



# Field Observation in Climatology and Environmental Hydrology

Module: Energy and mass exchange between  
the Earth's surface and the atmosphere

## Learning objectives

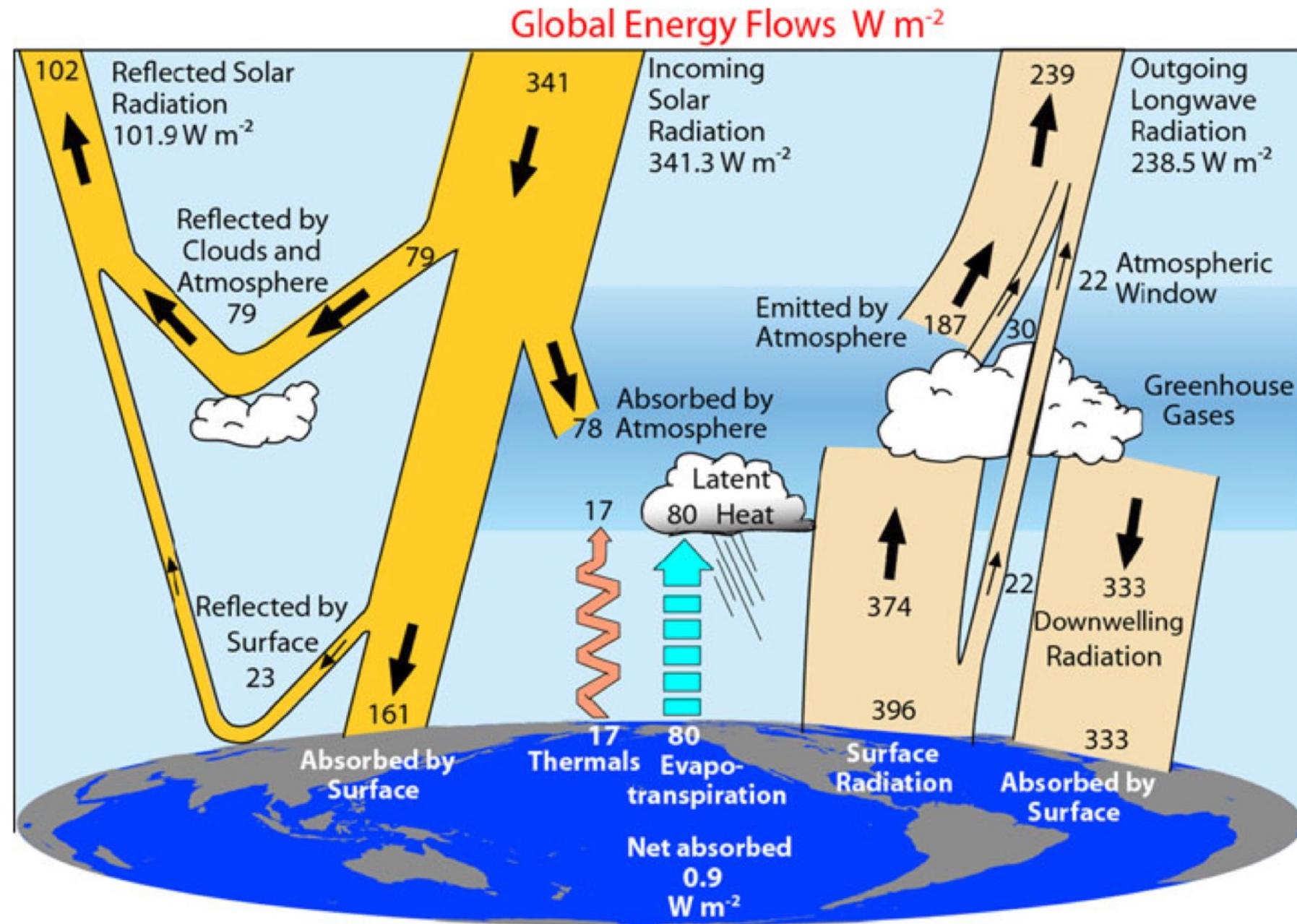
- ④ Properties of the Earth's surface
- ④ Energy and mass fluxes at the surface
- ④ Energy balance terms
- ④ Parametrizations of fluxes

# Why bother with the bottom boundary?

**... because**

- ④ without a bottom boundary there would be no boundary layer
- ④ Friction, heat and moisture fluxes from the surface modify the state of the BL
- ④ Heat and moisture fluxes are driven by the external forcings (radiation, transporation etc.)

# The global energy budget





# PLANCK'S LAW OF RADIATION

## Planck (1900):

Every body emits thermal radiation (energy), which depends on the temperature of the radiating body.

### Blackbody radiator:

- ◎ Body that completely absorbs incident electromagnetic radiation.
- ◎ It emits at the respective temperature with the maximum possible radiation intensity.
- ◎ In the mid- and far-IR range, natural land surfaces behave approximately like black bodies.

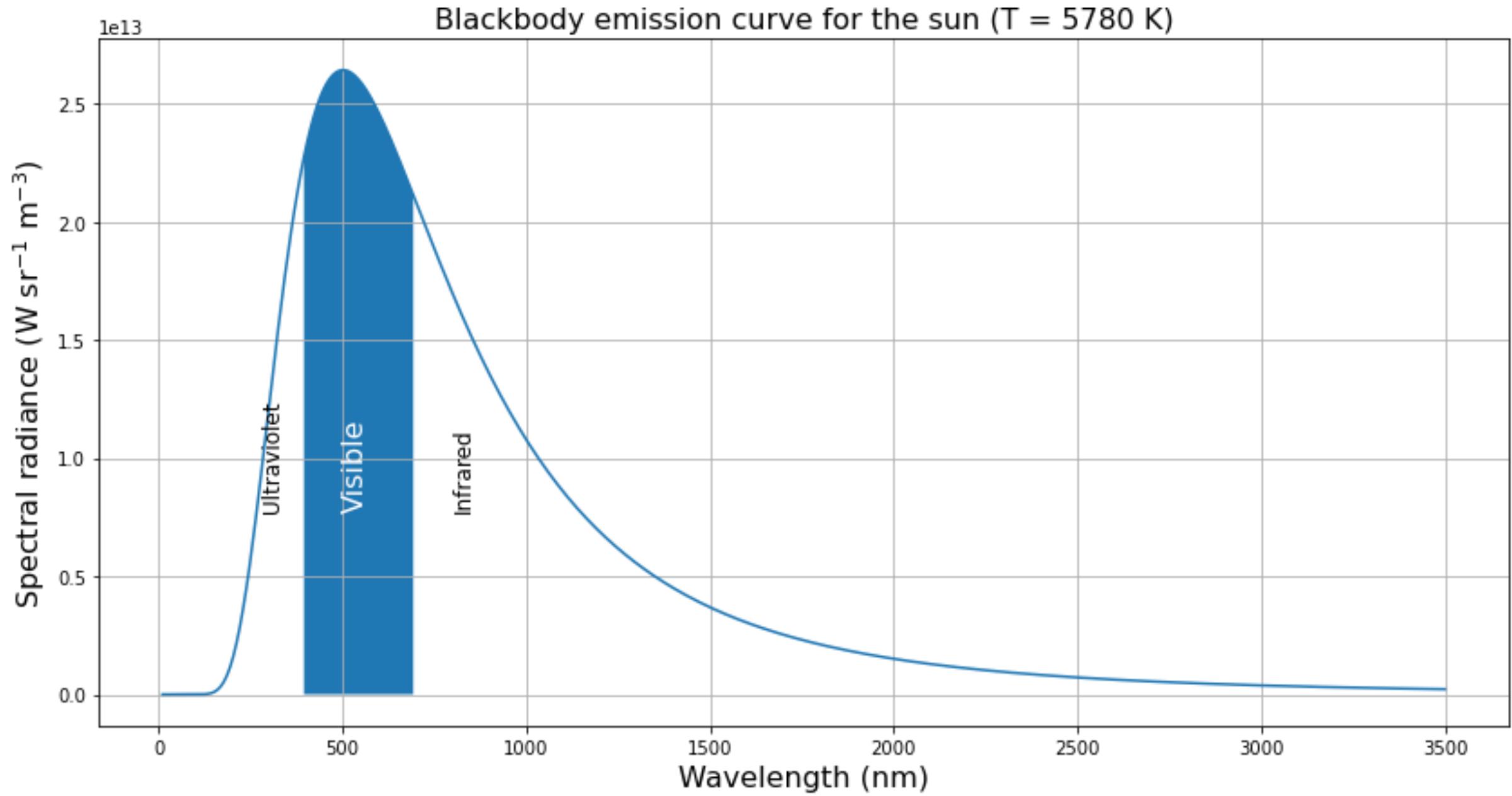
$$\frac{\partial Q}{\partial \lambda} = \frac{2hc^2}{\lambda^5 \left[ \exp\left(\frac{hc}{k\lambda T}\right) - 1 \right]}$$

$h \approx 6.626 * 10^{-34}$  Js (Plank'sche constant)

$k \approx 1.381 * 10^{-23}$  JK<sup>-1</sup> (Boltzmann-Constant)

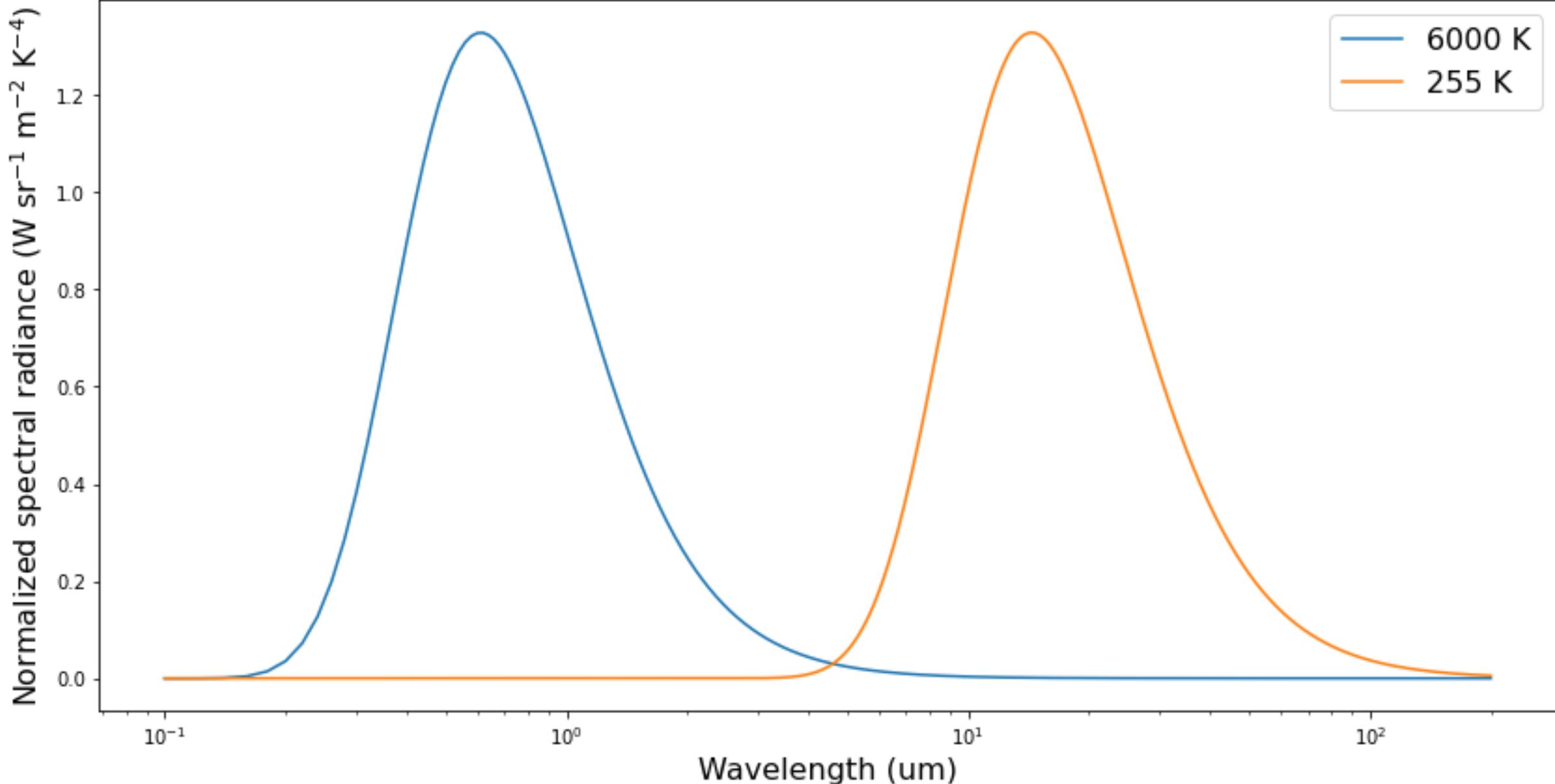
$c \approx 2.9979 * 10^8$  ms<sup>-1</sup> (Speed of light in a vacuum)

$\lambda$  = Wellenlänge



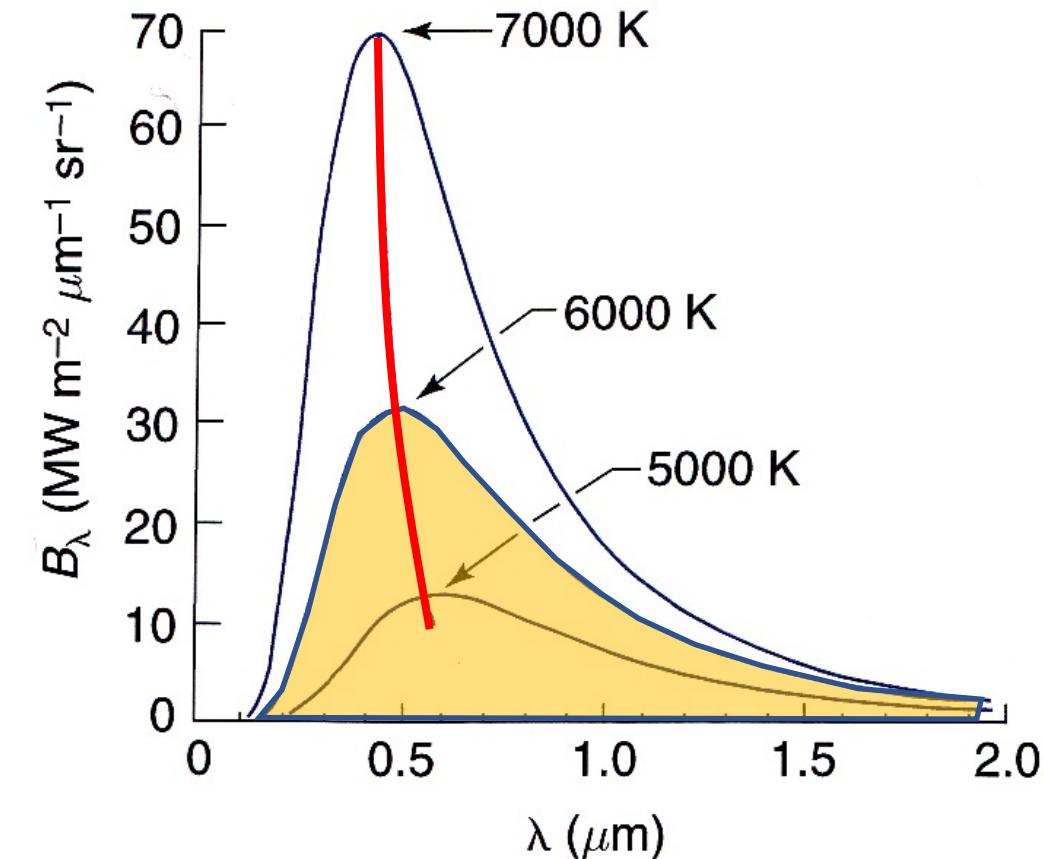
Source: Rose, 2020.

Normalized blackbody emission spectra  $T^{-4}\lambda B_\lambda$  for the sun ( $T_e = 6000$  K) and Earth ( $T_e = 255$  K)



Source: Rose, 2020.

# Stefan-Boltzmann Law



- ④ The curves describe the distribution of the energy over the different wavelengths
- ④ The areas under the curves describe the amount of radiated energy
- ④ The radiated energy is temperature-dependent, namely to the 4th power of the absolute temperature, more precisely:

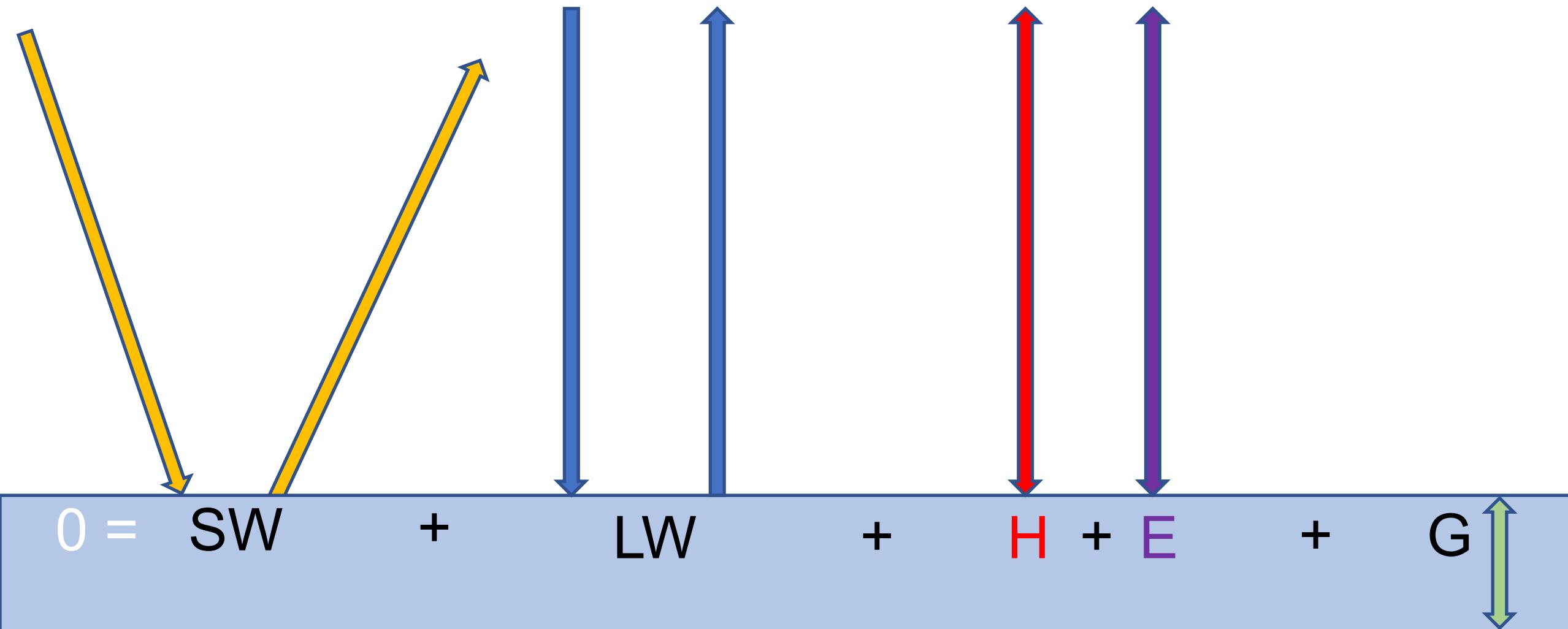
$$E = \sigma \cdot T^4 \quad \text{mit } \sigma = 5.67 \cdot 10^{-8} [\text{W/m}^2\text{K}^4]$$

- ④ → **Stefan-Boltzmann-Law**
- ④ The position of the emission maximum shifts to shorter and shorter wavelengths with increasing temperatures. The product of temperature and wavelength of the emission maximum is constant

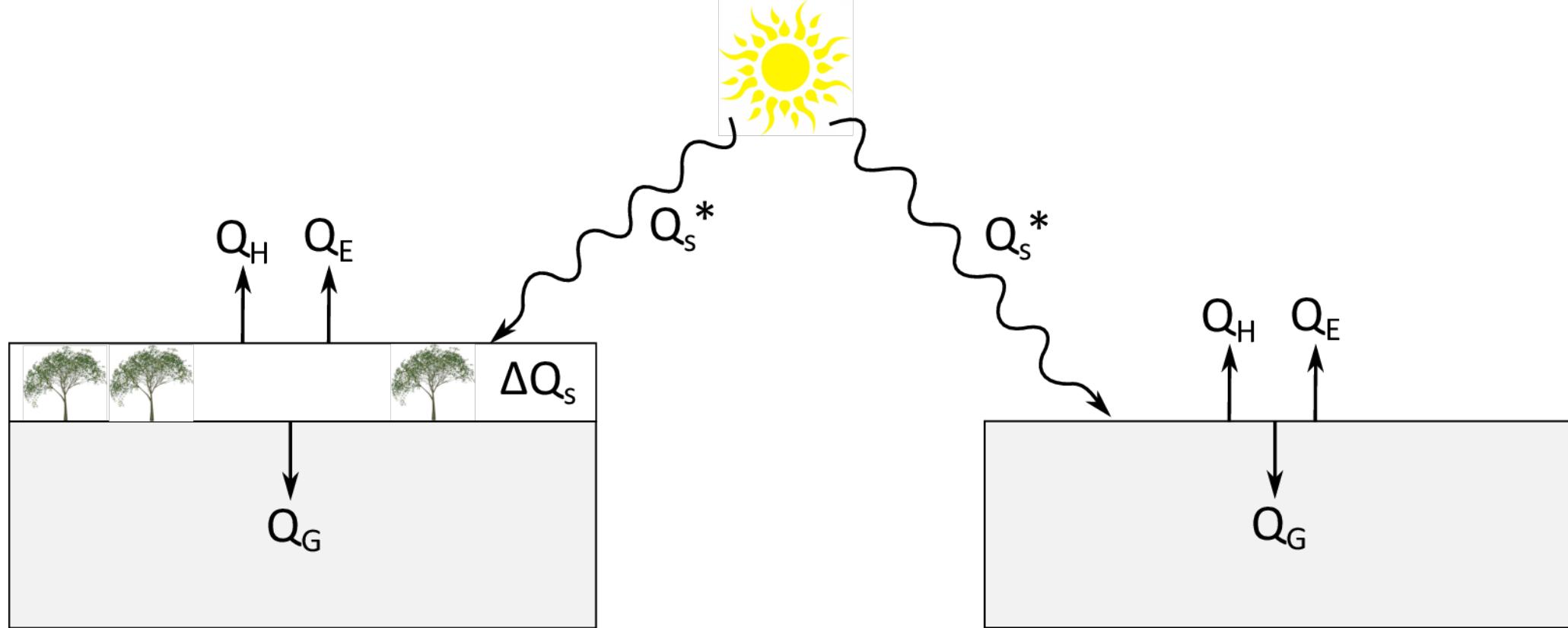
$$\lambda_{max} \cdot T = 2880 \mu\text{m} \cdot \text{K}$$

→ **Wien's law**

# Surface Energy Balance model (SEB)



# Surface Energy Balance



$$Q_s^* = Q_H + Q_E + Q_G + \Delta Q_s$$

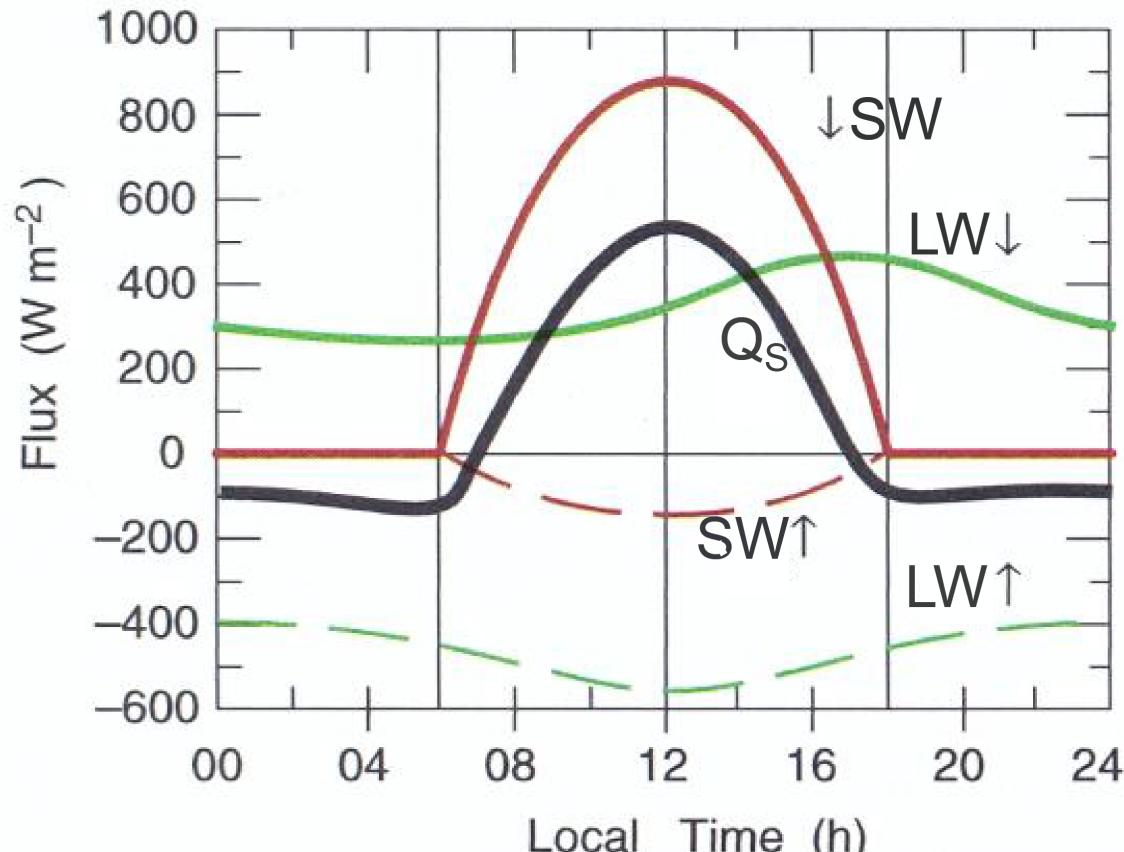
with  $Q_s^*$  the net radiation at the surface,  $Q_H$  the sensible heat flux,  $Q_E$  the latent heat flux,  $Q_G$  the ground heat flux, and  $\Delta Q_s$  the storage term (internal energy)

**FLUXES AWAY FROM SURFACE ARE POSITIVE, EXCEPT FOR NET RADIATION**

# Parametrization of radiation fluxes

$$Q_s^* = Q_H + Q_E + Q_G + \Delta Q_s$$

# Parametrization of radiation fluxes



$$Q_s^* = SW_u + SW_d + LW_u + LW_d$$

with  $SW_u$ : upwelling reflected shortwave radiation  
 $SW_d$ : downwelling shortwave radiation transmitted through the air  
 $LW_u$ : longwave (infrared, IR) radiation emitted up  
 $LW_d$ : longwave diffusive IR radiation down

# Shortwave radiation

$$SW_d = S_0 \cdot T_k \cdot \sin(\psi) \quad \text{for daytime (i.e. } \sin(\psi) \text{ is positive)}$$

$$SW_d = 0 \quad \text{for nighttime}$$

with the transmissivity (parametrization by Burridge and Gadd, 1974)

$$T_k = (0.6 + 0.2 \sin \psi) \cdot (1 - 0.4\sigma_{CH}) \cdot (1 - 0.7\sigma_{CM}) \cdot (1 - 0.4\sigma_{CL})$$

$\sigma_C$  represents the cloud cover fraction, and H, M, and L signify high, middle, and low clouds

and the local elevation angle (Zhang and Anthes, 1982)

$$\sin \psi = \sin \phi \sin \delta_s - \cos \phi \cos \delta_s \cos \left[ \left( \frac{\pi t_{UTC}}{12} - \lambda_e \right) \right]$$

$\phi$  : latitude (positive north) in radians

$\lambda$  : longitude (positive west) in radians

$t_{UTC}$  : Coordinated Universal Time in hours

$\delta_s$  is the solar declination angle (angle of the sun above the equator, in radians)

$$\delta_s = \phi_r \cos \left[ \frac{2\pi(d - d_r)}{d_y} \right]$$

$\phi_r$  : latitude of the Tropic of Cancer (0.409 radians)

$d$  : number of the day of the year

$d_r$  : day of the summer solstice (173)

$d_y$  : average number of days per year

# Albedo

$$SW_u = \alpha \cdot SW_d$$

Surface	a in %
Fresh snow	75-95
Wet snow	60-70
Firn	40-70
Glacier ice	30-45
Impure Glacier ice	20-30
Ocean, lakes	6-12
Wet sand	15-30
Dry sand	25-40
Rocks	10-40
Concrete	10-35
Dark soil	5-10
Forest	10-20
Meadows and fields	10-30

# Longwave radiation

with emissivities

$$\epsilon_a = 0.23 \cdot 0.433 \cdot \left( \frac{100 \cdot f \cdot E_{sat}(T_a)}{T_a} \right)^{1/8}$$

$$\epsilon_s = 1.0$$

with  $f$  the relative humidity,  $E_{sat}$  the saturation water vapour pressure, and  $T_a$  the air temperature.

$$LW_d = \epsilon_a \cdot \sigma \cdot T_a^4$$

$$LW_u = \epsilon_s \cdot \sigma \cdot T_0^4$$

# Parametrization of ground heat flux

$$Q_s^* = Q_H + Q_E + Q_G + \Delta Q_s$$

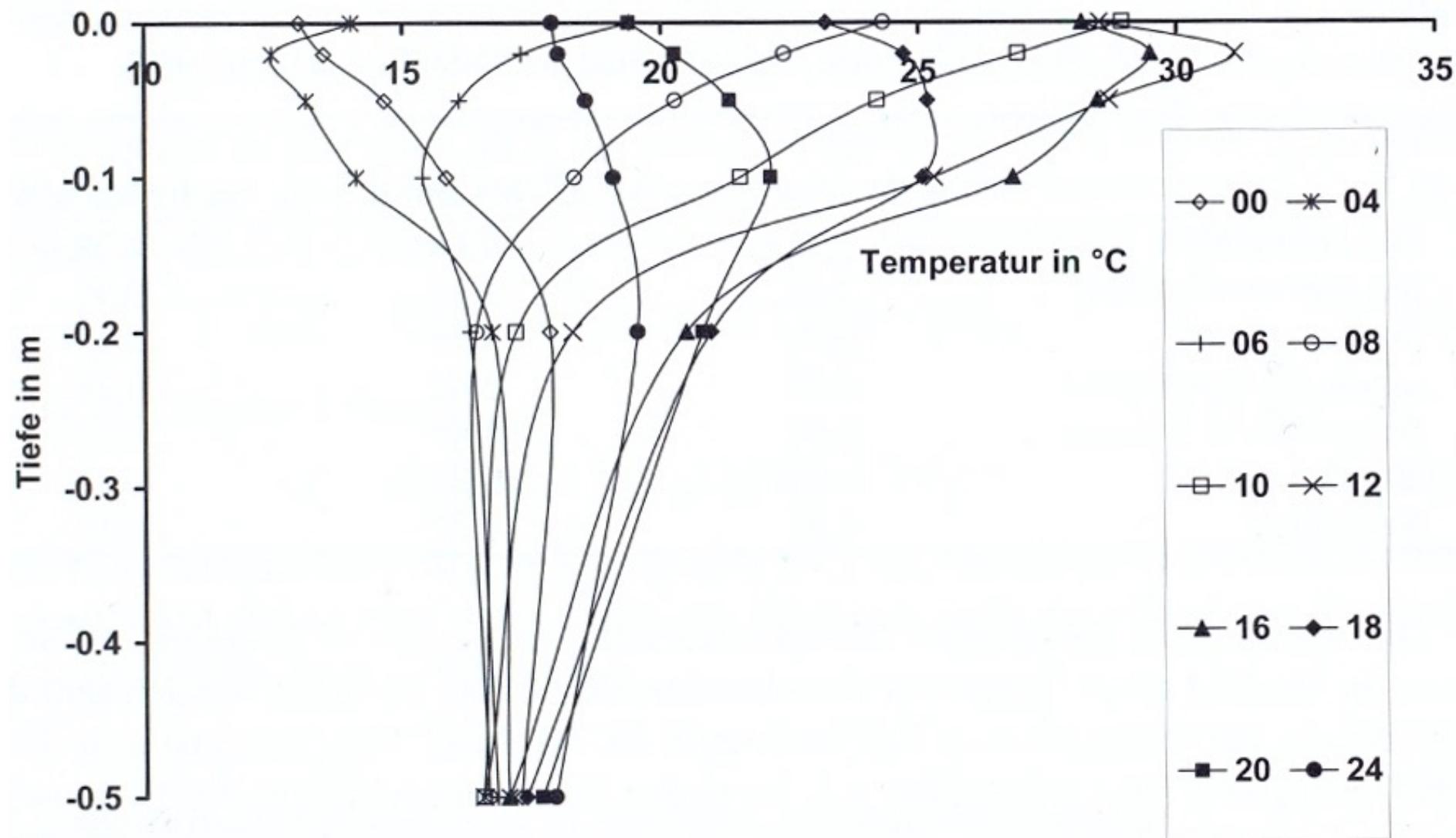
# Ground heat flux

Ground flux represents the heat flux into the ground measured at the top of the soil.

## Properties

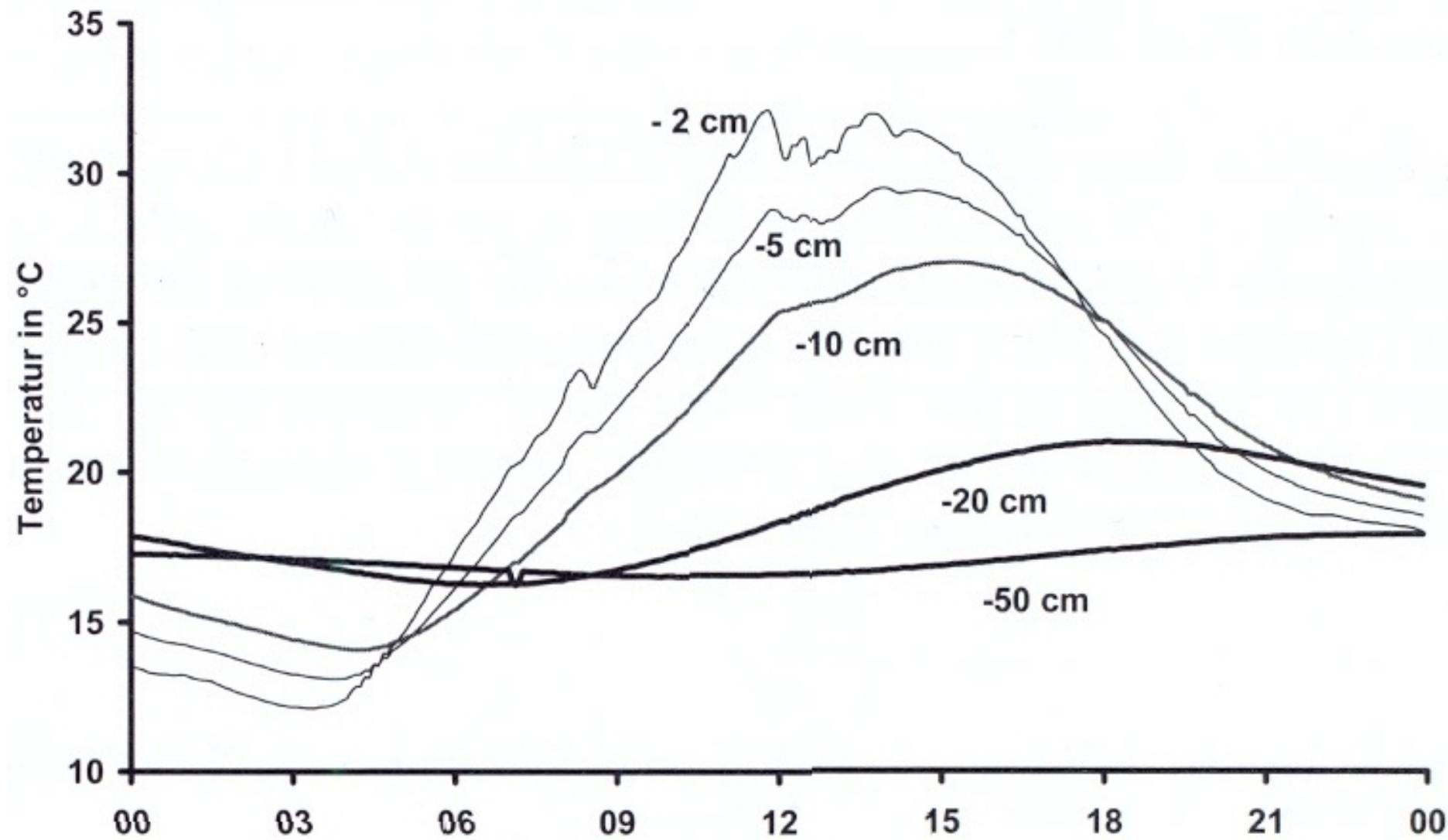
- ④ Small but significant component of the surface energy budget
- ④ The flux is related to the skin temperature
- ④ If not measured, we need to parametrize it

# Ground heat flux



Temperature profiles at indicated hours (Foken, 2008).

# Ground heat flux



Daily cycle of soil temperatures in various depths (Foken, 2008).

# Ground heat flux

Ground heat flux:

$$Q_G = -k_g \frac{\partial T}{\partial z} \quad (\text{Fourier's law})$$

Temporal temperature change:

$$\frac{\partial T}{\partial t} = - \left( \frac{1}{c_g} \right) \frac{\partial Q_g}{\partial z}$$

Heat conductivity equation:

$$\frac{\partial T}{\partial t} = \nu_g \frac{\partial^2 T}{\partial z^2}$$

with  $k_g$  : Thermal molecular conductivity [ $W m^{-1} K^{-1}$ ]

$c_g$  : Soil heat capacity [ $W m^{-3} K^{-1}$ ]

$\nu_g$  : Soil thermal diffusivity ( $\nu_g = k_g/c_g$ ) [ $m^2 s^{-1}$ ]

# Molecular Conductivity, Heat Capacity and Thermal Diffusivity

Surface	Thermal molecular conductivity $k_g$ in $[Wm^{-1} K^{-1}]$	Soil heat capacity $C_g$ in $10^6 [Wm^{-3} K^{-1}]$	Soil thermal diffusivity $\nu_g$ in $10^{-6} [m^2 s^{-1}]$
Granit	2.73	2.13	1.28
Wet sand	2.51	2.76	0.91
Dry sand	0.30	1.24	0.24
Sandy clay	0.92	2.42	0.38
Swamp	0.89	3.89	0.23
Old snow	0.34	0.84	0.40
Fresh snow	0.02	0.21	0.10
Pure ice	2.10	2.09	1.09

# Ground heat flux

## Amplitude Change with Depth

$$\Delta T(z) = \Delta T_{surface} \cdot \exp \left[ -z \left( \frac{\pi}{\nu_g P} \right)^{0.5} \right]$$

## Phase Shift

$$\Delta t = \left( \frac{\Delta z}{2} \right) \left[ \frac{P}{\pi \cdot \nu_G} \right]^{0.5}$$

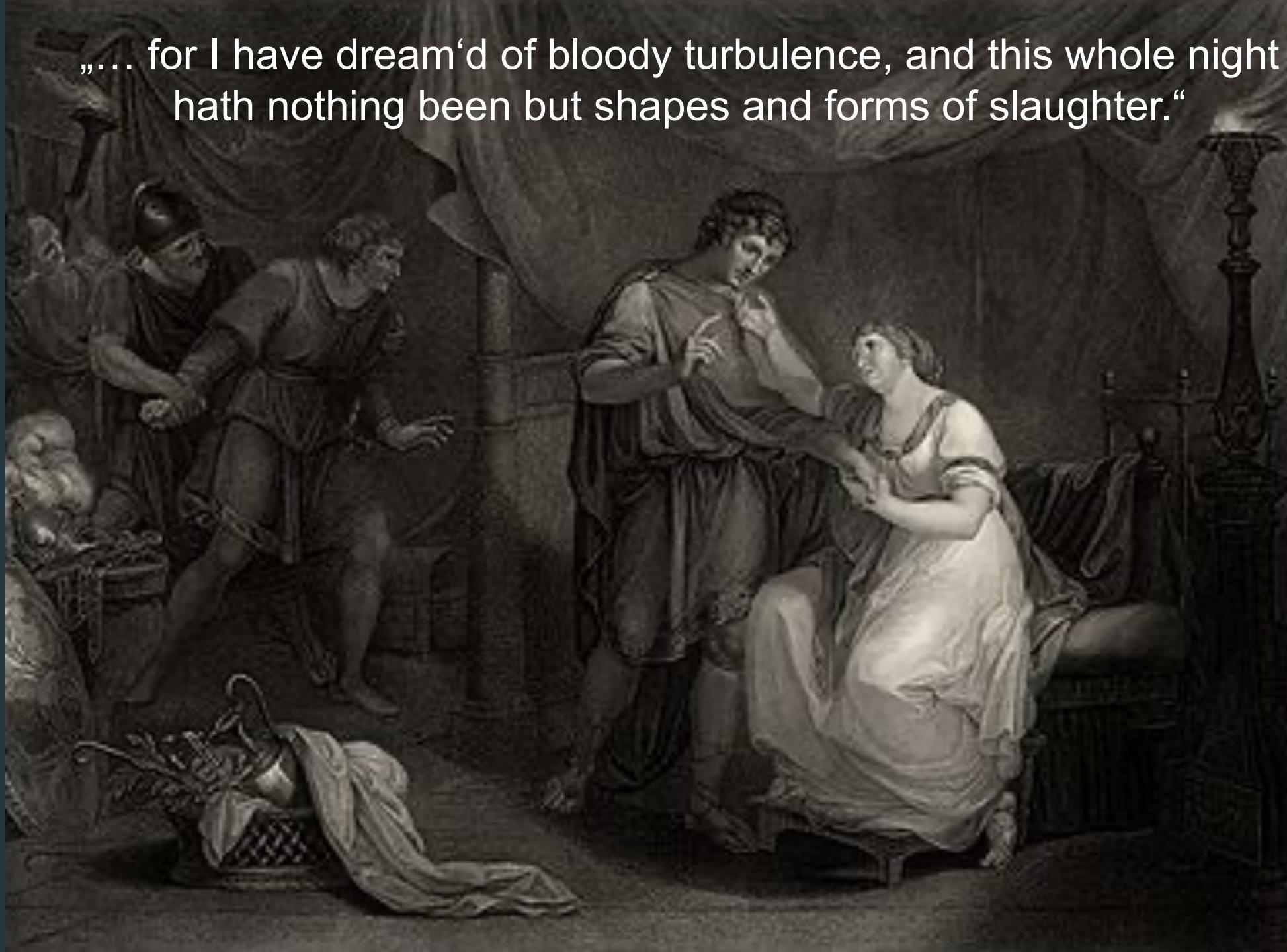
with  $\Delta T$  : Amplitude of wave  
 $P$  : Period of the cycle (daily or annual)

# Parametrization turbulent surface fluxes

$$Q_s^* = Q_H + Q_E + Q_G + \Delta Q_s$$

# William Shakespeare in „Troilus and Cressida“

„... for I have dream'd of bloody turbulence, and this whole night hath nothing been but shapes and forms of slaughter.“



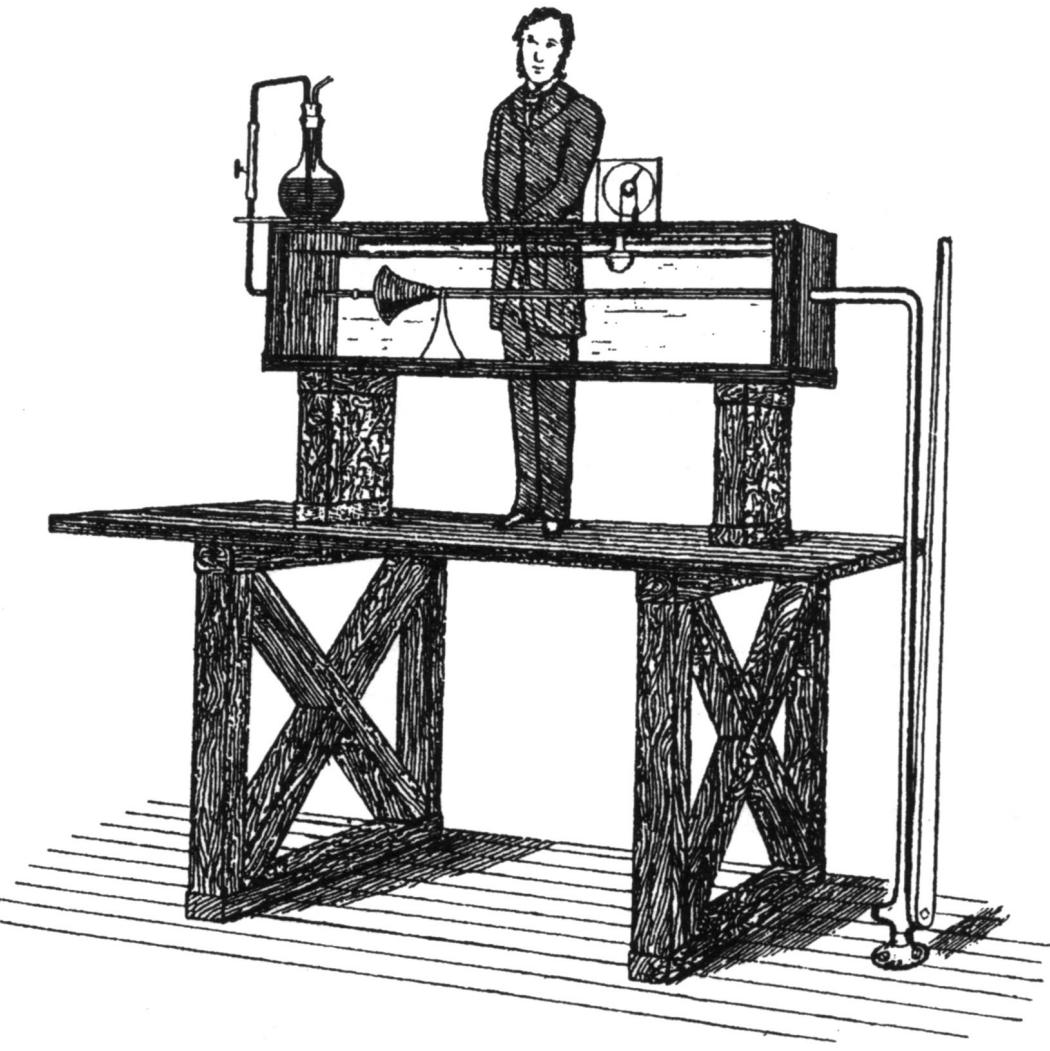
# Whirlpool of water from water from Leonardo Da Vinci (Anno 1513)





The great wave of Kanagawa from Katsushika Hokusai (ca. 1830).

# Osborne Reynolds (1842-1912)

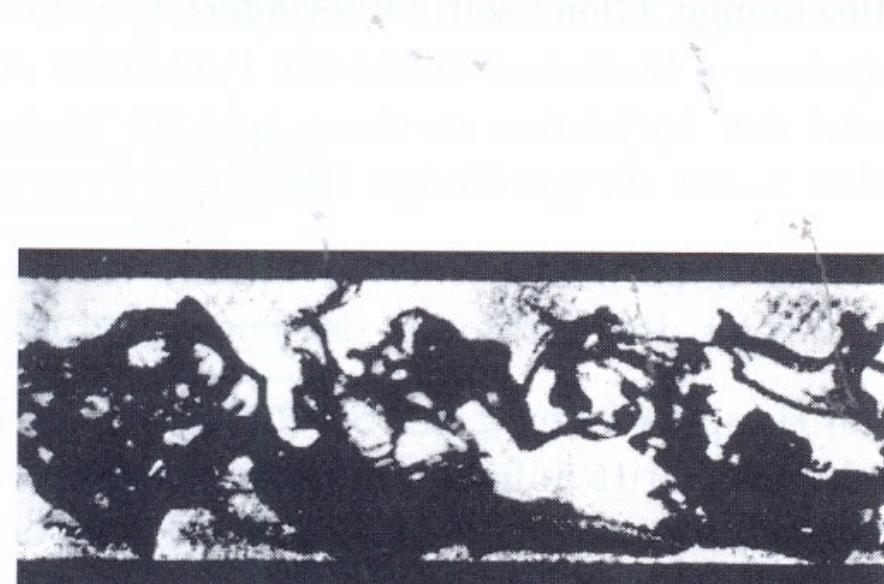
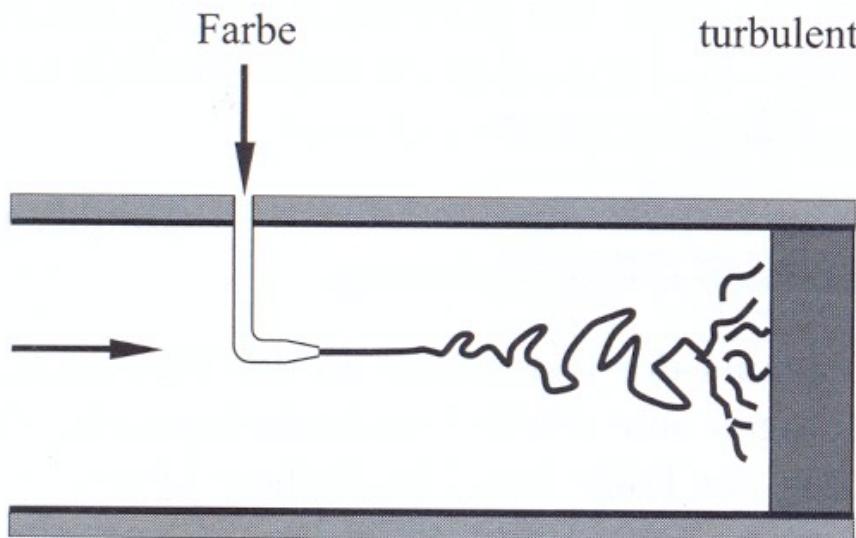
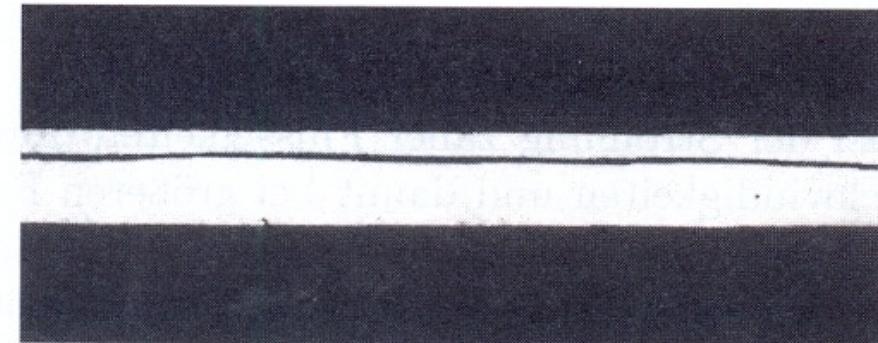
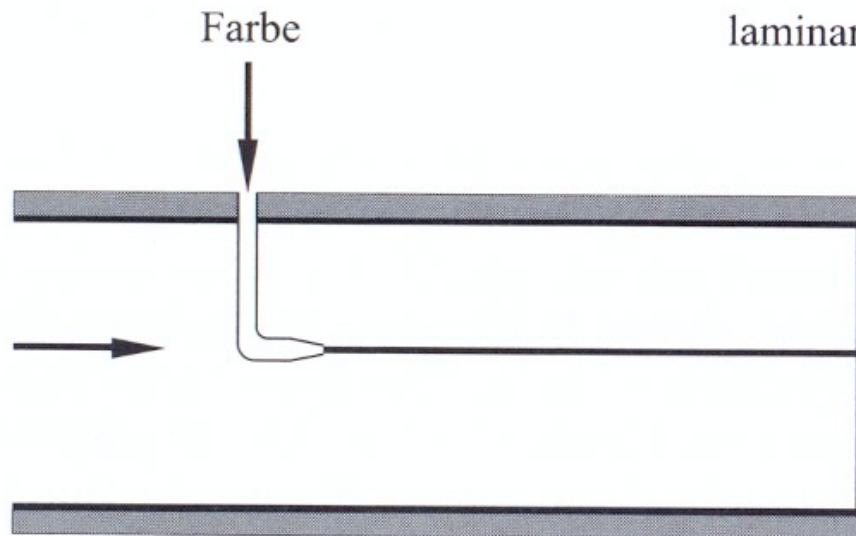


Reynolds experiment from 1883

*"The equations of motion had been subjected to such close scrunity, particularly by Professor Stokes, that there was small chance to discover anything new or faulty in them. It seemed to me possible, however, that they might contain evidence which had been overlooked."*

*"... either the elements of the fluid follow on another along lines of motion which lead in the most direct manner to their destinations, or they eddy about in sinous paths the most indirect possible."*

# Reynolds Experiment



Laminar and turbulent  
channel flow

Source: Oertel, 2008

# Reynolds Experiment



Laminar and turbulent  
channel flow

# Characteristics of turbulent flow

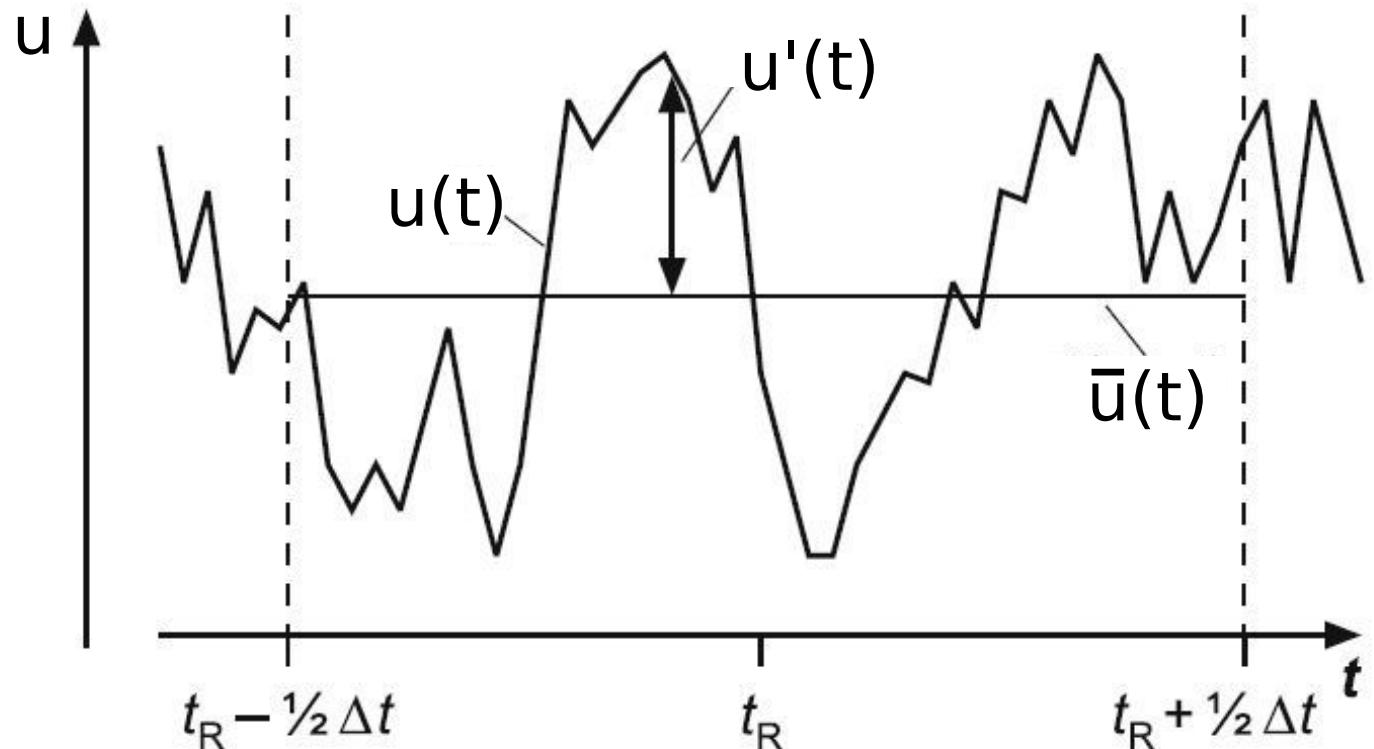
- ④ The flows are **rotational** and **three dimensional** (vorticity fluctuation are therefore important)
- ④ Flows are **dissipative**, so that energy must be supplied to maintain the turbulence
- ④ The fluid motions are **unpredictable** in detail
- ④ The rates of transfer and **mixing** are several orders of magnitude greater than the rate of **molecular diffusion**

# Important Concepts

- ④ Turbulence is stationary (statistical invariance with respect to time)
- ④ Turbulence is homogeneous (statistically invariant to translation in space)
- ④ Turbulence is isotropic (statistically independent of translation, rotation and reflection of the spatial axes)
- ④ Turbulence is ergodic, if homogeneous and stationary.

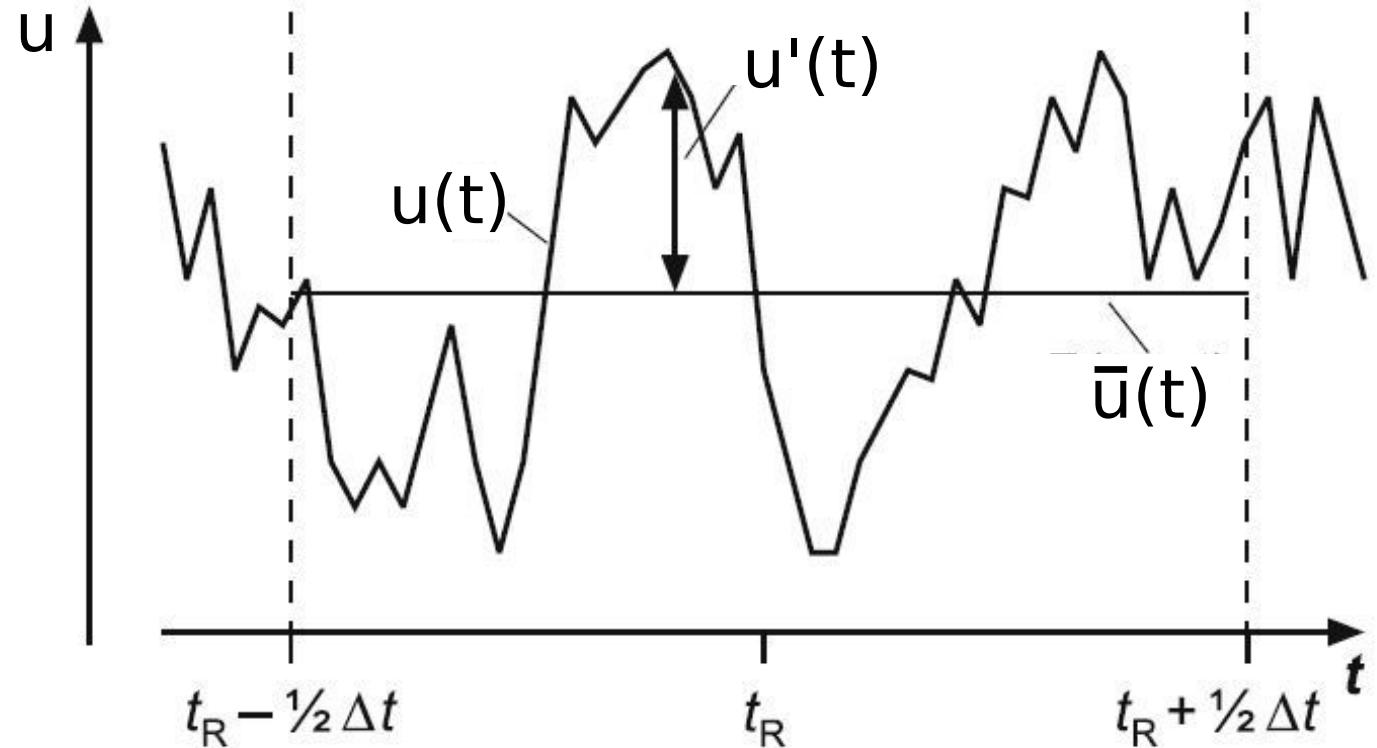
# Reynolds decomposition

$$u(t) = \bar{u}(t) + u'(t)$$



Decomposition of a time series, showing the gusts  $a'(t)$  of the actual instantaneous wind,  $a(t)$ , from the local mean,  $\bar{a}(t_R, \delta t)$ .

# Reynolds decomposition



$$\bar{u} = \overline{(\bar{u} + u')} = \bar{\bar{u}} + \bar{u}' = \bar{u} + \bar{u}'$$

This is only true, if  $\bar{u}' = 0$

# Properties of air masses

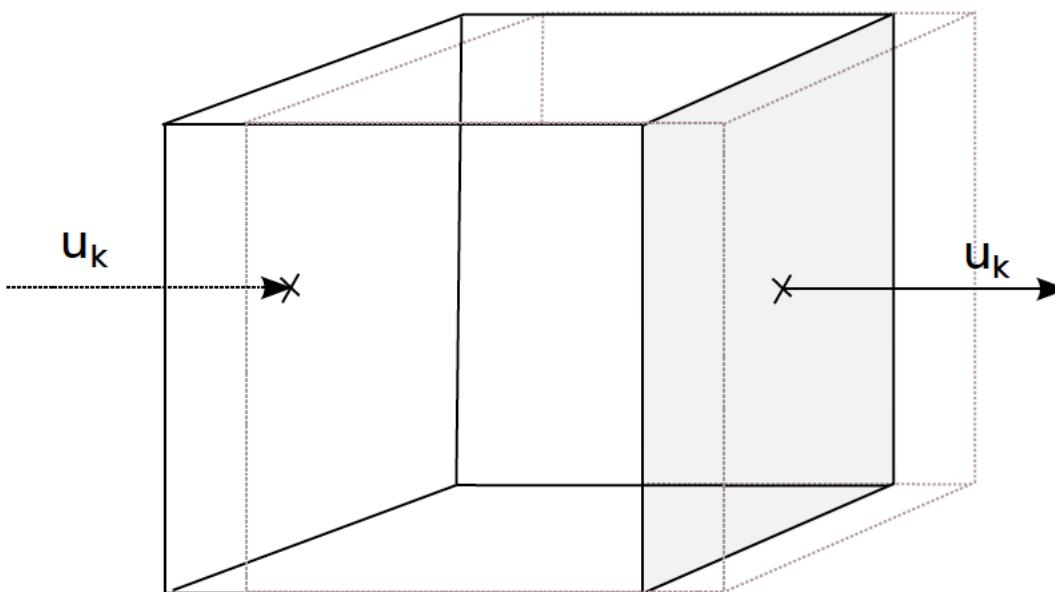
Air parcel contains properties, e.g. momentum, sensible heat, humidity, tracer concentration.

- ▷ **Momentum** [ $\text{kg m s}^{-1}$ ] is defined as the product of mass  $m$  and velocity  $\vec{v}$ .
- ▷ **Sensible heat** [ $\text{J kg}^{-1}$ ] is given as  $c_p \theta$ .
- ▷ **Specific humidity** [ $\text{kg kg}^{-1}$ ], ratio between mass of vapor and mass of wet air.

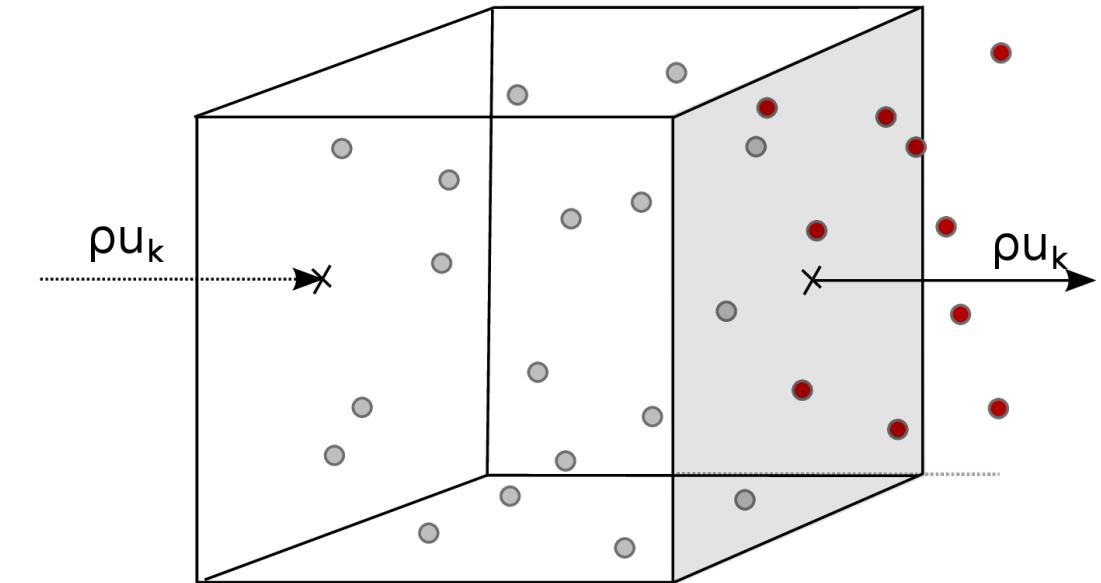


*Transport of specific properties are always related to the transport of air mass (mass flux).*

# Fluxes



Schematic sketch of volume flux



Schematic sketch of mass flux

Fluxes	Units	Description
$u_k$	$m s^{-1} = m^3 m^{-2} s^{-1}$	Volume flux
$\rho u_k$	$kg m^{-2} s^{-1}$	Mass flux
$\rho u_k e$	$kg m^{-2} s^{-1} \cdot \varepsilon \cdot kg^{-1} = \varepsilon m^{-2} s^{-1}$	Property flux

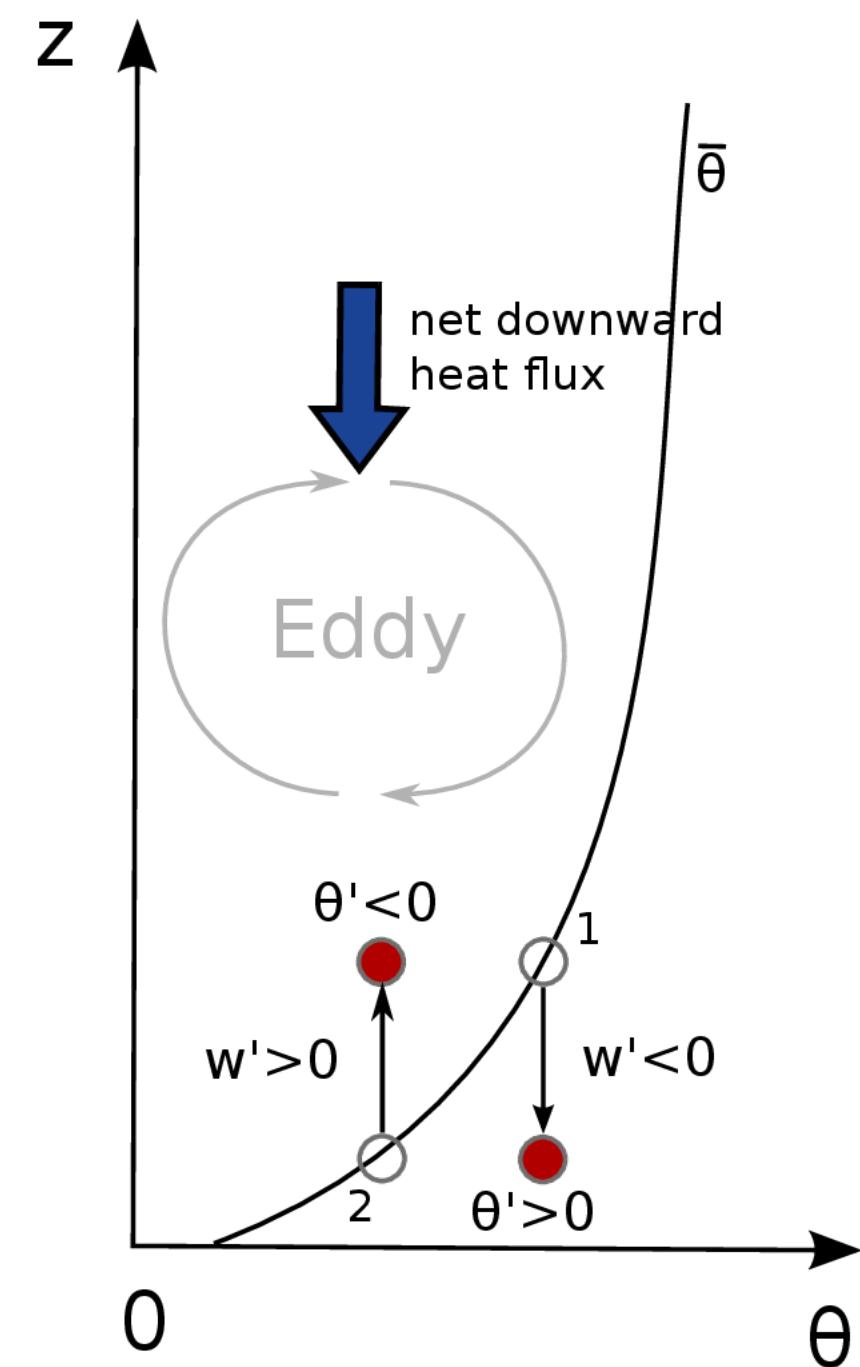
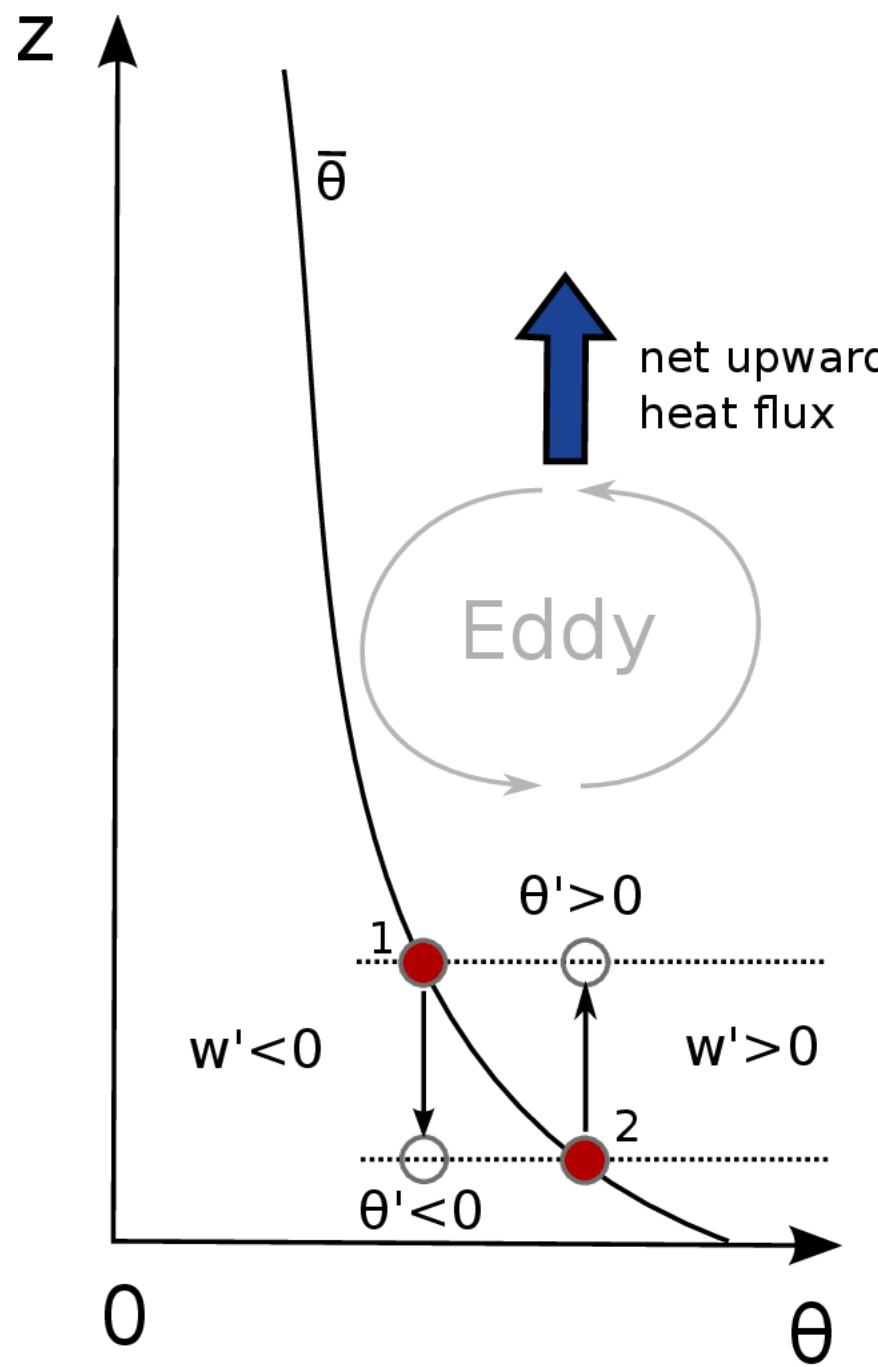
Table 1: Comparison of different fluxes, with  $k$  as the component of the wind speed ( $u_1 = u$ ,  $u_2 = v$ ,  $u_3 = w$ ) and  $\varepsilon$  any property. The dry air density is given by  $\rho$ .

# Reynolds decomposition of fluxes

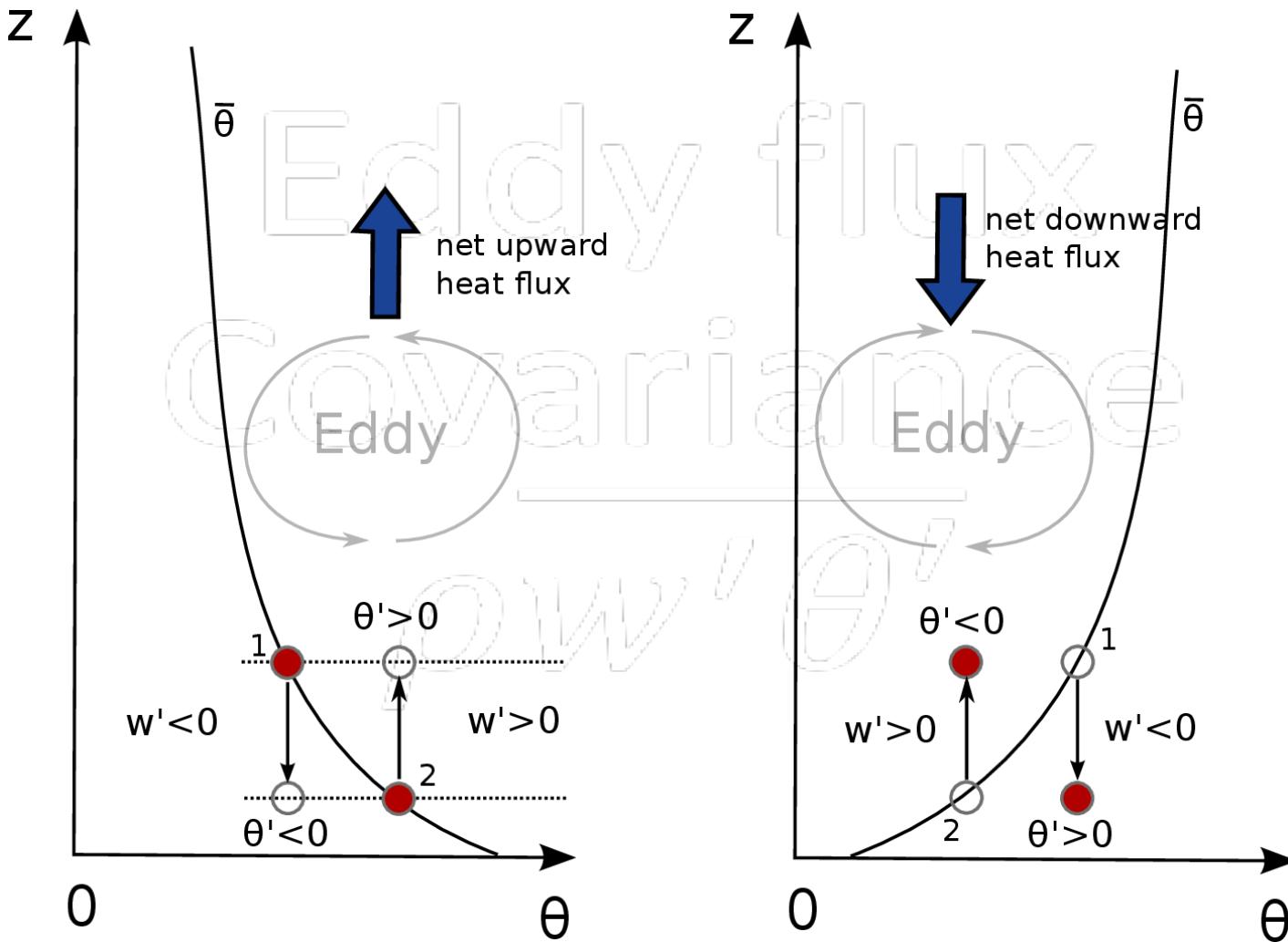
$$\begin{aligned}\overline{F_k^e} &= \rho \overline{u_k e} = \rho \cdot \overline{(\overline{u_k} + u'_k)(\bar{e} + e')} \\ &= \rho \overline{u_k e} + \rho \overline{u'_k e'}\end{aligned}$$

while  $\rho \overline{u_k e}$  is the **mean transport**  
 $\rho \overline{u'_k e'}$  is the **turbulent transport**

# Eddy flux Covariance $\rho \overline{w' \theta'}$



# Eddy flux Covariance

 $\rho \overline{w' \theta'}$ 


$w'$	+	+	-	-
$\theta'$	+	-	+	-
	warm air from below	cold air from below	warm air from above	cold air from above
$\overline{w'\theta'}$	+	-	-	+

# Overview: Kinematic fluxes

Vertical kinematic eddy sensible heat flux	$= \overline{w'\theta'}$	[K m s <sup>-1</sup> ]
Vertical kinematic eddy moisture flux	$= \overline{w'q'}$	[kg kg <sup>-1</sup> m s <sup>-1</sup> ]
Vertical kinematic eddy flux of u-momentum	$= \overline{u'w'}$	[m <sup>2</sup> s <sup>-2</sup> ]

# Turbulent heat fluxes

Vertical turbulent sensible heat flux

$$Q_H = c_p \cdot \rho \cdot \overline{w' \theta'} \quad [\text{W m}^{-2}]$$

Vertical turbulent latent heat flux

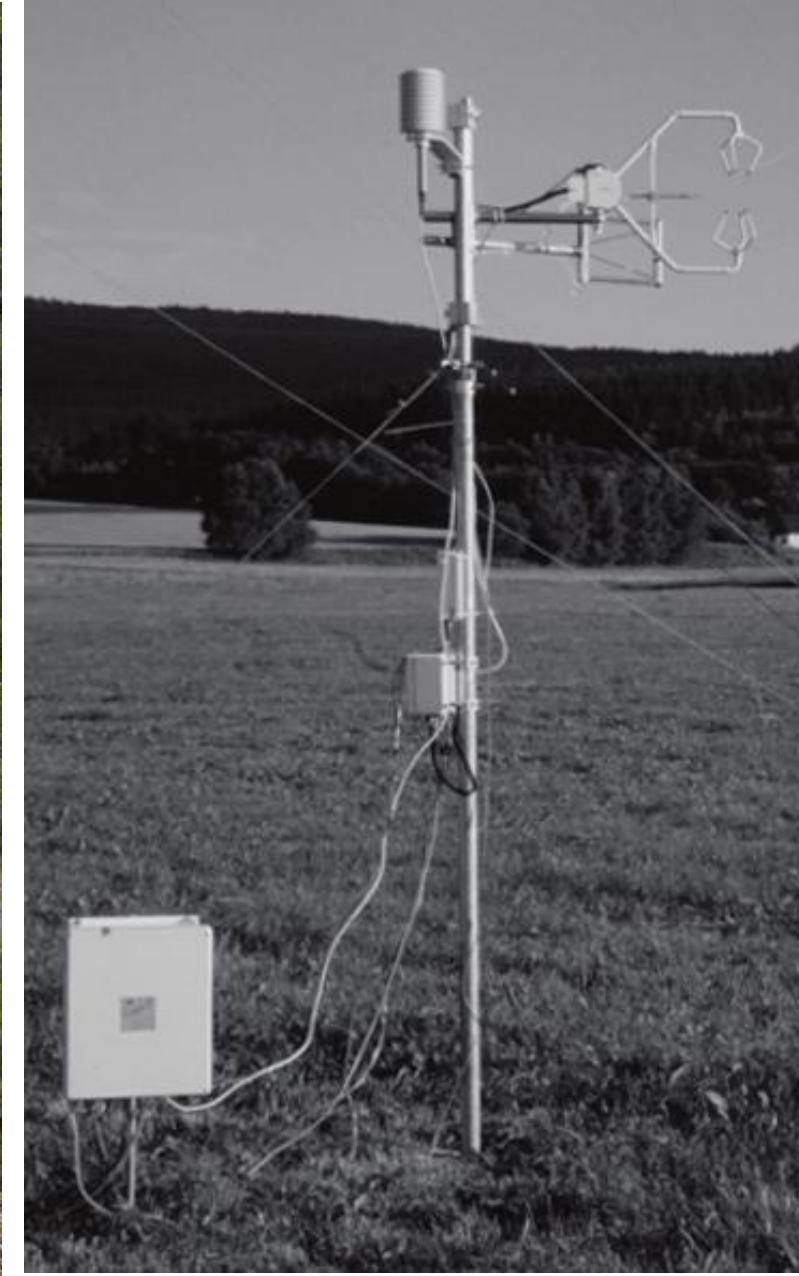
$$Q_E = L \cdot \rho \cdot \overline{w' q'} \quad [\text{W m}^{-2}]$$

with

$L$  : latent heat of vaporization of water 334 [ $\text{kJ kg}^{-1}$ ]

$c_p$ : specific heat of constant pressure for moist air 1.004 [ $\text{kJ kg}^{-1} \text{K}^{-1}$ ]

# Problem: Covariances



# K-theory First order (1. Method)

Parametrization of turbulent fluxes as

$$\overline{u'_k e'} = -K \frac{\partial \bar{e}}{\partial x_k}$$

with K the eddy diffusivity [m<sup>2</sup> s<sup>-1</sup>]

Different K-values are associated with different variables, K<sub>m</sub> for momentum, K<sub>H</sub> and K<sub>E</sub> for heat and latent heat fluxes.

$$K_H = K_E = 1.35 \cdot K_m \quad \text{for neutral conditions}$$

# Turbulent fluxes

Vertical turbulent heat flux

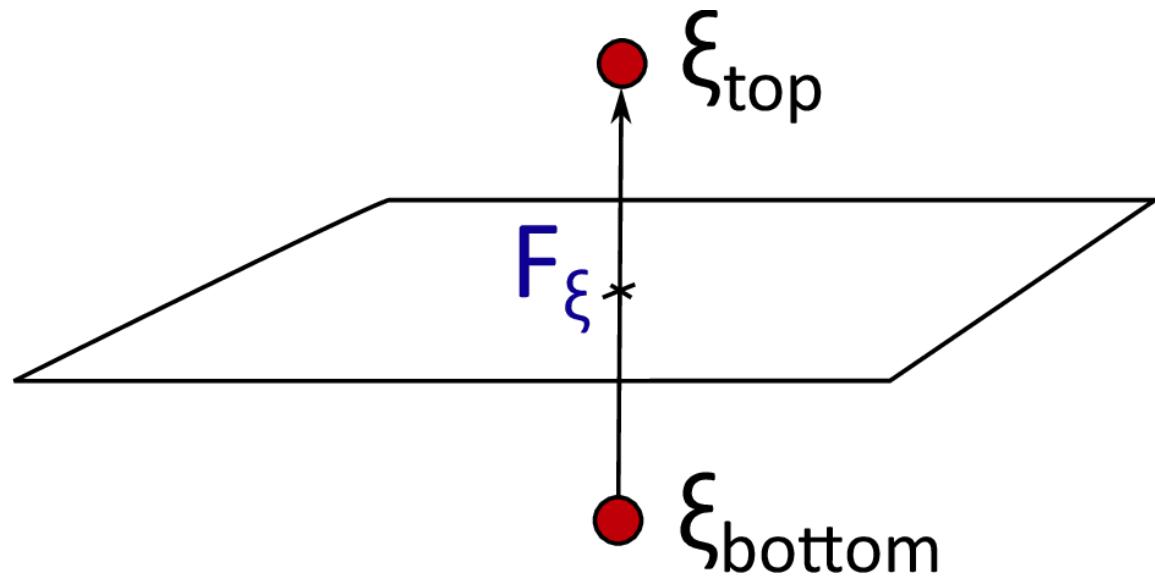
$$Q_H = c_p \cdot \rho \cdot \overline{w' \theta'} = c_p \cdot \rho \cdot K_H \frac{\partial \bar{\theta}}{\partial z} \quad [\text{W m}^{-2}]$$

Vertical turbulent latent heat flux

$$Q_E = L \cdot \rho \cdot \overline{w' q'} = L \cdot \rho \cdot K_E \frac{\partial \bar{q}}{\partial z} \quad [\text{W m}^{-2}]$$

with     $L$  : latent heat of vaporization of water 334 [KJ kg<sup>-1</sup>]  
 $c_p$  : specific heat at constant pressure for moist air 1006 [KJ kg<sup>-1</sup> K<sup>-1</sup>]

# Parametrization turbulent surface fluxes (2. Method)



$$F_\zeta = -U_T \cdot (\zeta_{top} - \zeta_{bottom})$$

with  $U_T$  the transport velocity [ $\text{m s}^{-1}$ ], and  $\zeta$  any variable

*The transport velocity is usually parametrized as a function of some measure of turbulence:*

$$U_T = C_D \cdot \bar{U}$$

with  $C_D$  the bulk transfer coefficient

# Parametrization turbulent surface fluxes

$$\overline{w'\theta'} = -C_H \cdot U \cdot (T_z - T_0)$$

$$\overline{w'q'} = -C_E \cdot U \cdot (q_z - q_0)$$

with  $C_H$  and  $C_E$  the bulk transfer coefficient, typical values range from 1e-3 to 1e-5  
( $C_H$  is the so-called Stanton number,  $C_E$  is the so-called Dalton number)

Subscript z represents values in the air near the surface (2 m or 10 m).  
Subscript 0 means the value in the top 1 mm of the soil or sea surface.

# Parametrization turbulent surface fluxes (Bulk Approach)

Turbulent sensible heat flux

$$H = \rho_a \cdot c_p \cdot C_h \cdot u \cdot (T_z - T_0)$$

$$C_h = \frac{\kappa^2}{\ln\left(\frac{z}{z_0}\right)^2}$$

Turbulent latent heat flux

$$C_E = \frac{\kappa^2}{\ln\left(\frac{z}{z_0}\right)^2}$$

$$E = \rho_a \cdot L \cdot C_E \cdot u \cdot (q_z - q_0)$$

with  $\rho$  : air density [kg m<sup>-3</sup>]

$c_p$  : specific heat of constant pressure for moist air 1006 [kJ kg<sup>-1</sup> K<sup>-1</sup>]

$L$  : latent heat of vaporization of water 334 [kJ kg<sup>-1</sup>]

# Drag coeff., measurement height and surface roughness

Statically neutral conditions in the surface layer

$$C_{DN} = \kappa^2 \left[ \ln \left( \frac{z}{z_0} \right) \right]^{-2}$$

often  $C_{DN} = C_{HN} = C_{EN}$ , and  $\kappa$  (0.4) the von Karman constant

Statically unstable/stable flows

$$C_D = \kappa^2 \left[ \ln \left( \frac{z}{z_0} \right) - \psi_M(\zeta) \right]^{-2}$$

$$C_H = \kappa^2 \left[ \ln \left( \frac{z}{z_0} \right) - \psi_M(\zeta) \right]^{-1} \left[ \ln \left( \frac{z}{z_0} \right) - \psi_H(\zeta) \right]^{-1}$$

- with  $\psi_M, \psi_H$  : Stability correction terms  
 $\zeta$  : Measure of stability ( $\zeta = z/L$ , while L is the Obukhov-Length)  
It is usually assumed that  $C_H = C_E$   
 $z_0$  : Roughness length [m]

# Bulk coefficients

## The coefficients depend on

- ④ Surface roughness (frictional skin drag, form drag, wave drag)
- ④ Measurement height (dramatic impact on the value of the drag coefficient)
- ④ Stability

# Aerodynamic roughness length $z_0$

## Properties

- ⌚ Height where wind speed becomes zero
- ⌚ Aerodynamic, because the only true determination of this parameter follows from measurements
- ⌚ Given observations of wind speed at two or more heights, it is easy to solve for  $z_0$  and  $u$
- ⌚ It is not equal to the height of the individual roughness elements
- ⌚ It does not change with wind speed, stability or stress

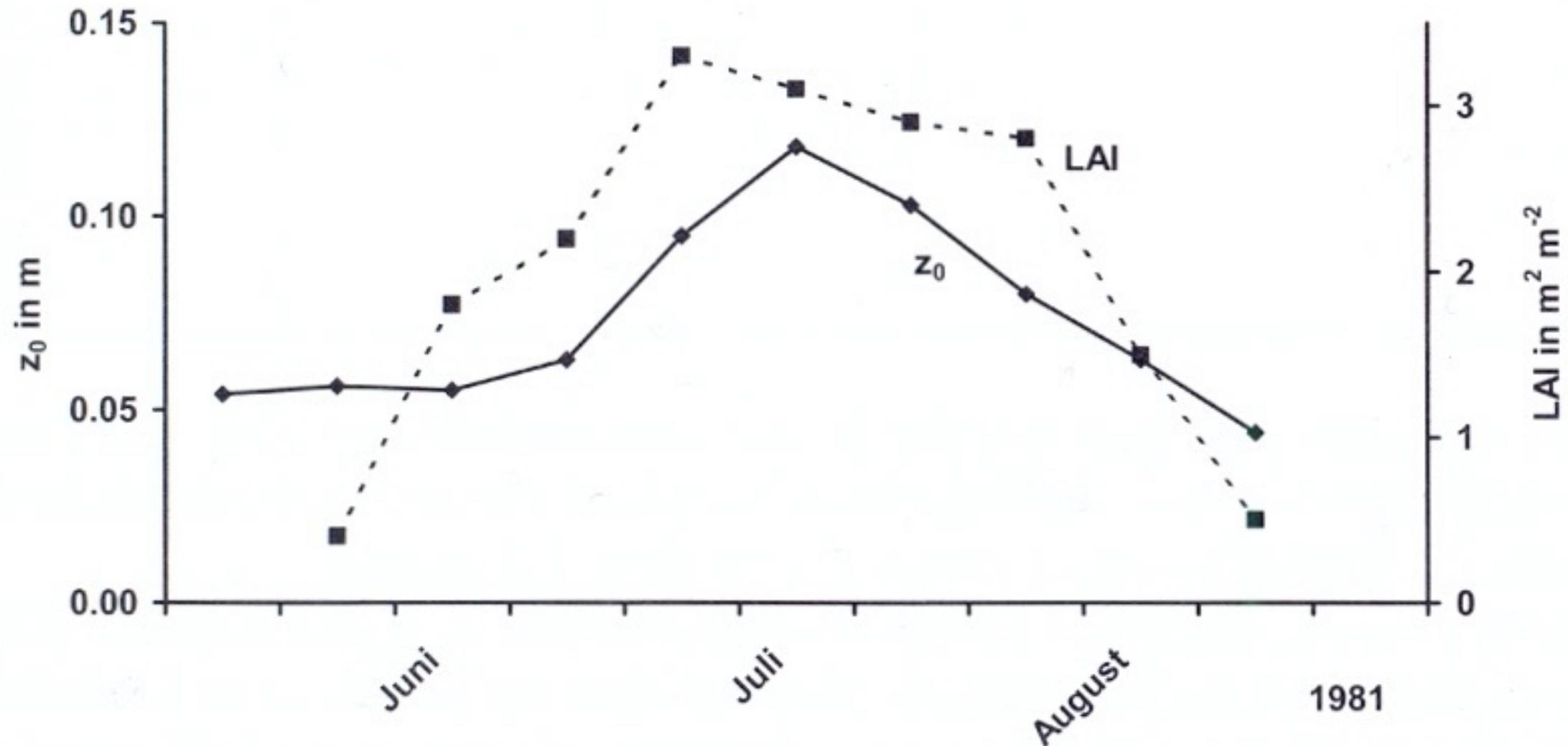
# Aerodynamic roughness length $z_0$

$$Z_0 = \frac{1}{10} h \quad [\text{m}]$$

with  $h$  the height of the roughness elements

Surface	$z_0$ in m
Snow without structure	$10^{-5} \dots 10^{-4}$
Calm water surface	$10^{-5} \dots 10^{-4}$
Sand desert	$10^{-4} \dots 10^{-3}$
Short grass (2-5 cm)	$2 \cdot 10^{-3} \dots 5 \cdot 10^{-3}$
Long grass (20-50 cm)	$2 \cdot 10^{-2} \dots 5 \cdot 10^{-2}$
Corn field	$2 \cdot 10^{-2} \dots 5 \cdot 10^{-2}$
Forest	$1 \dots 5$

# Aerodynamic roughness length $z_0$



Change of roughness height and the leaf area index (Foken, 2008).

# Bowen-Ratio Method (3. Method)

## Bowen-Ratio

$$Bo = \frac{Q_H}{Q_E} = \gamma \cdot \frac{\Delta\theta}{\Delta e}$$

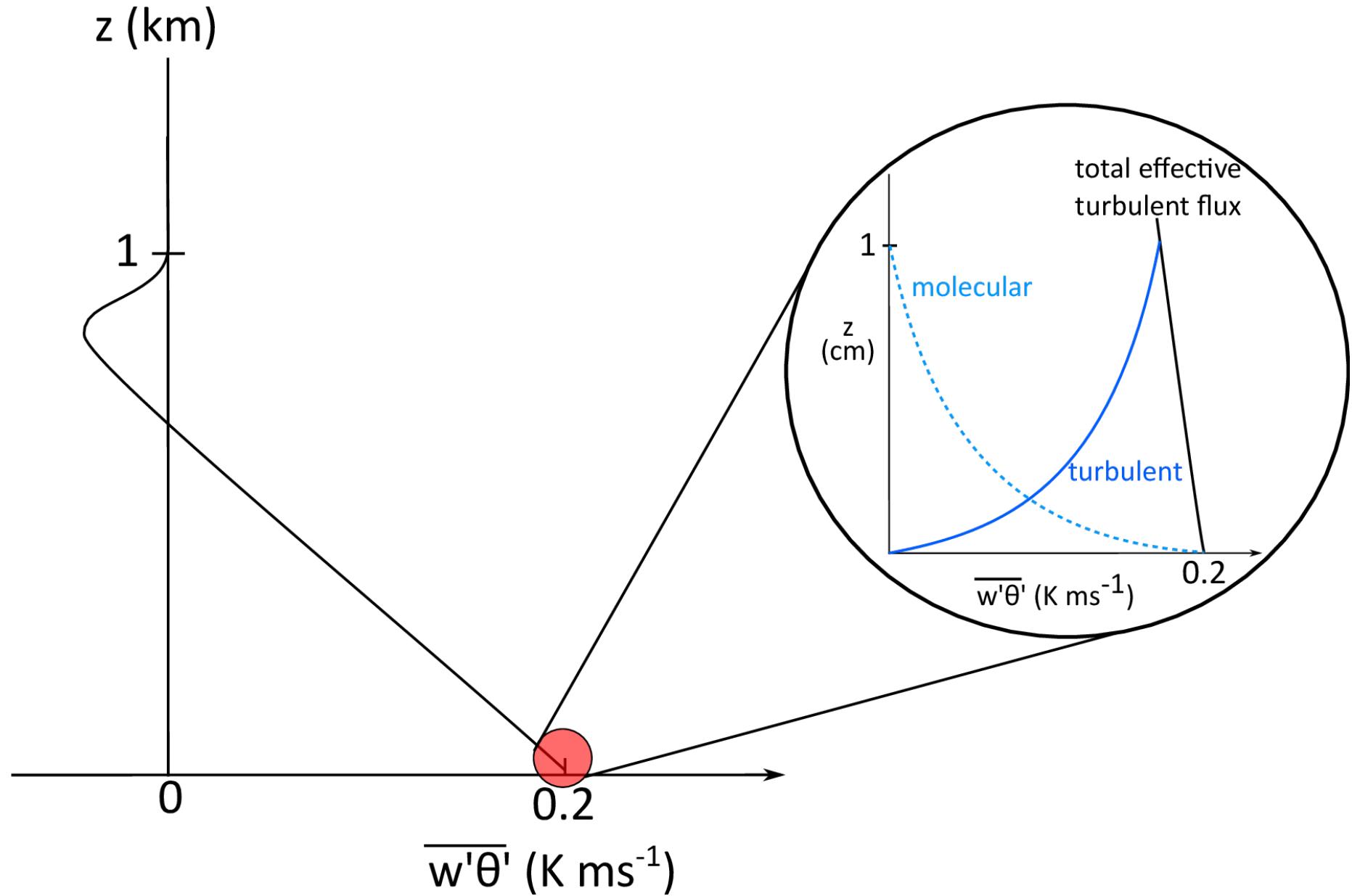
## Heat fluxes

$$Q_H = (Q_s^* - Q_G) \frac{Bo}{1 + Bo}$$

$$Q_E = \frac{Q_s^* - Q_G}{1 + Bo}$$

with  $\gamma$  : Psychromatic constant  $0.000667 [Pa K^{-1}]$  for 1000 hPa and  $20^\circ C$

# Effective surface turbulent flux

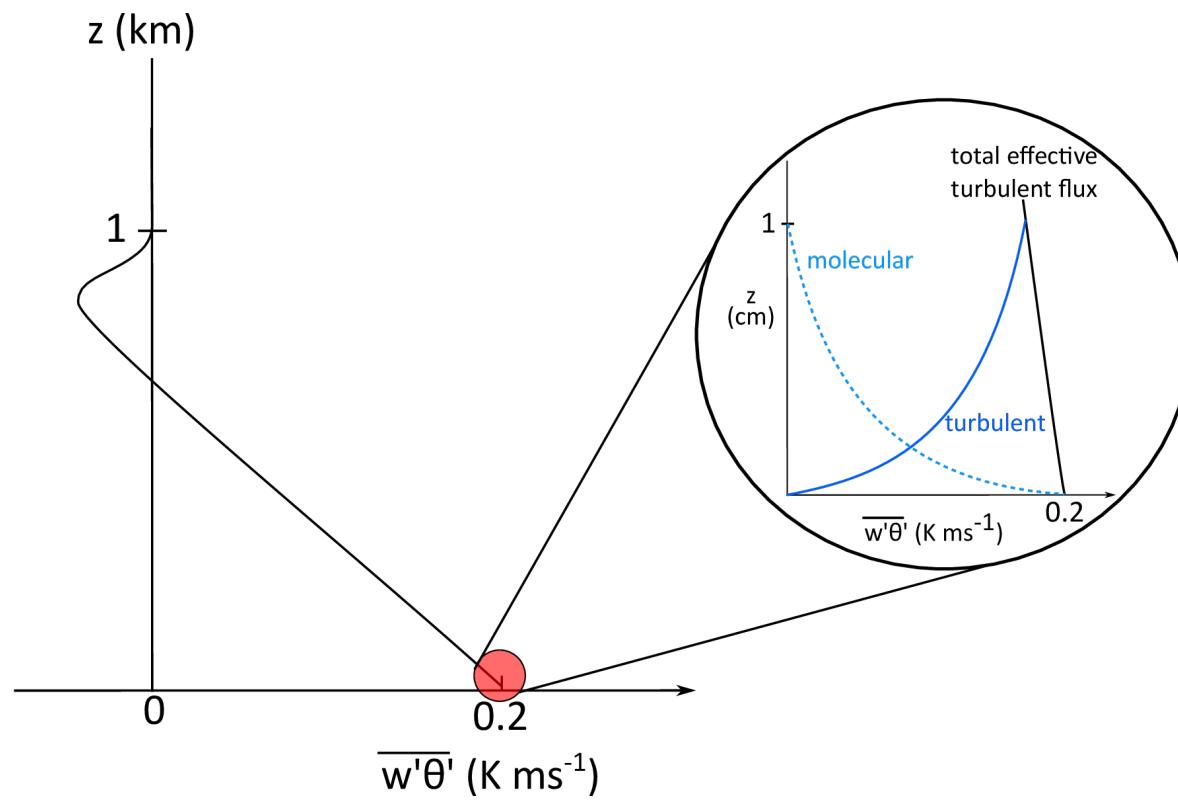


# Effective surface turbulent flux

## Molecular flux

$$Q_H = \nu_\theta \frac{\partial T}{\partial z} \quad [\text{W m}^{-2}]$$

with  $\nu_\theta$  the molecular thermal diffusivity ( $2.5 \cdot 10^{-2} \text{ W m}^{-1} \text{ K}^{-1}$ )



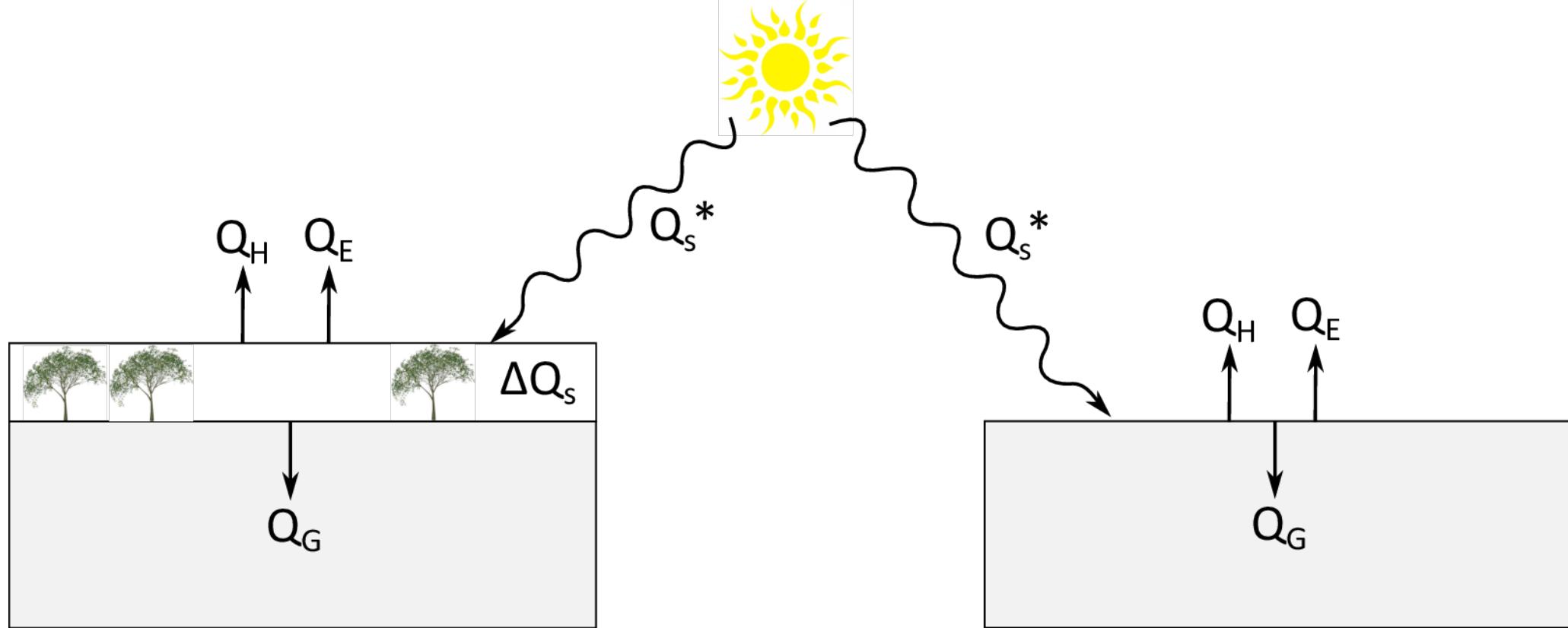
# Mirage (micro layer)





## Surface Energy Balance

# Surface Energy Balance

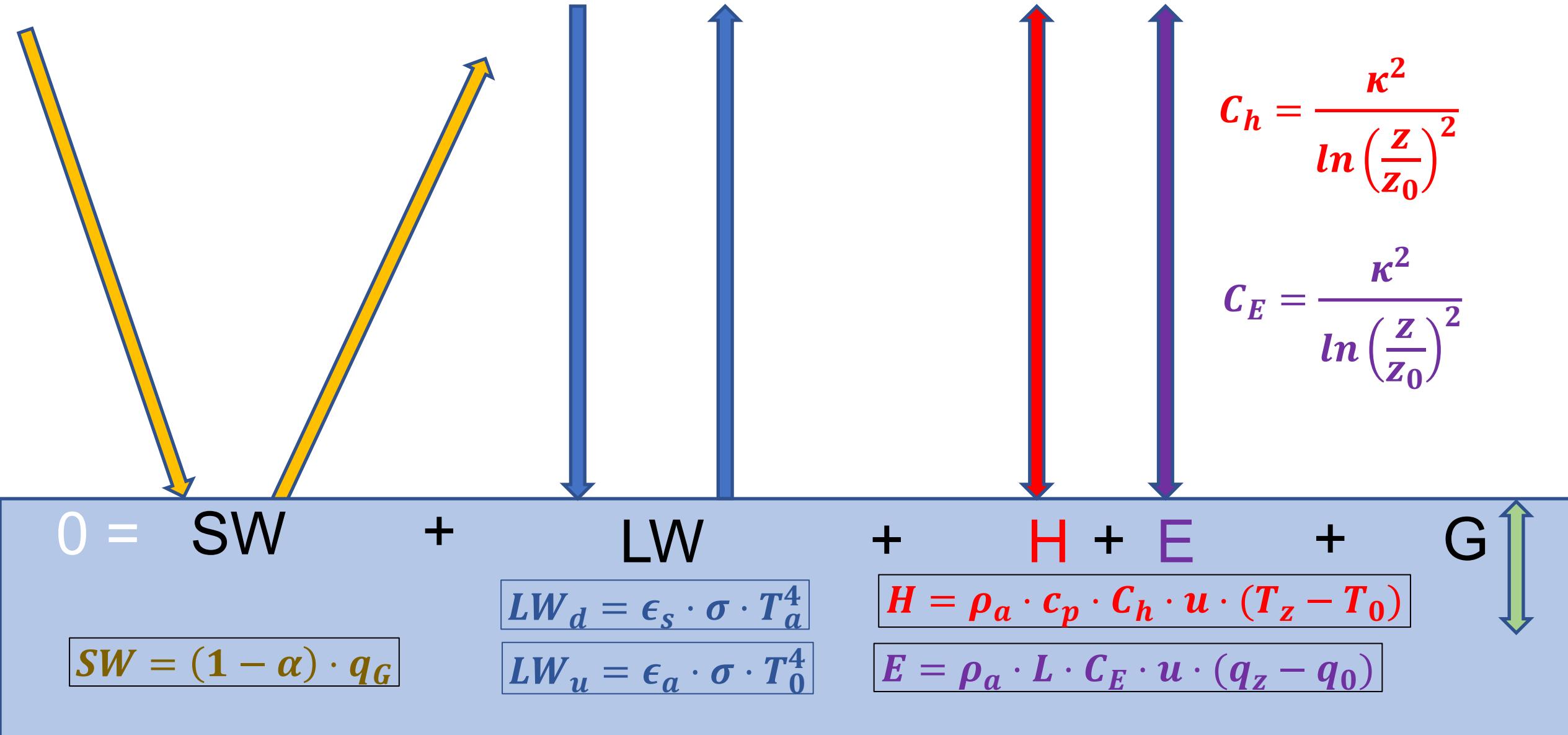


$$Q_s^* = Q_H + Q_E + Q_G + \Delta Q_s$$

with  $Q_s^*$  the net radiation at the surface,  $Q_H$  the sensible heat flux,  $Q_E$  the latent heat flux,  $Q_G$  the ground heat flux, and  $\Delta Q_s$  the storage term (internal energy)

**FLUXES AWAY FROM SURFACE ARE POSITIVE, EXCEPT FOR NET RADIATION**

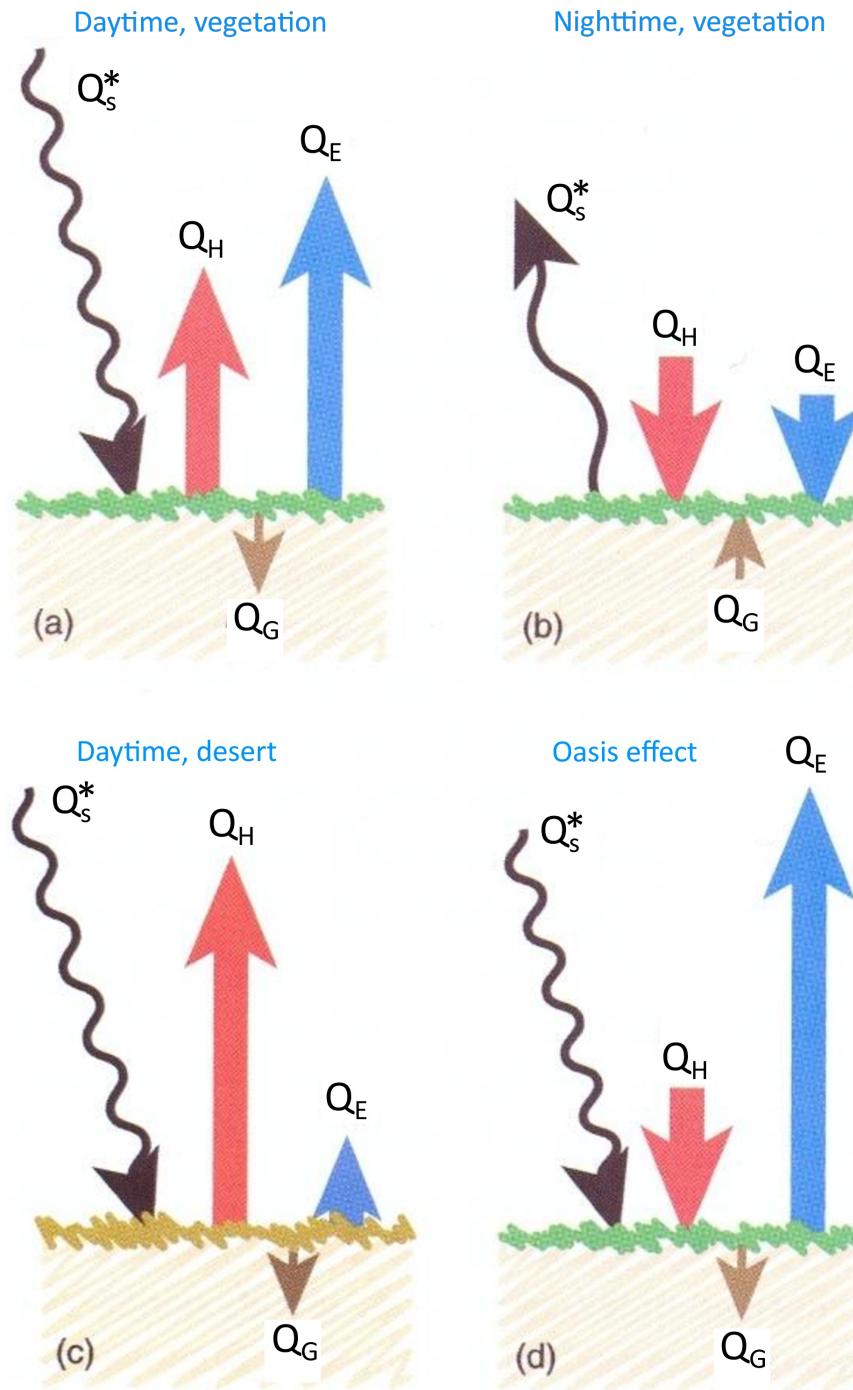
# Surface Energy Balance model (SEB)



What are the  
relevant  
fluxes?

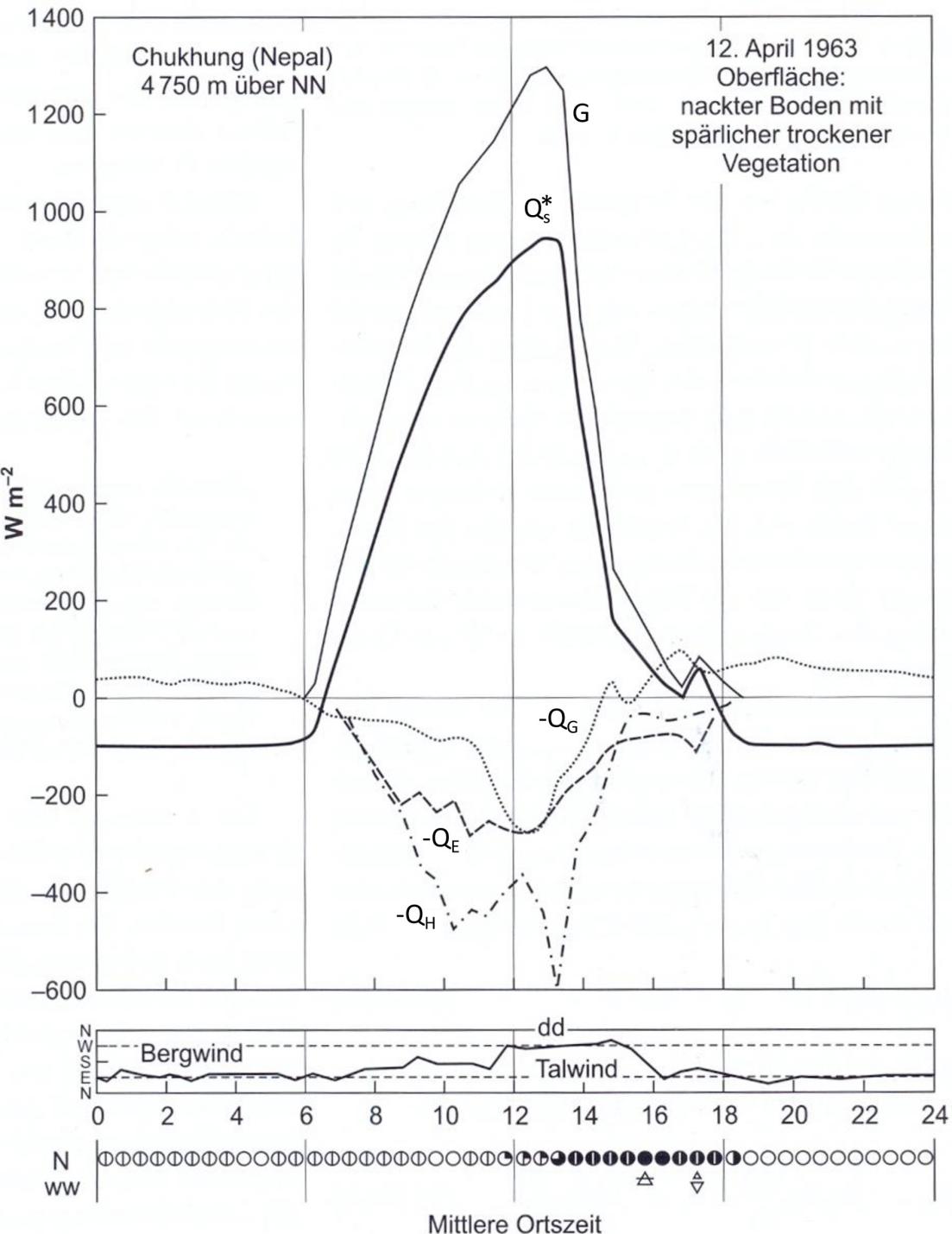


# Energy Balance Terms



Vertical cross-section sketch of net radiative input to the surface Flux, and resulting heat fluxes (modified after Wallace and Hobbs, 2006).

# Energy Balance Terms



Daily cycle of the energy balance components above moraine material in Nepal (modified after Krauss, 2008).

Fluxes				Situation
$Q_S$	$Q_G$	$Q_H$	$Q_E$	Generic case
$Q_S$	$Q_G$	$Q_H$		Dry soil
$Q_S$	$Q_G$		$Q_E$	Ocean, Lake
$Q_S$		$Q_H$	$Q_E$	Soil with low thermal conductivity
	$Q_G$	$Q_H$	$Q_E$	Night, cloud cover
$Q_S$	$Q_G$			Melting surface
$Q_S$		$Q_H$		Dry soil with low thermal conductivity
$Q_S$			$Q_E$	Intensive evapotranspiration
	$Q_G$	$Q_H$		Dry soil at night with cloud cover
	$Q_G$		$Q_E$	Ocean, Lake at cloudy night

	$Q_S$ ( $Wm^{-2}$ )	$Q_G$ ( $Wm^{-2}$ )	$Q_H$ ( $Wm^{-2}$ )	$Q_E$ ( $Wm^{-2}$ )	$W *$ ( $mm d^{-1}$ )	$Q_H / Q_E$
Forest	154	6	77	72	2.5	1.07
Potatoes	121	3	27	91	3.1	0.30
Alfalfa	131	1	3	127	4.4	0.02

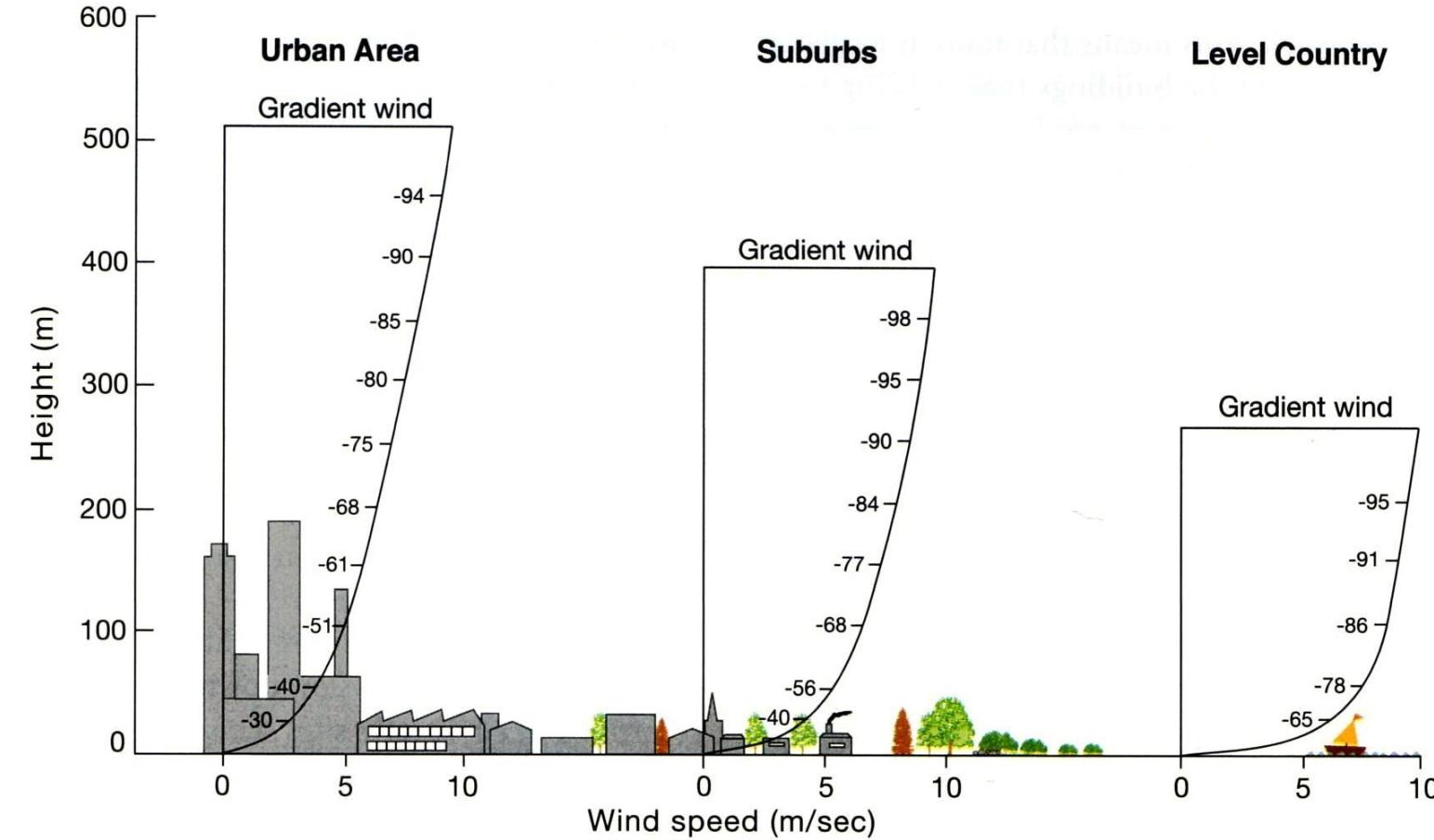
Surface flux measurements during daytime (Krauss, 2008)

## Properties

- ④ K-Theory for the parametrization of turbulent fluxes (surface layer)
- ④ Mixing-Length theory
- ④ Surface energy balance
- ④ Parametrization of the radiation
- ④ Parametrization of the surface fluxes (Bulk approach, Bowen-Ratio)
- ④ Bulk coefficients, roughness length
- ④ Ground heat flux

# Logarithmic Wind Profile

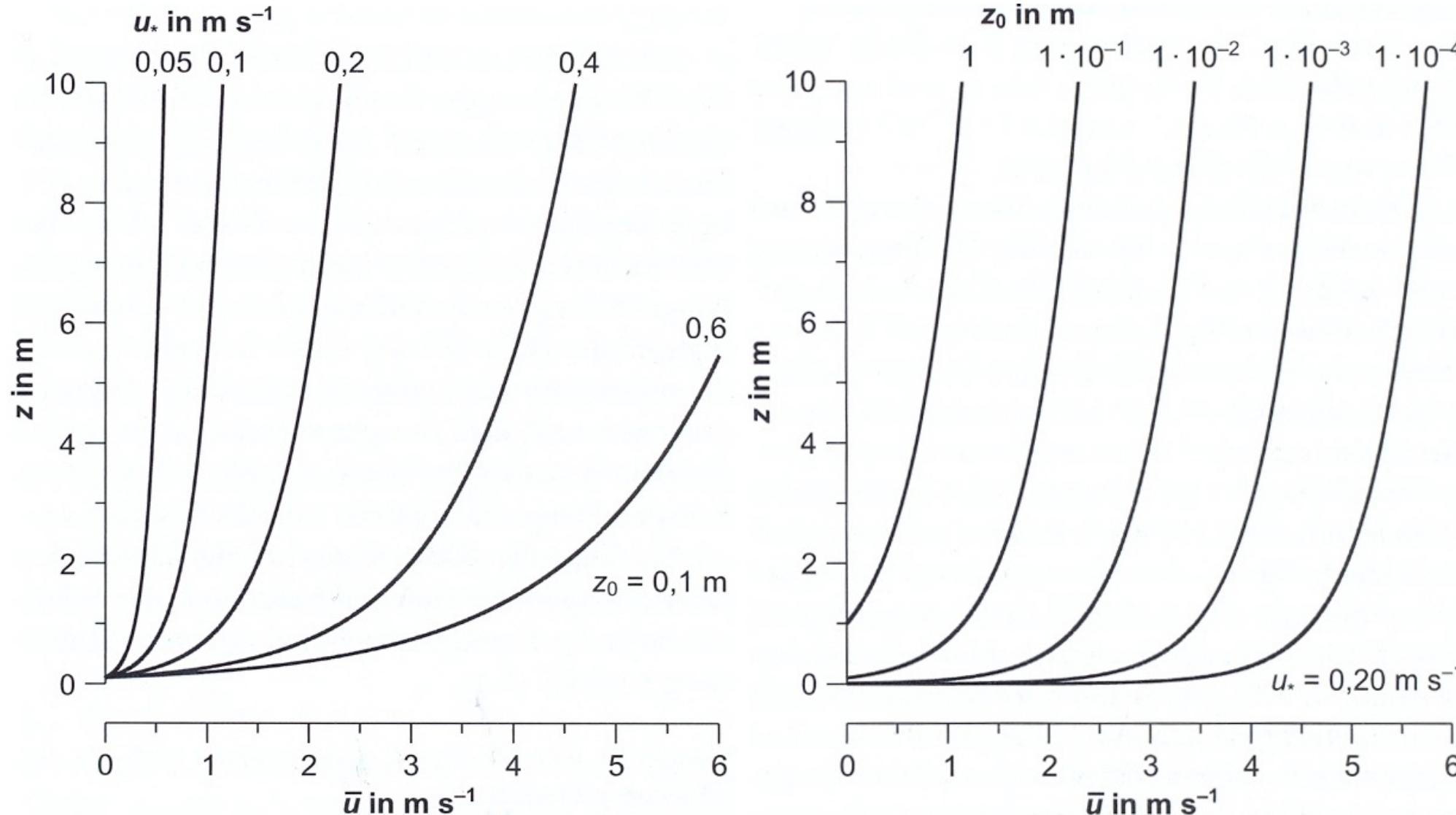
# Logarithmic wind profile - Neutral case



$$u(z) = \frac{u_*}{\kappa} \ln \left( \frac{z}{z_0} \right)$$

with  $u_*$  : friction velocity [ $\text{m s}^{-1}$ ]  
 $\kappa$  : Von Karman constant (0.4)  
 $z_0$  : Roughness length [m]

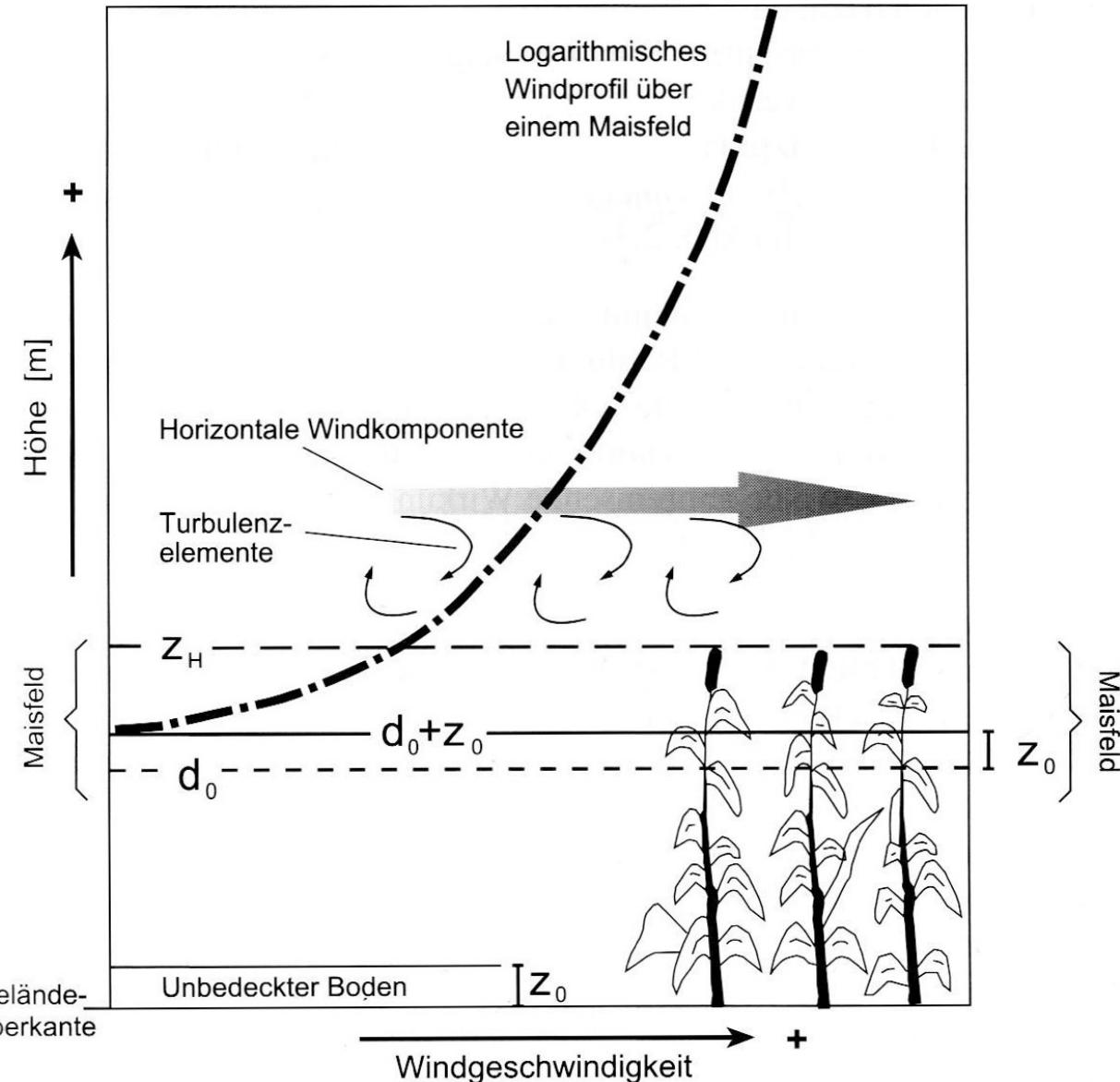
# Logarithmic wind profile - Neutral case



$$u(z) = \frac{u_*}{\kappa} \ln\left(\frac{z}{z_0}\right)$$

Wind profiles for neutral stability with constant roughness length (left) and friction velocity (right).

# Logarithmic wind profile – Displacement height



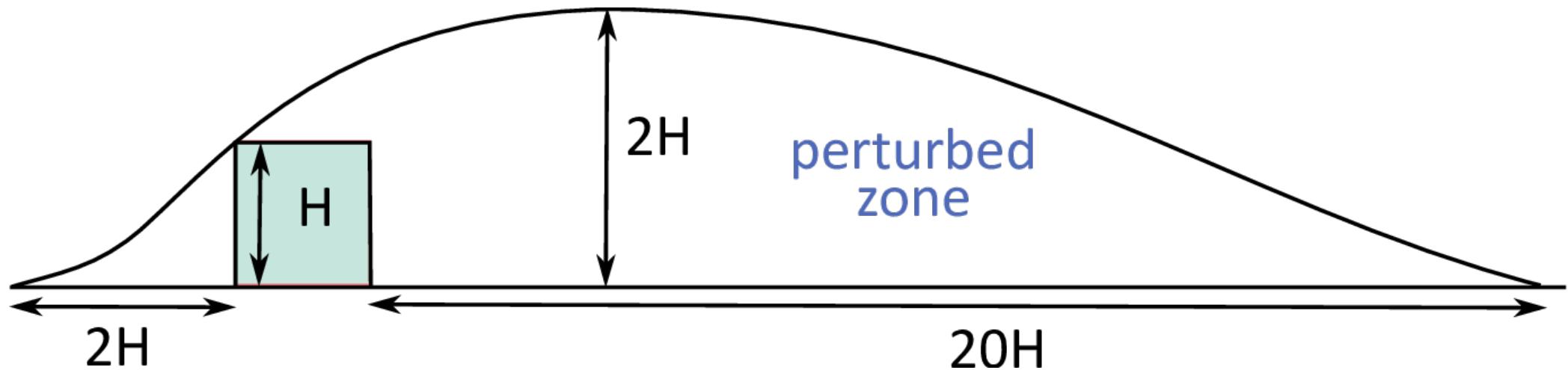
$$u(z) = \frac{u_*}{\kappa} \ln \left( \frac{z - d}{z_0} \right)$$

Influence of the surface structure on the vertical wind profile (Bendix, 2004)

## The logarithmic law applied only for

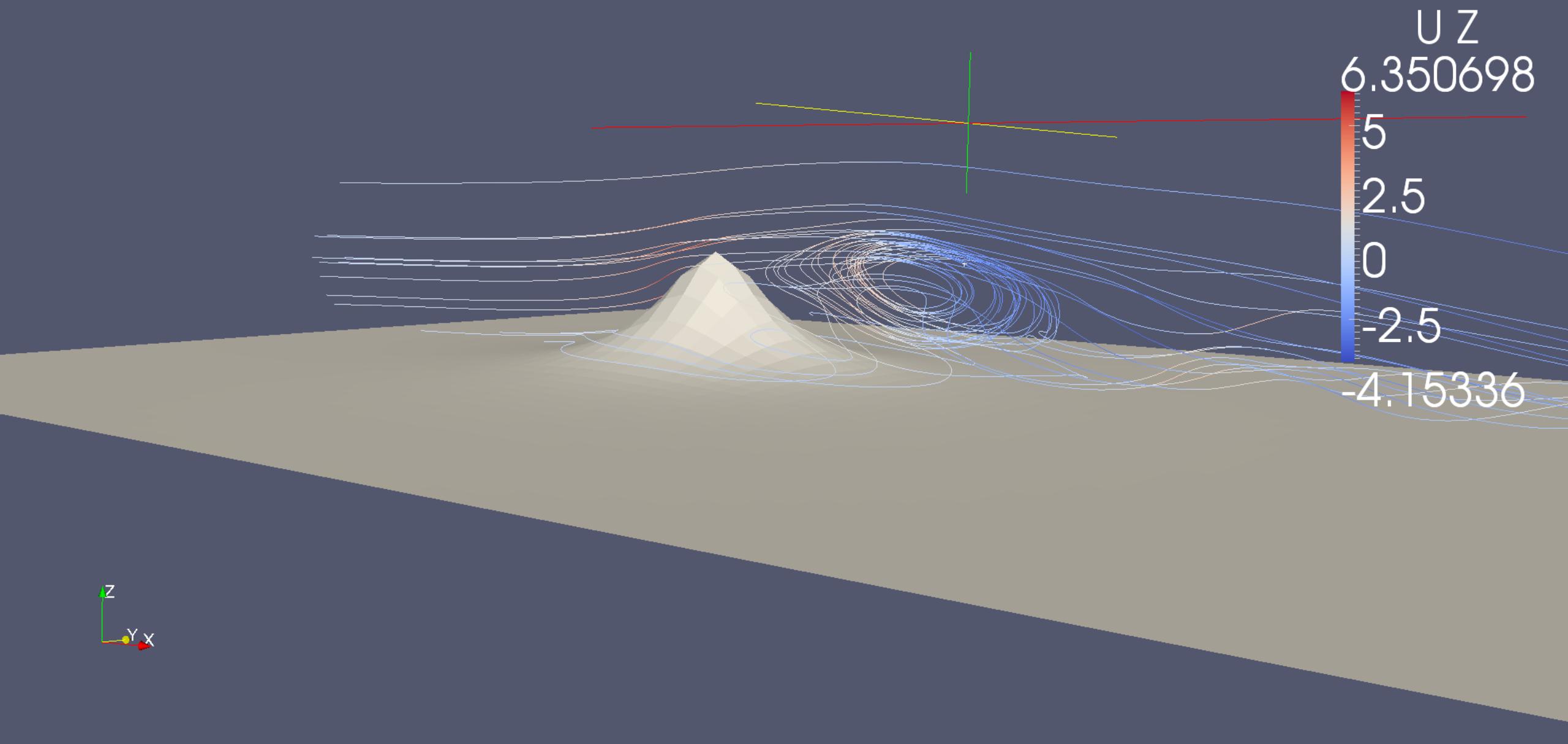
- ④ homogeneous and stationary flow
- ④ neutral stable atmospheric conditions
- ④ height  $z > 20 \cdot z_0 + d$
- ④ locations far from obstacles, i.e.  $> 20 \cdot H$  from wake, and  $> 2 \cdot H$  upstream from obstacle

# Obstacles

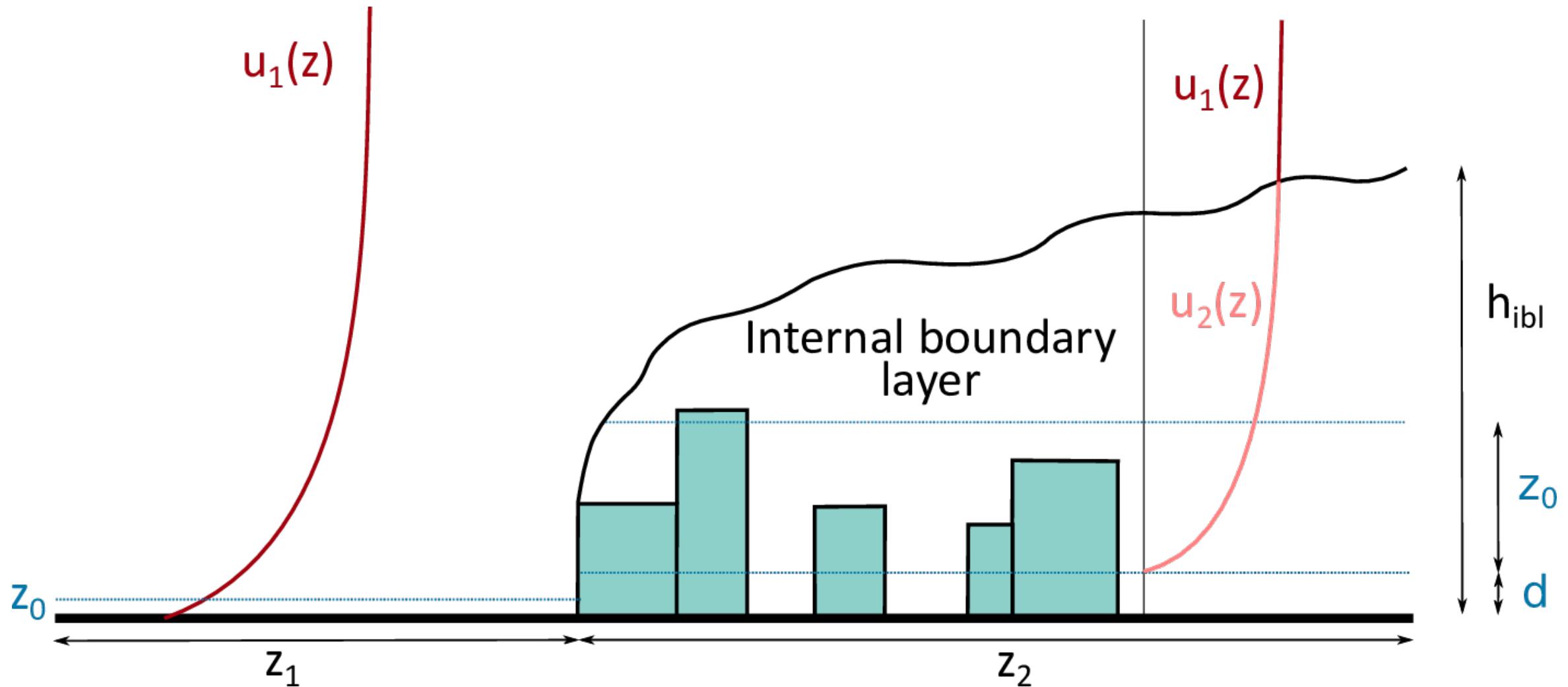


The effect of terrain roughness on the wind speed profile.

# Obstacles



# Internal boundary layer



Development of an internal boundary layer at the land-city transition.

## Practical relevance of the IBL

- ④ Profile measurements above the boundary layer
- ④ Wind shield for soil erosion
- ④ Wind energy

# Reminder

- ④ Logarithmic wind profile
- ④ Displacement height and roughness length
- ④ Boundary condition
- ④ Internal boundary layer