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i.e. constant input file and ideal sensors/actuators, control strategy
according to BSM1 description
(Results from Matlab/Simulink implementation by Dr Ulf Jeppsson, IEA, Lund
University, Sweden, May 21 2009 - based on Matlab R2008b (ver 7.7.0))
Influent characteristics
*******
   SI = 30 \text{ mg COD/l}
   SS = 69.5 \text{ mg COD/l}
   XI = 51.2 \text{ mg COD/l}
   XS = 202.32 \text{ mg COD/l}
   XBH = 28.17 \text{ mg COD/l}
   XBA = 0 mg COD/1
   XP = 0 mg COD/1

SO = 0 mg -COD/1
   SNO = 0 mg N/1
   SNH = 31.56 mg N/1
   SND = 6.95 mg N/1
   XND = 10.59 mg N/1
   SALK = 7 mol HCO3/m3
   TSS = 211.2675 \text{ mg } SS/1
Flow conditions
******
   Influent flow to WWTP = 18446 \text{ m}3/d
   Influent flow to AS = 53377.6075 \text{ m}3/d
   Internal recirculation = 16485.6075 m3/d
   Settler feed flow = 36892 m3/d
   Returned sludge flow = 18446 m3/d
   Wastage sludge flow = 385 m3/d
   Effluent flow = 18061 \text{ m}3/d
Input to AS
******
   SI = 30 \text{ mg COD/l}
   SS = 24.5463 \text{ mg COD/l}
   XI = 1149.1683 \text{ mg COD/l}
   XS = 113.7148 \text{ mg COD/l}
   XBH = 2533.1267 \text{ mg COD/l}
   XBA = 151.7894 \text{ mg COD/l}
   XP = 445.766 \text{ mg COD/l}
SO = 1.3088 mg -COD/l
   SNO = 8.8506 mg N/1
   SNH = 11.3461 mg N/1
   SND = 2.8366 mg N/1
   XND = 6.8699 \text{ mg N/l}
   SALK = 4.924 mol HCO3/m3
   TSS = 3295.1739 mg SS/1
Reactor 1
******
   SI = 30 \text{ mg COD/l}
   SS = 3.2439 \text{ mg COD/1}
   XI = 1149.1683 \text{ mg COD/l}
   XS = 98.6029 \text{ mg COD/l}
   XBH = 2552.1095 \text{ mg COD/l}
   XBA = 151.6721 mg COD/1
   XP = 446.9249 \text{ mg COD/l}
   SO = 0.0076964 \text{ mg } -COD/1
   SNO = 3.5133 mg N/1
   SNH = 11.8312 mg N/1
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SND = 1.3621 mg N/1

STEADY STATE RESULTS FOR CLOSEDLOOP

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XND = 6.1775 \text{ mg N/l}
    SALK = 5.3399 mol HCO3/m3
    TSS = 3298.8583 \text{ mg } SS/1
Reactor 2
*****
    SI = 30 \text{ mg COD/l}
    SS = 1.6707 \text{ mg COD/l}
   XI = 1149.1683 \text{ mg COD/l}
   XS = 91.7032 \text{ mg COD/1}
   XBH = 2552.3711 \text{ mg COD/l}
   XBA = 151.5303 \text{ mg COD/l}
   XP = 448.0839 \text{ mg COD/1}
    SO = 6.0271e-05 \text{ mg } -COD/1
    SNO = 1 mg N/1
    SNH = 12.5482 mg N/1
    SND = 0.78899 mg N/1
    XND = 5.9537 \text{ mg N/l}
    SALK = 5.5706 \text{ mol } HCO3/m3
    TSS = 3294.6426 \text{ mg } SS/1
Reactor 3
******
    SI = 30 \text{ mg COD}/1
   SS = 1.2195 \text{ mg COD/l}
   XI = 1149.1683 \text{ mg COD/l}
   XS = 69.6594 \text{ mg COD/l}
   XBH = 2560.2025 \text{ mg COD/1}
   XBA = 152.6873 \text{ mg COD/l}
   XP = 449.6336 \text{ mg COD/l}
   SO = 1.635 \text{ mg } -COD/1
   SNO = 6.2289 \text{ mg N/l}
   SNH = 7.3197 mg N/1
   SND = 0.8307 \text{ mg N/l}
   XND = 4.7131 \text{ mg N/l}
    SALK = 4.8236 \text{ mol } HCO3/m3
   TSS = 3286.0133 \text{ mg } SS/1
Reactor 4
*****
   SI = 30 \text{ mg COD/l}
   SS = 0.97326 \text{ mg COD/l}
   XI = 1149.1683 \text{ mg COD/l}
   XS = 54.4484 \text{ mg COD/l}
   XBH = 2563.3104 \text{ mg COD/l}
   XBA = 153.7108 \text{ mg COD/l}
   XP = 451.1853 \text{ mg COD/1}
SO = 2.4745 mg -COD/1
    SNO = 11.0693 mg N/1
    SNH = 2.7825 mg N/1
    SND = 0.75276 \text{ mg N/l}
    XND = 3.8403 \text{ mg N/l}
    SALK = 4.1538 mol HCO3/m3
    TSS = 3278.8674 \text{ mg } SS/1
Reactor 5
*****
   SI = 30 \text{ mg COD/l}
   SS = 0.80801 \text{ mg COD/l}
   XI = 1149.1683 \text{ mg COD/l}
   XS = 44.4828 \text{ mg COD/l}
   XBH = 2562.8514 \text{ mg COD/l}
   XBA = 154.163 \text{ mg COD/l}
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XP = 452.7367 \text{ mg COD/l}
   SO = 2 mg - COD/1
   SNO = 13.5243 \text{ mg N/l}
   SNH = 0.67193 mq N/1
   SND = 0.6645 \text{ mg N/l}
   XND = 3.2605 \text{ mg N/l}
   SALK = 3.8277 \text{ mol } HCO3/m3
   TSS = 3272.5517 \text{ mg } SS/1
Settler underflow
******
   SI = 30 \text{ mg COD/l}
   SS = 0.80801 \text{ mg COD/l}
   XI = 2247.1366 \text{ mg COD/l}
   XS = 86.9837 \text{ mg COD/l}
   XBH = 5011.5177 mg COD/1
   XBA = 301.4575 mg COD/1
   XP = 885.3022 \text{ mg COD/1}
SO = 2 mg -COD/1
   SNO = 13.5243 \text{ mg N/l}
   SNH = 0.67193 mg N/1
   SND = 0.6645 \text{ mg N/l}
   XND = 6.3757 \text{ mg N/l}
   SALK = 3.8277 \text{ mol } HCO3/m3
   TSS = 6399.2982 \text{ mg } SS/1
Settler effluent
******
   SI = 30 \text{ mg COD/l}
   SS = 0.80801 \text{ mg COD/l}
   XI = 4.39 \text{ mg COD/l}
   XS = 0.16993 \text{ mg COD/l}
   XBH = 9.7905 mg COD/1
   XBA = 0.58893 \text{ mg COD/1}
   XP = 1.7295 \text{ mg COD/l}
   SO = 2 mq - COD/1
   SNO = 13.5243 \text{ mg N/l}
   SNH = 0.67193 mg N/1
   SND = 0.6645 \text{ mg N/l}
   XND = 0.012455 \text{ mg N/l}
   SALK = 3.8277 \text{ mol } HCO3/m3
   TSS = 12.5016 \text{ mg } SS/1
Settler internal (1 is top layer)
*********
   TSS1 = 12.5016 mg SS/1
   TSS2 = 18.1183 mg SS/1
   TSS3 = 29.548 mg SS/1
   TSS4 = 69.0015 mg SS/1
   TSS5 = 356.2825 \text{ mg } SS/1
   TSS6 = 356.2825 \text{ mg SS/l}
   TSS7 = 356.2825 \text{ mg } SS/1
   TSS8 = 356.2825 \text{ mg } SS/1
   TSS9 = 356.2825 \text{ mg } SS/1
   TSS10 = 6399.2982 \text{ mg } SS/1
Other variables
   Trad. sludge age (XS + XP + XI + XBH + XBA in reactors) = 7.3273 days
   Spec. sludge age (XBH + XBA in reactors and settler) = 9.139 days
   Total hydraulic retention time = 15.6118 hours
   Reactor hydraulic retention time = 7.8053 hours
   Thickening factor at bottom of settler(TSSu/TSSfeed) = 1.9554
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Thinning factor at top of settler (TSSeff/TSSfeed) = 0.0038201

Dimensions ******

Reactor 1 is anoxic
Volume reactor 1 = 1000 m3
Reactor 2 is anoxic
Volume reactor 2 = 1000 m3
Reactor 3 is aerobic
Volume reactor 3 = 1333 m3
Reactor 4 is aerobic
Volume reactor 4 = 1333 m3
Reactor 5 is aerobic
Volume reactor 5 = 1333 m3
Settler height = 4 m
Settler area = 1500 m2
Settler volume = 6000 m3