

# Notes on AIMove exercises

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## 1 Forward kinematics (FK) for a planar robot manipulator

The forward kinematics of a planar robot manipulator is defined as

$$\mathbf{f} = \begin{bmatrix} \mathbf{l}^\top \cos(\mathbf{L}\mathbf{x}) \\ \mathbf{l}^\top \sin(\mathbf{L}\mathbf{x}) \\ \mathbf{1}^\top \mathbf{x} \end{bmatrix} = \begin{bmatrix} l_1 \cos(x_1) + l_2 \cos(x_1 + x_2) + l_3 \cos(x_1 + x_2 + x_3) + \dots \\ l_1 \sin(x_1) + l_2 \sin(x_1 + x_2) + l_3 \sin(x_1 + x_2 + x_3) + \dots \\ x_1 + x_2 + x_3 + \dots \end{bmatrix},$$

with  $\mathbf{x}$  the state of the robot (joint angles),  $\mathbf{f}$  the position of the robot end-effector,  $\mathbf{l}$  a vector of robot links lengths,  $\mathbf{L}$  a lower triangular matrix with unit elements, and  $\mathbf{1}$  a vector of unit elements.

The position and orientation of all articulations can similarly be computed with the forward kinematics function

$$\tilde{\mathbf{f}} = \begin{bmatrix} \mathbf{L} \text{diag}(\mathbf{l}) \cos(\mathbf{L}\mathbf{x}), & \mathbf{L} \text{diag}(\mathbf{l}) \sin(\mathbf{L}\mathbf{x}), & \mathbf{L}\mathbf{x} \end{bmatrix}^\top = \begin{bmatrix} \tilde{f}_{1,1} & \tilde{f}_{1,2} & \tilde{f}_{1,3} & \dots \\ \tilde{f}_{2,1} & \tilde{f}_{2,2} & \tilde{f}_{2,3} & \dots \\ \tilde{f}_{3,1} & \tilde{f}_{3,2} & \tilde{f}_{3,3} & \dots \end{bmatrix},$$

with

$$\begin{aligned} \tilde{f}_{1,1} &= l_1 \cos(x_1), \\ \tilde{f}_{2,1} &= l_1 \sin(x_1), \\ \tilde{f}_{3,1} &= x_1, \\ \tilde{f}_{1,2} &= l_1 \cos(x_1) + l_2 \cos(x_1 + x_2), \\ \tilde{f}_{2,2} &= l_1 \sin(x_1) + l_2 \sin(x_1 + x_2), \\ \tilde{f}_{3,2} &= x_1 + x_2, \\ \tilde{f}_{1,3} &= l_1 \cos(x_1) + l_2 \cos(x_1 + x_2) + l_3 \cos(x_1 + x_2 + x_3), \\ \tilde{f}_{2,3} &= l_1 \sin(x_1) + l_2 \sin(x_1 + x_2) + l_3 \sin(x_1 + x_2 + x_3), \\ \tilde{f}_{3,3} &= x_1 + x_2 + x_3, \\ &\vdots \end{aligned}$$

In Python, by ignoring the orientation part, this can be coded as

```
1 D = 3 #State space dimension (joint angles)
2 x = np.ones(D) * np.pi / D #Robot pose
3 l = np.array([2, 2, 1]) #Links lengths
4 L = np.tril(np.ones([D,D])) #Transformation matrix
5 f = np.array([L @ np.diag(l) @ np.cos(L @ x), L @ np.
    diag(l) @ np.sin(L @ x)]) #Forward kinematics
```

## 2 Linear quadratic tracking (LQT)

The LQT problem is formulated as the minimization of the cost

$$\begin{aligned} c &= (\boldsymbol{\mu}_T - \mathbf{x}_T)^\top \mathbf{Q}_T (\boldsymbol{\mu}_T - \mathbf{x}_T) \\ &\quad + \sum_{t=1}^{T-1} \left( (\boldsymbol{\mu}_t - \mathbf{x}_t)^\top \mathbf{Q}_t (\boldsymbol{\mu}_t - \mathbf{x}_t) + \mathbf{u}_t^\top \mathbf{R}_t \mathbf{u}_t \right) \\ &= (\boldsymbol{\mu} - \mathbf{x})^\top \mathbf{Q} (\boldsymbol{\mu} - \mathbf{x}) + \mathbf{u}^\top \mathbf{R} \mathbf{u}, \end{aligned} \quad (1)$$

with  $\mathbf{x} = [\mathbf{x}_1^\top, \mathbf{x}_2^\top, \dots, \mathbf{x}_T^\top]^\top$  the evolution of the state variable and  $\mathbf{u} = [\mathbf{u}_1^\top, \mathbf{u}_2^\top, \dots, \mathbf{u}_{T-1}^\top]^\top$  the evolution of the control variable.  $\boldsymbol{\mu} = [\boldsymbol{\mu}_1^\top, \boldsymbol{\mu}_2^\top, \dots, \boldsymbol{\mu}_T^\top]^\top$  represents the evolution of the tracking target.  $\mathbf{Q} = \text{blockdiag}(\mathbf{Q}_1, \mathbf{Q}_2, \dots, \mathbf{Q}_T)$  represents the evolution of the required tracking precision, and  $\mathbf{R} = \text{blockdiag}(\mathbf{R}_1, \mathbf{R}_2, \dots, \mathbf{R}_{T-1})$  represents the evolution of the cost on the control inputs.

The evolution of the system is linear, described by  $\mathbf{x}_{t+1} = \mathbf{A}_t \mathbf{x}_t + \mathbf{B}_t \mathbf{u}_t$ , yielding  $\mathbf{x} = \mathbf{S}_x \mathbf{x}_1 + \mathbf{S}_u \mathbf{u}$  at trajectory level, see Appendix B for details.

The solution of (1) subject to  $\mathbf{x} = \mathbf{S}_x \mathbf{x}_1 + \mathbf{S}_u \mathbf{u}$  is analytic, given by

$$\hat{\mathbf{u}} = (\mathbf{S}_u^\top \mathbf{Q} \mathbf{S}_u + \mathbf{R})^{-1} \mathbf{S}_u^\top \mathbf{Q} (\boldsymbol{\mu} - \mathbf{S}_x \mathbf{x}_1).$$

The residuals of this least squares solution provides information about the uncertainty of this estimate, in the form of a full covariance matrix (at control trajectory level)

$$\hat{\Sigma}^u = (\mathbf{S}_u^\top \mathbf{Q} \mathbf{S}_u + \mathbf{R})^{-1}.$$

## Appendices

### A Newton's method for minimization

Newton's method attempts to solve  $\min_x f(x)$  or  $\max_x f(x)$  from an initial guess  $x_1$  by using a sequence of second-order Taylor approximations of  $f$  around the iterates, see Fig. 1. The second-order Taylor expansion of  $f$  around  $x_k$  is

$$f(x_k + t) \approx f(x_k) + f'(x_k)t + \frac{1}{2}f''(x_k)t^2. \quad (2)$$

The next iterate  $x_{k+1} = x_k + t$  is defined so as to minimize this quadratic approximation in  $t$ . If the second derivative is positive, the quadratic approximation is a convex function of  $t$ , and its minimum can be found by setting the derivative to zero. Since

$$\frac{d}{dt} \left( f(x_k) + f'(x_k)t + \frac{1}{2}f''(x_k)t^2 \right) = f'(x_k) + f''(x_k)t, \quad (3)$$

the minimum is achieved for

$$t = -\frac{f'(x_k)}{f''(x_k)}. \quad (4)$$

Newton's method thus performs the iteration

$$x_{k+1} = x_k - \frac{f'(x_k)}{f''(x_k)}. \quad (5)$$

The geometric interpretation of Newton's method is that at each iteration, it amounts to the fitting of a paraboloid to the surface of  $f(x)$  at  $x_k$ , having the same slopes and curvature as the surface at that point, and then proceeding to the maximum or minimum of that paraboloid. Note that if  $f$  happens to be a quadratic function, then the exact extremum is found in one step. Note also that Newton's method is often modified to include a step size (e.g., estimated with line search).

The multidimensional case similarly provides

$$\mathbf{x}_{k+1} = \mathbf{x}_k - \mathbf{H}(\mathbf{x}_k)^{-1} \mathbf{g}(\mathbf{x}_k), \quad (6)$$

with  $\mathbf{g}$  and  $\mathbf{H}$  the gradient and Hessian matrix of  $f$  (vector and square matrix, respectively).

### Gauss-Newton algorithm

The Gauss-Newton algorithm is a special case of Newton's method in which the cost is quadratic (sum of squared function values), with  $f(\mathbf{x}) = \sum_{i=1}^R r_i^2(\mathbf{x}) = \mathbf{r}^\top \mathbf{r}$ , and by ignoring the second-order derivative terms of the Hessian. The gradient and Hessian can in this case be computed with

$$\mathbf{g} = 2\mathbf{J}_r^\top \mathbf{r}, \quad \mathbf{H} \approx 2\mathbf{J}_r^\top \mathbf{J}_r, \quad (7)$$

where  $\mathbf{J}_r \in \mathbb{R}^{R \times D}$  is the Jacobian matrix of  $\mathbf{r} \in \mathbb{R}^R$ . The update rule then becomes

$$\mathbf{x}_{k+1} = \mathbf{x}_k - (\mathbf{J}_r^\top(\mathbf{x}_k) \mathbf{J}_r(\mathbf{x}_k))^{-1} \mathbf{J}_r^\top(\mathbf{x}_k) \mathbf{r}(\mathbf{x}_k) \quad (8)$$

$$= \mathbf{x}_k - \mathbf{J}_r^\dagger(\mathbf{x}_k) \mathbf{r}(\mathbf{x}_k). \quad (9)$$

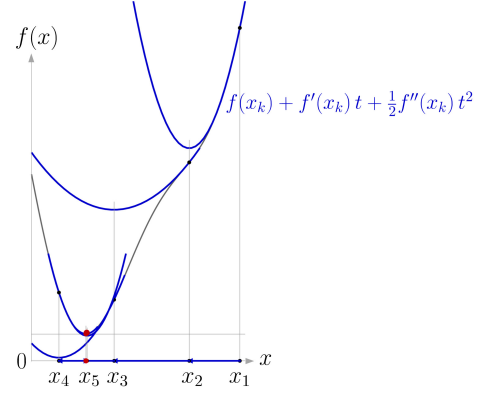


Figure 1: Newton's method for minimization, starting from an initial estimate  $x_1$  and converging to a local minimum (red point) after 5 iterations.

### B System dynamics at trajectory level

The evolution of a system  $\mathbf{x}_{t+1} = g(\mathbf{x}_t, \mathbf{u}_t)$  (expressed in discrete form), can be approximated by the linear system

$$\mathbf{x}_{t+1} = \mathbf{A}_t(\mathbf{x}_t, \mathbf{u}_t) \mathbf{x}_t + \mathbf{B}_t(\mathbf{x}_t, \mathbf{u}_t) \mathbf{u}_t, \quad \forall t \in \{1, \dots, T\}$$

with states  $\mathbf{x}_t \in \mathbb{R}^D$  and control commands  $\mathbf{u}_t \in \mathbb{R}^d$ .

With the above linearization, we can express all states  $\mathbf{x}_t$  as an explicit function of the initial state  $\mathbf{x}_1$ . By writing

$$\begin{aligned} \mathbf{x}_2 &= \mathbf{A}_1 \mathbf{x}_1 + \mathbf{B}_1 \mathbf{u}_1, \\ \mathbf{x}_3 &= \mathbf{A}_2 \mathbf{x}_2 + \mathbf{B}_2 \mathbf{u}_2 = \mathbf{A}_2(\mathbf{A}_1 \mathbf{x}_1 + \mathbf{B}_1 \mathbf{u}_1) + \mathbf{B}_2 \mathbf{u}_2, \\ &\vdots \\ \mathbf{x}_T &= \left( \prod_{t=1}^{T-1} \mathbf{A}_{T-t} \right) \mathbf{x}_1 + \left( \prod_{t=1}^{T-2} \mathbf{A}_{T-t} \right) \mathbf{B}_1 \mathbf{u}_1 + \\ &\quad \left( \prod_{t=1}^{T-3} \mathbf{A}_{T-t} \right) \mathbf{B}_2 \mathbf{u}_2 + \dots + \mathbf{B}_{T-1} \mathbf{u}_{T-1}, \end{aligned}$$

in a matrix form, we get an expression of the form  $\mathbf{x} = \mathbf{S}_x \mathbf{x}_1 + \mathbf{S}_u \mathbf{u}$ , with

$$\underbrace{\begin{bmatrix} \mathbf{x}_1 \\ \mathbf{x}_2 \\ \mathbf{x}_3 \\ \vdots \\ \mathbf{x}_T \end{bmatrix}}_{\mathbf{x}} = \underbrace{\begin{bmatrix} \mathbf{I} \\ \mathbf{A}_1 \\ \mathbf{A}_2 \mathbf{A}_1 \\ \vdots \\ \prod_{t=1}^{T-1} \mathbf{A}_{T-t} \end{bmatrix}}_{\mathbf{S}_x} \mathbf{x}_1 + \underbrace{\begin{bmatrix} \mathbf{0} & \mathbf{0} & \dots & \mathbf{0} \\ \mathbf{B}_1 & \mathbf{0} & \dots & \mathbf{0} \\ \mathbf{A}_2 \mathbf{B}_1 & \mathbf{B}_2 & \dots & \mathbf{0} \\ \vdots & \vdots & \ddots & \vdots \\ \left( \prod_{t=1}^{T-2} \mathbf{A}_{T-t} \right) \mathbf{B}_1 & \left( \prod_{t=1}^{T-3} \mathbf{A}_{T-t} \right) \mathbf{B}_2 & \dots & \mathbf{B}_{T-1} \end{bmatrix}}_{\mathbf{S}_u} \underbrace{\begin{bmatrix} \mathbf{u}_1 \\ \mathbf{u}_2 \\ \vdots \\ \mathbf{u}_{T-1} \end{bmatrix}}_{\mathbf{u}},$$

where  $\mathbf{S}_x \in \mathbb{R}^{dT \times d}$ ,  $\mathbf{x}_1 \in \mathbb{R}^d$ ,  $\mathbf{S}_u \in \mathbb{R}^{dT \times d(T-1)}$  and  $\mathbf{u} \in \mathbb{R}^{d(T-1)}$ .

### Transfer matrices for single integrator

A single integrator is simply defined as  $\mathbf{x}_{t+1} = \mathbf{x}_t + \mathbf{u}_t \Delta t$ , corresponding to  $\mathbf{A}_t = \mathbf{I}$  and  $\mathbf{B}_t = \mathbf{I} \Delta t$ ,  $\forall t \in$

$\{1, \dots, T\}$ , and transfer matrices  $\mathbf{S}_x = \mathbf{1}_T \otimes \mathbf{I}_D$ , and  $\mathbf{S}_u = \begin{bmatrix} \mathbf{0}_{D, D(T-1)} \\ \mathbf{L}_{T-1, T-1} \otimes \mathbf{I}_D \Delta t \end{bmatrix}$ , where  $\mathbf{L}$  is a lower triangular matrix and  $\otimes$  is the Kronecker product operator.