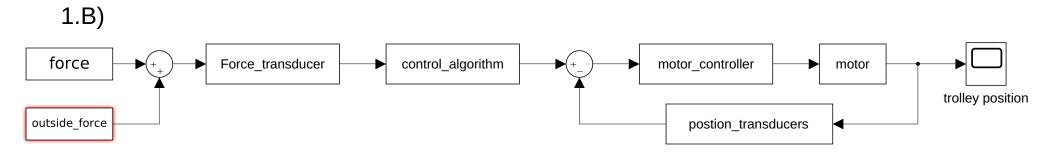
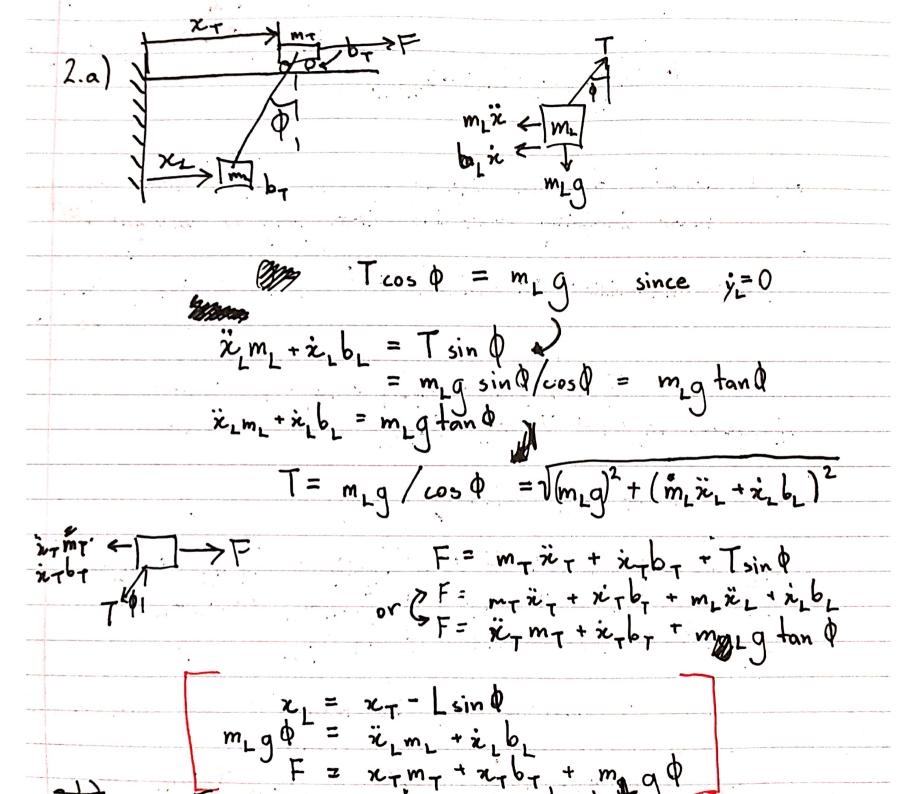
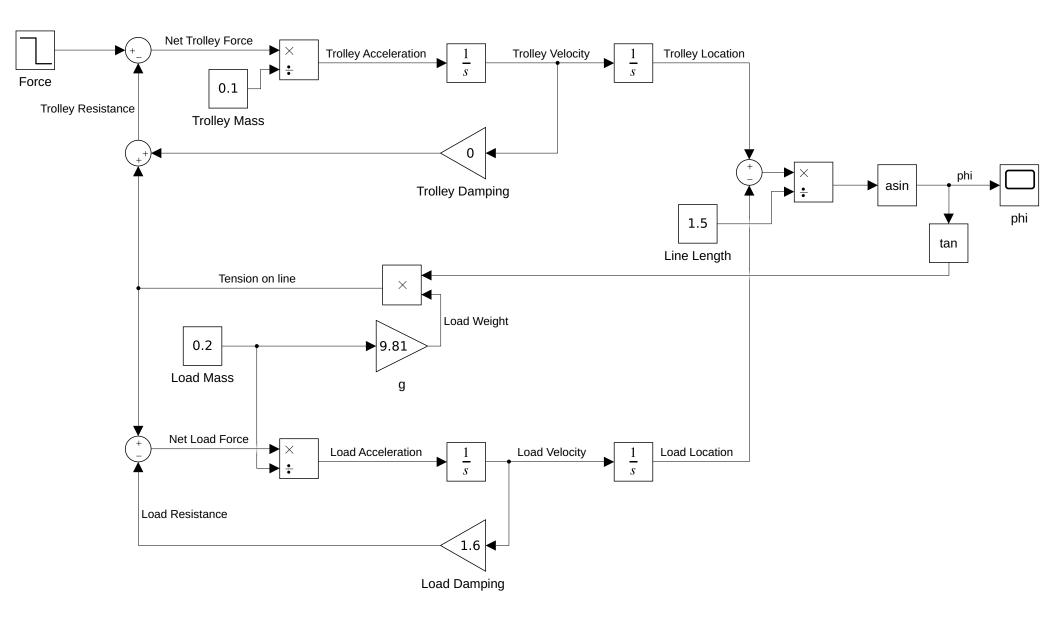
1.a)	Inpi	At when	1343 A.	Ontpu	t's				
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I would design a control system to ensure that the load is brought to the right location using the crane. To improve its efficiency of the crane we would design it to minimise of, the angle the load line takes, this would require a closed bop system of us monitoring of because it cannot be controlled directly, but as a result of the other controlled inputs.







2.c) Transfer function linking \$\Phi\$ to \$\pi\_\tau\$. Linearize the system assuming \$\Phi \approx 0\$ prior to Laplace transform. When  $\phi \approx 0 : -\sin(\phi) \doteq \phi$  $\therefore$   $+an(\phi) = \phi$  $cos(\Phi) \doteq \# \{$ Linearized functions for the system:  $F = \ddot{x}_{T}m_{T} + \dot{x}_{T}b_{T} + m_{L}g\phi$   $m_{L}g\phi = \ddot{x}_{L}m_{L} + \dot{x}_{L}b_{L}$   $x_{L} = x_{T} - L\phi$ (1)(2) (3) $\begin{array}{lll}
\mathcal{L}\{(1)\} = (4) \Rightarrow & F = s^2 X_T m_T + s X_T b_T + m_L g \Phi \\
\mathcal{L}\{(2)\} = (5) \Rightarrow & m_L g \Phi = s^2 X_L m_L + s X_L b_L \\
\mathcal{L}\{(3)\} = (6) \Rightarrow & X_L = X_T - b_{-} \Phi
\end{array}$ Laplace transform Use (B) to express XL as XT and & in (5):  $m_{L}g = s^{2}X_{L}m_{L} + sX_{L}b_{L} \qquad X_{L} = X_{T} - L\phi$   $= X_{L}(s^{2}m_{L} + sb_{L}) \qquad X_{L} = X_{T} - L\phi$  $m_{L}g = (X_{T} - L\Phi)(s^{2}m_{L} + sb_{L})$   $m_{L}g + L(s^{2}m_{L} + sb_{L})\Phi = X_{T}(s^{2}m + sb_{L})$   $(m_{L}g + s^{2}Lm_{L} + sLb_{L})\Phi = X_{T}(s^{2}m + sb_{L})$  $\frac{\phi(s)}{X_{T}(s)} = \frac{s^{2}m_{L} + sb_{L}}{s^{2}Lm_{L} + sLb_{L} + m_{L}q}$ m\_=0.2 m\_=0.1 6\_=1.6 L=15 Using the values required of my section  $\frac{\phi(s)}{\chi_{7}(s)} = \frac{s^{2}(0.2) + s(1.6)}{s^{2}(1.5)(0.1) + s(1.5)(1.6) + (0.7)(9.81)} = \frac{0.2s^{2} + 1.6s}{0.3s^{2} + 2.4s + 1.862}$ 

```
2.d) Find \frac{\phi(6)}{V_{7}(5)} " using same assuptions as .c)
    F = \ddot{x}_{\tau} m_{\tau} + \dot{x}_{\tau} b_{\tau} + m_{L} g d = \dot{v}_{\tau} m_{\tau} + v_{\tau} b_{\tau} + m_{L} g d , v_{\tau} = \dot{x}_{\tau} (1)
m_{L} g d = \ddot{x}_{L} m_{L} + \dot{x}_{L} b_{L} = \dot{v}_{L} m_{L} + v_{L} b_{L} , v_{L} = \dot{x}_{L} (2)
L d = x_{\tau} - x_{L} 
= \sqrt{x_{\tau} m_{\tau} + v_{\tau} b_{\tau} + m_{L} g d} , v_{\tau} = \dot{x}_{\tau} (1)
= \sqrt{x_{\tau} m_{\tau} + v_{\tau} b_{\tau} + m_{L} g d} , v_{\tau} = \dot{x}_{\tau} (1)
= \sqrt{x_{\tau} m_{\tau} + v_{\tau} b_{\tau} + m_{L} g d} , v_{\tau} = \dot{x}_{\tau} (1)
= \sqrt{x_{\tau} m_{\tau} + v_{\tau} b_{\tau} + m_{L} g d} , v_{\tau} = \dot{x}_{\tau} (1)
= \sqrt{x_{\tau} m_{\tau} + v_{\tau} b_{\tau} + m_{L} g d} , v_{\tau} = \dot{x}_{\tau} (2)
                   \frac{d}{dL} \rightarrow L\dot{\Phi} = v_T - v_L \qquad (3)
  Laplace of all
   2\{(1)\} = (4) \Rightarrow F = sV_{T}m_{T} + V_{T}b_{T} + m_{L}g\Phi
2\{(2)\} = (5) \Rightarrow m_{L}g\Phi = sV_{L}m_{L} + V_{L}b_{L} = V_{L}(sm_{L}+b_{L})
2\{(3)\} = (6) \Rightarrow sL\Phi = V_{T} - V_{L}
  Rearrange (6) for V_L, V_L = V_T - sL\phi (7)
 Use (7) in (5)
                    m_L g \Phi = V_L (sm_L + b_L) = (V_T - sL\Phi)(sm_L + b_L)
      m_{g} \Phi + sL(sm_{L} + b_{L}) \Phi = V_{T}(sm_{L} + b_{L})
(m_{g} + s^{2}Lm_{L} + sLb_{L}) \Phi = V_{T}(sm_{L} + b_{L})
       \frac{\phi(s)}{V_{T}(s)} = \frac{sm_{L} + b_{L}}{s^{2}Lm_{L} + sLb_{L} + mg^{4}}
In my case this will result in Using the values of my section b_=1.6 L=1.5 m_=0.2 m_=0.1
\frac{\phi(s)}{\chi(s)} = \frac{s(0.2) + 1.6}{s^2(1.5)(0.2) + s(1.5)(1.6) + (0.2)(9.81)} = \frac{0.2s + 1.6}{0.3s^2 + 2.4s + 1.962}
```