	
3	$(s+1)(s^2+s+1)$	
4	$(s^2 + 1.8478s + 1)(s^2 + 0.7654s + 1)$	
5	$(s+1)(s^2+0.6180s+1)(s^2+1.6180s+1)$	
6	$(s^2 + 1.414s + 1)(s^2 + 0.5176s + 1)(s^2 + 1.9319s + 1)$	
7	$(s+1)(s^2+0.445s+1)(s^2+1.247s+1)(s^2+1.802s+1)$	

14. Design a digital lowpass Butterworth filter to meet the following specifications.

- Passband cutoff frequency: $\omega_p = 0.15\pi$
- Stopband cutoff frequency: $\omega_s = 0.35\pi$
- Passband ripple: $-3dB \le |H(e^{j\omega})| \le 0dB$, $|\omega| \le \omega_n$
- Stopband ripple: $|H(e^{j\omega}) \le -20dB$, $\omega_s \le |\omega| \le \pi$

Use impuse invariance method.

Solution:

Given,

$$\alpha_{max} = 3dB$$
, $\alpha_{min} = 20dB$, $\omega_{p} = 0.15\pi$, $\omega_{s} = 0.35\pi$

$$\varepsilon^2 = 10^{0.1\alpha_{max}} - 1 = 10^{0.3} - 1 = 0.995 ==> \varepsilon = 0.998$$

 $\delta^2 = 10^{0.1\alpha_{min}} - 1 = 10^2 - 1 = 99 ==> \delta = 9.95$

Using the impulse invariance design procedure, we have noted that the relation between frequency in the continuous-time and discrete-time domains is $\omega = \Omega T$, where T is merely a design parameter. Leaving T as an arbitrary constant for now, we obtain

$$\Omega_{p} = \frac{\omega_{p}}{T} = \frac{0.47124}{T}, \text{ and } \Omega_{s} = \frac{\omega_{s}}{T} = \frac{1.0996}{T}$$

$$\therefore N = \frac{\log_{10}\left(\frac{\delta}{\varepsilon}\right)}{\log_{10}\left(\frac{\Omega_{s}}{\Omega_{p}}\right)} = \frac{\log_{10}\left(\frac{9.95}{0.998}\right)}{\log_{10}\left(\frac{1.0996}{0.47124}\right)} = \frac{0.998}{0.369} = 2.712$$

Since the number of poles must be an integer, we round up to N = 3.

Matching the frequency response exactly at passband produces,

$$\Omega_c = \frac{\Omega_p}{\frac{1}{\varepsilon_N^{\frac{1}{N}}}} = \frac{0.4716}{T}$$

For N = 3 and Ω_c = 1 (Normalized Transfer function)

$$H(s) = \frac{1}{(s+1)(s^2+s+1)}$$

(This can be obtained from formula as well as table given)

This transfer function is normalized for Ω_c = 1. However Ω_c = 0.4716/T, we need to denormalise H(s) by Ω_c = 0.4716/T

$$H(s)|s = {}^{S}/_{\Omega_{c}} = \frac{{\Omega_{c}}^{3}}{(s + \Omega_{c})(s^{2} + \Omega_{c}s + {\Omega_{c}}^{2})} = \frac{\left(\frac{0.4716}{T}\right)^{3}}{\left(s + \frac{0.4716}{T}\right)\left(s^{2} + \frac{0.4716}{T}s + \left(\frac{0.4716}{T}\right)^{2}\right)}$$

Using partial fractions we can rewrite the system function of the continuous-time prototype filter as

$$H(s) = \sum_{k=1}^{N} \frac{A_k}{s - s_k},$$

where the parameters A_k are the continuous time residues of the poles s_k .

Using the MATLAB routine *residue* we find the residues for the three poles, producing the transfer function

$$H(s) = \frac{0.4719}{s + \frac{0.4716}{T}} \pm \frac{0.236 - 0.136j}{s - \frac{-0.236 + 0.408j}{T}} + \frac{-0.236 + 0.136j}{s - \frac{-0.236 - 0.408j}{T}}$$

The corresponding discrete-time filter has the transfer function

$$H(z) = \sum_{k=1}^{N} \frac{A_k}{1 - e^{s_k T} z^{-1}}$$

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Note that the poles of the continuous-time filter, s_k are all of the form of a (generally complex) constant divided by the parameter T. Since s_k is multiplied by T wherever it appears in the equation for H(z) above, the specific value chosen for T has no effect at all on the discrete-time filter that results from the design process. Hence we normally let T=1 for simplicity. This produces the transfer function

$$H(z) = \frac{0.4716}{1 - e^{-0.4716}z^{-1}} + \frac{-0.236 - 0.136j}{1 - e^{(-0.236 + 0.408j)}z^{-1}} + \frac{-0.236 + 0.136j}{1 - e^{(-0.236 - 0.408j)}z^{-1}}$$
Combining we get,
$$H(z) = \frac{0.4716}{1 - 0.624z^{-1}} + \frac{-0.472 + 0.341z^{-1}}{1 - 1.45z^{-1} + 0.624z^{-2}}$$

