

# Notes on Semi-Lagrangian Time Integration

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## 1 Related work

- First report of semi-Lagrangian formulation for weather prediction by Wiin-Nielsen [Wiin-Nielsen, 1959].
- Semi-Lagrangian formulation for barotropic atmosphere by Sawyer [Sawyer, 1963]. Formulation which is based on conserving its vorticity along the trajectories (eq. (1)) based on wind field.
- Robert studied this in combination with implicit time integration using non-divergent barotropic vorticity equation [Robert, 1981].
  - Here, he first identified that explicit time integration methods leads to 700 times smaller errors than the overall ones for the fast gravity modes, hence justifying implicit treatment of them. Similar arguments with Rossby waves lead to a 40 times smaller error for explicit treatment of the non-linear advection, hence justifying semi-Lagrangian methods.
  - A divergence diffusion and time filter were added to this model and removing them caused instabilities. This was accounted for by the *Coriolis effect not treated semi-implicitly* and the semi-Lagrangian formulation was only put on the vorticity equation.
- A new formulation, tackling the aforementioned issues was investigated for **primitive meteorological equations** by Robert [Robert, 1982].
  - **A three time level scheme** was used (departure, arrival and centered points)
  - This used a centered difference scheme for the velocity and geopotential prognostic variables, hence leading to a 2nd order accurate scheme.
- Numerical study in ECMWF’s model by Temperton [Temperton, 1995]
  - Different treatments of the Coriolis effect in three-time-level schemes were studied.
  - Method 1) **Semi-implicit treatment of Coriolis term** using two-time-level scheme (see [Cote and Staniforth, 1988]):
    - \* Simply solve linear equation including Coriolis term (see also T-REXI for linear SWE on rotating sphere).
    - \* Advantage: Also suitable for *two-time-level schemes*.
    - \* Drawback in rotated or stretched coordinate systems: Solving for implicit system of equations gets *significantly more expensive*.
    - \* This paper also proposed a **reduced Gaussian grid** transformation for the velocity fields, since no anti-aliasing is required.
  - Method 2) Consider Coriolis effect before & at the end of the trajectories as part of the velocity field (see ROCHAS, M. 1990. ARPEGE Documentation, Part 2, Ch. 6 (available from Météo-France)):
    - \* The Coriolis term is absorbed into the velocity field  $v + 2\Omega \times r$ .
    - \* Coriolis term is added at departure points and subtracted at arrival points.
    - \* Approximations of spherical geometry in determination of trajectories according to [Ritchie and Beaudoin, 1994] provided “bad” results.
    - \* Avoiding these approximations led to good results, leading this method to be the targeted standard three-time-level scheme in IFS (in 1995).
- ECMWF IFS model:
  - The three-level-time SL-SI scheme [Ritchie et al., 1995], operational from 1991 to Dec. 1996.
  - **“1997 version”: The two-level-time SL-SI scheme** [Temperton et al., 2001], operational from Dec. 1996 to 1998.
    - Issues: Noise showing up for large time step sizes => Reduction of time step size
- Hortal developed the Stable Extrapolation Two-Time-Level Scheme (SETTLS) scheme [Hortal, 2002]:
  - Tackle problem of extrapolation in a two-level-time SL-SI scheme
- Richies 1986, Semi-Lagrangian Advection on a Gaussian Grid [Ritchie, 1987].
  - Interpolating and non-interpolating SL schemes.
  - TODO: more

## 2 Sidenotes

- Gaussian grids:
  - linear Gaussian grid: No anti-aliasing
  - quadratic Gaussian Grid: Alias-free computation of quadratic terms

## 3 List of symbols

Symbol	Description
$\frac{d}{dt}$	Total derivative
$F$	PDE $F = N + L$ in total derivative formulation
$N$	Nonlinearities without nonlinear advection
$L$	Linearities
$R = R(t)$	Position
$V = V(t)$	Velocity
$\cdot_D$	Subscript $D$ for value at departure point
$\cdot_A$	Subscript $A$ for value at arrival point

## 4 SWE equation

Given the velocity-based formulation

$$\begin{aligned}\frac{\partial \Phi}{\partial t} &= -\nabla \cdot (\Phi V) \\ \frac{\partial V}{\partial t} &= -\nabla \Phi - f k \times V - V \cdot \nabla V\end{aligned}$$

and using the total material derivative

$$\frac{D}{Dt} = \frac{\partial}{\partial t} + V \cdot \nabla$$

we can write

$$\begin{aligned}\frac{D\Phi}{Dt} &= -\Phi \nabla \cdot V \\ \frac{DV}{Dt} &= -\nabla \Phi - f k \times V.\end{aligned}$$

Using a linearization around  $\Phi = \bar{\Phi} + \Phi'$ , we get

$$\begin{aligned}\frac{D\Phi'}{Dt} &= -\bar{\Phi} \nabla \cdot V - \Phi' \nabla \cdot V \\ \frac{DV}{Dt} &= -\nabla \Phi' - f k \times V\end{aligned}$$

and we can split this equation into linear and non-linear parts.

For a compact notation, let  $U = (\Phi', V)^T = (\Phi', u, v)^T$  be the vector of the vectors of variables. We can then write

$$\frac{DU}{Dt} = L_g(U) + L_f(U) + N_d(U)$$

with the gravity modes

$$L_g(U) = \begin{bmatrix} -\bar{\Phi} \nabla \cdot V \\ -\nabla \Phi' \end{bmatrix}$$

the Coriolis effect

$$L_f(U) = \begin{bmatrix} 0 \\ -f k \times V \end{bmatrix}$$

and the nonlinear divergence

$$N_d(U) = \begin{bmatrix} -\Phi' \nabla \cdot V \\ 0 \end{bmatrix}$$

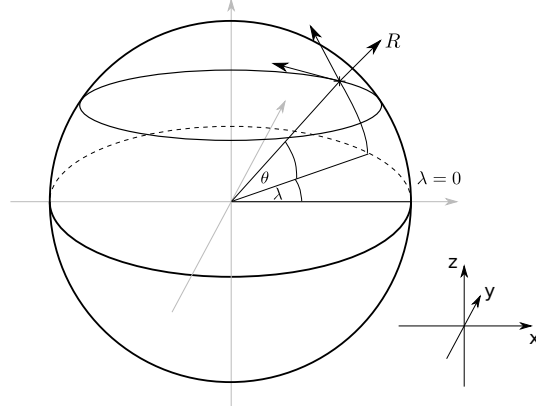


Figure 1: Gaussian and Cartesian coordinate system displaying points and velocity basis for given Gaussian angles.

## 5 Angular and Cartesian coordinate systems

In this section, we gather the equations required to get from Gaussian space to Cartesian space for points and velocities, see Fig. 1.

### 5.1 Point: Gaussian $\rightarrow$ Cartesian

Given a Gaussian coordinate  $(\lambda, \theta)$  the Cartesian coordinate  $R$  can be computed via

$$R = \begin{bmatrix} \cos \lambda \cos \theta \\ \sin \lambda \cos \theta \\ \sin \theta \end{bmatrix}.$$

### 5.2 Point: Cartesian $\rightarrow$ Gaussian

Given a Cartesian coordinate  $R$ , the Gaussian coordinate is given by

$$\lambda = \arctan(R_y/R_x) + \begin{cases} \pi & \text{if } R_x < 0 \\ 2\pi & \text{if } R_y < 0 \\ 0 & \text{else} \end{cases}$$

and

$$\theta = \arccos(-R_z) - \pi/2.$$

### 5.3 Velocity: Gaussian $\rightarrow$ Cartesian / Cartesian $\rightarrow$ Gaussian

Since there's no scaling involved, the transformation matrices for vectors (such as velocity) are the same as for point transformations.

### 5.4 Velocity basis

For a velocity given in Cartesian coordinates we first determine the basis at the particular lat/lon coordinate  $R$ . On a unit sphere, the first basis vector perpendicular to the surface is trivially given by  $B_R = R$ . The vector along the longitude is then given by

$$B_{Lon} = \begin{bmatrix} -\sin \lambda \\ \cos \lambda \\ 0 \end{bmatrix}$$

where we also see that

$$\begin{aligned} R \cdot B_{Lon} &= \begin{bmatrix} \cos \lambda \cos \theta \\ \sin \lambda \cos \theta \\ \sin \theta \end{bmatrix} \cdot \begin{bmatrix} -\sin \lambda \\ \cos \lambda \\ 0 \end{bmatrix} \\ &= -\sin \lambda \cos \lambda \cos \theta + \cos \lambda \sin \lambda \cos \theta = 0 \end{aligned}$$

and using the cross product, we get

$$\begin{aligned}
B_{Lat} &= B_{Lon} \times R \\
&= \begin{bmatrix} -\sin \lambda \\ \cos \lambda \\ 0 \end{bmatrix} \times \begin{bmatrix} \cos \lambda \cos \theta \\ \sin \lambda \cos \theta \\ \sin \theta \end{bmatrix} \\
&= \begin{bmatrix} \cos \lambda \sin \theta \\ \sin \lambda \sin \theta \\ -\sin \lambda \sin \lambda \cos \theta - \cos \lambda \cos \lambda \cos \theta \end{bmatrix} \\
&= \begin{bmatrix} \cos \lambda \sin \theta \\ \sin \lambda \sin \theta \\ -\cos \theta \end{bmatrix}
\end{aligned}$$

where we check that  $B_{Lat} \cdot B_{Lon} = 0$  and

$$\begin{aligned}
B_{Lat} \cdot R &= \begin{bmatrix} \cos \lambda \sin \theta \\ \sin \lambda \sin \theta \\ -2 \cos \theta \end{bmatrix} \cdot \begin{bmatrix} \cos \lambda \cos \theta \\ \sin \lambda \cos \theta \\ \sin \theta \end{bmatrix} \\
&= \cos^2 \lambda \sin \theta \cos \theta + \sin^2 \lambda \sin \theta \cos \theta - \cos \theta \sin \theta \\
&= (\cos^2 \lambda + \sin^2 \lambda) \sin \theta \cos \theta - \cos \theta \sin \theta \\
&= 0.
\end{aligned}$$

Using dot products, we can gain the lon/lat velocities from the Cartesian ones by computing

$$V^A(\lambda, \theta, t) = \begin{bmatrix} B_{Lon}^T \\ B_{Lat}^T \\ B_R^T \end{bmatrix} V^C(\lambda, \theta, t)$$

with  $B_R^T V^C = 0$ .

## 6 Two or three time level scheme

### 6.1 Two time level scheme (variant LVL\_two)

Following [Hortal, 2002], we write for the variables  $X$

$$\frac{dX}{dt} = L + N$$

with  $d/dt$  the total derivative,  $L$  the linearized part and  $N$  all terms treated as nonlinearities.

The 1997 version discretized this equation with an averaging as

$$\frac{X_A^{t+\Delta t} - X_D^t}{\Delta t} = \frac{1}{2} (L_A^{t+\Delta t} + L_D^t) + \frac{1}{2} (N_D^{t+\frac{\Delta t}{2}} + N_A^{t+\frac{\Delta t}{2}}).$$

Subscript  $A$  marks the arrival points which are aligned at grid cells and subscript  $D$  marks the departure points which typically require an interpolation.

### 6.2 Three time level schemes (variant LVL\_three [not implemented])

We just consider a two-time level scheme here, since the three-level scheme don't seem to be used anymore.

## 7 Semi-Lagrangian methods

For all Semi-Lagrangian methods we assume the departure point to be already known. Calculating the departure point is discussed in Section (5) since the computation of departure points is based on an implicit semi-Lagrangian way, hence on the following methods.

## 7.1 Two-level-time SL-SI scheme (variant SL\_extrapol [not implemented])

(See [Temperton et al., 2001]) Following [Hortal, 2002], we write for the variables  $X$

$$\frac{dX}{dt} = L + N$$

with  $d/dt$  the total derivative,  $L$  the linearized part and  $N$  all nonlinearly treated terms.

The 1997 version discretized this equation with an averaging as

$$\frac{X_A^{t+\Delta t} - X_D^t}{\Delta t} = \frac{1}{2} (L_A^{t+\Delta t} + L_D^t) + \frac{1}{2} (N_D^{t+\frac{\Delta t}{2}} + N_A^{t+\frac{\Delta t}{2}}). \quad (1)$$

Subscripts  $A$  mark the arrival points which are aligned at grid cells and subscripts  $D$  mark the departure points which typically require an interpolation.

Superscripts  $t + \Delta t$  mark the unknowns at the next time step and  $t + \frac{\Delta t}{2}$  mark quantities computed by linear extrapolation in time from variables at time  $t$  and  $t - \Delta t$ .

The movement along the trajectories for a position  $R$  and velocity  $V$  is given by

$$\frac{dR}{dt} = V.$$

In the 1997 version, the arrival point is approximated by

$$R_A^{t+\Delta t} \approx R_D^t + \Delta t \cdot V_M^{t+\frac{\Delta t}{2}}$$

where the departure positions  $R_D$  are to be computed. Here, also the velocities between the time steps is computed by an extrapolation. Given the departure points, Eq. (1) can be solved. However, for non-constant  $V$ , this method turned out to be unstable [Hortal, 2002, Durran, 1999].

## 7.2 SETTLS (variant SL\_SETTLS)

See [Hortal, 2002].

As a first step, the approximation of the arrival point is based on a 2nd order Taylor expansion

$$\begin{aligned} R_A^{t+\Delta t} &\approx R_D^t + \Delta t \cdot \left[ \frac{dR}{dt} \right]_D^t + \frac{(\Delta t)^2}{2} \cdot \left[ \frac{d^2 R}{dt^2} \right]_{AV} \\ &= R_D^t + \Delta t \cdot V_D^t + \frac{(\Delta t)^2}{2} \cdot \left[ \frac{dV}{dt} \right]_{AV} \end{aligned}$$

with  $AV$  some average. Based on numerical studies, the averaging was chosen to be

$$\left[ \frac{dV}{dt} \right]_{AV} \approx \left[ \frac{dV}{dt} \right]^{t-\frac{\Delta t}{2}} \approx \frac{V_A^t - V_D^{t-\Delta t}}{\Delta t}.$$

Finally, the equation reads

$$\begin{aligned} R_A^{t+\Delta t} &\approx R_D^t + \Delta t \cdot V_D^t + \frac{(\Delta t)^2}{2} \cdot \frac{V_A^t - V_D^{t-\Delta t}}{\Delta t} \\ &= R_D^t + \frac{\Delta t}{2} \cdot ([2V^t - V^{t-\Delta t}]_D + V_A^t). \end{aligned}$$

Note, that this equation solely depends on the velocity field at time  $t - \Delta t$  and at  $t$  and that is solved iteratively, similar to [Temperton et al., 2001] to determine the departure points. Based on the information in Section (8) on departure point, we can use the approximation of the departure point to evaluate quantities with  $\llbracket \cdot \rrbracket_D$ .

$$R_D^t \approx R_A^{t+\Delta t} - \frac{\Delta t}{2} \cdot \left( \left[ \underbrace{2V^t - V^{t-\Delta t}}_{\text{extrapolated velocities}} \right]_D + V_A^t \right). \quad (2)$$

Again, this is solved iteratively until the departure point has been determined. Based on this, we can use the interpolation at the departure point and the same equation to advect other state variables along the Lagrangian trajectory with the same equation.

Using the midpoint trapezoidal rule, we get

$$\frac{X_A^{t+\Delta t} - X_D^t}{\Delta t} = \frac{1}{2} (L_A^{t+\Delta t} + L_D^t) + N_*^{t+\frac{1}{2}\Delta t} \quad (3)$$

with the non-linearities at the half of the trajectory approximated by extrapolation

$$N_*^{t+\frac{1}{2}\Delta t} = \frac{1}{2} ([2N^t - N^{t-\Delta t}]_D + N^t).$$

We need to solve Eq. 3 which is accomplished by rearranging it to a Helmholtz problem

$$\begin{aligned} X_A^{t+\Delta t} &= X_D^t + \frac{1}{2}\Delta t (L_A^{t+\Delta t} + L_D^t) + \Delta t N_*^{t+\frac{1}{2}\Delta t} \\ \underbrace{X_A^{t+\Delta t} - \frac{1}{2}\Delta t L_A^{t+\Delta t}}_{\text{Helmholtz problem}} &= \underbrace{X_D^t + \frac{1}{2}\Delta t L_D^t + \Delta t N_*^{t+\frac{1}{2}\Delta t}}_{\text{K: Right hand side at departure point}}. \end{aligned}$$

The equation

$$X_A^{t+\Delta t} - \frac{1}{2}\Delta t L_A^{t+\Delta t} = K$$

can be solved with an existing backward Euler solver by considering

$$\begin{aligned} \frac{X^{t+\Delta t} - X^t}{\Delta t} &= L X^{t+\Delta t}, \\ X^{t+\Delta t} - \Delta t L X^{t+\Delta t} &= X^t \end{aligned}$$

hence we can use a half backward Euler solver for the linear parts.

### 7.3 Semi-Lagrangian EXP SETTLS (variant SL\_EXP\_SETTLS)

See [Peixoto and Schreiber, 2019]. Compute

$$\begin{aligned} U_{SLEX}^{n+1} &= e^{\Delta t L} U_D^n + \Delta t e^{\Delta t L} \tilde{N}^{n+\frac{1}{2}} \\ &= e^{\Delta t L} \left( U_D^n + \Delta t \tilde{N}^{n+\frac{1}{2}} \right) \end{aligned}$$

using

$$\tilde{N}_e^{n+\frac{1}{2}} = \frac{1}{2} \left[ 2\tilde{N}^n - e^{\Delta t L} \tilde{N}^{n-1} \right]_D + \frac{1}{2} \tilde{N}^n.$$

- 1. Step “SL”: Compute departure points used to evaluate  $[]_D$  terms.
- 2. Step “U departure”: Compute  $U_D^n$ .
- 3. Steps “nonlinear”
  - a) Compute  $\tilde{N}$  and  $\tilde{N}^{n-1}$  by evaluating non-linearities (maybe including the Coriolis term).
  - b) Compute  $\tilde{N}_D^{n+\frac{1}{2}} = \left[ 2\tilde{N}^n - e^{\Delta t L} \tilde{N}^{n-1} \right]_D$ .
  - c) Compute  $\tilde{N}_e^{n+\frac{1}{2}} = \frac{1}{2} \left( \tilde{N}_D^{n+\frac{1}{2}} + \tilde{N}^n \right)$ .
  - d)  $K = U_D^n + \Delta t \tilde{N}^{n+\frac{1}{2}}$
- 4. Step “finalize”: Compute  $U_{SLEX}^{n+1} = e^{\Delta t L} (K)$ .

## 8 Departure points

In all methods, an iterative way is used to compute departure point  $R(t - \Delta t)$  for given velocity  $V()$  and arrival point  $R(t)$ . All points are given in vector space and the origin at a sphere with radius  $a$ .

### 8.1 General iterative approach to determine the midpoint

See [Ritchie, 1987]. All approaches are based on an iterative way to approximate the midpoint. This is described in the following section. Based on the midpoint, it's easy to also get a 2nd order accurate method.

## 8.2 Ritchies 1985 version (variant DP\_ritchie [not implemented])

See [Ritchie, 1987]. Ritchie used an approximated version by first assuming the velocity vector in 3D, also tracing it back along this linearized velocity and then projecting the resulting point back to the earth's surface.

### 8.2.1 Introduction

This approach starts with a Taylor expansion and an implicit system to solve for to compute the departure point

$$R^*(t) = R(t + \Delta t) - \Delta t V(t) + O(\Delta t^2) \quad (4)$$

where  $R(t + \Delta t)$  is known and  $R(t)$  as well as  $V(t)$  need to be computed.

### 8.2.2 Computing midpoint of trajectory (via normalization)

First of all, we assume  $V(t)$  to be already available. However,  $R^*(t)$  would still be off the sphere's surface which can be fixed with a normalization

$$\begin{aligned} R(t) &= b R^*(t) \\ &= b (R(t + \Delta t) - \Delta t V(t)) \end{aligned} \quad (5)$$

and since we require  $|R^*(t)| = a$ , we get

$$\begin{aligned} l &= |R(t + \Delta t) - \Delta t V(t)| \\ &= ((R(t + \Delta t) - \Delta t V(t)) \cdot (R(t + \Delta t) - \Delta t V(t)))^{1/2} \\ &= \left( a^2 - 2\Delta t R(t + \Delta t) V(t) + \Delta t^2 V(t)^2 \right)^{1/2} \end{aligned}$$

Projecting  $R(t)$  on the sphere's surface yields

$$\begin{aligned} R(t) &= (R(t + \Delta t) - \Delta t V(t)) \cdot \frac{a}{l} \\ &= (R(t + \Delta t) - \Delta t V(t)) \cdot \left( 1 - 2\Delta t R(t + \Delta t) V(t) / a^2 + \Delta t^2 V(t)^2 / a^2 \right)^{-1/2} \\ &= (R(t + \Delta t) - \Delta t V(t)) \cdot b \end{aligned}$$

with

$$b = \left( 1 + \Delta t^2 V(t)^2 / a^2 - 2\Delta t V(t) R(t + \Delta t) / a^2 \right)^{-1/2}. \quad (6)$$

We can then use Eq. 4

$$R(t + \Delta t) = R(t) + \Delta t V(t) + O(\Delta t^2)$$

to replace  $R(t + \Delta t)$  yielding

$$\begin{aligned} b &= \left( 1 + \Delta t^2 V(t)^2 / a^2 - 2\Delta t V(t) (R(t) + \Delta t V(t) + O(\Delta t^2)) / a^2 \right)^{-1/2} \\ &= \left( 1 + \Delta t^2 V(t)^2 / a^2 - 2\Delta t V(t) R(t) / a^2 - 2\Delta t^2 V(t)^2 / a^2 - 2\Delta t O(\Delta t^2) V(t) / a^2 \right)^{-1/2} \\ &= \left( 1 - \Delta t^2 V(t)^2 / a^2 - 2\Delta t V(t) R(t) / a^2 - 2\Delta t O(\Delta t^2) V(t) / a^2 \right)^{-1/2}. \end{aligned} \quad (7)$$

Using

$$\begin{aligned} V(t) \cdot R(t) &= \sum_n V_n(t) R_n(t) \\ &= \sum_n \frac{1}{2} \frac{d}{dt} (R_n(t))^2 \\ &= \frac{1}{2} \frac{d}{dt} \sum_n (R_n(t))^2 \\ &= \frac{1}{2} \frac{d}{dt} (R(t) \cdot R(t)) \\ &= \frac{1}{2} \frac{d}{dt} \{ |R(t)|^2 \} \end{aligned}$$



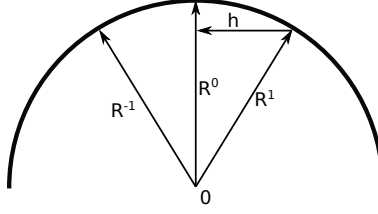


Figure 2: Sketch to compute  $R^{-1} = R(t - \Delta t)$ .

we can simplify the equation to

$$b = \left(1 - \Delta t^2 V(t)^2 / a^2 + O(\Delta t^3)\right)^{-1/2}.$$

Next, we use a Taylor series approximation

$$\begin{aligned} f(\Delta t) &= (1 - \Delta t)^{-1/2} \\ &\approx 1 + \Delta t \left(-\frac{1}{2}\right) (1 - 0)^{-\frac{3}{2}} (-1) + O(\Delta t^2) \\ &= 1 + \Delta t \frac{1}{2} + O(\Delta t^2) \end{aligned}$$

we finally get the correction factor

$$b = 1 + \frac{1}{2} \Delta t V(t) / a + O(\Delta t^2)$$

which

we can use to compute new location  $R(t) = b(R(t + \Delta t) - \Delta t V(t))$ .

### 8.2.3 Midpoint rule

Based on the new departure location  $R(t)$  we use this as part of a midpoint rule to compute  $R(t - \Delta t)$  using the sketch in Figure 2 where we use  $R^n = R(t + n\Delta t)$ .

We parametrize the vector  $h(\gamma) = \gamma R^0 - R^1$  and request it to be orthogonal to  $b$  via

$$\begin{aligned} h(\gamma) \cdot R^0 &= 0 \\ (\gamma R^0 - R^1) \cdot R^0 &= 0 \\ \gamma R^0 \cdot R^0 &= R^1 \cdot R^0 \\ \gamma &= \frac{R^1 \cdot R^0}{R^0 \cdot R^0}. \end{aligned}$$

Finally, we can compute  $R$  via

$$\begin{aligned} R^{-1} &= R^1 + 2h \\ &= R^1 + 2(\gamma R^0 - R^1) \\ &= R^1 + 2\left(\frac{R^1 \cdot R^0}{R^0 \cdot R^0} R^0 - R^1\right) \\ &= R^1 + 2\left(\frac{R^1 \cdot R^0}{R^0 \cdot R^0} R^0 - R^1\right) \\ &= 2 \frac{R^1 \cdot R^0}{R^0 \cdot R^0} R^0 - R^1 \end{aligned}$$

and with  $R^0 \cdot R^0 = a^2$  we get

$$R(t - \Delta t) = 2 [R(t) \cdot R(t + \Delta t) / a^2] R(t) - R(t + \Delta t).$$

### 8.2.4 Full iteration scheme (realization of variant DP\_ritchie)

The iteration will solve Eq. (5) iteratively. The iterative scheme with the  $k$ -th iteration is given by

$$R_{k+1}(t) = b_{k+1} (R(t + \Delta t) - \Delta t V_{k+1}(t))$$

with  $V_{k+1}(t)$  to be computed by interpolation. The iteration is started with  $R_0(t) = R(t + \Delta t)$  which is the arrival point. Given the Equations in Section 5 we can compute the velocity  $V^C$  in Cartesian space and hence solve Eq. (6)

$$b_k = \left( 1 - \Delta t^2 V_k^C(t)^2 - 2\Delta t V_k^C(t) \cdot R_k(t) \right)^{-1/2}.$$

The iterations  $R_{k+1}$  can be executed until sufficient convergence is reached. However, two iterations are sufficient to gain 2nd order accuracy.

Finally, the departure position  $R(t - \Delta t)$  can be calculated with a midpoint rule (see Eq. (8.2.3))

$$R(t - \Delta t) = 2 \left[ R(t) \cdot R(t + \Delta t) / a^2 \right] R(t) - R(t + \Delta t).$$

Based on this, we can use the interpolation at the departure point and the same equation to advect other state variables along the Lagrangian trajectory with the same equation.

### 8.3 SETTLS (variant DP\_SETTLS)

This method is based on the SETTLS SL method in Section

## 9 Sphere approximation of trajectory

This section describes how to approximate the movement of a point for a given velocity

$$R(t) = R(t + \Delta t) - \Delta t V(t + \Delta t)$$

on a sphere.

### 9.1 Linear approximation with normalization (SP\_normalize)

This method assumes the velocity to act on the plane planar to the sphere. Then, the arrival point is projected back to the sphere with a normalization. Section (5) describes this method.

### 9.2 Other versions (variant DP\_TODO)

Other versions basically differ in the way how the velocity vector is applied on the arrival point. E.g. using exact tracing on the sphere's surface.

## 10 Coriolis effect

### 10.1 Semi-implicit treatment of Coriolis effect (variant CE\_implicit)

See [Cote and Staniforth, 1988], [Ritchie et al., 1995]. 1st discussed method in [Temperton, 1995]. Simply treat it as part of the linear part  $L$ .

### 10.2 SL treatment of Coriolis effect (variant CE\_lagrangian)

See ROCHAS, M. 1990, 2nd method in [Temperton, 1995]. The underlying idea is to use the definition of the material derivative

$$\frac{D}{Dt} = \frac{\partial}{\partial t} + V \cdot \nabla$$

and

$$\frac{\partial}{\partial t} f k \times R = f k \times V$$

to rewrite the momentum equation to

$$\begin{aligned}
\frac{DV}{Dt} &= -\nabla\Phi - fk \times V \\
\frac{\partial}{\partial t}V + V \cdot \nabla V &= -\nabla\Phi - \frac{\partial}{\partial t}fk \times R \\
\frac{\partial}{\partial t}V + V \cdot \nabla(V + fk \times R) + \frac{\partial}{\partial t}fk \times R &= -\nabla\Phi \\
\frac{\partial}{\partial t}(V + fk \times R) + V \cdot \nabla(V + fk \times R) &= -\nabla\Phi \\
\frac{DV + fk \times R}{Dt} &= -\nabla\Phi.
\end{aligned}$$

According to the aforementioned related work, this takes the calculated departure points in the same way as from the previous work.

However, for the velocities, the the Coriolis effect is added at the departure point and simply subtracted again at the arrival points. Note, that the  $R$  coordinate at the departure and arrival point must be used for this.

### 10.3 Nonlinear treatment of Coriolis effect (variant CE\_nonlinear)

## 11 Interpolation order

The big question here is where to use which order. Some particular orders have been inferred for the computation of the trajectory and for the interpolation of the state variables

### 11.1 1) Linear

First order accurate interpolation

### 11.2 2) Cubic

Third order accurate interpolation. Limiters might be used.

## 12 Linear or quadratic Gaussian grid for interpolation

### 12.1 1) Linear Gaussian grid (variant INT\_linear)

Reduced computation costs since no anti-aliasing is required

### 12.2 2) Quadratic Gaussian grid (variant INT\_quadratic)

Additional computation costs because of anti-aliasing strategy

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