ECE 447: Control Systems

goal: approximate nonlinear system behavior using linear systems

(a) linearization  $\leftarrow \dot{x} = f(x,u) \simeq A \cdot Sx + B \cdot Su$ , Sx = x - xe

where  $A = \partial_x f(x_e, u_e)$ ,  $B = \partial_u f(x_e, u_e)$ ,  $Su = u - u_e$ 

 $\leftarrow x(t) = e^{At} x(0)$  solves  $\dot{x} = Ax$ (b) matrix exponential

(homogeneous response) to initial condition

where  $e^{X} = I + X + \frac{1}{2}X^{2} + \frac{1}{3}X^{3} + \dots = \sum_{k=-\infty}^{\infty} \frac{1}{k!}X^{k}$ 

(c) convolution equation  $\leftarrow x(t) = e^{At}x(0) + \int_{-\infty}^{t} e^{A(t-\tau)}Bu(t)d\tau$ (particular response) to cantrol input solves &= Ax+Bre

· linear output y=(x+Du has

step response CA-'eA+B-CA-'B+D

(a) linearization

[AMV2 Ch 6.] [Nu7 Ch 2.11]

-> so the important guestian

Few physical elements display truly linear characteristics. For example the relation between force on a spring and displacement of the spring is always nonlinear to some degree. The relation between current through a resistor and voltage drop across it also deviates from a straight-line relation. However, if in each case the relation is reasonably linear, then it will be found that the system behavior will be very close to that obtained by assuming an ideal, linear physical element, and the analytical simplification is so enormous that we make linear assumptions wherever we can possibly do so in

is not "is my system linear."

but instead "is linearity

a good approximation?"

Robert H. Cannon, Dynamics of Physical Systems, 1967 [Can03].

ex: "rocket flight" (really: pendulum)

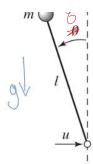


good conscience.

· state x = (g, g) - ongle, velocity

· input u - horizontal acceleration of prot





- · input u honzantal acceleration of prot
- · (DE) ml² ; = mglsing x ; + lu cos ;

$$\ddot{X} = \begin{bmatrix} \dot{g} \\ \dot{g} \end{bmatrix} = \begin{bmatrix} \dot{g} \\ 9/\varrho \sin g - \frac{\lambda}{m \ell^2} \dot{g} + \frac{1}{m \ell} u\cos g \end{bmatrix} = f(X, u)$$

$$k \in \mathbb{Z}$$

we previously determined that 
$$u_e = 0$$
 has  $x_e = \begin{bmatrix} k.77 \\ 0 \end{bmatrix} = \begin{bmatrix} 8e \\ 3e \end{bmatrix}$ 

as equilibria ~ we will approximate f arand (Xe, Ue) Using Taylor series:

-> compute first-order Taylor somes of f wit x & re @ (xe, ve)

$$- f((g, \dot{g}), u) = \begin{bmatrix} \dot{g} \\ \ddot{g}(g, \dot{g}, u) \end{bmatrix}$$

- g = g is the first-order Taylor series of g wrt (gig) & u

$$-\frac{8}{8}(8,8,1) = 2 \sin 8$$

$$-\frac{2}{8} \cos 8$$

$$+\frac{1}{8} \cos 8$$

$$= 2 \sin \theta \qquad 2 \cdot (8 - 8e)$$

$$- \frac{1}{m^2} \cos \theta \qquad - \frac{1}{m^2} \cos \theta \qquad - \frac{1}{m^2} \cos \theta \qquad + \frac$$

= 1 12 · single · (9 - 6e)

 $line = \frac{9}{6} \cdot (g - k\pi) - \frac{\alpha}{mn^2} \cdot g + \frac{1}{mn} \cdot u$ 

$$\frac{\text{linear}}{2} \longrightarrow \frac{9}{2} \cdot (g - k\pi) - \frac{\alpha}{m\ell^2} \cdot g + \frac{1}{m\ell} \cdot u$$

o more generally, for nonlinear system (NL)  $\dot{x} = f(x,u)$ ,  $x \in \mathbb{R}^n$ , every with equilibrium (xe, ue) E IR" xIRP s.t. "x'e = f(xe, ue) = 0 then  $\dot{x} = f(x, u) \simeq f(x_e, u_e) + \left[\frac{2}{2x}f(x_e, u_e)(x - x_e)\right] + O(|x - x_e||^2)$  $+ \frac{2}{2u} f(x_{e}, u_{e}) \cdot (u - u_{e}) + O(||u - u_{e}||^{2})$ 

our "linearization" "higher-order" terms

where  $\frac{\partial}{\partial x} f = \left[ \frac{\partial}{\partial x_{i}} f_{i} \right]_{i,i} = \left[ \frac{\partial}{\partial x_{i}} f_{i} \right]_{i,j} = \left[ \frac{\partial}{\partial x_{i}} f$ "Jacobian" derivative

ile an nxn matrix, eRm [Dx, fn - ... Dx, fn]

$$\frac{\partial}{\partial u}f = \left[\frac{\partial}{\partial u_{\ell}}f_{i}\right]_{i,\ell} = \left[\frac{\partial}{\partial u_{i}}f_{i}\right]_{i,\ell} \frac{\partial}{\partial u_{i}}f_{i} - \cdots \frac{\partial}{\partial u_{p}}f_{i}$$

$$\in \mathbb{R}^{n \times p}$$

$$\left[\frac{\partial}{\partial u_{\ell}}f_{i}\right]_{i,\ell} = \left[\frac{\partial}{\partial u_{\ell}}f_{i}\right]_{i,\ell} - \cdots + \left[\frac{\partial}{\partial u_{p}}f_{i}\right]_{i,\ell}$$

$$\left[\frac{\partial}{\partial u_{\ell}}f_{i}\right]_{i,\ell} - \cdots + \left[\frac{\partial}{\partial u_{p}}f_{i}\right]_{i,\ell}$$

and  $\frac{\partial}{\partial x} f(x_e, u_e) = \frac{\partial}{\partial x} f|_{x=u_e} = \frac{\partial}{\partial u} f(x_e, u_e) = \frac{\partial}{\partial u} f|_{x=u_e} = \frac{\partial}{\partial u} f|_{u=u_e}$ 

kso if we let Sx = x-xe, Su = u-Ve

we have (L)  $8x \sim A \cdot 8x + B \cdot 8u$ ,  $A = \frac{2}{2x} f(x_e, u_e)$ 

 $B = \frac{2}{2nl} f(x_e, u_e)$ 

i.e. (NL) is approximately egyal to (L),  $B = \frac{3}{5} u f(x_e, u_e)$  which is a linear time-invariant system?

(b) matrix exponential [AMV2 Ch 6.2] [NV7 Ch 4.11 & Appendix I] o recall the homogeneous solution to scalar (DE) if tag = 0 are, with x = y be state of (DE),  $x(t) = e^{-at}x(a)$ where e: ( -> ( is defined by a power series  $: 3 \mapsto 1 + 3 + \frac{1}{2} \cdot 3^2 + \frac{1}{3!} \cdot 3^3 + \dots = \sum_{k=0}^{\infty} \frac{1}{k!} \cdot 3^k$ and satisfies  $\frac{d}{dt}e^{-at} = -ae^{at}$   $(k! = k \cdot (k-1) \cdot (k-2) \cdot - 2 \cdot 1)$  is read as "k factorial"  $\star$  the power series converges for every  $\xi \in \mathbb{C}$   $\to$  cmazingly, it also makes sense for  $X \in \mathbb{C}^{n \times n}$ . well-defined b/c matrix mult. - is associative  $C: \mathbb{C}_{N\times N} \to \mathbb{C}_{N\times N}$ exp =  $: X \longrightarrow I + X + \frac{1}{2}X \cdot X + \frac{1}{3!}X \cdot X \cdot X + \dots = \sum_{k=0}^{\infty} \frac{1}{k!}X^k$ \* this power series converges for every  $X \in \mathbb{C}^{n \times n}$   $(V) = e^X = exp$  $= e_X = exb(x)$ -> show that  $\frac{d}{dt}e^{At} = Ae^{At}$ ,  $A \in \mathbb{C}^{n \times n}$ ,  $t \in \mathbb{R}$ using definition of e<sup>At</sup> as a power series:  $-\frac{d}{dt}e^{At} = \frac{d}{dt}\left(\sum_{k=0}^{\infty}\frac{1}{k!}(At)^{k}\right) = \frac{d}{dt}\left(I + At + \frac{1}{2}(At)\cdot(At) + \cdots\right)$ 

lec-fa21 Page 4

$$-\frac{d}{dt}e^{At} = \frac{d}{dt}\left(\sum_{k=0}^{\infty}\frac{1}{k!}(At^k)\right) = \frac{d}{dt}\left(I + At + \frac{1}{2}(At)\cdot(At) + \cdots\right)$$

$$= 0 + A + A^2t + \frac{1}{2}A^3t^2 + \cdots \qquad A \cdot t \cdot A \cdot t = A \cdot A \cdot t \cdot t = A^2t^2$$

$$= A \cdot \left(I + A + \frac{1}{2}A^2t^2 + \cdots\right) \qquad \frac{d}{dt}\left(\frac{1}{k!}(At^k)\right) = \frac{d}{dt}\left(\frac{1}{k!}A^k \cdot t^k\right)$$

$$= A \cdot \sum_{k=0}^{\infty}\frac{1}{k!}A^kt^k = Ae^{At} \qquad \nabla \qquad = \frac{1}{(k-1)!}A^kt^{k-1}$$

$$+ \text{ we canclude that } \qquad x(t) = e^{At} \cdot x(0) \text{ solves } \qquad x = Ax, x \in \mathbb{R}^n \text{ o}$$

$$\Rightarrow \text{ campare with } \qquad y(t) = \sum_{k=1}^{\infty} c_k e^{Skt}, \quad \{c_k\}_{k=1}^n \text{ are determined by}$$

$$\text{the initial candition } \left\{\frac{d^k}{dt^k}y(0)\right\}_{k=0}^{n-1}$$

the initial condition 
$$\{\frac{d^{k}}{dt^{k}}y(0)\}_{k=0}^{n-1}$$

where  $e^{X} = I + X + \frac{1}{2}X^{2} + \frac{1}{3}X^{3} + \dots = \sum_{k=0}^{\infty} \frac{1}{2}X^{k}$ 

ex:  $\ddot{g} = u$  (dable integrator)

with  $x = \begin{bmatrix} 9 \end{bmatrix}$  we have  $\frac{d}{dt}x = \begin{bmatrix} \frac{9}{6} \end{bmatrix} = \begin{bmatrix} 0 & 1 \end{bmatrix} \begin{bmatrix} 8 \\ 9 \end{bmatrix} + \begin{bmatrix} 6 \end{bmatrix} u$ 

onoting that  $A \cdot A = A^{2} = 0$  ( $\Rightarrow A^{k} = A^{k^{2}} \cdot A^{2} = 0$ ,  $k > 2$ )

so we compute  $e^{At} = I + At = \begin{bmatrix} 1 & t \\ 0 & 1 \end{bmatrix}$ 

homogeneous solution  $\begin{bmatrix} g(t) \\ g(t) \end{bmatrix} = \chi(t) = e^{At} \chi(0) = \begin{bmatrix} 1 & t & f & g(0) \\ 0 & 1 & g(0) \end{bmatrix}$ agrees with physical/signal  $\longrightarrow = \begin{bmatrix} g(0) + t \cdot g(0) \\ g(0) \end{bmatrix}$ intuition: in the absence of forcing, a mass mores at constant speed

ex: spring-mass w no damping:  $\ddot{g} + \omega^2 g = u$ outh  $x = \begin{bmatrix} g \\ g \\ w \end{bmatrix} \Rightarrow \dot{x} = \begin{bmatrix} \dot{g} \\ \dot{g} \\ w \end{bmatrix} = \begin{bmatrix} 0 & \omega \end{bmatrix} \begin{bmatrix} g \\ \dot{g} \\ w \end{bmatrix} + \begin{bmatrix} 0 \\ 1 \end{bmatrix} u$   $= A \times + B u$   $\Rightarrow verify e^{At} = \begin{bmatrix} \cos \omega t & \sin \omega t \end{bmatrix} \text{ via differentiation}$ 

-> verify  $e^{At} = \begin{bmatrix} \cos \omega t & \sin \omega t \\ -\sin \omega t & \cos \omega t \end{bmatrix}$  via differentiation

oso 
$$\left[\frac{g(t)}{g(t)}\right] = \chi(t) = e^{At} \chi(0) = \left[\frac{\cos \omega t \sin \omega t}{\sin \omega t}\right] \left[\frac{g(0)}{g(0)}\right] = \left[\frac{\sin \omega t}{g(0)}\right] \left[\frac{g(0)}{g(0)}\right] = \left[\frac{\cos \omega t}{g(0)}\right] = \left[\frac$$

ex:  $A = \begin{bmatrix} 6 & \omega \\ -\omega & 5 \end{bmatrix}$  < recall  $\lambda(A) = 6 \pm j\omega$ 

-> verify 
$$e^{At} = e^{St} \begin{bmatrix} \cos \omega t & \sin \omega t \\ -\sin \omega t & \cos \omega t \end{bmatrix}$$
 by differentiation

(c) convolution equation [AMV2 Ch 6.3] [NV7 Ch 4.11 \( \) App.I] oconsides the state-space LTI system 
$$\hat{x} = Ax + Bu$$

fact: given  $x(o) \in IR^n$  and  $u: [o,t] \rightarrow IR^p$ ,

 $x(t) = e^{At}x(o) + \int_{o}^{t} e^{A(t-\tau)}Bu(\tau)d\tau \leftarrow convolution$ 

homogeneous response particular response to  $x(o)$ 

-> verify this formula by differentiation (recall Leibniz's formula for differentiating on integral)

o consider 
$$\mathring{x} = Ax + Bu$$
 with  $x = Ax + Bu$  with  $y = Cx + Du$   $y = Cx + Du$   $y = Cx + Du$   $y = Cx + Du$ 

so that  $y(t) = Cx(t) + Du(t)$ 

$$= Ce^{At}x(0) + P^{t}Ce^{A(t-z)}Bu(z)dz + Du(t)$$

lec-fa21 Page

= CeAtx(o) + Pt CeA(t-z) Bu(z)dz + Du(t)

homogeneus output

partialar output olet's examine the response to unit step  $\mu(z) = \{1, \tau > 0\}$  i.e. the step response, when  $\chi(0) = 0$  $P^{t}$   $Ce^{A(t-z)}$   $B\mu(z)dz + D\mu(t) (=0)$  when t<0, so assume t>0: assuming to:  $= C \int_{0}^{t} A(t-\tau) d\tau B + D$ assuming A invertible: =  $C \left[ -A^{-1}e^{A(t-\tau)} \right]^{T=t} B + D$ note: e = I + O+ 202 = C (-A-1 e A-0 + A-1 e At) B+D  $= CA^{-1}e^{At}B - CA^{-1}B + D$ transient steady-state step response step response -assuming A stable, ie. all eigenvalues have regentive real part: lin e At -> 0, so transient -> 0 as t >0 > step response to u as above 1.5 Overshoot  $M_{\rm p}$ 

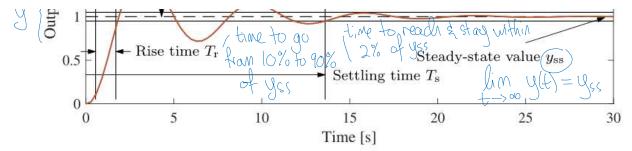


Figure 6.9: Sample step response. The rise time, overshoot, settling time, and steady-state value give the key performance properties of the signal.

note: Mp, Tr, Ts are independent of step size