

# ECEN 611 Homework 4: Gap Function and Mutual Inductance for Salient Pole Rotor

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## Problem 3

**Problem 3)** Assume the steady state currents flowing in the conductors (consider sinusoidal winding distribution) of the device shown below are:

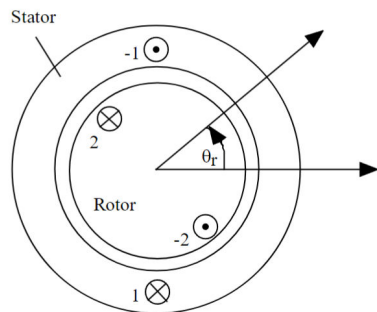
$$i_1 = I_{s1} \cos \omega_1 t \quad , \quad i_2 = I_{s2} \cos(\omega_2 t + \phi_2)$$

Assume also that during steady state operation the rotor speed is constant thus:

$$\theta_r = \omega_r t + \theta_r(0)$$

where  $\theta_r(0)$  is the rotor displacement at time zero. Determine the rotor speeds at which the device produces a nonzero average torque during steady state operation if

- (a)  $\omega_1 = \omega_2 = 0$ ;      (b)  $\omega_1 = \omega_2 \neq 0$ ;      (c)  $\omega_1 \neq 0, \omega_2 = 0$ .



```
syms I positive real
syms N_s

syms phi
syms theta_r
```

```

assume( 0 <= theta_r <= 2*pi )

NS = 1;

T = 2*pi;

digits(4)

```

## Stator Counting & Winding Function

```

statorCountingFunction(phi) = piecewise( ...
    0 <= phi < pi/2, 0, ...
    pi/2 <= phi < 3/2*pi, -N_s, ...
    3/2*pi <= phi < T, 0 ...
);

disp("Original Stator Counting Function  $\phi \in [0 T]$  :")

```

Original Stator Counting Function  $\phi \in [0 T]$  :

```
disp(statorCountingFunction(phi))
```

$$\begin{cases} 0 & \text{if } \phi \in \left[0, \frac{\pi}{2}\right) \\ -N_s & \text{if } \phi \in \left[\frac{\pi}{2}, \frac{3\pi}{2}\right) \\ 0 & \text{if } \phi \in \left[\frac{3\pi}{2}, 2\pi\right) \end{cases}$$

```

statorCountingFunction_ext(phi) = piecewise( ...
    -2*T <= phi < -T, statorCountingFunction(phi+2*T), ...
    -T <= phi < 0, statorCountingFunction(phi+T), ...
    0 <= phi < T, statorCountingFunction(phi), ...
    T <= phi <= 2*T, statorCountingFunction(phi-T) ...
);

disp("Extended Stator Counting Function  $\phi \in [-2T 2T]$  :")

```

Extended Stator Counting Function  $\phi \in [-2T 2T]$  :

```
disp(statorCountingFunction_ext(phi))
```

$$\left\{ \begin{array}{ll} 0 & \text{if } \phi \in \left[-4\pi, -\frac{7\pi}{2}\right) \\ -N_s & \text{if } \phi \in \left[-\frac{7\pi}{2}, -\frac{5\pi}{2}\right) \\ 0 & \text{if } \phi \in \left[-\frac{5\pi}{2}, -\frac{3\pi}{2}\right) \\ -N_s & \text{if } \phi \in \left[-\frac{3\pi}{2}, -\frac{\pi}{2}\right) \\ 0 & \text{if } \phi \in \left[-\frac{\pi}{2}, \frac{\pi}{2}\right) \\ -N_s & \text{if } \phi \in \left[\frac{\pi}{2}, \frac{3\pi}{2}\right) \\ 0 & \text{if } \phi \in \left[\frac{3\pi}{2}, \frac{5\pi}{2}\right) \\ -N_s & \text{if } \phi \in \left[\frac{5\pi}{2}, \frac{7\pi}{2}\right) \\ 0 & \text{if } \phi \in \left[\frac{7\pi}{2}, 4\pi\right) \end{array} \right.$$

```
statorCountingFunction_ext_avg = 1/T * int(statorCountingFunction_ext, phi, [0 T]);
statorWindingFunction_ext(phi) = statorCountingFunction_ext -
statorCountingFunction_ext_avg
```

```
statorWindingFunction_ext(phi) =
```

$$\left\{ \begin{array}{ll} \frac{5734161139222659 \pi N_s}{36028797018963968} & \text{if } \phi \in \left[-4\pi, -\frac{7\pi}{2}\right) \\ \frac{5734161139222659 \pi N_s}{36028797018963968} - N_s & \text{if } \phi \in \left[-\frac{7\pi}{2}, -\frac{5\pi}{2}\right) \\ \frac{5734161139222659 \pi N_s}{36028797018963968} & \text{if } \phi \in \left[-\frac{5\pi}{2}, -\frac{3\pi}{2}\right) \\ \frac{5734161139222659 \pi N_s}{36028797018963968} - N_s & \text{if } \phi \in \left[-\frac{3\pi}{2}, -\frac{\pi}{2}\right) \\ \frac{5734161139222659 \pi N_s}{36028797018963968} & \text{if } \phi \in \left[-\frac{\pi}{2}, \frac{\pi}{2}\right) \\ \frac{5734161139222659 \pi N_s}{36028797018963968} - N_s & \text{if } \phi \in \left[\frac{\pi}{2}, \frac{3\pi}{2}\right) \\ \frac{5734161139222659 \pi N_s}{36028797018963968} & \text{if } \phi \in \left[\frac{3\pi}{2}, \frac{5\pi}{2}\right) \\ \frac{5734161139222659 \pi N_s}{36028797018963968} - N_s & \text{if } \phi \in \left[\frac{5\pi}{2}, \frac{7\pi}{2}\right) \\ \frac{5734161139222659 \pi N_s}{36028797018963968} & \text{if } \phi \in \left[\frac{7\pi}{2}, 4\pi\right) \end{array} \right.$$

```
figure
```

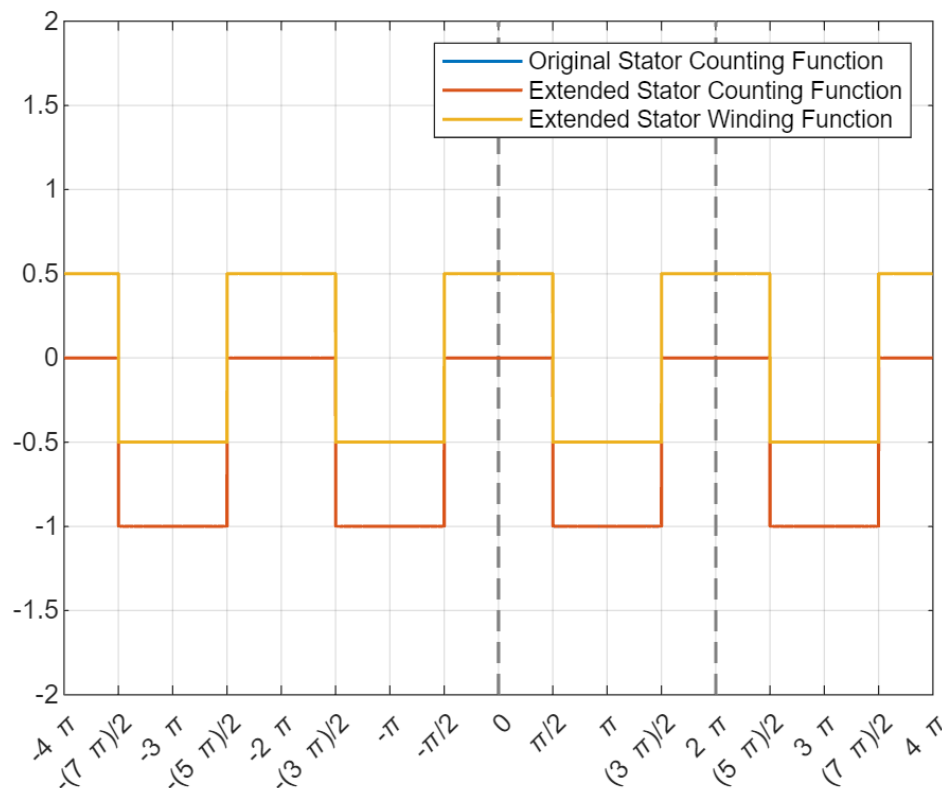
```
fplot(subs(statorCountingFunction(phi), N_s, NS), [-2*T 2*T], ...
      "DisplayName", "Original Stator Counting Function", ...
```

```

"LineWidth", 1.2)
hold on
fplot(subs(statorCountingFunction_ext(phi), N_s, NS), [-2*T 2*T], ...
      "DisplayName", "Extended Stator Counting Function", ...
      "LineWidth", 1.2)
fplot(subs(statorWindingFunction_ext(phi), N_s, NS), [-2*T 2*T], ...
      "DisplayName", "Extended Stator Winding Function", ...
      "LineWidth", 1.2)
hold off
ylim([-2 2])
grid on
legend

ax = gca;
S = sym(ax.XLim(1):pi/2:ax.XLim(2));
ax.XTick = double(S);
ax.XTickLabel = arrayfun(@texlabel,S,'UniformOutput',false);

```



## Rotor Counting & Winding Function

```

syms N_r
NR = 1;

turnsRotorNum = [0 1 -1 0] * N_r; % number of turns at each location:
replace Nt with 1 for simplicity
turnsRotorPhi = [0 T/4 T/2 T/4]; % angle of each location

```

```
turnsRotorNumLevel = cumsum(turnsRotorNum)
```

```
turnsRotorNumLevel = (0 Nr 0 0)
```

```
rotor_winding_turning_phi = theta_r + cumsum(turnsRotorPhi)
```

```
rotor_winding_turning_phi =
```

$$\left( \theta_r \quad \theta_r + \frac{\pi}{2} \quad \theta_r + \frac{3\pi}{2} \quad \theta_r + 2\pi \right)$$

```
rotorCountingFunction(phi) = turnsRotorNumLevel(1);
```

```
phiReference = 0;
```

```
for k = 1:length(rotor_winding_turning_phi)-1
```

```
    thisPhi = rotor_winding_turning_phi(k);
```

```
    nextPhi = rotor_winding_turning_phi(k+1);
```

```
    rotorCountingFunction(phi) = piecewise(thisPhi <= phi < nextPhi,  
turnsRotorNumLevel(k), ...
```

```
                                phiReference <= phi < thisPhi,
```

```
rotorCountingFunction);
```

```
end
```

### Original Rotor Counting Function $\phi \in [\theta_r \theta_r + T]$

```
disp("Original Rotor Counting Function: ");
```

```
Original Rotor Counting Function:
```

```
disp(rotorCountingFunction(phi));
```

$$\begin{cases} 0 & \text{if } 2\theta_r + 3\pi \leq 2\phi \wedge \phi < \theta_r + 2\pi \\ N_r & \text{if } 2\phi < 2\theta_r + 3\pi \wedge 2\theta_r + \pi \leq 2\phi \\ 0 & \text{if } 2\phi < 2\theta_r + \pi \wedge 0 \leq \phi \wedge (\phi < \theta_r \vee (\theta_r \leq \phi \wedge 2\phi < 2\theta_r + \pi)) \end{cases}$$

### Extended Rotor Counting Function $\phi \in [\theta_r - 2T \theta_r + 2T]$

```
rotorCountingFunction_ext(phi) = piecewise( ...  
    theta_r - 2*T <= phi < theta_r - T, rotorCountingFunction(phi+2*T), ...  
    theta_r - T <= phi < theta_r,      rotorCountingFunction(phi+T), ...  
    theta_r <= phi < theta_r + T,      rotorCountingFunction(phi), ...  
    theta_r + T <= phi < theta_r + 2*T, rotorCountingFunction(phi-T) ...  
)
```

```
rotorCountingFunction_ext(phi) =
```

$$\left\{ \begin{array}{ll} 0 & \text{if } 2\theta_r \leq 2\phi + 5\pi \wedge \phi + 2\pi < \theta_r \\ N_r & \text{if } 2\phi + 5\pi < 2\theta_r \wedge 2\theta_r \leq 2\phi + 7\pi \wedge \phi \in \mathbb{R} \\ 0 & \text{if } (\phi < \theta_r \wedge 2\theta_r \leq 2\phi + \pi) \vee (2\phi + 7\pi < 2\theta_r \wedge \theta_r \leq \phi + 4\pi \wedge \phi \in \mathbb{R} \wedge (\phi + 4\pi < \theta_r \vee (2\phi + \\ N_r & \text{if } 2\theta_r \leq 2\phi + 3\pi \wedge \phi \in \mathbb{R} \wedge 2\phi + \pi < 2\theta_r \\ 0 & \text{if } (2\theta_r + 3\pi \leq 2\phi \wedge \phi < \theta_r + 2\pi) \vee (2\phi + 3\pi < 2\theta_r \wedge \theta_r \leq \phi + 2\pi \wedge \phi \in \mathbb{R} \wedge (\phi + 2\pi < \theta_r \vee \\ N_r & \text{if } 2\phi < 2\theta_r + 3\pi \wedge \phi \in \mathbb{R} \wedge 2\theta_r + \pi \leq 2\phi \\ 0 & \text{if } (2\theta_r + 7\pi \leq 2\phi \wedge \phi < \theta_r + 4\pi) \vee (\theta_r \leq \phi \wedge 2\phi < 2\theta_r + \pi \wedge (\phi < \theta_r \vee (\theta_r \leq \phi \wedge 2\phi < 2\theta_r + \\ N_r & \text{if } 2\phi < 2\theta_r + 7\pi \wedge 2\theta_r + 5\pi \leq 2\phi \wedge \phi \in \mathbb{R} \\ 0 & \text{if } 2\phi < 2\theta_r + 5\pi \wedge \theta_r + 2\pi \leq \phi \wedge \phi \in \mathbb{R} \wedge (\phi < \theta_r + 2\pi \vee (2\phi < 2\theta_r + 5\pi \wedge \theta_r + 2\pi \leq \phi)) \end{array} \right.$$

### Extended Rotor Winding Function $\varphi \in [\theta_r - 2T \ \theta_r + 2T]$

```
% assume( theta < T )
rotorCountingFunction_ext_avg = 1/T * int(rotorCountingFunction_ext, phi, [0 T]);
rotorWindingFunction_ext = rotorCountingFunction_ext - rotorCountingFunction_ext_avg

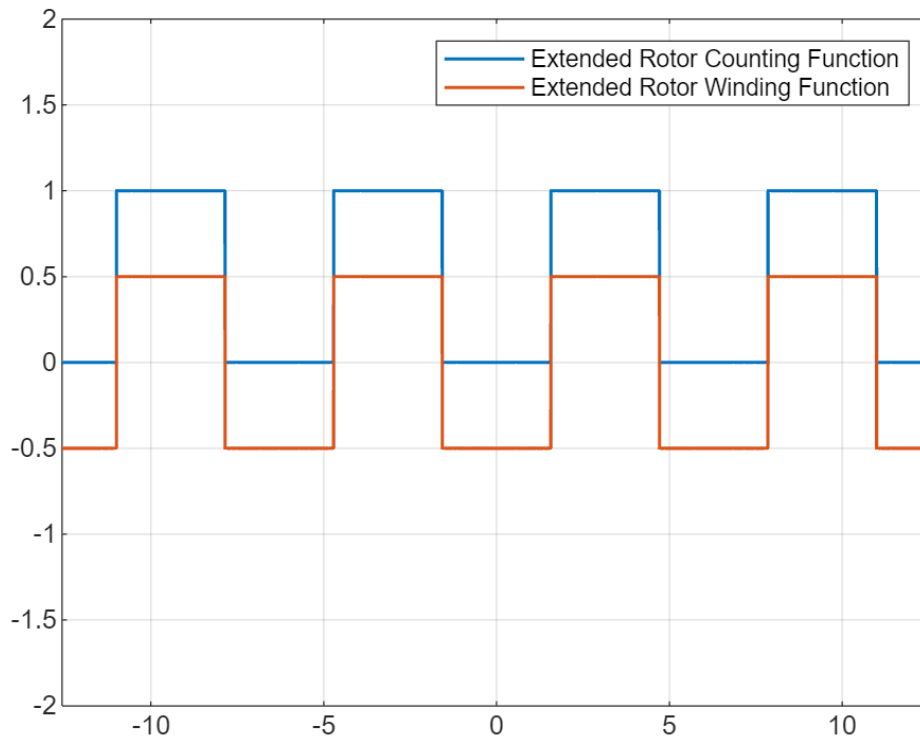
rotorWindingFunction_ext(phi) =
```

$$\left\{ \begin{array}{ll}
\frac{5734161139222659 N_r \left( \theta_r - \frac{3\pi}{2} \right)}{36028797018963968} - \frac{5734161139222659 N_r \left( \theta_r - \frac{\pi}{2} \right)}{36028797018963968} & \text{if } 2\theta_r \leq 2\phi + 5\pi \wedge \theta_r \in \\
- \frac{5734161139222659 \pi N_r}{36028797018963968} & \text{if } 2\theta_r \leq 2\phi + 5\pi \wedge \left( \theta_r, \right. \\
N_r - \frac{5734161139222659 N_r \left( \theta_r - \frac{\pi}{2} \right)}{36028797018963968} + \frac{5734161139222659 N_r \left( \theta_r - \frac{3\pi}{2} \right)}{36028797018963968} & \text{if } 2\phi + 5\pi < 2\theta_r \wedge 2\theta_r, \\
N_r - \frac{5734161139222659 \pi N_r}{36028797018963968} & \text{if } 2\phi + 5\pi < 2\theta_r \wedge 2\theta_r, \\
\frac{5734161139222659 N_r \left( \theta_r - \frac{3\pi}{2} \right)}{36028797018963968} - \frac{5734161139222659 N_r \left( \theta_r - \frac{\pi}{2} \right)}{36028797018963968} & \text{if } \theta_r \in \left( \frac{\pi}{2}, \frac{3\pi}{2} \right) \wedge ((\phi < \\
- \frac{5734161139222659 \pi N_r}{36028797018963968} & \text{if } \left( \theta_r \in \left[ \frac{3\pi}{2}, 2\pi \right] \vee \theta_r : \right. \\
N_r - \frac{5734161139222659 N_r \left( \theta_r - \frac{\pi}{2} \right)}{36028797018963968} + \frac{5734161139222659 N_r \left( \theta_r - \frac{3\pi}{2} \right)}{36028797018963968} & \text{if } 2\theta_r \leq 2\phi + 3\pi \wedge \theta_r \in \\
N_r - \frac{5734161139222659 \pi N_r}{36028797018963968} & \text{if } 2\theta_r \leq 2\phi + 3\pi \wedge \left( \theta_r, \right. \\
\frac{5734161139222659 N_r \left( \theta_r - \frac{3\pi}{2} \right)}{36028797018963968} - \frac{5734161139222659 N_r \left( \theta_r - \frac{\pi}{2} \right)}{36028797018963968} & \text{if } \theta_r \in \left( \frac{\pi}{2}, \frac{3\pi}{2} \right) \wedge ((2\theta_r \\
- \frac{5734161139222659 \pi N_r}{36028797018963968} & \text{if } \left( \theta_r \in \left[ \frac{3\pi}{2}, 2\pi \right] \vee \theta_r : \right. \\
N_r - \frac{5734161139222659 N_r \left( \theta_r - \frac{\pi}{2} \right)}{36028797018963968} + \frac{5734161139222659 N_r \left( \theta_r - \frac{3\pi}{2} \right)}{36028797018963968} & \text{if } 2\phi < 2\theta_r + 3\pi \wedge \theta_r \in \\
N_r - \frac{5734161139222659 \pi N_r}{36028797018963968} & \text{if } 2\phi < 2\theta_r + 3\pi \wedge \left( \theta_r, \right. \\
\frac{5734161139222659 N_r \left( \theta_r - \frac{3\pi}{2} \right)}{36028797018963968} - \frac{5734161139222659 N_r \left( \theta_r - \frac{\pi}{2} \right)}{36028797018963968} & \text{if } \theta_r \in \left( \frac{\pi}{2}, \frac{3\pi}{2} \right) \wedge ((2\theta_r \\
- \frac{5734161139222659 \pi N_r}{36028797018963968} & \text{if } \left( \theta_r \in \left[ \frac{3\pi}{2}, 2\pi \right] \vee \theta_r : \right. \\
N_r - \frac{5734161139222659 N_r \left( \theta_r - \frac{\pi}{2} \right)}{36028797018963968} + \frac{5734161139222659 N_r \left( \theta_r - \frac{3\pi}{2} \right)}{36028797018963968} & \text{if } 2\phi < 2\theta_r + 7\pi \wedge 2\theta_r, \\
N_r - \frac{5734161139222659 \pi N_r}{36028797018963968} & \text{if } 2\phi < 2\theta_r + 7\pi \wedge 2\theta_r, \\
\frac{5734161139222659 N_r \left( \theta_r - \frac{3\pi}{2} \right)}{36028797018963968} - \frac{5734161139222659 N_r \left( \theta_r - \frac{\pi}{2} \right)}{36028797018963968} & \text{if } 2\phi < 2\theta_r + 5\pi \wedge \theta_r \in \\
- \frac{5734161139222659 \pi N_r}{36028797018963968} & \text{if } 2\phi < 2\theta_r + 5\pi \wedge \left( \theta_r, \right.
\end{array} \right.$$

```

figure
fplot(subs(rotorCountingFunction_ext(phi),[theta_r N_r], [0 NR]), [-2*T 2*T], ...
      "DisplayName", "Extended Rotor Counting Function", ...
      "LineWidth", 1.2)
hold on
fplot(subs(rotorWindingFunction_ext(phi),[theta_r N_r], [0 NR]), [-2*T 2*T], ...
      "DisplayName", "Extended Rotor Winding Function", ...
      "LineWidth", 1.2)
hold off
ylim([-2 2])
grid on
legend

```



## Stator Winding Magnetizing Inductance

```

syms mu_o r l g
Lss = mu_o*r*l/g * int( statorWindingFunction_ext * statorWindingFunction_ext, ...
                        phi, [0 T]);

```

```

Lss_simplified = subs( simplify( vpa(Lss) ) )

```

```

Lss_simplified =

```

$$\frac{1.571 N_s^2 l \mu_o r}{g}$$

```

% Lss_simplified = subs( simplify( vpa(Lss) ), N_s^2*l*mu_o*r/g, 1 )

```



## Rotor Winding Magnetizing Inductance

```
syms mu_o r l g
```

```
Lrr_integrand = subs(rotorWindingFunction_ext * rotorWindingFunction_ext, theta_r,  
0:T/8:T);
```

```
tic
```

```
Lrr = vpa( simplify( mu_o*r*l/g * int( Lrr_integrand, phi, [0 T] ) ) )
```

```
Lrr =
```

$$\left( \frac{1.571 N_r^2 l \mu_o r}{g} \frac{1.571 N_r^2 l \mu_o r}{g} \frac{1.571 N_r^2 l \mu_o r}{g} \frac{1.571 N_r^2 l \mu_o r}{g} \frac{1.571 N_r^2 l \mu_o r}{g} \frac{1.571 N_r^2 l \mu_o r}{g} \frac{1.5}{g} \right)$$

```
toc
```

Elapsed time is 1.354199 seconds.

```
Lrr = Lrr(1)
```

```
Lrr =
```

$$\frac{1.571 N_r^2 l \mu_o r}{g}$$

Rotor Winding Magnetizing Inductance is independent of rotor angle.

## Stator-Rotor Winding Mutual Inductance

$$L_{BA} = \frac{\mu_0 r l}{g} \int_0^{2\pi} N_B(\phi) N_A(\phi) d\phi \quad (1.75)$$

```
Lsr_integrand = simplify( vpa( rotorWindingFunction_ext *  
statorWindingFunction_ext ) )
```

```
Lsr_integrand(phi) =
```

[illegible]

```
% Lsr_integrand = vpa( rotorWindingFunction_ext * statorWindingFunction_ext )
```

```
tic
Lsr = mu_o*r*l/g * int(Lsr_integrand, phi, [0 T]);
toc
```

Elapsed time is 22.924358 seconds.

```
Lsr_simplified = subs( simplify( vpa(Lsr) ), N_r*N_s*l*mu_o*r/g, 1 )
```

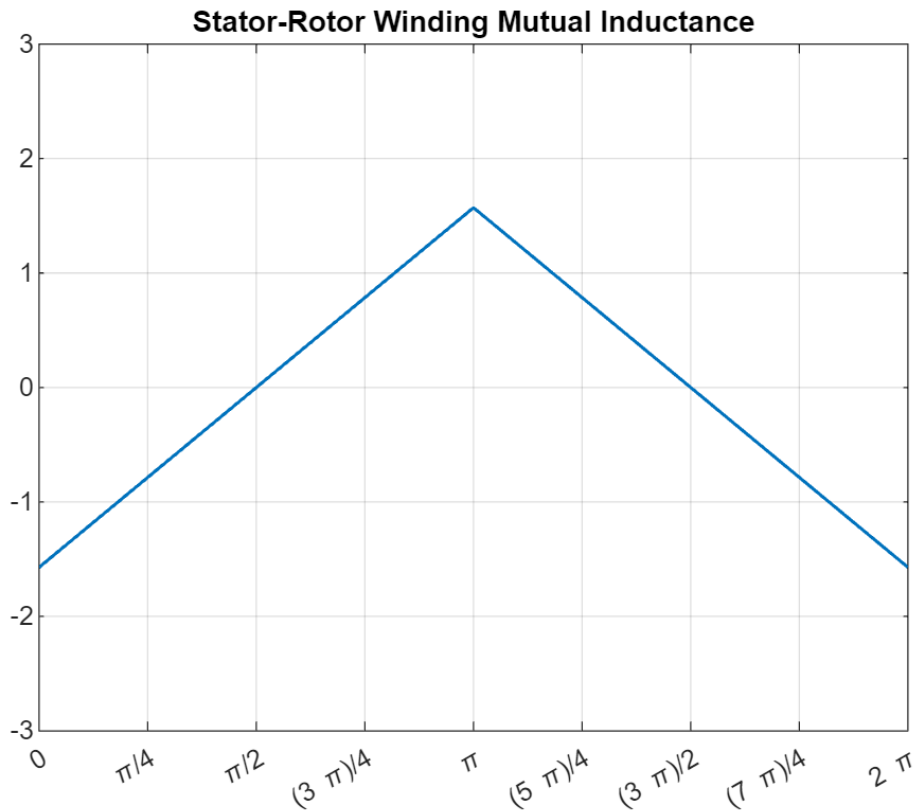
```
Lsr_simplified =
```

$$\begin{cases} -1.571 & \text{if } \theta_r = 0 \\ -9.183e-7 & \text{if } \theta_r = 4.712 \\ -3.673e-6 & \text{if } \theta_r = 4.712 \\ 1.571 & \text{if } \theta_r = 3.142 \\ 1.571 & \text{if } \theta_r = 3.142 \\ 2.356 - 0.5 \theta_r & \text{if } \theta_r \in (4.712, 4.712] \\ 0.75 \theta_r - 1.178 & \text{if } \theta_r \in [1.571, 1.571] \\ 1.571 & \text{if } \theta_r \in (3.142, 3.142) \\ 4.712 - 1.0 \theta_r & \text{if } 4.712 < \theta_r \vee \theta_r \in (3.142, 4.712) \\ 1.0 \theta_r - 1.571 & \text{if } \theta_r \in (0.0, 1.571) \vee \theta_r \in (1.571, 3.142) \end{cases}$$

figure

```
fplot(Lsr_simplified, [0 T], ...
      "LineWidth", 1.2)
ylim([-3 3])
grid on
title("Stator-Rotor Winding Mutual Inductance")

ax = gca;
S = sym(ax.XLim(1):pi/4:ax.XLim(2));
ax.XTick = double(S);
ax.XTickLabel = arrayfun(@texlabel,S, 'UniformOutput', false);
```



```
% Fourier Series of Lsr
digits(4)
```

```
a0 = vpa( (1/T) * int( Lsr_simplified, theta_r, [0 T], ...
    'IgnoreSpecialCases', true) )
```

```
a0 = 6.047e-5
```

```
syms n
```

```
an = (2/T) * int( Lsr_simplified * cos(n * theta_r), theta_r, [0 T]);
bn = (2/T) * int( Lsr_simplified * sin(n * theta_r), theta_r, [0 T]);
```

```
orderOfHarmonics = 1:13;
an_13 = vpa( simplify( subs(an, n, orderOfHarmonics) ) );
bn_13 = vpa( simplify( subs(bn, n, orderOfHarmonics) ) );
```

```
tolerance = 1e-4;
```

```
an_13(abs(an_13) < tolerance) = 0
```

```
an_13 = (-1.273 0 -0.1415 0 -0.05093 0 -0.02599 0 -0.01572 0 -0.01052 0 -0.007533)
```

```
bn_13(abs(bn_13) < tolerance) = 0
```

```
bn_13 = (0 0 0 0 0 0 0 0 0 0 0 0 0)
```

```
Lsr_fourier_filtered = a0 + ...
    sum(an_13 .* cos(orderOfHarmonics .* theta_r) + ...
        bn_13 .* sin(orderOfHarmonics .* theta_r))
```

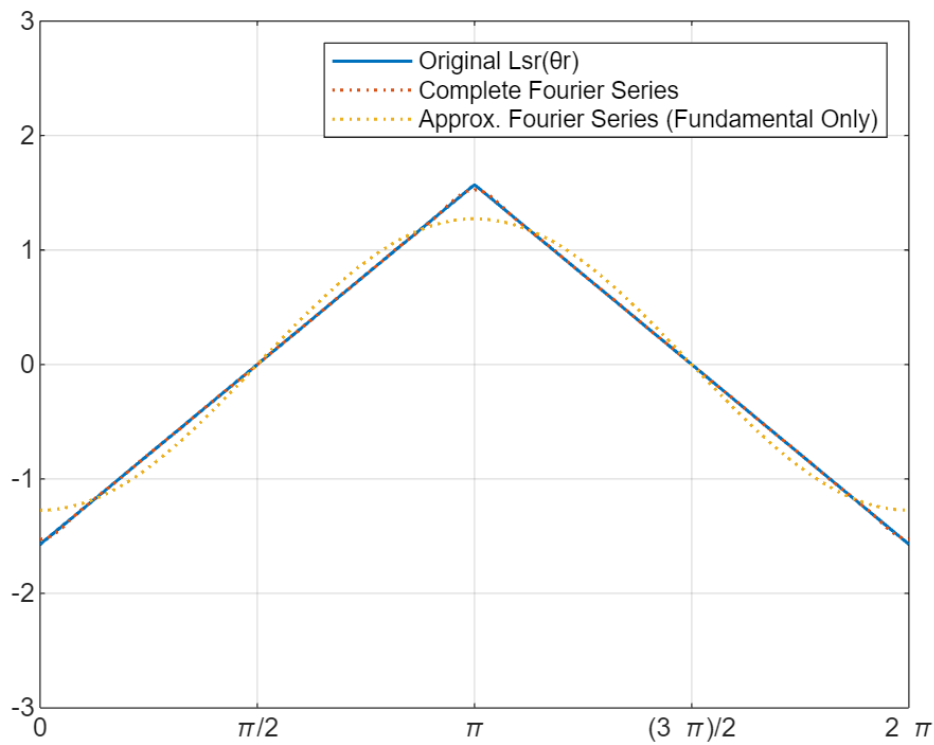
```
Lsr_fourier_filtered =
6.047e-5 - 0.05093 cos(5 θr) - 0.02599 cos(7 θr) - 0.01572 cos(9 θr) - 0.01052 cos(11 θr) - 0.007533 cos
```

```
Lsr_fourier_approx = an_13(1) * cos(orderOfHarmonics(1) * theta_r)
```

```
Lsr_fourier_approx = -1.273 cos(θr)
```

```
figure
fplot(Lsr_simplified, [0 T], ...
    "DisplayName", "Original Lsr(θr)", ...
    "LineWidth", 1.2)
hold on
fplot(Lsr_fourier_filtered, [0 T], ...
    "DisplayName", "Complete Fourier Series", ...
    "LineStyle", ":", ...
    "LineWidth", 1.2 ...
)
fplot(Lsr_fourier_approx, [0 T], ...
    "DisplayName", "Approx. Fourier Series (Fundamental Only)", ...
    "LineStyle", ":", ...
    "LineWidth", 1.2 ...
)
hold off
ylim([-3 3])
grid on
legend

ax = gca;
S = sym(ax.XLim(1):pi/2:ax.XLim(2));
ax.XTick = double(S);
ax.XTickLabel = arrayfun(@texlabel,S,'UniformOutput',false);
```



## Torque Production

```
syms I_s1 omega_1 I_s2 omega_2
syms t
syms phi_2 omega_r theta_r

magnitude = [I_s1 I_s2];
omega = [omega_1 omega_2];
angle = [ omega_1*t omega_2*t + phi_2 ];
current = magnitude .* cos(angle);
i1 = current(1)
```

$$i1 = I_{s1} \cos(\omega_1 t)$$

$$i2 = \text{current}(2)$$

$$i2 = I_{s2} \cos(\phi_2 + \omega_2 t)$$

## Reluctance Torque

$$\text{reluctanceTorque} = 1/2 * (i1^2 \cdot \text{diff}(L_{ss}, \text{theta}_r) + i2^2 \cdot \text{diff}(L_{rr}, \text{theta}_r))$$

$$\text{reluctanceTorque} = 0.0$$

## Alignment Torque

$$\text{disp}(L_{sr\_fourier\_approx})$$

$$-1.273 \cos(\theta_r)$$

```
alignmentTorque = i1 * i2 * diff(Lsr_fourier_approx, theta_r)
```

$$\text{alignmentTorque} = 1.273 I_{s1} I_{s2} \cos(\phi_2 + \omega_2 t) \cos(\omega_1 t) \sin(\theta_r)$$

### Total Torque

```
totalTorque = simplify( reluctanceTorque + alignmentTorque )
```

$$\text{totalTorque} = 1.273 I_{s1} I_{s2} \cos(\phi_2 + \omega_2 t) \cos(\omega_1 t) \sin(\theta_r)$$

```
syms omega_r omega_r0 omega_m delta
totalTorque = subs(totalTorque, theta_r, omega_m*t + delta)
```

$$\text{totalTorque} = 1.273 I_{s1} I_{s2} \cos(\phi_2 + \omega_2 t) \sin(\delta + \omega_m t) \cos(\omega_1 t)$$

$$T = -I_{sm} I_{rm} M \cos \omega_s t \cos(\omega_r t + \alpha) \sin(\omega_m t + \delta)$$

$$T = -\frac{I_{sm} I_{rm} M}{4} \begin{bmatrix} \sin\{(\omega_m + (\omega_s + \omega_r))t + \alpha + \delta\} + \\ \sin\{(\omega_m - (\omega_s + \omega_r))t - \alpha + \delta\} + \\ \sin\{(\omega_m + (\omega_s - \omega_r))t - \alpha + \delta\} + \\ \sin\{(\omega_m - (\omega_s - \omega_r))t + \alpha + \delta\} \end{bmatrix}$$

Given the transformation above, it is clear that the average value of each term is zero unless the coefficient of  $t$  is zero.

Unfortunately, MATLAB seems incapable of performing such a transformation using Product-to-Sum Trigonometric Identities

$$\cos(A)\cos(B) = 1/2 [\cos(A+B) + \cos(A-B)]$$

$$\sin(A)\cos(B) = 1/2 [\sin(A+B) + \sin(A-B)]$$

as you can see if you uncomment the following code.

```
% expanded_totalTorque = expand(totalTorque)
% rewritten_totalTorque = rewrite(expanded_totalTorque, 'sin')
% simplified_totalTorque = simplify(rewritten_totalTorque)
% final_totalTorque = expand(simplified_totalTorque)
```

Although, MATLAB can do this the other way round:

```
syms A B
ccSum = 1/2*(cos(A+B)+cos(A-B))
```

```
ccSum =
```

$$\frac{\cos(A+B)}{2} + \frac{\cos(A-B)}{2}$$

```
ccProduct = simplify(ccSum)
```

$$\text{ccProduct} = \cos(A) \cos(B)$$

```
ssSum = 1/2*(sin(A+B)+sin(A-B))
```

```
ssSum =
```

$$\frac{\sin(A+B)}{2} + \frac{\sin(A-B)}{2}$$

```
ssProduct = simplify(ssSum)
```

$$\text{ssProduct} = \cos(B) \sin(A)$$

Well, let us realize it manually:

```
% Define the four sine terms
```

```
term1 = sin((omega_m + (omega_1 + omega_2))*t + phi_2 + delta);
```

```
term2 = sin((omega_m - (omega_1 + omega_2))*t - phi_2 + delta);
```

```
term3 = sin((omega_m + (omega_1 - omega_2))*t - phi_2 + delta);
```

```
term4 = sin((omega_m - (omega_1 - omega_2))*t + phi_2 + delta);
```

```
% Combine them with the coefficient
```

```
totalTorque_manual = (1.273 * I_s1 * I_s2 / 4) * (term1 + term2 + term3 + term4);
```

```
% Simplify and verify
```

```
simplify(vpa(totalTorque_manual))
```

$$\text{ans} = 1.273 I_{s1} I_{s2} \cos(\phi_2 + \omega_2 t) \sin(\delta + \omega_m t) \cos(\omega_1 t)$$

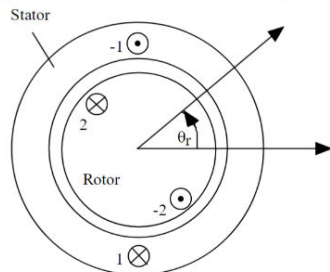
```
vpa(totalTorque)
```

$$\text{ans} = 1.273 I_{s1} I_{s2} \cos(\phi_2 + \omega_2 t) \sin(\delta + \omega_m t) \cos(\omega_1 t)$$

## Rotor Speed $\omega_r$

where  $\theta_r(0)$  is the rotor displacement at time zero. Determine the rotor speeds at which the device produces a nonzero average torque during steady state operation if

(a)  $\omega_1 = \omega_2 = 0$ ; (b)  $\omega_1 = \omega_2 \neq 0$ ; (c)  $\omega_1 \neq 0, \omega_2 = 0$ .





Determine the rotor speeds at which the device produces a nonzero average torque during steady state operation if

**(a) When  $\omega_1 = \omega_2 = 0$**

DC current supply. Single phase machine.

```
totalTorque_case_a = subs(totalTorque_manual, omega, [0 0])
```

```
totalTorque_case_a =  

$$\frac{1273 I_{s1} I_{s2} (2 \sin(\delta - \phi_2 + \omega_m t) + 2 \sin(\delta + \phi_2 + \omega_m t))}{4000}$$

```

```
totalTorque_case_a = subs(totalTorque_case_a, omega_m, 0)
```

```
totalTorque_case_a =  

$$\frac{1273 I_{s1} I_{s2} (2 \sin(\delta - \phi_2) + 2 \sin(\delta + \phi_2))}{4000}$$

```

```
% totalTorque_case_a_avg = 1/T * int( ...  
%     subs(totalTorque_case_a, omega_r*t, theta_r), ...  
%     theta_r, [0 T])
```

Only when  $\omega_m = 0$  can the device produce a nonzero average torque.

**(b) When  $\omega_1 = \omega_2 \neq 0$**

Let's assume  $\omega_1 = \omega_2 = \omega_1$

```
totalTorque_case_b = subs(totalTorque_manual, omega(2), omega_1)
```

```
totalTorque_case_b =  

$$\frac{1273 I_{s1} I_{s2} (\sin(\delta + \phi_2 + t (2 \omega_1 + \omega_m)) + \sin(\delta - \phi_2 + \omega_m t) - \sin(\phi_2 - \delta + t (2 \omega_1 - \omega_m)) + \sin(\delta + \phi_2 +$$
  
4000
```

```
% totalTorque_case_b_avg = simplify( ...  
%     expand( ...  
%         vpa( 1/T * int(totalTorque_case_b, t, [0 T/omega_m]) ) ...  
%     ) ...  
% );
```

Either

$$2 \omega_1 + \omega_m = 0 \Rightarrow \omega_m = -2\omega_1$$

and

$$\delta - \phi_2 \neq 0 \Rightarrow \delta \neq \phi_2$$

```
totalTorque_case_b_nonZero = simplify(subs(totalTorque_case_b, omega_m, 2*omega_1))
```

```
totalTorque_case_b_nonZero =
```

$$\frac{1273 I_{s1} I_{s2} (\sin(\delta - \phi_2) + \sin(\delta - \phi_2 + 2 \omega_1 t) + \sin(\delta + \phi_2 + 2 \omega_1 t) + \sin(\delta + \phi_2 + 4 \omega_1 t))}{4000}$$

or

$$\omega_m = 0 \text{ and} \\ \delta \neq 0, \phi_2 \neq 0$$

```
totalTorque_case_b_nonZero = simplify(subs(totalTorque_case_b, omega_m, 0))
```

$$\text{totalTorque\_case\_b\_nonZero} = \\ \frac{1273 I_{s1} I_{s2} \sin(\delta) (\cos(\phi_2 + 2 \omega_1 t) + \cos(\phi_2))}{2000}$$

will result in a non-zero torque.

### (c) When $\omega_1 \neq 0$ , $\omega_2 = 0$

```
totalTorque_case_c = subs(totalTorque_manual, omega(2), 0)
```

$$\text{totalTorque\_case\_c} = \\ \frac{1273 I_{s1} I_{s2} (\sin(\delta - \phi_2 + t (\omega_1 + \omega_m)) + \sin(\delta + \phi_2 - t (\omega_1 - \omega_m)) - \sin(\phi_2 - \delta + t (\omega_1 - \omega_m)) + \sin(\delta + \phi_2 + t (\omega_1 + \omega_m)))}{4000}$$

```
totalTorque_case_c_nonZero = subs(totalTorque_case_c, omega_m, [omega_1 -omega_1])
```

$$\text{totalTorque\_case\_c\_nonZero} = \\ \left( \frac{1273 I_{s1} I_{s2} (\sin(\delta - \phi_2) + \sin(\delta - \phi_2 + 2 \omega_1 t) + \sin(\delta + \phi_2) + \sin(\delta + \phi_2 + 2 \omega_1 t))}{4000} - \frac{1273 I_{s1} I_{s2} (\sin(\delta - \phi_2) + \sin(\delta + \phi_2))}{4000} \right)$$

Only when  $\omega_m = |\omega_1|$  the device can produce a non-zero torque.