

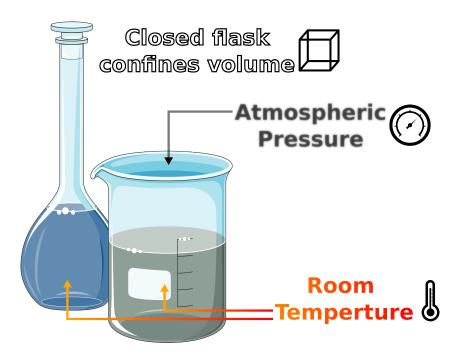
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#### Molecular Dynamics (SS2025) Exercise 4

## Pressure and Temperature Coupling in MD Simulations

### Report Tasks

- 1. For all 12 simulations, list  $\sigma_{\rm V}^2$  and  $\kappa_{\rm T}$  tabularly and plot  $E_{\rm tot}$ , V and P as a function of time. Discuss differences and similarities between barostats and choices of  $\tau_{\rm P}$ .
- 2. Calculate  $\kappa_T$  for TIP4P and SPC/E Water and compare to the experimental value.
- 3. Briefly, describe the differences in  $E_{\rm kin}$ ,  $E_{\rm pot}$ ,  $\rho$ , H and  $E_{\rm tot}$  for the standard and non-standard simulation. Try to explain said differences and propose an MD-based method to verify your explanation.



**Figure 1:** The application of a thermodynamic ensemble (NVT, NPT) is required to mimic the physical conditions in the wet lab. High accuracy algorithms for barostatting and thermostatting are crucial to yield realistic results from an MD simulation.<sup>1</sup>

## The Choice of the Coupling Constant Matters

After last week's tutorial about temperature coupling, everything in this tutorial is centered around pressure coupling and the isothermic-isobaric ensemble. The final goal is to calculate

<sup>&</sup>lt;sup>1</sup>Flask images were taken from https://smart.servier.com/ (CC-BY 3.0)



the isothermal compressibility  $\kappa_T$  which depends on the volume fluctuations of the simulation. Thus, if the simulation does not reproduce accurate volume fluctuations, as a result of pressure coupling,  $\kappa_T$  will be erroneous.

Just like in temperature coupling, a barostat can be tuned by adjusting its coupling parameter  $\tau_{\rm P}$ . This parameter defines how tight the system's pressure is coupled. For a thorough comparative analysis, six different coupling constants  $\tau_{\rm P}$  and two barostats (Berendsen and Parrinello-Rahman) should be tested in simulations of a TIP3P water box. The MDP files can be found in the download repository, with missing values for the  $\tau_{\rm P}$ -option and the barostat in the NPT input files. The values to be screened are listed in table 1.

In the previous three exercises, the input files were usually pre-made and ready to use. In this exercise, creating the GRO and TOP file is part of the task. A good starting point would be the command gmx solvate. This command offers a variety of options to solvate systems or create them from scratch. Since the command is quite versatile, it is recommended to read the GROMACS documentation to figure out the crucial flags and options. Set the box dimensions to  $2.504 \times 2.504 \times 2.50$ 

Unfortunately, gmx solvate regularly fails to squeeze the requested amount of solvent into the simulation box. Hence, the <code>-maxsol</code> flag should be set to 1 so that we can use the resulting one-water GRO file as input for <code>gmx insert-molecules</code> <sup>4</sup>. This command fills a given box with the required number of water molecules (523) and unlike <code>gmx solvate</code> it tries to meet the specifications as many times as given in <code>-try</code>. The generated single-water GRO file should be used for the <code>-ci</code> flag. Finally, <code>gmx pdb2gmx</code> creates the respective TOP file, herein with the TIP3P water model and the Amber99sb-ildn forcefield. An exemplary workflow for creating the aqueous system is shown below.

As a reminder, you should make sure to keep directories and naming conventions within your projects clean and consistent. Thus, names should be kept as short as possible and as informative as necessary in order to maintain a good overview. Anyhow, the simulation sequence consists of a minimisation, followed by an NVT Simulation and then by the NPT-Ensemble. The values for  $\tau_P$  can be found in the following table. For certain  $\tau_P$  values adjusting the -maxwarn flag of gmx grompp might be necessary.

**Table 1:**  $\tau_{\rm P}$  values to be selected for simulations.

$\tau_{\mathrm{P}}/\mathrm{ps}^{-1} \mid 0.05$	0.1	0.5	1	5	10
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For the Parrinello-Rahman barostat and  $\tau_P$  values above  $0.1\,\mathrm{ps}^{-1}$ , the option nstpcouple = 1 must be deleted in the respective MDP files. For each NPT-simulation, plot the Volume V and Pressure P against time and calculate the variance of the volume  $\sigma_V^2$  over the course of

<sup>&</sup>lt;sup>2</sup>The manual creation of the two missing files is an optional sub-task. If time is limited, this task may be skipped by using tip3pbox.gro and tip3p.top from last weeks exercise.

<sup>&</sup>lt;sup>3</sup>https://manual.gromacs.org/documentation/2018/user-guide/cmdline.html

<sup>&</sup>lt;sup>4</sup>https://manual.gromacs.org/documentation/2018/user-guide/cmdline.html



the simulation. Concerning the plots, the first few frames may be excluded, if they are not representative for an equilibrated system by using gmx energy -b <FRAME> .  $\sigma_V^2$  represents the volume fluctuations which are linked to the isothermal compressibility  $\kappa_T$  to be calculated for each  $\tau_P$  as well. Tabulate the various values of  $\sigma_V^2$  and  $\kappa_T$  and feature the plots in the report. Additionally, discuss which of the  $\tau_P$  and barostats delivers results comparable to the literature<sup>5</sup> value of  $\kappa_T^{\text{TIP3P}} = 6.3 \times 10^{-5} \, \text{bar}^{-1}$  and why others may fail. The command gmx energy is highly recommended to conduct the result collection. The formula GROMACS uses to calculate  $\kappa_T$  comprises the volume fluctuations RMSD(V), the temperature T, the Boltzmann constant  $k_B$  and the average volume  $\langle V \rangle$ .<sup>6</sup>

$$\kappa_{\rm T} = \frac{\text{MSD}(V)}{k_{\rm B}T\langle V \rangle} \tag{1}$$

The command is analogous to the one used in the prior exercise to obtain the isochoric heat capacity. The *energetic* properties, that you need to pick from the interactive menu can be deduced from the formula above.

gmx energy -f <ENERGYFILE> -o <OUTPUTFILE> -fluct\_props -nmol <NUMBER>

## Influence of the Water Model on the Isothermal Compressibility

In this task, two water models should be simulated in order to investigate the influence of different water models on  $\kappa_{\rm T}$ . Optimally, the experimental value  $^7$   $\kappa_{\rm T}^{\rm exp}=4.52\times 10^{-5}\,{\rm bar}^{-1}$  for 298.15 K is retained from the simulation runs. The water models in question are the SPC/E and TIP4P water model. This time, the simulation procedure includes an energy minimisation, an NVT- and NPT-equilibration, conlcuded by the preproduction and production run. It is common practice to use the Berendsen thermostat and barostat for the NVT- and NPT-equilibrations since it is robust and computationally inexpensive. The pre-production and production runs are usually simulated with the Nose-Hoover and Parrinello-Rahman algorithms for high fidelity production data. The pre-production run facilitates the system adjusting itself to the enhanced algorithms. As shown in last week's tutorial, some algorithms sample a certain ensemble more reliably which implies the introduction of physical changes that the system has to adapt to. The transition time necessary for this adaptation should not be included in the analysis since it is not representative of the thermodynamic equilibrium. The data for result computation should stem only from the fully equilibrated production run.

In order to save time, nsteps in the MDP files can be adjusted based on the MD runs from the first task. Simulations should be long enough to collect sufficient data to compute results, but not longer (feel free to play around with the nsteps option).

All necessary MDP files are given or can be repurposed and the TOP and GRO files can be obtained via the aforementioned workflow. SPC/E is a three-site water model and TIP4P is a four-site water model, thus the correct option for the <code>-cs</code> flag must be ensured.

```
gmx solvate [...] | gmx insert-molecules [...] | gmx pdb2gmx [...] # Procedure of obtaining GRO
and TOP file
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Once the simulations have finished, gmx energy is recommended to evaluate which of the water models performs better with respect to  $\kappa_{\rm T}$ .

<sup>&</sup>lt;sup>5</sup>https://doi.org/10.1063/5.0020514

<sup>&</sup>lt;sup>6</sup>Allen M., Tildesley D. Computer Simulations of Liquids. Oxford. Clarendon Press. 1987. p.53

<sup>&</sup>lt;sup>7</sup>https://doi.org/10.1063/5.0050841





# Simulation Behaviour for Large $\tau_{\text{\tiny T}}$ Values

In the preceding tasks, strengths and weaknesses between algorithms were uncovered and parameter choices for  $\tau_P$  were examined as well as the feasibility of different water models. Thus, our thoughts revolved mostly around the pressure coupling aspect within MD simulations. This last task, serves as a reminder that a simulation consists of a delicate interplay of various algorithms and their settings.

Therefore, two simulation setups shall be compared with each other. One features a relatively tight pressure coupling and a high  $\tau_{\rm T}$  value, corresponding to infrequent corrections to the temperature. Meanwhile, the  $\tau_{\rm T}$  and  $\tau_{\rm P}$  values of the other setup can be considered standard. The system itself is exactly the same as in the second task. Therefore, the only differences lie in the MDP files deposited in the moodle directory. Said files, standard.mdp and non\_standard.mdp, should be used to simulate the NVT-equilibrated SPC/E system from the second task. Once the simulation is done, use gmx energy to calculate and plot the kinetic energy  $E_{\rm kin}$ , the potential energy  $E_{\rm pot}$ , the density  $\rho$ , the enthalpy H and the total energy  $E_{\rm tot}$  of the two simulations.

Include your plots in the report and discuss differences in their appearances. Try to come up with an explanation for your observations and propose a simulation related way to test your hypothesis.