

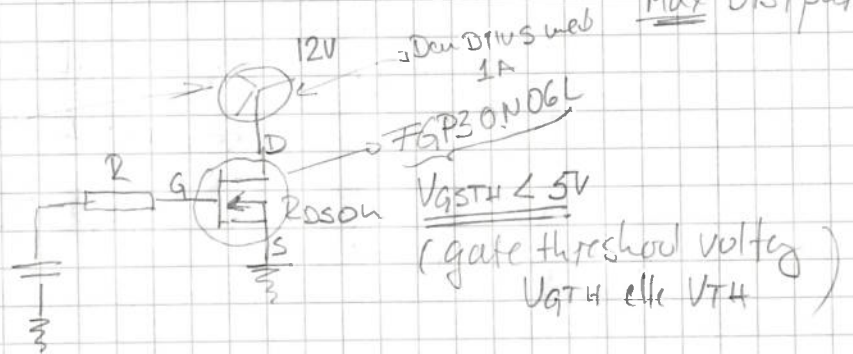
Heat sink

$$\left. \begin{aligned} R_{\theta JA} &= 62,5^\circ\text{C/W} \\ T_{j(\text{max})} &= 175^\circ\text{C} \end{aligned} \right\} \text{datablad}$$

$$P_D = \frac{(\max(T_J - T_A))}{R_{\theta JA}}$$

$$P_D = \frac{175 - 25}{62,5} = 2,4 \text{ W} \quad \text{Max Dissipation}$$

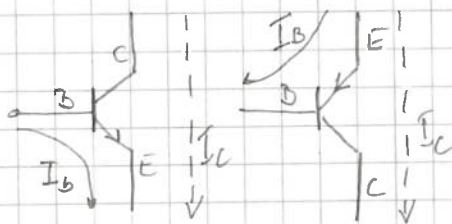
$$\begin{aligned} P &= R \times I^2 \\ &= R_{DS} \times I^2 \\ &= 35 \text{ m}\Omega \times I^2 \\ &= 35 \text{ mW} \end{aligned}$$



NPN

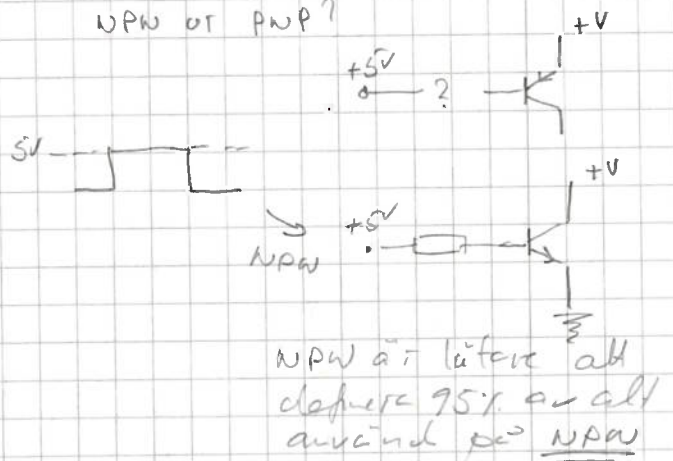
PNP

NPN or PNP?



$$I_C = (\beta_{FE}) I_B$$

β
förstärknings faktor
(värde i datablad)

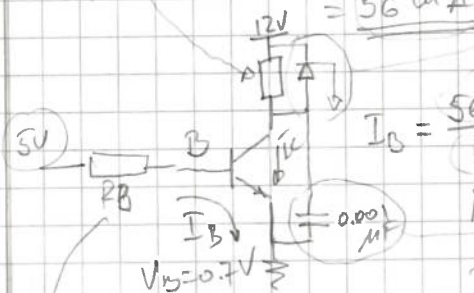


$\beta = 100$ (for PN2222A)

4 anslutningar och specifik
0,67W vid 12V

$$\frac{0,67 \text{ W}}{12 \text{ V}} = 0,558 \text{ A}$$

$$= 56 \text{ mA}$$

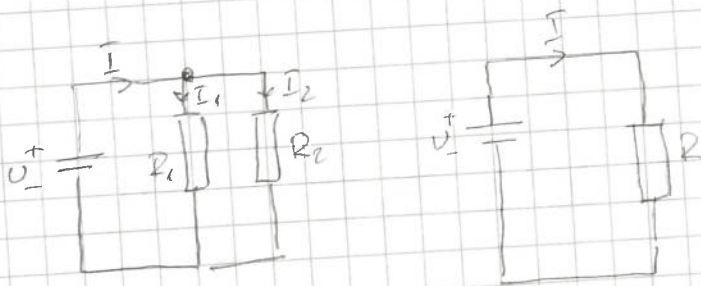


$$R_B = ? \Rightarrow I_B = \frac{5 - 0,7}{R_B} \approx R_B = \frac{5 - 0,7}{0,01} = 4300 \Omega$$

klepp diode
när transistoren tar off:
→ magnetiskt fält ökar
spänningen

att bli säkert
Transistor kan
Load

kapacitans
tar bort spets
spike bort
/ dämpa



$$\frac{1}{R'} = \frac{1}{R_1} + \frac{1}{R_2} = \frac{R_1 R_2}{R_1 + R_2}$$

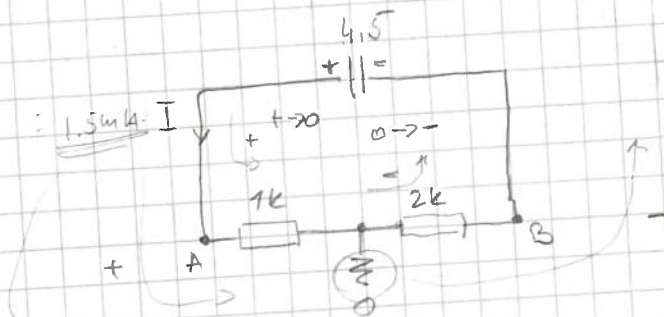
$$U = I_1 \cdot R_1 = I \cdot R' = I \cdot \frac{R_1 R_2}{R_1 + R_2}$$

Division mit R_1

$$I_1 = \frac{U}{R_1} = \frac{I \cdot \frac{R_1 R_2}{R_1 + R_2}}{R_1} = \frac{R_2}{R_1 + R_2} I$$

Division mit R_2

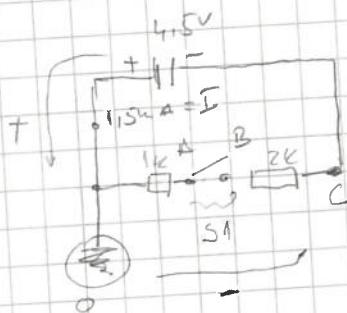
$$I_2 = \frac{U}{R_2} = \frac{I \cdot \frac{R_1 R_2}{R_1 + R_2}}{R_2} = \frac{R_1}{R_1 + R_2} I$$



$$I = \frac{U}{R_1 + R_2} = \frac{4.5}{3k} = 1.5 \mu A$$

$$U_A = I \cdot R = 1k \cdot 1.5 \mu A = 1.5V$$

$$U_B = -I \cdot R = 2k \cdot 1.5 \mu A = -3V$$



$S_1 = \text{Öffnen}$

$A = 0$

$B = 4.5V$

$S_2 = \text{Schließen}$

$A = -1.5V$

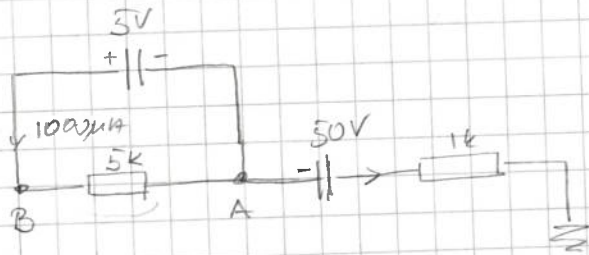
$B = -1.5V$

$$I = \frac{U}{R_1 + R_2} = \frac{4.5}{3k} = 1.5 \mu A$$

$$U_A = -I \cdot R = -1.5 \mu A \cdot 1k = -1.5V$$

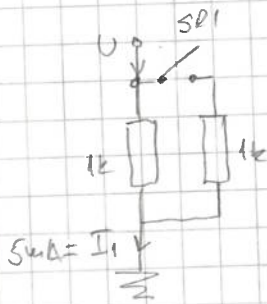
$$U_A = U_B$$

$$U_C = -I \cdot R = -1.5 \mu A \cdot 2k = 3V$$



$$U_A = -50V$$

$$U_B = I \cdot R - U_A = 1\mu A \cdot 5k - 50V = 5 - 50V = -45V$$



$$U = \frac{I}{R} = \frac{5\mu A}{1k} = \frac{5\mu A}{1k} - 5V$$

När SP1 är stängd:

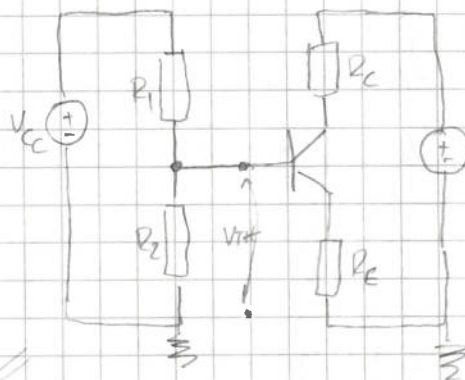
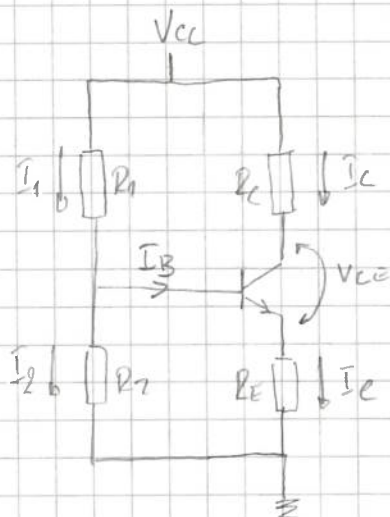
$$R_1 // R_2 = \frac{R_1 R_2}{R_1 + R_2} = \frac{1 \cdot 1}{1 + 1} = 0,5 k\Omega = 500 \Omega$$

$$\frac{1}{R} = \frac{R_1 + R_2}{R_1 R_2} \Rightarrow R = \frac{R_1 R_2}{R_1 + R_2}$$

$$I = \frac{U}{R} = \frac{5V}{500} = 10\mu A$$

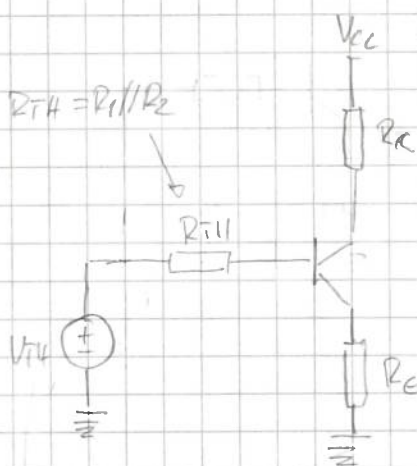
parallell resistor koplijs \rightarrow minskat resistor \Rightarrow öka ström
 \rightarrow öka resistor \Rightarrow minskat ström
 serie resistor koplijs

Voltage Divider Bias Circuit I



$$V_{TH} = V_{CC} \frac{R_2}{R_1 + R_2}$$

$$R_{TH} = R_1 // R_2$$



$$V_{TH} = \frac{R_2}{R_1 + R_2} V_{CC}$$

$$\begin{aligned} * V_{TH} - I_B R_{TH} - V_{BE} - I_E R_E &= 0 \\ \Rightarrow V_{TH} - I_B R_{TH} - V_{BE} - (\beta + 1) I_B R_E &= 0 \\ I_B &= \frac{V_{TH} - V_{BE}}{R_{TH} + (\beta + 1) R_E} \end{aligned}$$

$$I_C = \beta I_B$$

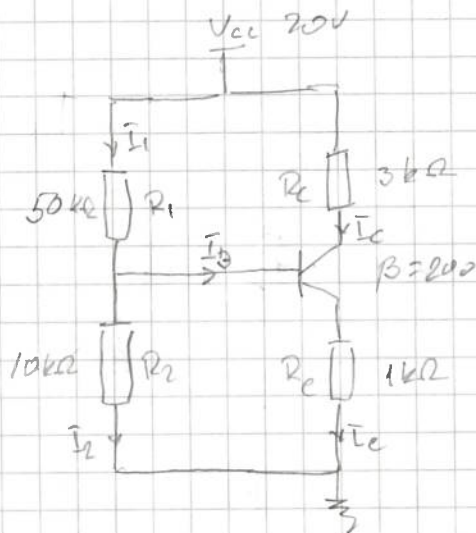
$$I_E = (\beta + 1) I_B$$

$$* V_{CC} - I_C R_C - V_{CE} - I_E R_E = 0$$

$$V_{CE} = V_{CC} - I_C (R_C + R_E)$$

$I_C = I_E$ ej exakt korrekt
pga I_E är lite
större än I_C
(approximation)

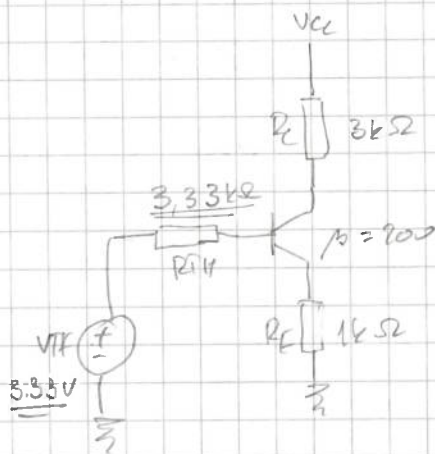
Voltage Divider Bias Circuit II



$$V_{TH} = \frac{R_2}{R_1 + R_2} V_{CC} = \frac{10k}{10k + 50k} \cdot 20V$$

$$V_{TH} = 3.33V$$

$$R_{TH} = 10k // 50k = \frac{10k \cdot 50k}{10k + 50k} = 8.33k$$



$$I_B = \frac{V_{TH} - V_{BE}}{R_{TH} + (\beta + 1)R_E} = \frac{3.33V - 0.7V}{8.33k\Omega + 201 \cdot 1000\Omega}$$

$$I_B = 12.56 \mu A$$

$$I_C = \beta \cdot I_B = 200 \cdot 12.56 \mu A = 2.513 \text{ mA}$$

$$V_{CE} = V_{CC} - I_C(R_C + R_E) = 9.948V$$

$$Q_{\text{point}} : I_C = 2.513 \text{ mA}$$

$$V_{CE} = 9.948V$$

$$\text{if } \beta = 100 \Rightarrow I_C = 2.405 \text{ mA}$$

$$V_{CE} = 10.38V$$

$$\text{if } \beta = 300 \Rightarrow I_C = 2.551 \text{ mA}$$

$$V_{CE} = 9.796V$$

Method :

$$\text{if } R_2 \leq \frac{1}{10} \beta R_E$$

$$V_B = \frac{R_2}{R_1 + R_2} V_{CC}$$

$$V_E = V_B - 0.7$$

$$I_E = \frac{V_E}{R_E} = I_C$$

$$V_{CC} - I_C R_C - V_{CE} - I_E R_E = 0$$

$$V_{CE} = V_{CC} - I_C(R_C + R_E)$$

Ex:

$$R_2 \leq \frac{1}{10} \beta R_E$$

$$10k\Omega \leq 20k\Omega$$

\Rightarrow we can use

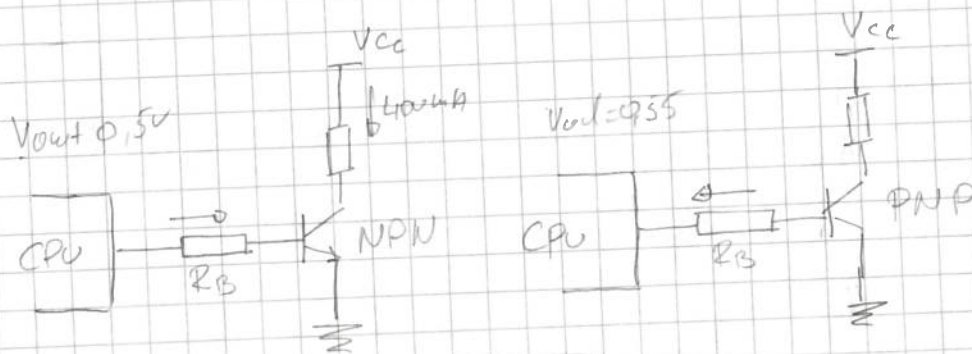
new Method.

$$V_B = 3.33V$$

$$V_E = 2.63V$$

$$I_E = 2.63 \mu A = I_C$$

BJT - Switch Circuit



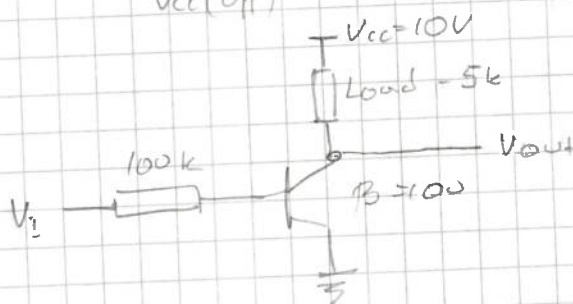
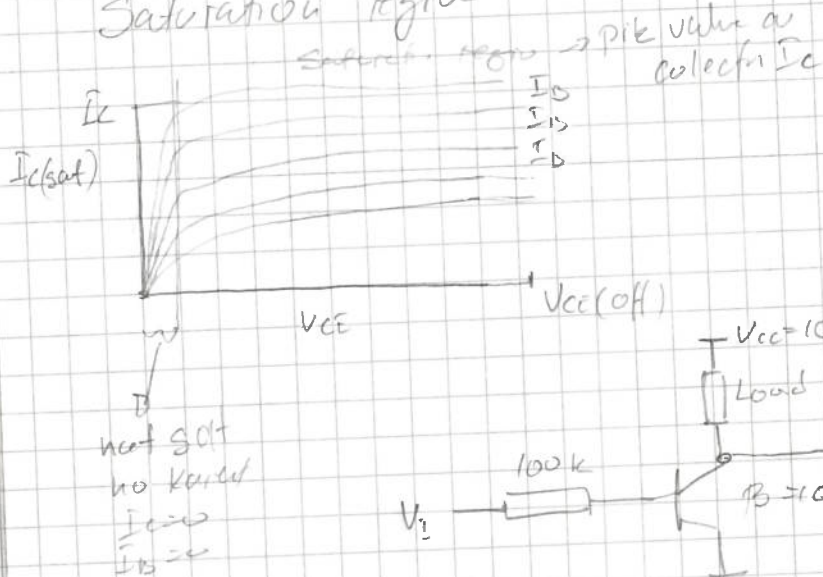
if $V_{out} = 0V$
 $I_B = 0A$
 $I_C = 0A$

if $V_{out} = 5V$
 $I_B > 0A$
 $I_C >> 0A$

if $V_{out} = 0V$
 $I_B > 0A$
 $I_C >> 0A$

if $V_{out} = 5V$
 $I_B = 0A$
 $I_C = 0A$

Saturation region

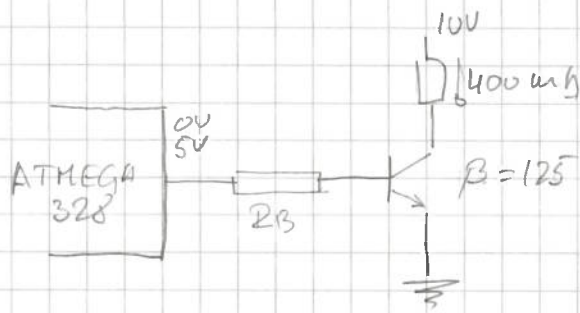


For $V_I = 0V$
 $I_B = 0V$
 $I_C = 0V$
 $V_{out} = 10V$

For $V_I = 10V$
 $I_B = \frac{10V - 0.7V}{100k} = 93 \mu A$

$I_C = \frac{10V - 0}{5k} = 2mA$

In saturation mode: $I_B > \frac{I_C}{\beta} \Rightarrow 93 \mu A > \frac{2mA}{100}$



$$I_B \gg \frac{I_C}{\beta}$$

$$I_B \gg \frac{400\mu A}{125}$$

$$I_B \gg 3.2\mu A$$

$$\text{Välj: } I_B = 5 \cdot 3.2\mu A = 16\mu A$$

$$I_B = 16\mu A = \frac{5V - 0.7V}{R_B}$$

$$R_B = \frac{4.3V}{16\mu A} = 268.75\Omega$$

Välj mindre \nearrow pga I_B