

# **EE4580 –Quasi-Optical Systems**

## **Elliptical lens**

### **MATLAB Instruction**

**27 Feb. 2020**

# Description

Write a Matlab program to analyze and design a planar antenna placed at the focal point of an elliptical lens made of a material with a certain  $\epsilon_r$ . Suppose that the lens is illuminated by a planar antenna operating at 100GHz and whose far field inside an infinite medium has the following expression:

$$E_{far}^a(\theta, \phi) = \cos^n \theta (\cos \phi \hat{\theta} - \sin \phi \hat{\phi}) \frac{e^{-jk_d r}}{r}$$

Where  $k_d = \sqrt{\epsilon_r} k_0$

Provide the following plots:

- The far field of the planar antenna in the infinite medium ( $\epsilon_r = 11.9$ ) for  $n = 3$ .
- Plot the equivalent aperture current distribution of an elliptical lens with  $\epsilon_r = 11.9$ ,  $D = 6\lambda_0$ , and  $\theta_0 = 55^\circ$  in the main planes of the antenna.
- Plot the far field patterns radiated by the lens. Compare with the far field of an equivalent uniform aperture (airy pattern).
- Give an estimation of the directivity and gain of such lens antenna.
- Find the phase center of the lens antenna.

# Feeding antenna

## Step 1: Write a routine to evaluate the radiation of the lens feed

```
[Eth, Eph, Prad] = FeedLens(kd, r, th, ph, n)
```

Antenna far field:

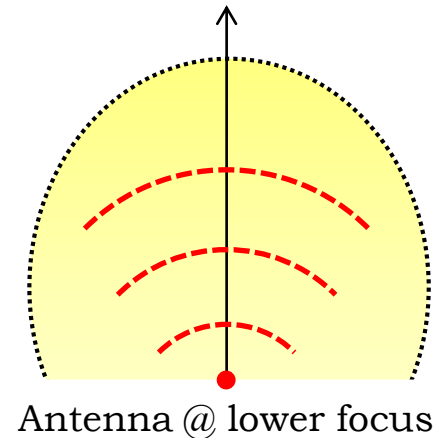
$$E_{far}^a(\theta, \phi) = \cos^3 \theta (\cos \phi \hat{\theta} - \sin \phi \hat{\phi}) \frac{e^{-jk_d r}}{r}$$

Where  $k_d = \sqrt{\epsilon_r} k_0$ ,  $\epsilon_r = 11.9$

Power radiated by the antenna (inside the lens):

$$P_{rad}^{feed} = \int_0^{2\pi} \int_0^{\pi/2} U(\theta, \phi) \sin \theta d\theta d\phi$$

$$U(\theta, \phi) = \frac{|E_{far}^a((\theta, \phi))|^2}{2\zeta_d} r^2 \quad \zeta_d = \zeta_0 / \sqrt{\epsilon_r}$$



# Elliptical lens antenna

## Step 2: Write a routine to evaluate the equivalent aperture current distribution of an elliptical lens antenna

```
[Jx, Jy] = LensAperture(th, ph, r, e, er, n);
```

### 1) Lens geometry

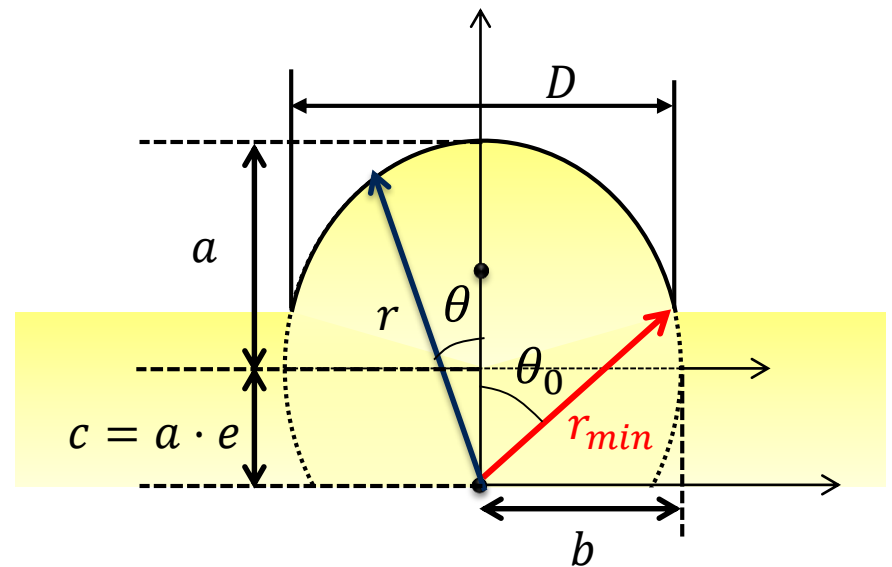
$$D = 6\lambda_0, \theta_0 = 55^\circ, e = 1/\sqrt{\epsilon_r}$$

$$r = a \frac{1 - e^2}{1 - e \cos \theta} \quad \longrightarrow \quad a, b, c$$

### 2) Surface Parametrization

$$\rho = r \sin \theta \in \left[0, \frac{D}{2}\right] \quad \phi \in [0, 2\phi]$$

$$\left(\frac{z - c}{a}\right)^2 + \left(\frac{\rho}{b}\right)^2 = 1 \quad \longrightarrow \quad \theta = \text{atan} \frac{\rho}{z}$$



# Ellipsoid Parameters

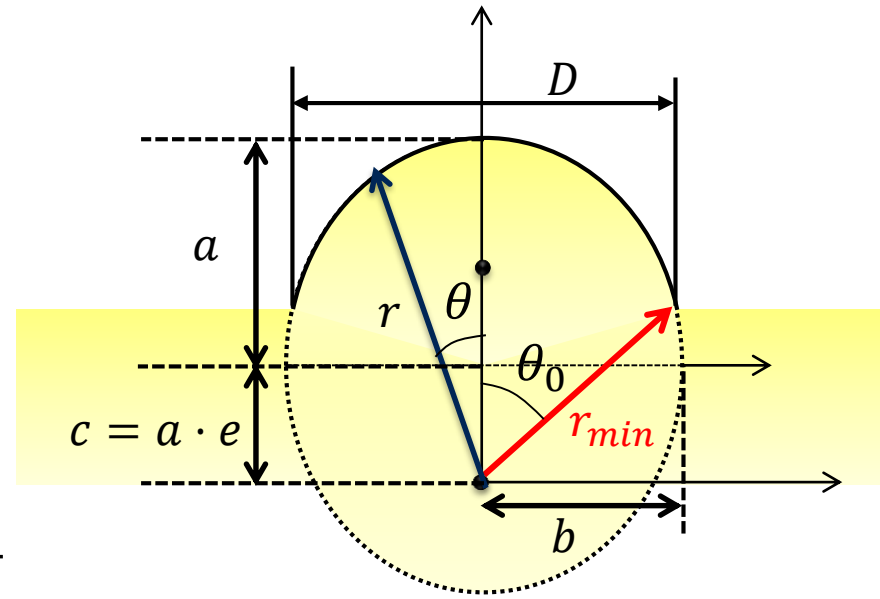
$$\sin \theta_0 = \frac{D/2}{r_{min}} \quad \Rightarrow \quad r_{min} = \frac{D/2}{\sin \theta_0}$$

$$r = a \frac{1 - e^2}{1 - e \cos \theta} \quad \Rightarrow \quad r_{min} = a \frac{1 - e^2}{1 - e \cos \theta_0}$$

$$a = r_{min} \frac{(1 - e \cos \theta_0)}{1 - e^2}$$

$$c = a \cdot e$$

$$b = \sqrt{a^2 - c^2}$$



# Equivalent current distribution

$$\vec{J}_s(\vec{\rho}) \approx \hat{z} \times \vec{H}_t|_S = -\frac{1}{\zeta_0} \left( \tau^{\parallel}(\theta_i) E_i^{\theta}(\vec{r}) \hat{\rho} + \tau^{\perp}(\theta_i) E_i^{\phi}(\vec{r}) \hat{\phi} \right) \frac{S(\vec{r})}{r} \left[ e^{-jk_0 r'} e^{-jk_a r} \right]$$

Constant phase term can be neglected

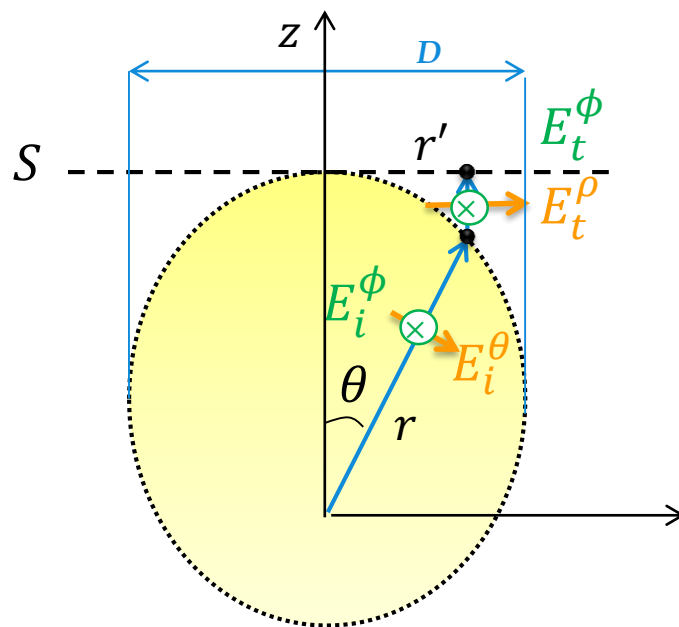
## 3) Equivalent current

$$\hat{\rho} = \hat{x} \cos \phi + \hat{y} \sin \phi \quad \hat{\phi} = -\hat{x} \sin \phi + \hat{y} \cos \phi$$

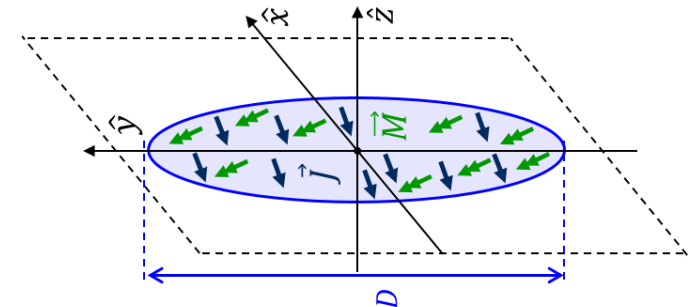
$$E_{far}^a(\theta, \phi) = \cos^3 \theta (\cos \phi \hat{\theta} - \sin \phi \hat{\phi}) \frac{e^{-jk_a r}}{r}$$

$$\rightarrow \vec{E}_i(\vec{r}) = \left( E_i^{\theta}(\theta, \phi) \hat{\theta} + E_i^{\phi}(\theta, \phi) \hat{\phi} \right) \frac{e^{-jk_a r}}{r}$$

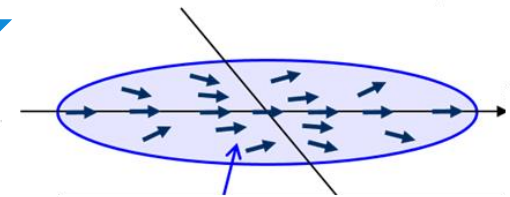
$$\vec{J}_s(\vec{\rho}) \approx -\frac{2}{\zeta_0} \left( \hat{x} \left( \tau^{\parallel}(\theta_i) E_i^{\theta}(\theta, \phi) \cos \phi - \tau^{\perp}(\theta_i) E_i^{\phi}(\theta, \phi) \sin \phi \right) + \hat{y} \left( \tau^{\parallel}(\theta_i) E_i^{\theta}(\theta, \phi) \sin \phi + \tau^{\perp}(\theta_i) E_i^{\phi}(\theta, \phi) \cos \phi \right) \right) \frac{S(\vec{r})}{r}$$



Both  $\vec{J}_s(\vec{\rho})$  and  $\vec{M}_s(\vec{\rho})$



$2 \vec{J}_s(\vec{\rho})$



# Equivalent current distribution

$$\vec{J}_s(\vec{r}) \approx -\frac{2}{\zeta_0} \left( \hat{x} \left( \tau^{\parallel}(\theta_i) E_i^{\theta}(\theta, \phi) \cos \phi - \tau^{\perp}(\theta_i) E_i^{\phi}(\theta, \phi) \sin \phi \right) + \hat{y} \left( \tau^{\parallel}(\theta_i) E_i^{\theta}(\theta, \phi) \sin \phi + \tau^{\perp}(\theta_i) E_i^{\phi}(\theta, \phi) \cos \phi \right) \right) \frac{S(\vec{r})}{r}$$

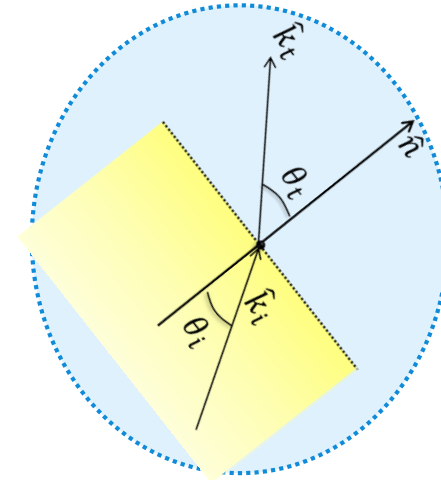
## 4) Transmission coefficients

$$\tau^{\perp} = 1 + \Gamma^{\perp} = \frac{2\zeta_0 \cos \theta_i}{\zeta_0 \cos \theta_i + \zeta_d \cos \theta_t}$$

$$\tau^{\parallel} = (1 + \Gamma^{\parallel}) \frac{\cos \theta_i}{\cos \theta_t} = \frac{2\zeta_0 \cos \theta_i}{\zeta_0 \cos \theta_t + \zeta_d \cos \theta_i}$$

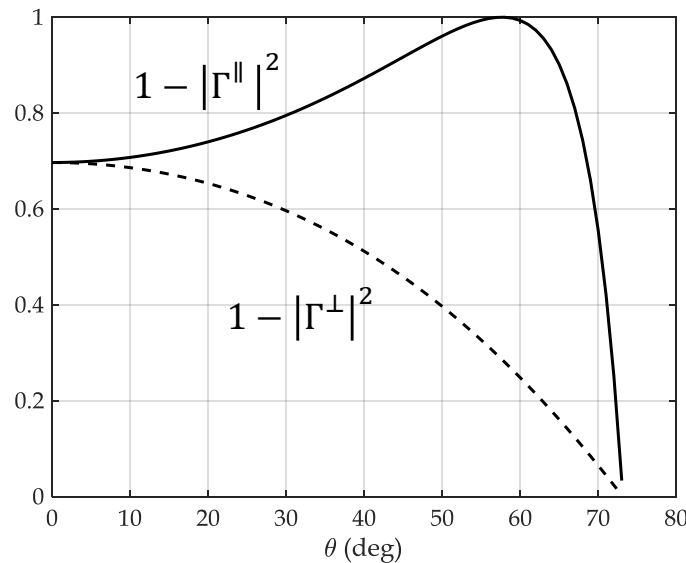
Relate  $\theta$  to  $\theta_i$ :

$$\begin{cases} \cos \theta_i = \hat{k}_i \cdot \hat{n} = \frac{1 - e \cos \theta}{\sqrt{1 + e^2 - 2e \cos \theta}} \\ \cos \theta_t = \hat{k}_t \cdot \hat{n} = \frac{\cos \theta - e}{\sqrt{1 + e^2 - 2e \cos \theta}} \end{cases}$$



## 5) Spreading factor

$$S(\vec{r}) = \sqrt{\frac{\cos \theta_t e \cos \theta - 1}{\cos \theta_i e - \cos \theta}} = 1$$



$$\hat{n} = \frac{(\cos \theta - e) \hat{z} + \sin \theta \hat{\rho}}{\sqrt{1 + e^2 - 2e \cos \theta}}$$

# Far field of the lens antenna

## Step 3: Far field radiation of the lens antenna

$$k_{xf} = k_0 \sin \theta_f \cos \phi_f$$

$$k_{yf} = k_0 \sin \theta_f \sin \phi_f$$

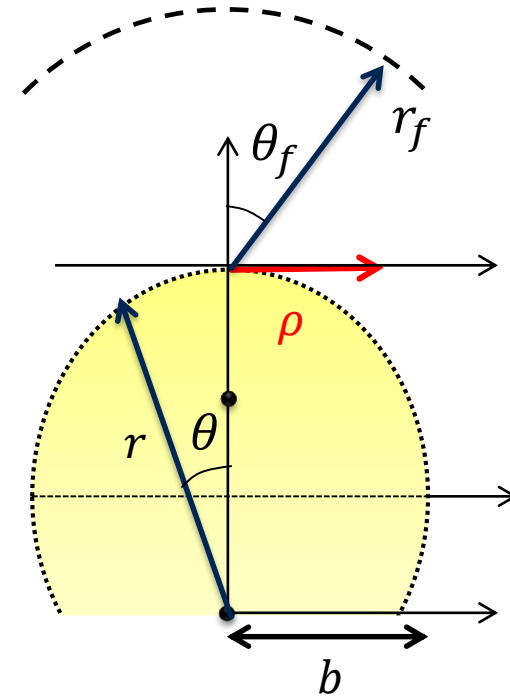
$$k_{zf} = k_0 \cos \theta_f$$

Calculate FT of currents:

$$J_s^{x/y}(k_{xf}, k_{yf}) = \int_0^a \int_0^{2\pi} J_s^{x/y}(\rho, \phi) e^{jk_{xf}\rho \cos(\phi)} e^{jk_{yf}\rho \sin(\phi)} \rho d\rho d\phi$$

Calculate far field:

$$\vec{E}_{lens}^{far}(\vec{r}_f) = jk_{zf} \tilde{G}_{fs}^{ej}(k_{xf}, k_{yf}) \vec{J}_s(k_{xf}, k_{yf}) \frac{e^{-jk_0 r_f}}{2\pi r_f}$$



Coordinate system for radiation outside the lens:  $[r_f, \theta_f, \phi_f]$



# Dir. & gain of the lens antenna

## Step 4: directivity and gain of the lens antenna

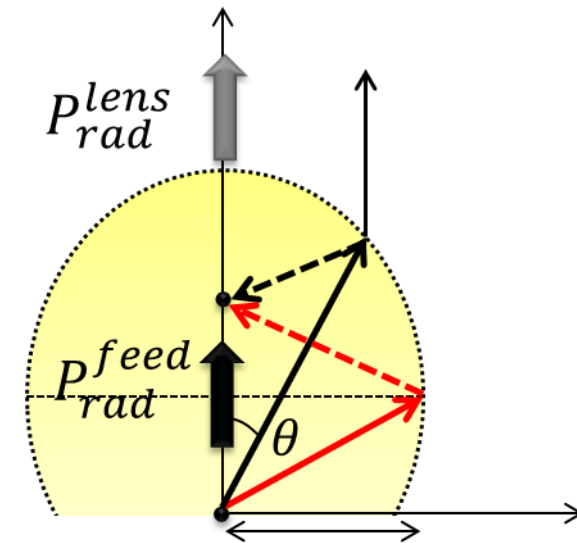
Calculate directivity  $D(\theta_f, \phi_f) = 4\pi U_{lens}/P_{rad}^{lens}$

$$U_{lens}(\theta_f, \phi_f) = \frac{|\vec{E}_{lens}^{ff}(\theta_f, \phi_f)|^2}{2\zeta_0} r_f^2$$

$$P_{rad}^{lens} = \int_0^{2\pi} \int_0^{\pi/2} U_{lens} \sin\theta_f d\theta_f d\phi_f$$

Radiation efficiency of the lens eff.:  $\eta_{rad} = \frac{P_{rad}^{lens}}{P_{rad}^{feed}}$

Gain:  $G(\theta_f, \phi_f) = D(\theta_f, \phi_f)\eta_{rad}$

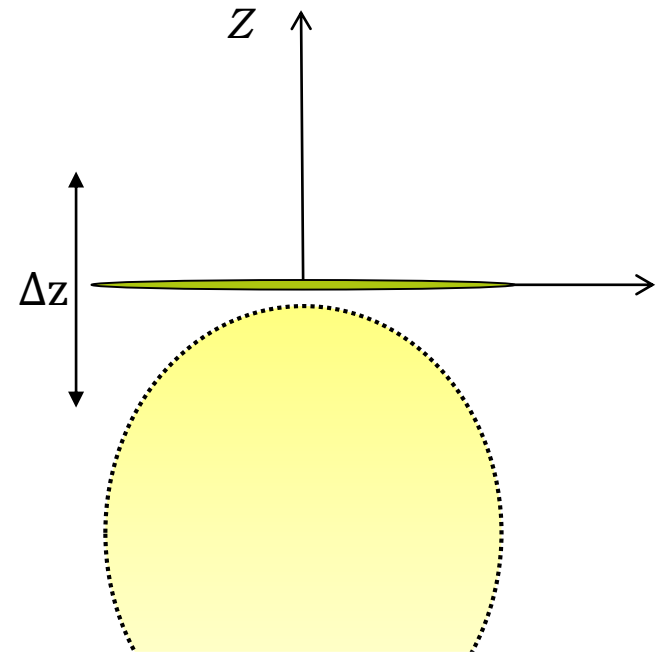


# Phase center

## Step 5: Phase center evaluation

Change in the z-origin of the reference system causes a phase shift in the far field:

$$\vec{E}_{lens}^{ff}(\Delta z) = \vec{E}_{lens}^{ff}(\Delta z = 0)e^{jk_0 \cos \theta_f \Delta z}$$



To evaluate the phase center:

- Plot the phase in the two main planes as a function of  $\Delta z$
- Do a parametric analysis for  $\Delta z \in [-3\lambda_0, 3\lambda_0]$
- The phase center will be the  $\Delta z$  where the variation of the phase in the main lobe is the lowest