

# Computational Models for the Growth of Closed Bacterial Cell Envelopes

Paul Schulze

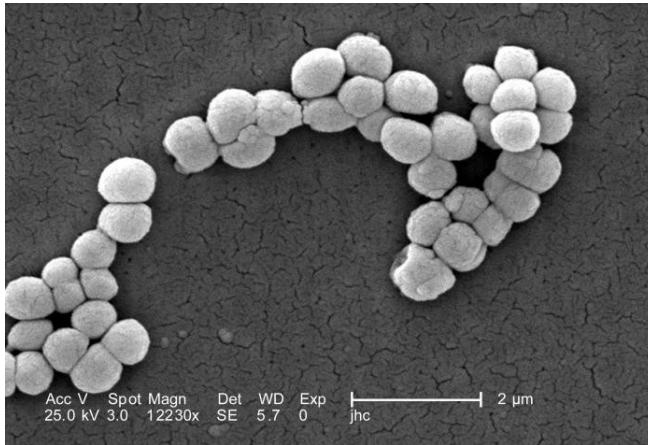
2023-01-19

# Outline

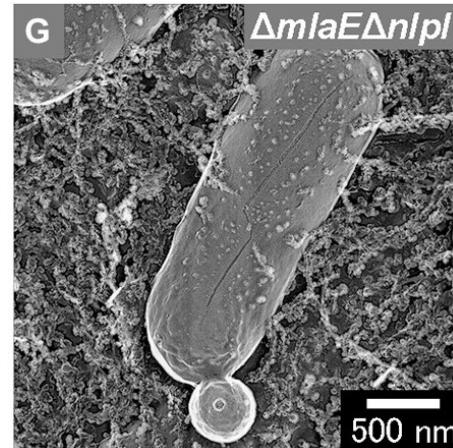
- Introduction
- Spring-based model
  - Idea behind the model
  - Results
- Finite-element-based model
  - Idea behind the model
  - Results
- Summary
- Outlook

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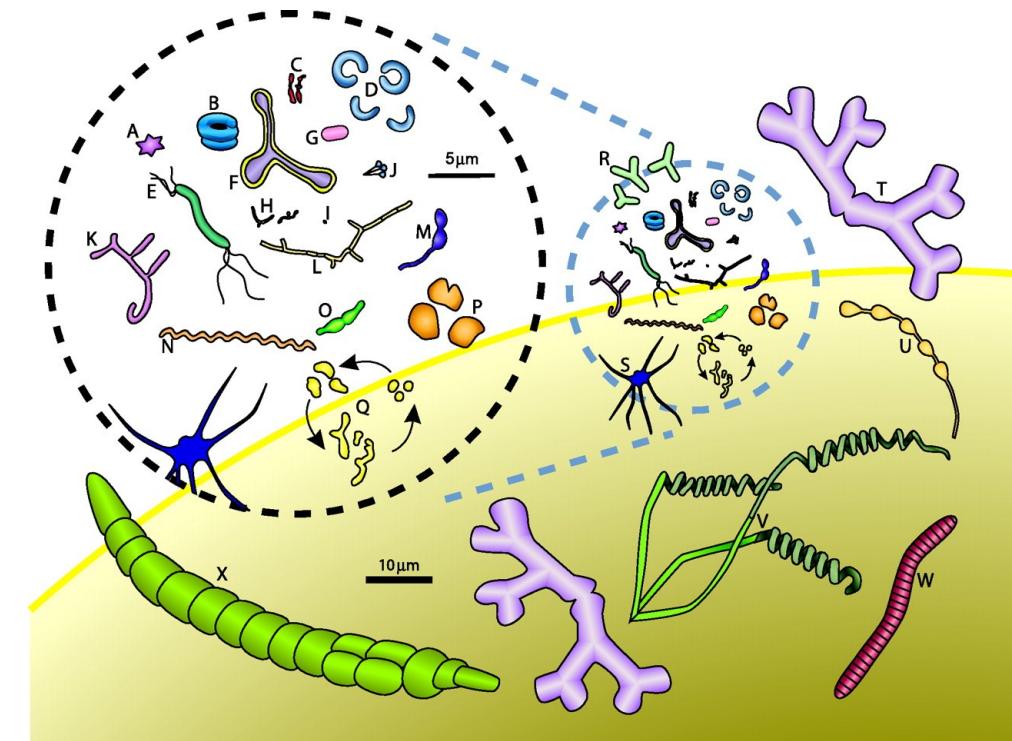
# Shapes of bacteria



Carr, J. H. (2007) Public Health Image Library (PHIL), CDC



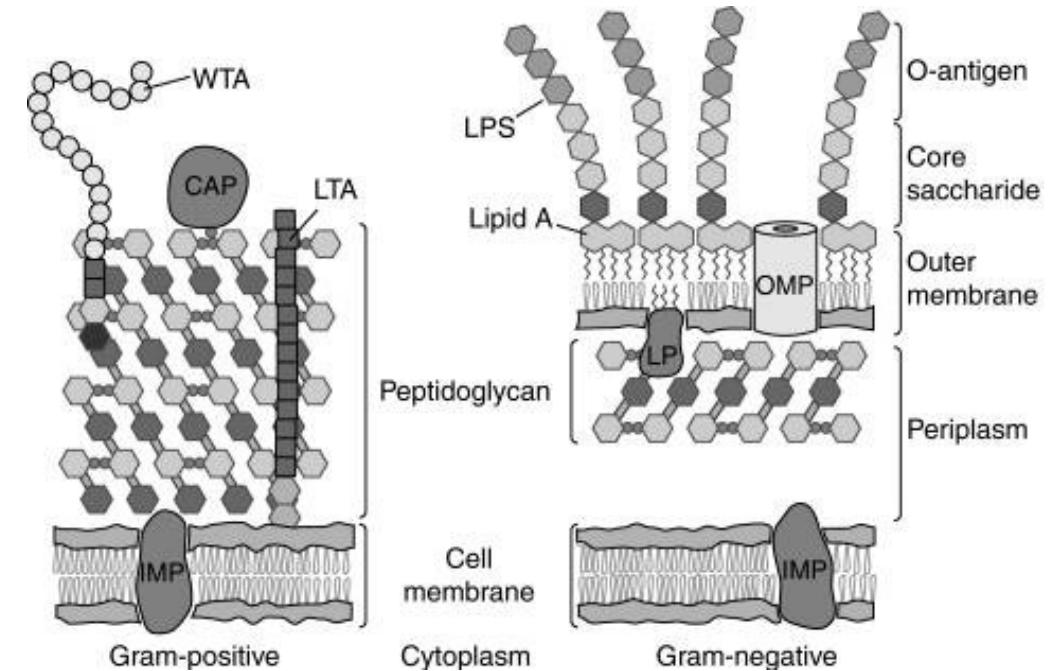
Ojima, Y. (2021) Microbial Physiology and Metabolism



Young, K. D. (2006) Microbiology and molecular biology reviews

# The cell wall determines the shape

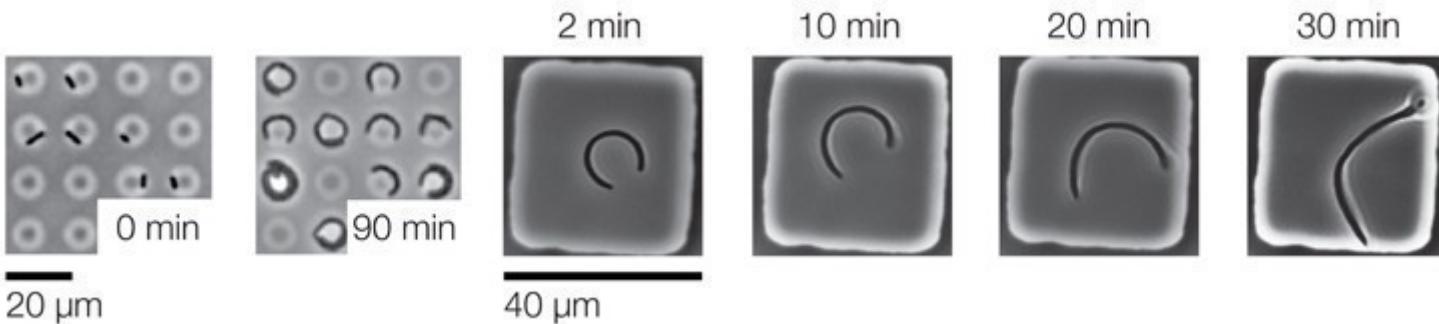
- Composed of Peptidoglycan
- Protects against *osmotic pressure*
- Two classes of bacteria
  - Gram-positive: Thick cell wall
  - Gram-negative: Thin cell wall



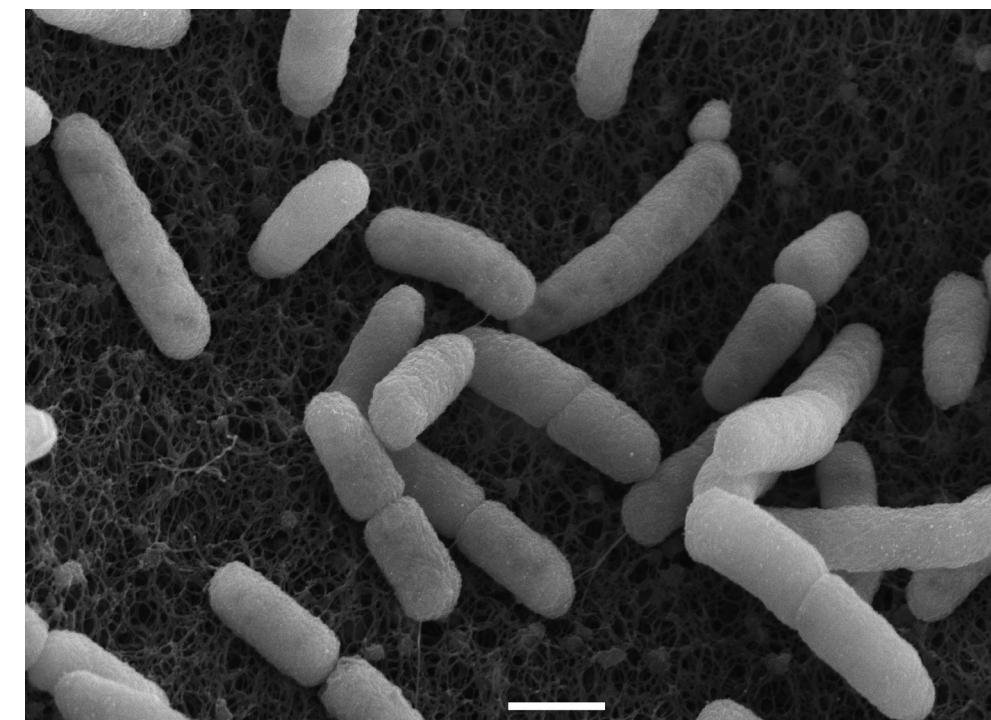
Silhavy, T. J. (2010) in Cold Spring Harbor perspectives in biology

# Shape preservation in bacteria

- Shape is consistent through generations
- Shape is recovered after disturbance
- Shape changes in response to the environment

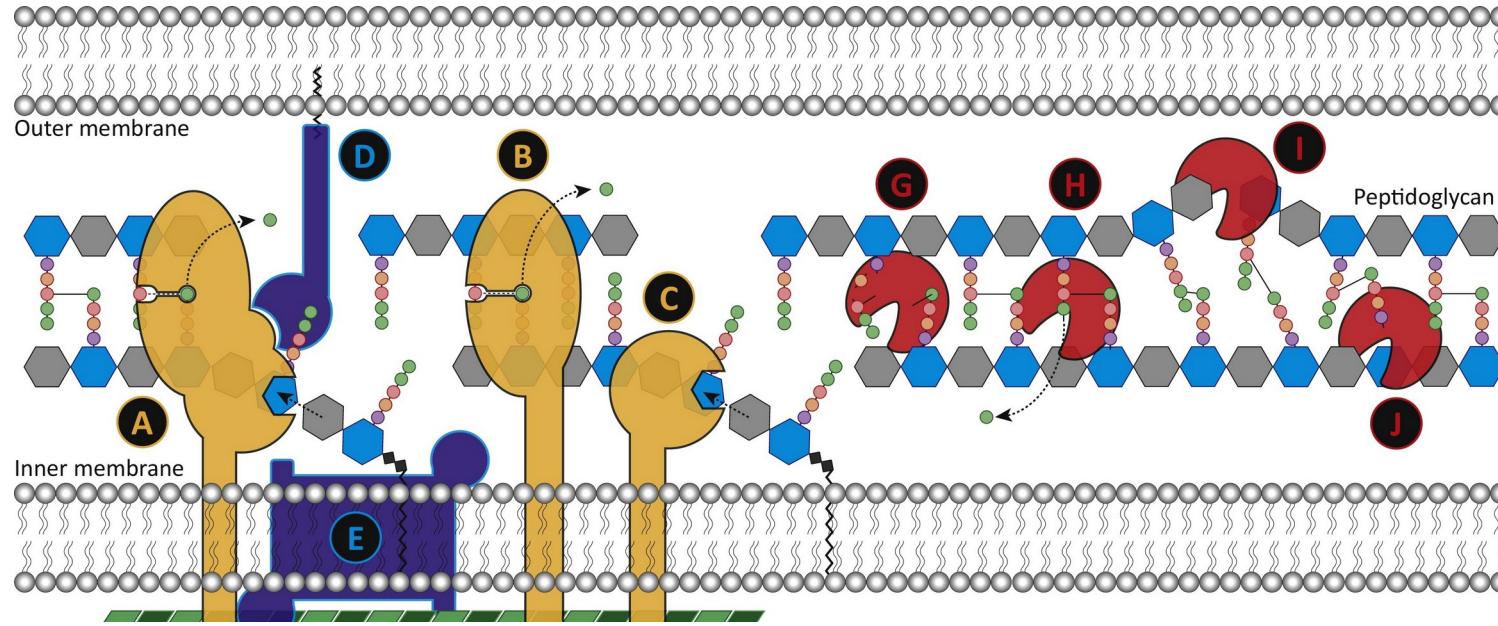


Reproduced from: Felix Wong et al. (2017) Nature microbiology



Gudrun Holland, Michael Laue/RKI

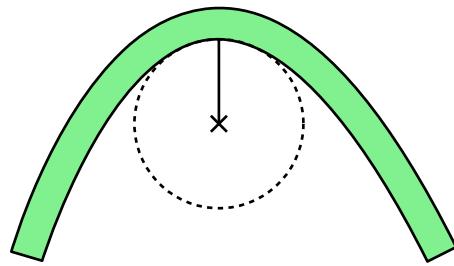
# Peptidoglycan remodelling



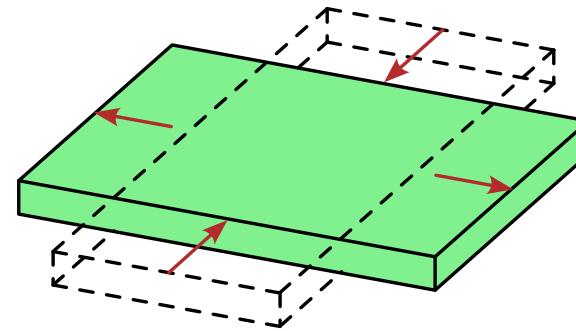
- **PG synthases** assemble the PG network
- **PG hydrolases** modify existing PG
- Guided by *mechanical / geometrical cues?*

# Growth model for the bacterial shell

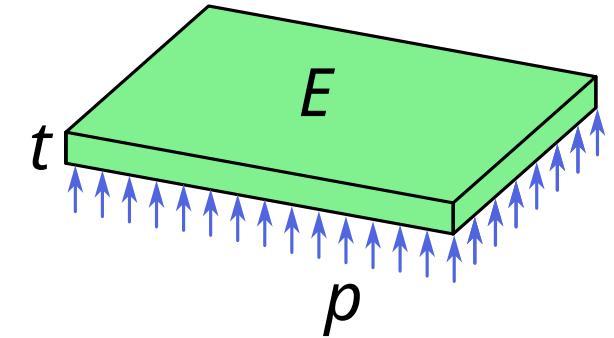
- Mechanical properties of the cell wall
- Turgor pressure
- Growth rates are based on local cues



Curvature



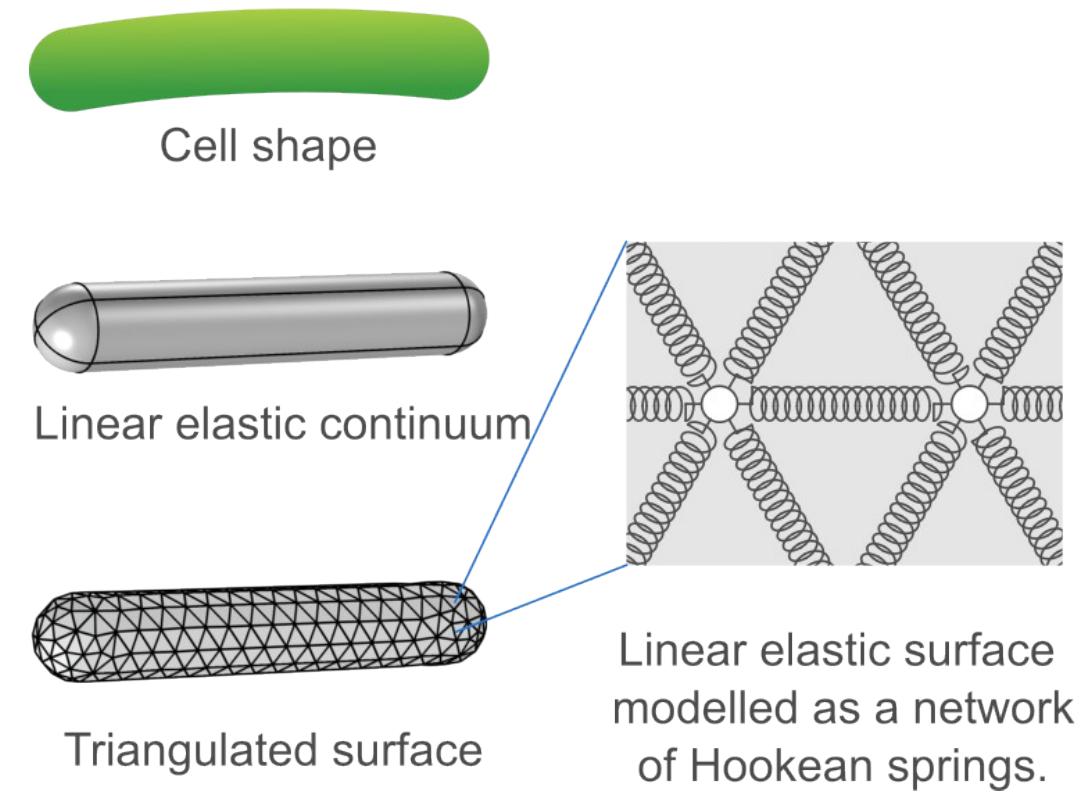
Strain



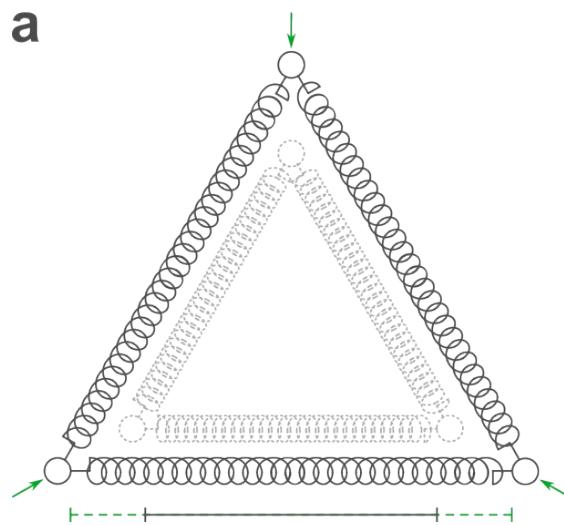
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# Spring-based model of the shell

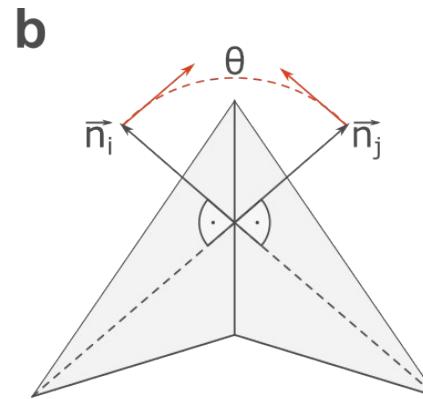
- Linear elastic continuum
  - Young's modulus  $E$
  - Thickness  $t$
- Spring network
  - Spring stiffness  $k_s$
  - Bending stiffness  $k_b$
- Mapping:  
 $E, t \rightarrow k_s, k_b$



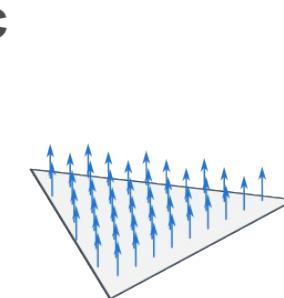
# Energy function



Spring Energy



Bending Energy

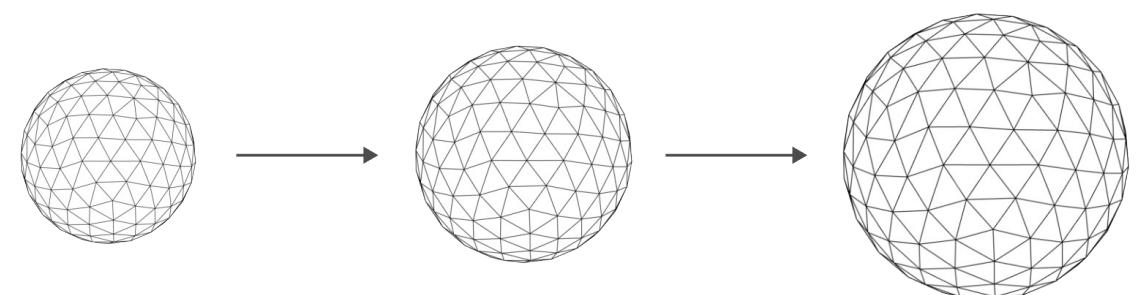
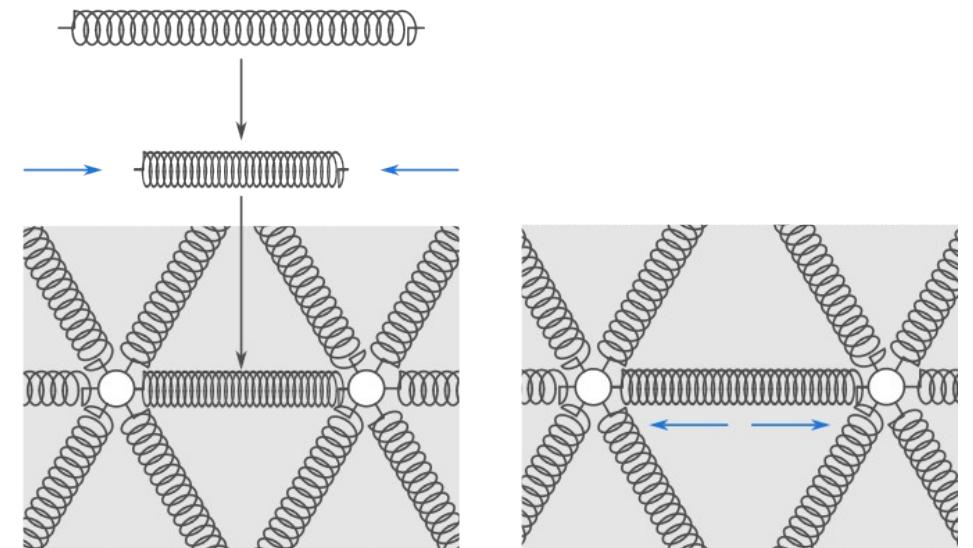


Pressure Energy

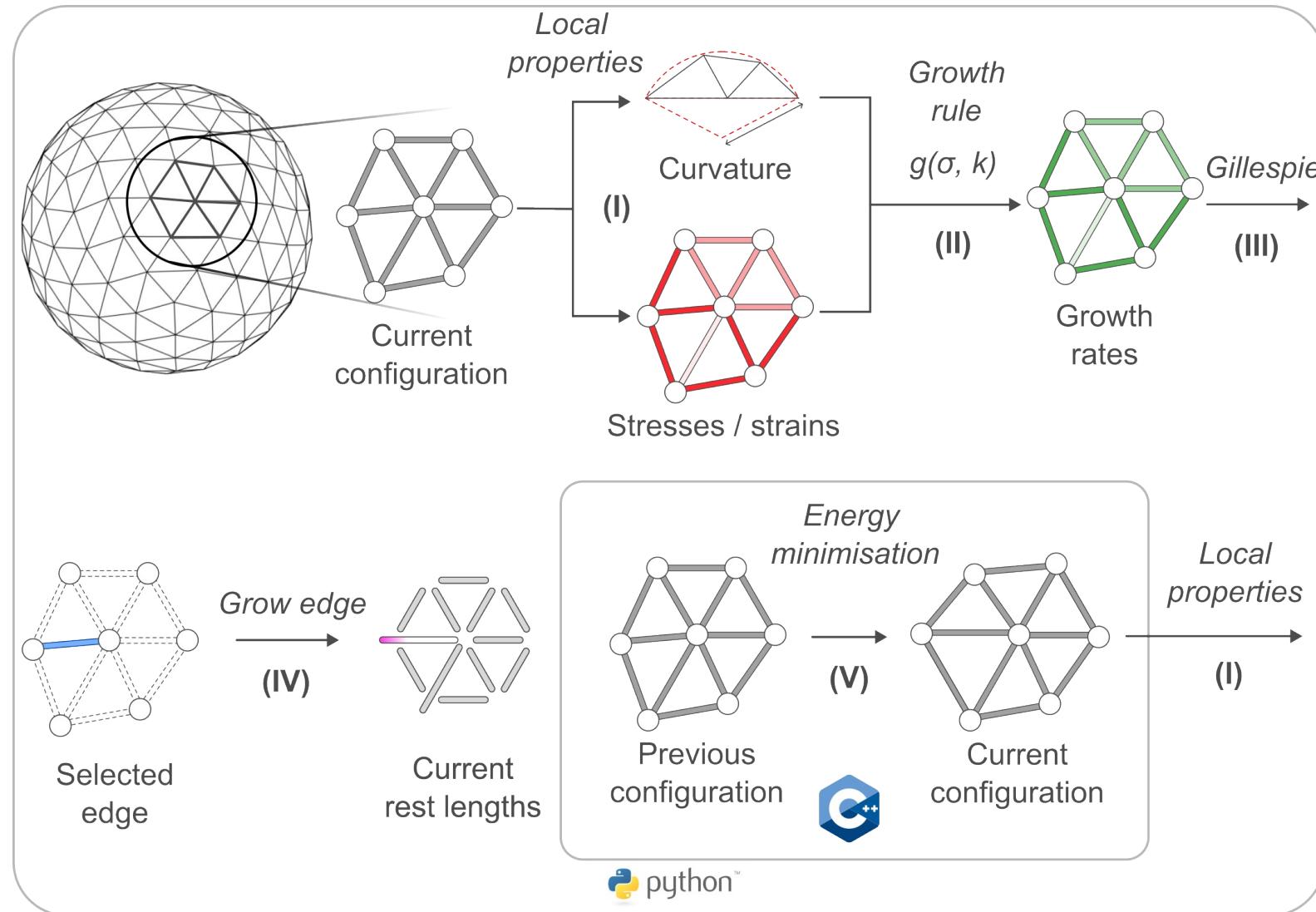
$$E = \sum_e^{\text{edges}} \frac{k_s}{2} (l_e - l_{0,e})^2 + \sum_{\{i,j\}(\text{adj.})}^{\text{triangles}} k_b (1 - \vec{n}_i \cdot \vec{n}_j) - pV$$

# Iterative growth

- Increasing rest lengths  $l_{e,0}$
- Mesh topology is consistent between growth steps

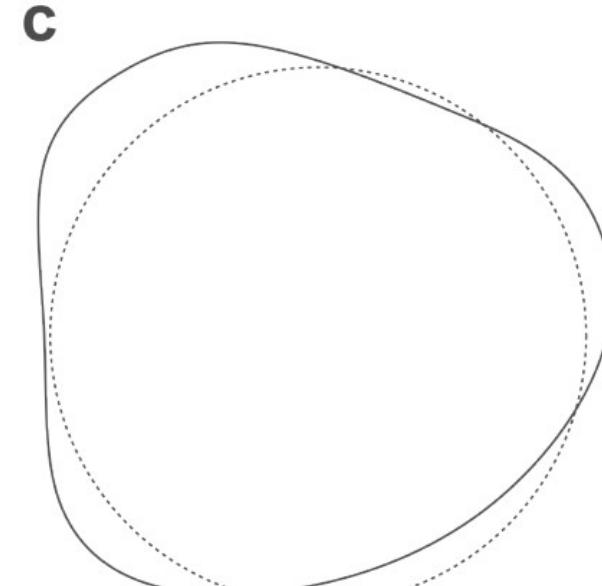
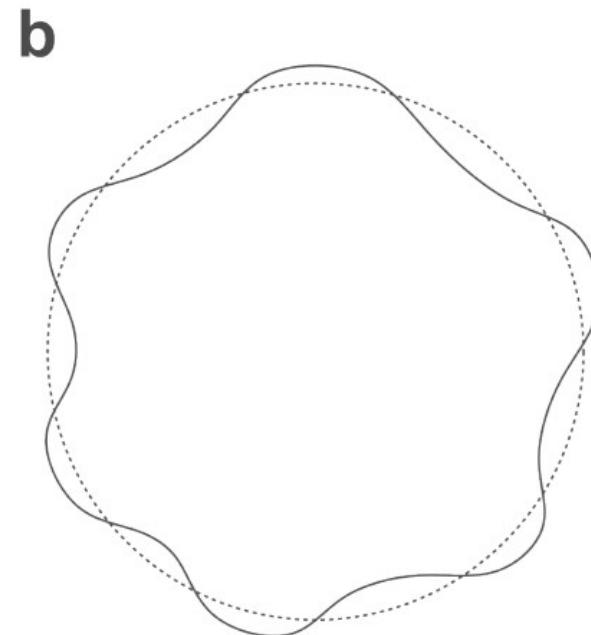
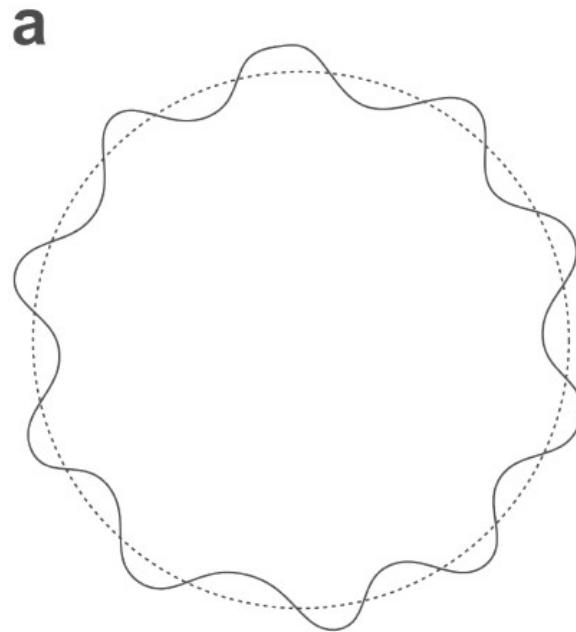


# Simulation flowchart



- Introduction
- **Spring-based model**
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# Observables



Roughness



Asphericity

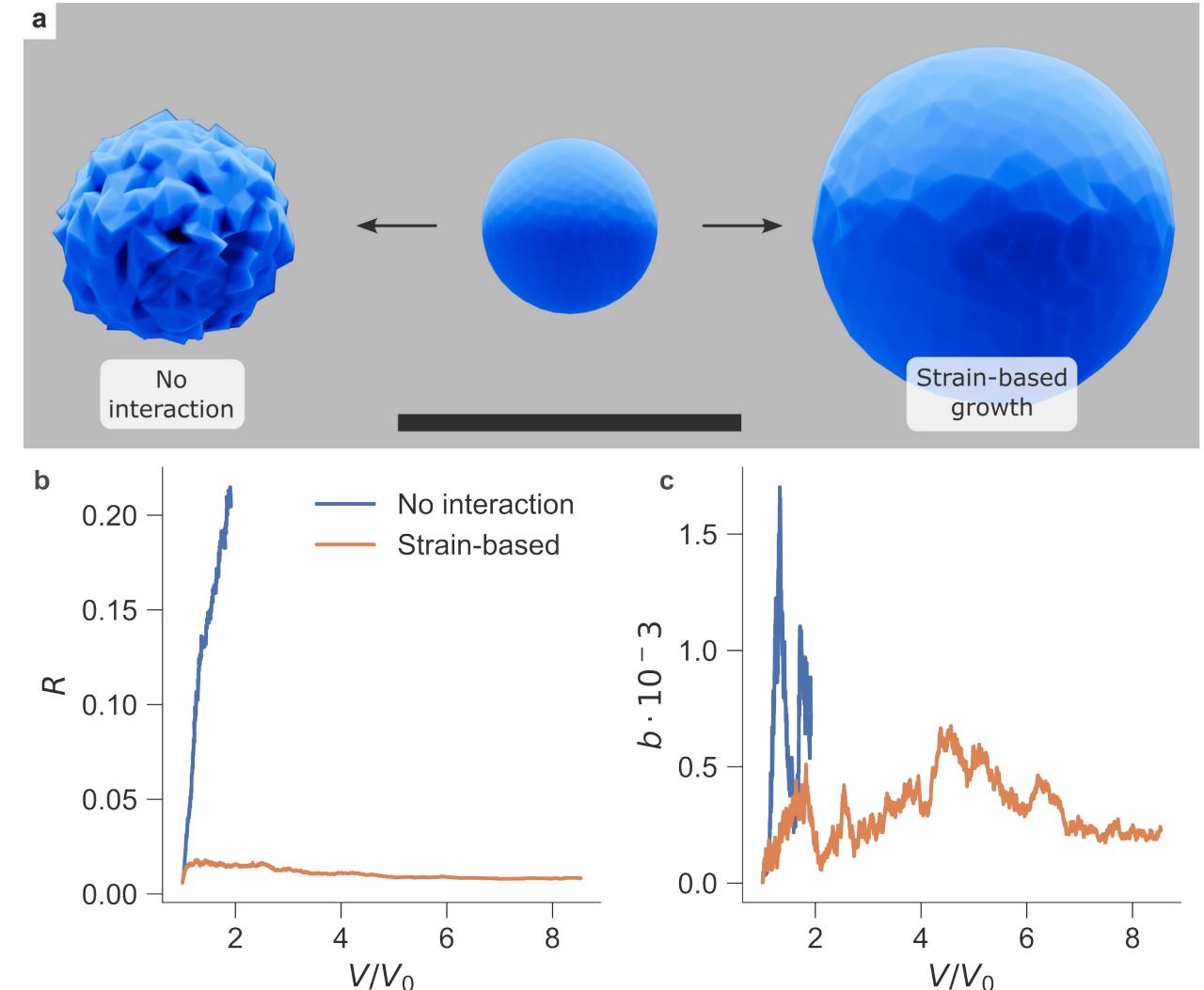


# Random vs. strain-based growth

Strain-based growth rates:

$$\varepsilon_e = (l_e - l_{e,0})/l_{e,0}$$

$$\lambda_e = -\lambda_0 + \lambda_1 \varepsilon_e$$



# Random vs. strain-based growth

Strain-based growth rates:

$$\varepsilon_e = (l_e - l_{e,0})/l_{e,0}$$

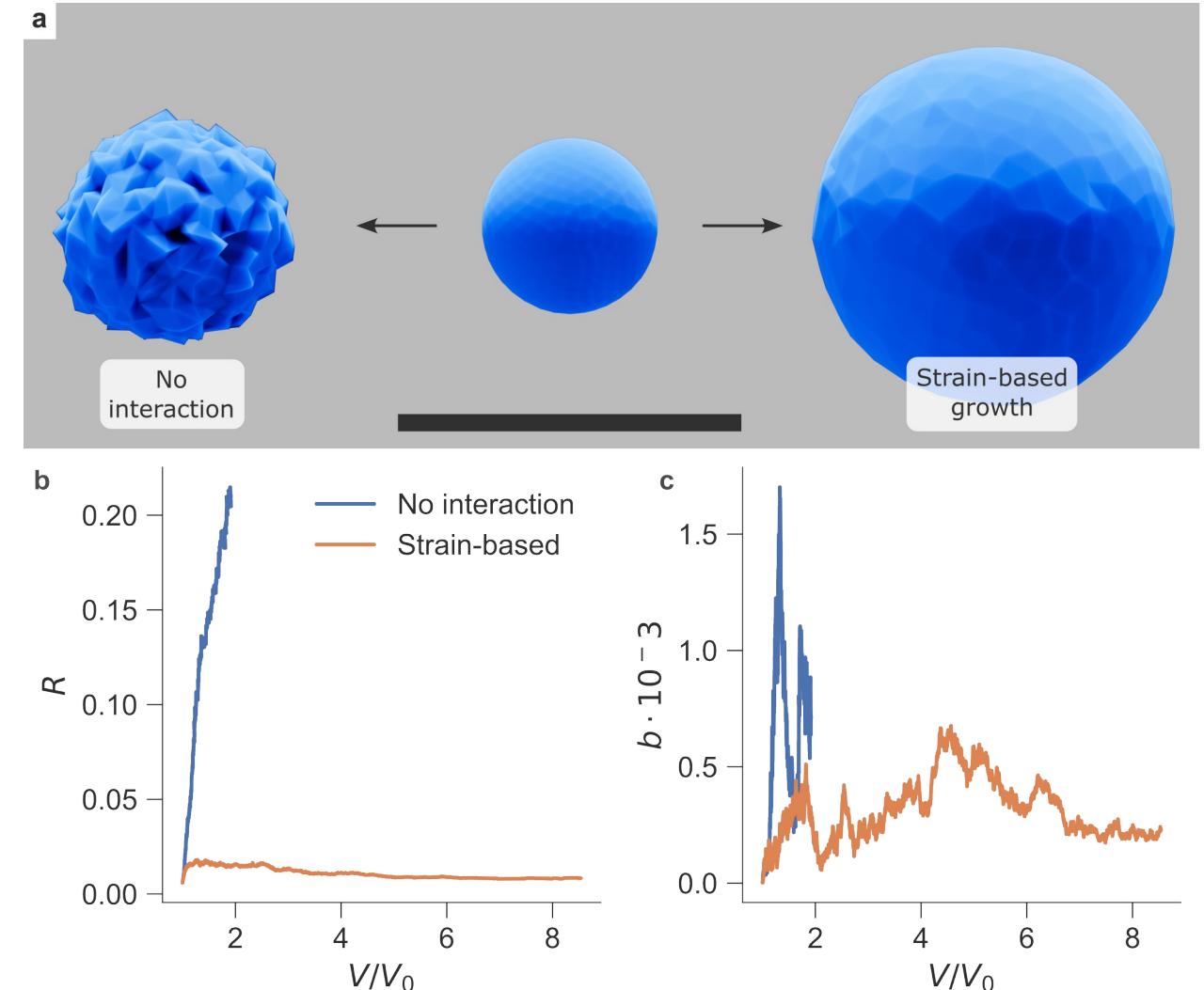
$$\lambda_e = -\lambda_0 + \lambda_1 \varepsilon_e$$

Random

- Spherical shape
- Surface **roughness**

Strain-based

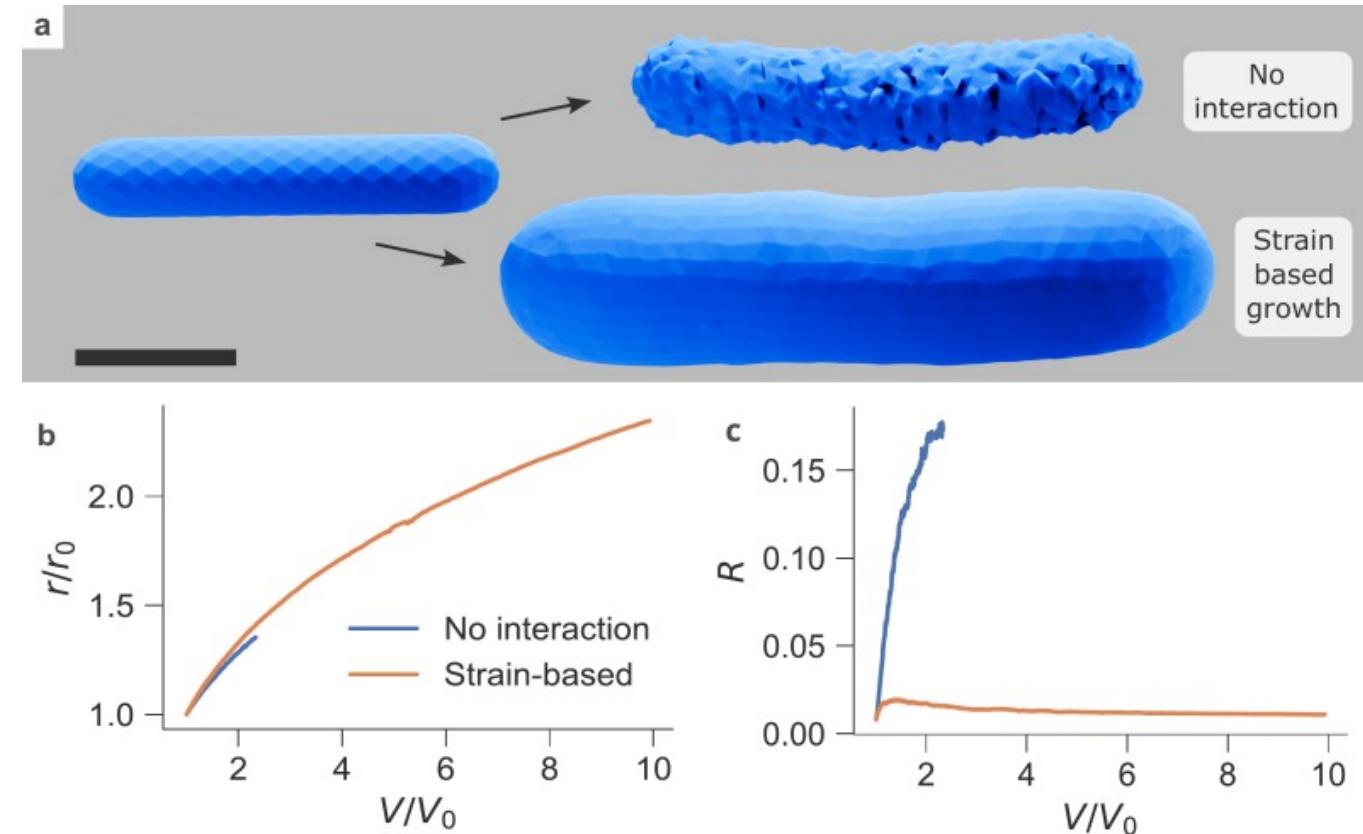
- Spherical shape
- **Smooth** surface



# Random vs. strain-based growth

Strain-based growth rates:

$$\lambda_e = -\lambda_0 + \lambda_1 \varepsilon_e$$



# Random vs. strain-based growth

Strain-based growth rates:

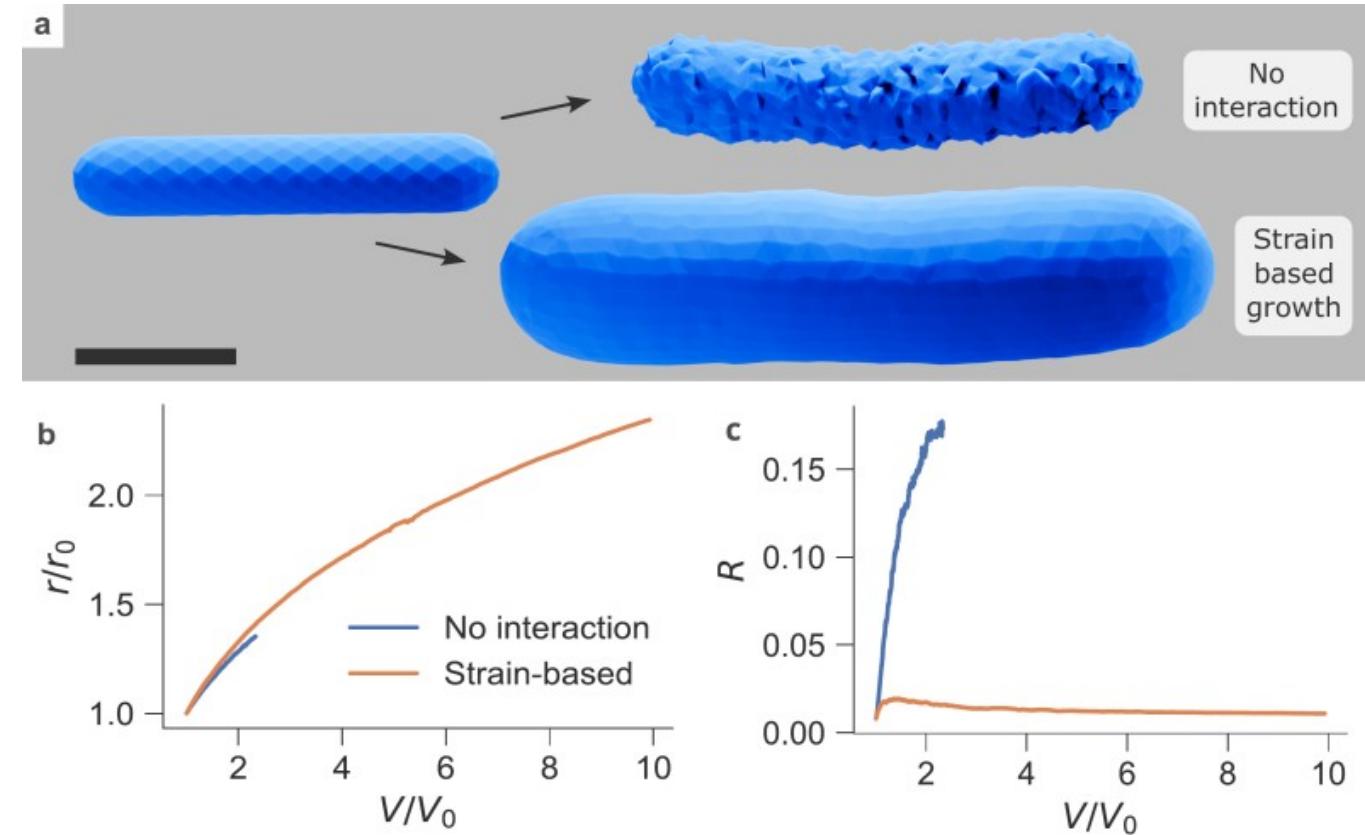
$$\lambda_e = -\lambda_0 + \lambda_1 \varepsilon_e$$

Random growth

- Cylindrical shape
- Surface **roughness**

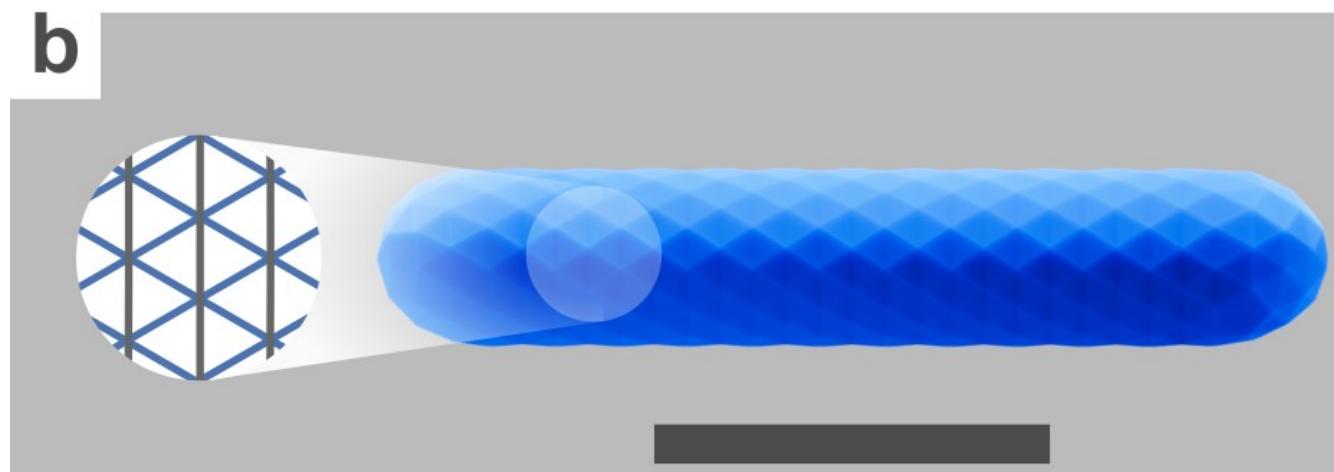
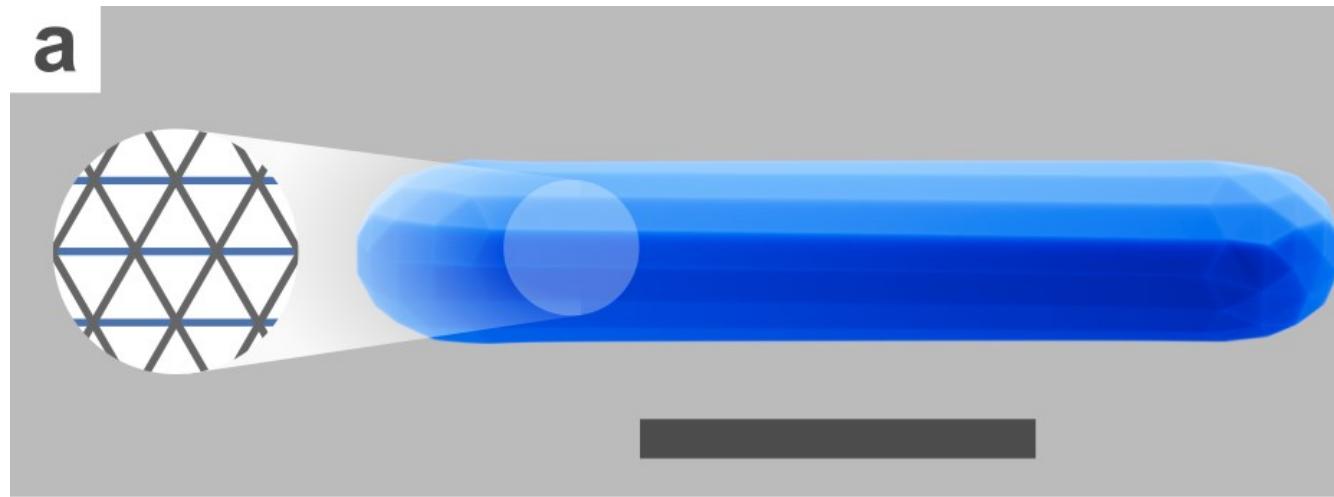
Strain-based growth

- Cylindrical shape
- **Smooth** surface

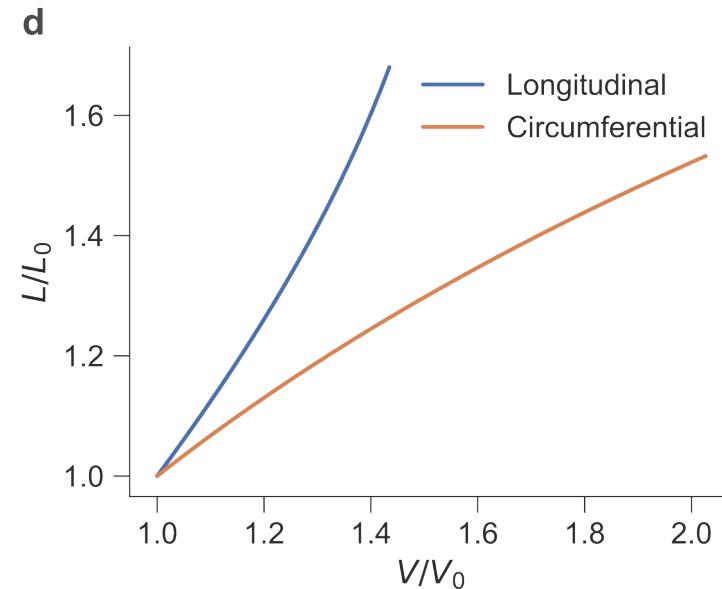
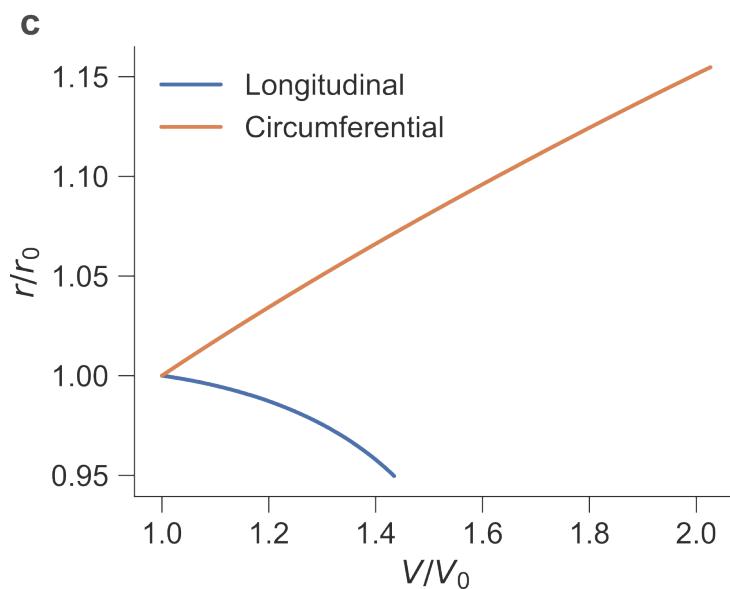
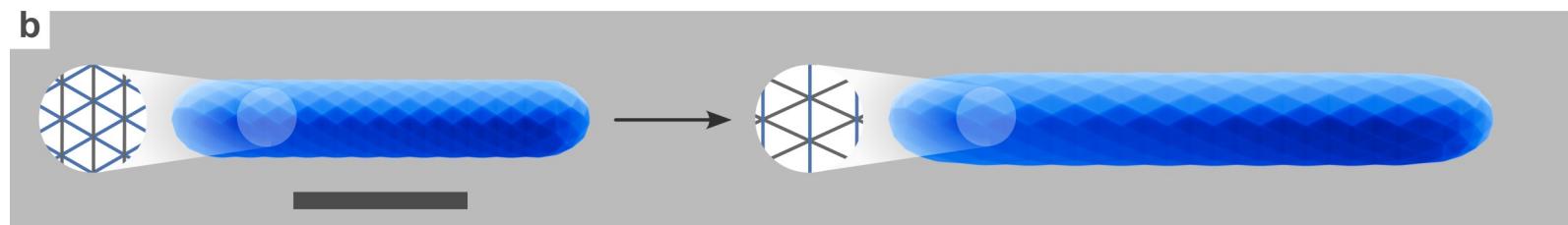
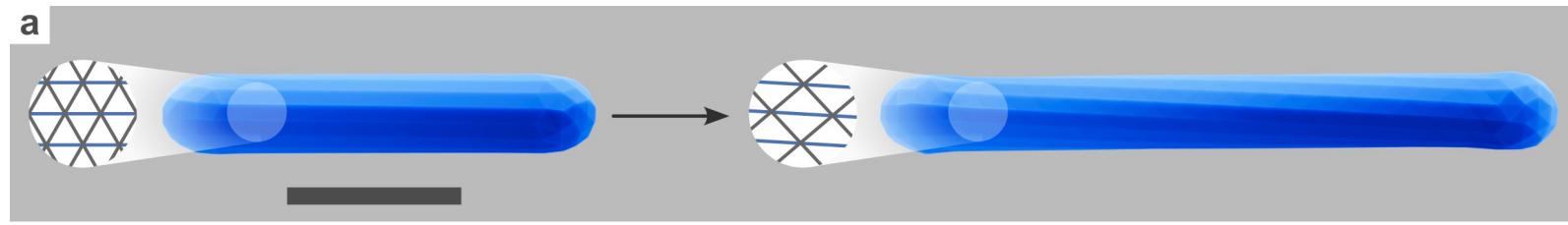


⇒ Radius is not conserved

# Directed growth: Mesh alignment

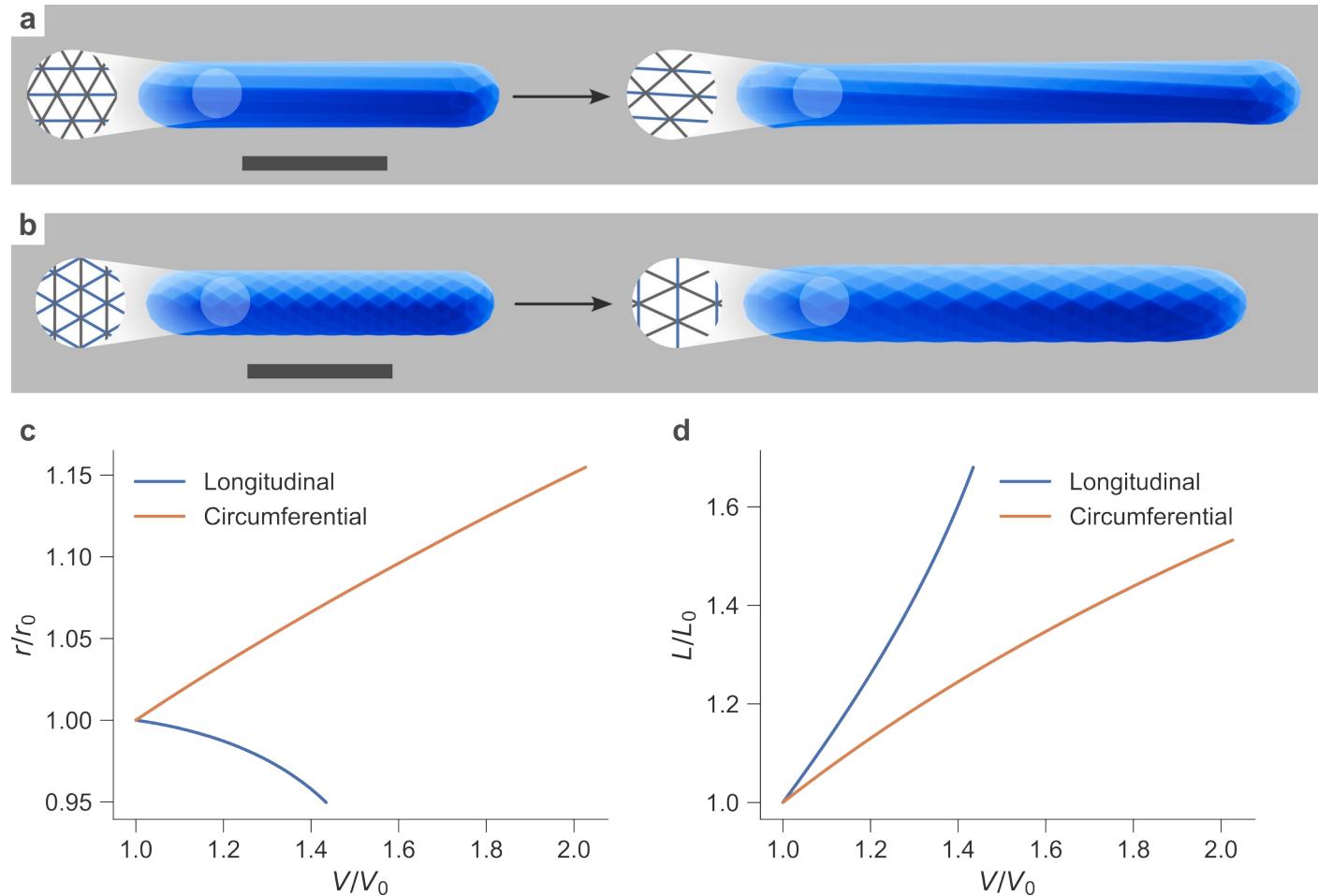


# Directed growth: Mesh alignment



# Spring-based model: Limitations

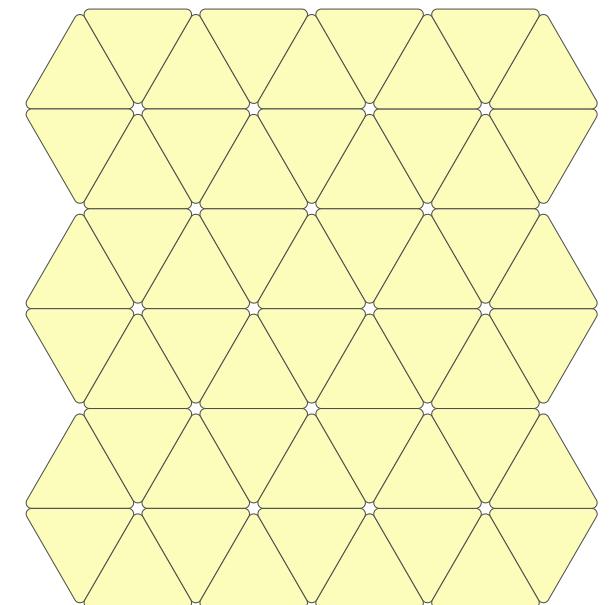
- Dependence on *mesh alignment*
  - Acute angles in triangles  
→ Not linear elastic
  - Hyperelasticity
- Alternative model



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# Finite element method

- Method to solve partial differential equations (PDEs)
- Solve for deformations of complex geometries under outside forces
- Surface is divided into elements
- Solution is evaluated at nodes
- Interpolated for a full solution



# Finite element method

Strain for triangular element:

$$\vec{\varepsilon} = [B]\vec{u}_{\text{element}} = \begin{bmatrix} \varepsilon_{11} \\ \varepsilon_{22} \\ 2\varepsilon_{12} \end{bmatrix} = \begin{bmatrix} \frac{\partial N_a}{\partial x_1} & 0 & \frac{\partial N_b}{\partial x_1} & 0 & \frac{\partial N_c}{\partial x_1} & 0 \\ 0 & \frac{\partial N_a}{\partial x_2} & 0 & \frac{\partial N_b}{\partial x_2} & 0 & \frac{\partial N_c}{\partial x_2} \\ \frac{\partial N_a}{\partial x_1} & \frac{\partial N_a}{\partial x_2} & \frac{\partial N_b}{\partial x_1} & \frac{\partial N_b}{\partial x_2} & \frac{\partial N_c}{\partial x_1} & \frac{\partial N_c}{\partial x_2} \end{bmatrix} \begin{bmatrix} u_1^{(a)} \\ u_2^{(a)} \\ u_1^{(b)} \\ u_2^{(b)} \\ u_1^{(c)} \\ u_2^{(c)} \end{bmatrix}$$

# Finite element method

Strain for triangular element:

$$\vec{\varepsilon} = [B]\vec{u}_{\text{element}} = \begin{bmatrix} \varepsilon_{11} \\ \varepsilon_{22} \\ 2\varepsilon_{12} \end{bmatrix} = \begin{bmatrix} \frac{\partial N_a}{\partial x_1} & 0 & \frac{\partial N_b}{\partial x_1} & 0 & \frac{\partial N_c}{\partial x_1} & 0 \\ 0 & \frac{\partial N_a}{\partial x_2} & 0 & \frac{\partial N_b}{\partial x_2} & 0 & \frac{\partial N_c}{\partial x_2} \\ \frac{\partial N_a}{\partial x_1} & \frac{\partial N_a}{\partial x_2} & \frac{\partial N_b}{\partial x_1} & \frac{\partial N_b}{\partial x_2} & \frac{\partial N_c}{\partial x_1} & \frac{\partial N_c}{\partial x_2} \end{bmatrix} \begin{bmatrix} u_1^{(a)} \\ u_2^{(a)} \\ u_1^{(b)} \\ u_2^{(b)} \\ u_1^{(c)} \\ u_2^{(c)} \end{bmatrix}$$

Stress-strain relation:

$$\begin{bmatrix} \sigma_{11} \\ \sigma_{22} \\ \sigma_{12} \end{bmatrix} = [D] \begin{bmatrix} \varepsilon_{11} \\ \varepsilon_{22} \\ \varepsilon_{12} \end{bmatrix} = \frac{E}{(1-\nu)^2} \begin{bmatrix} 1 & \nu & 0 \\ \nu & 1 & 0 \\ 0 & 0 & (1-\nu)/2 \end{bmatrix} \begin{bmatrix} \varepsilon_{11} \\ \varepsilon_{22} \\ \varepsilon_{12} \end{bmatrix}$$

# Finite element method

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$$\vec{\varepsilon} = [B]\vec{u}_{\text{element}} = \begin{bmatrix} \varepsilon_{11} \\ \varepsilon_{22} \\ 2\varepsilon_{12} \end{bmatrix} = \begin{bmatrix} \frac{\partial N_a}{\partial x_1} & 0 & \frac{\partial N_b}{\partial x_1} & 0 & \frac{\partial N_c}{\partial x_1} & 0 \\ 0 & \frac{\partial N_a}{\partial x_2} & 0 & \frac{\partial N_b}{\partial x_2} & 0 & \frac{\partial N_c}{\partial x_2} \\ \frac{\partial N_a}{\partial x_1} & \frac{\partial N_a}{\partial x_2} & \frac{\partial N_b}{\partial x_1} & \frac{\partial N_b}{\partial x_2} & \frac{\partial N_c}{\partial x_1} & \frac{\partial N_c}{\partial x_2} \end{bmatrix} \begin{bmatrix} u_1^{(a)} \\ u_2^{(a)} \\ u_1^{(b)} \\ u_2^{(b)} \\ u_1^{(c)} \\ u_2^{(c)} \end{bmatrix}$$

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Strain energy:

$$U = \frac{1}{2} \vec{\varepsilon}^T \vec{\sigma} = \frac{1}{2} \vec{\varepsilon}^T [D] \vec{\varepsilon}.$$

# Finite element method

$$\vec{\varepsilon} = [B]\vec{u}_{\text{element}} \quad U = \frac{1}{2}\vec{\varepsilon}^T \vec{\sigma} = \frac{1}{2}\vec{\varepsilon}^T [D]\vec{\varepsilon}.$$

# Finite element method

$$\vec{\varepsilon} = [B]\vec{u}_{\text{element}} \quad U = \frac{1}{2}\vec{\varepsilon}^T \vec{\sigma} = \frac{1}{2}\vec{\varepsilon}^T [D]\vec{\varepsilon}.$$

Strain energy for element:  $W_{\text{element}} = \frac{1}{2}\vec{u}_{\text{element}}^T (A_{\text{element}}[B]^T [D][B])\vec{u}_{\text{element}}$

# Finite element method

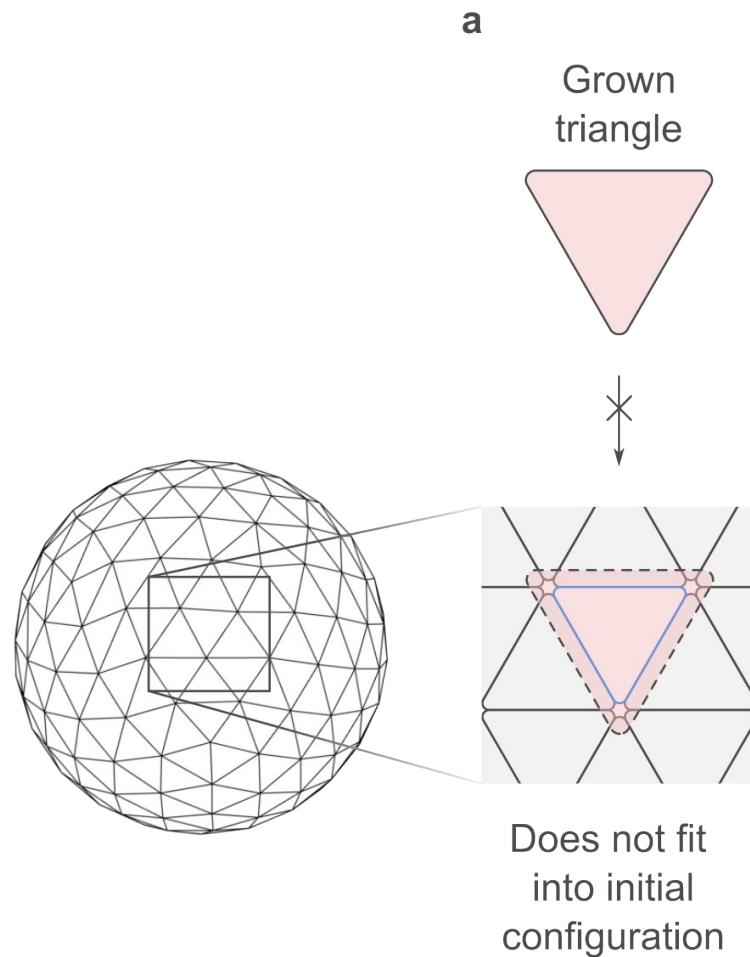
$$\vec{\varepsilon} = [B]\vec{u}_{\text{element}} \quad U = \frac{1}{2}\vec{\varepsilon}^T \vec{\sigma} = \frac{1}{2}\vec{\varepsilon}^T [D]\vec{\varepsilon}.$$

Strain energy for element:  $W_{\text{element}} = \frac{1}{2}\vec{u}_{\text{element}}^T (A_{\text{element}}[B]^T [D][B])\vec{u}_{\text{element}}$

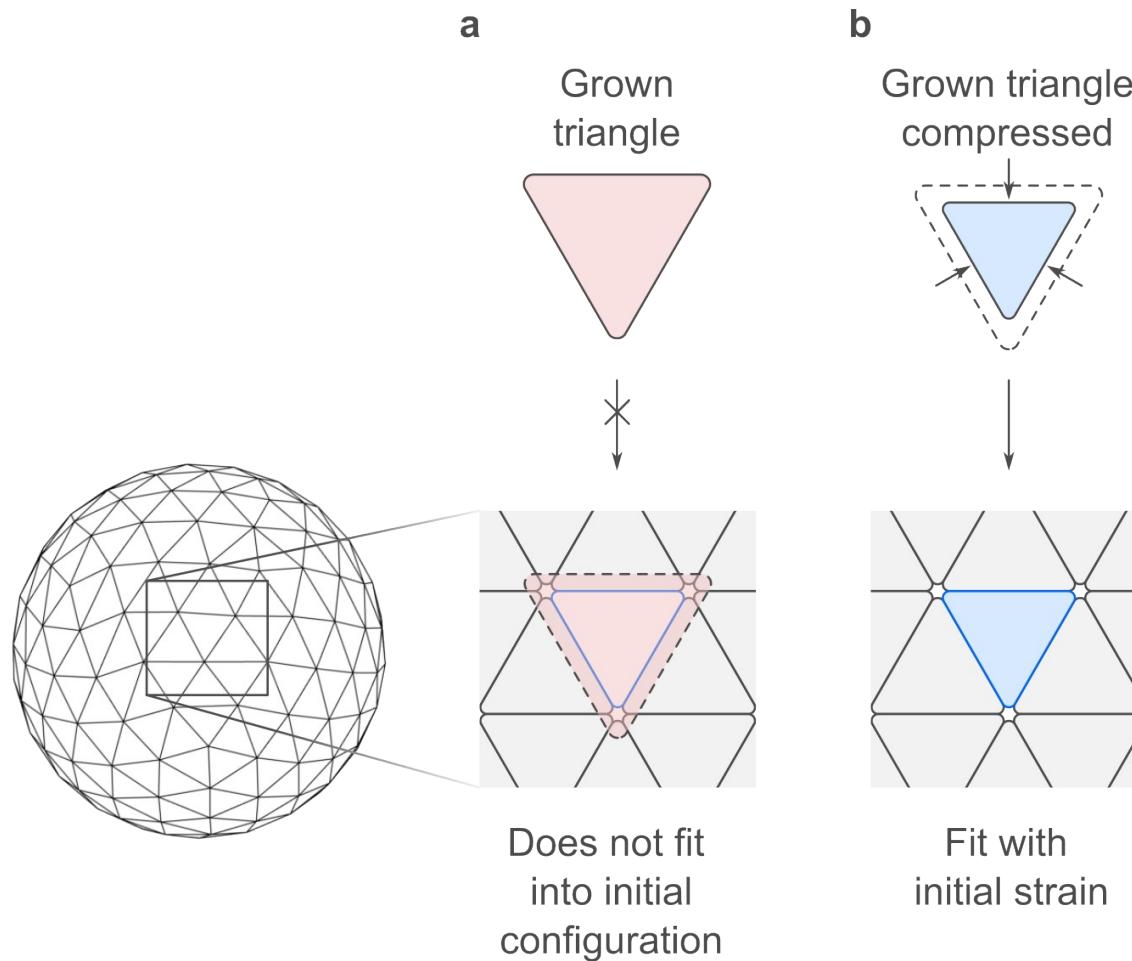
Total strain energy:  $W = \sum_{\text{elements}} W_{\text{element}} = \frac{1}{2} \sum_{\text{elements}} \vec{u}_{\text{element}}^T K_{\text{element}} \vec{u}_{\text{element}}$

Minimize  $W$  with respect to  $u \rightarrow$  Deformations

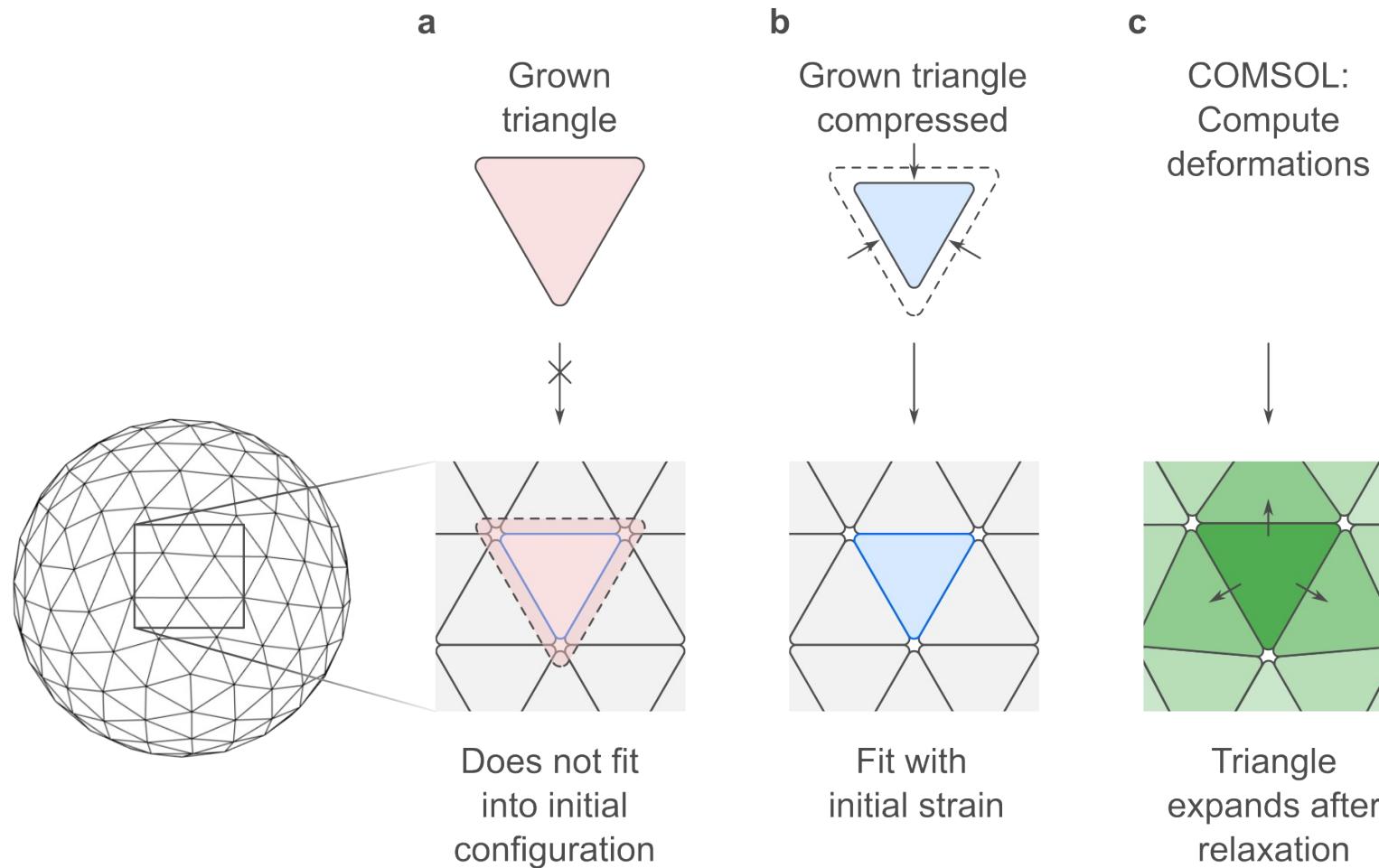
# Finite-element-based Model



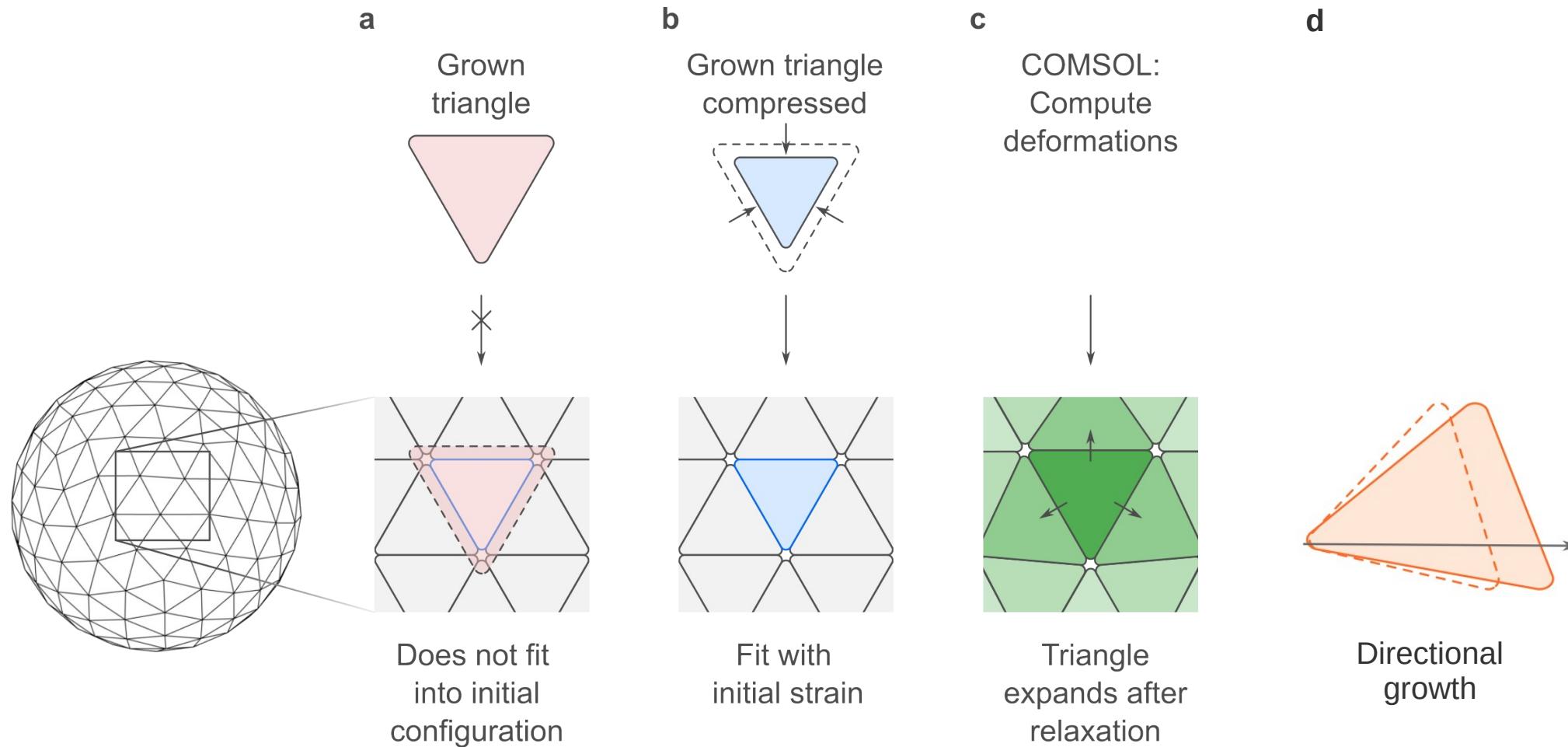
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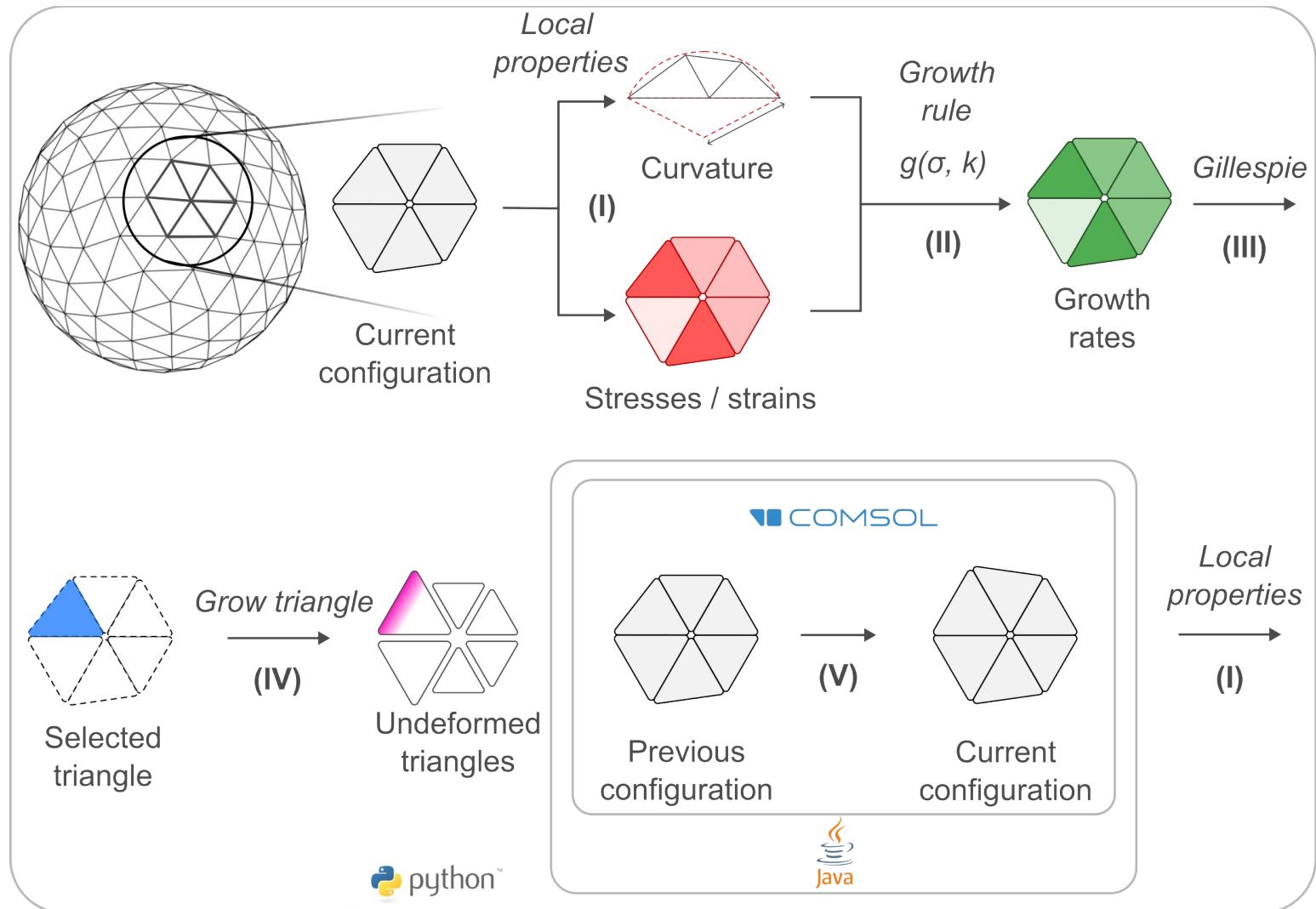
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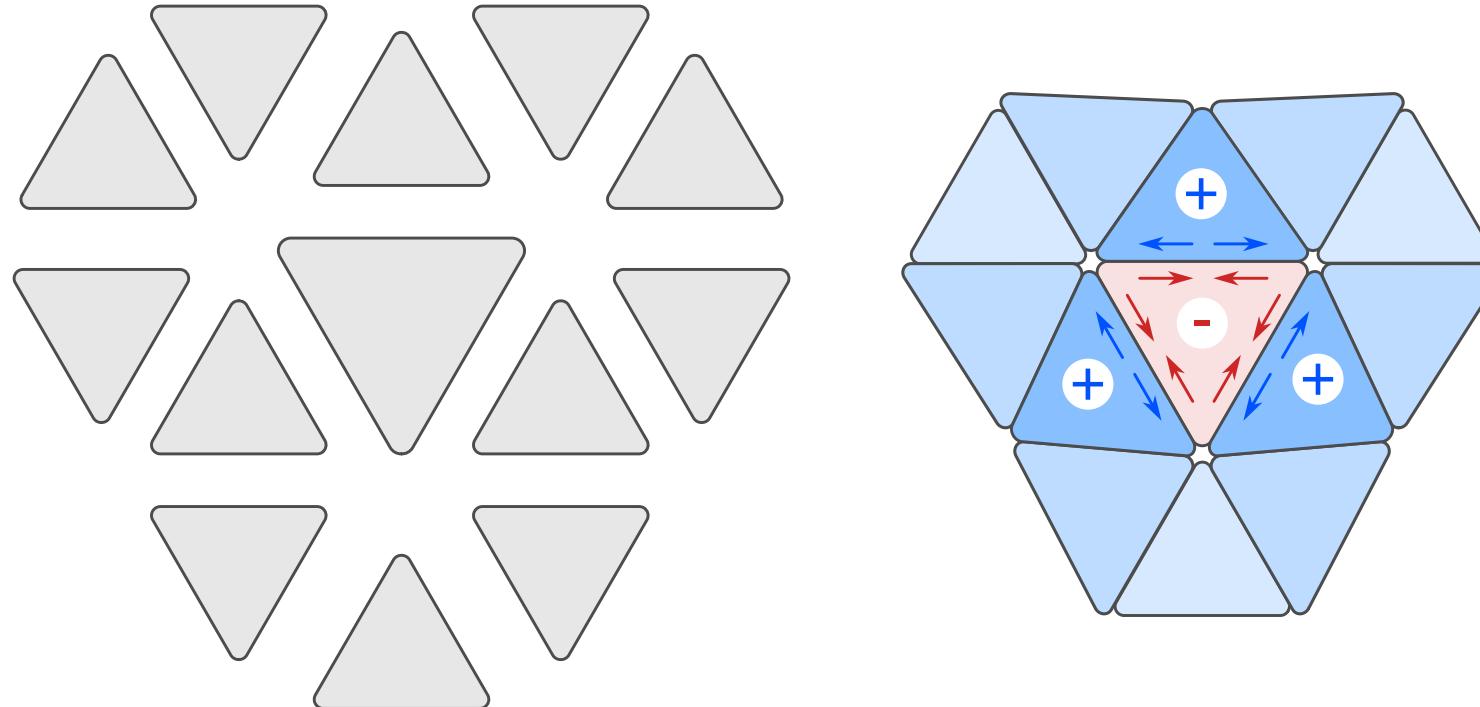


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# Observable: Surface stresses



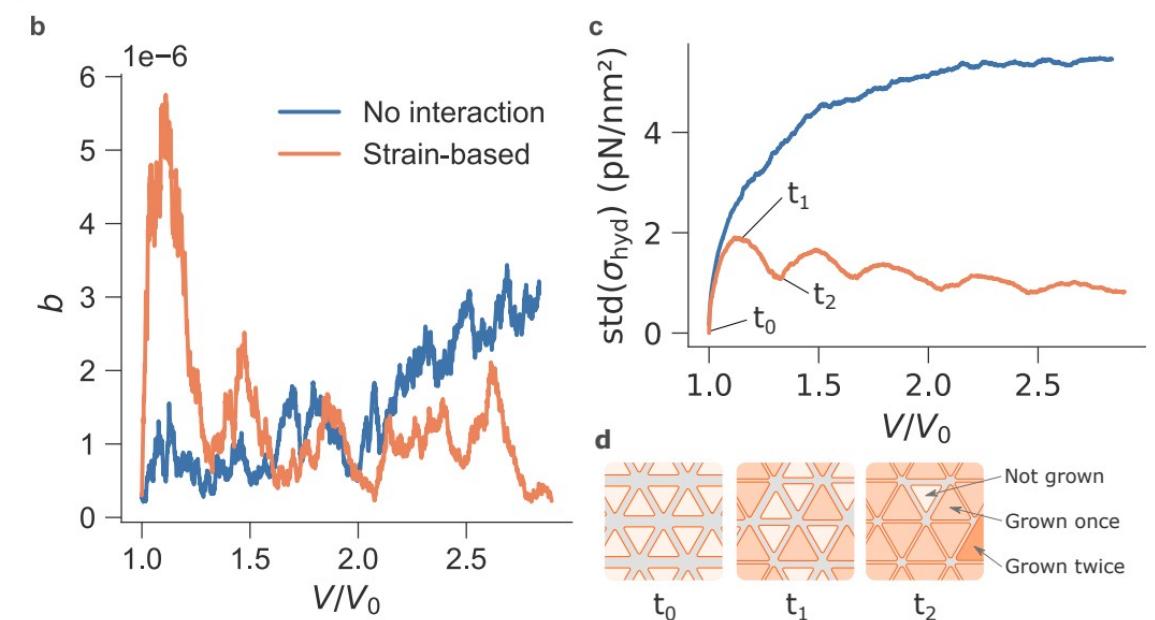
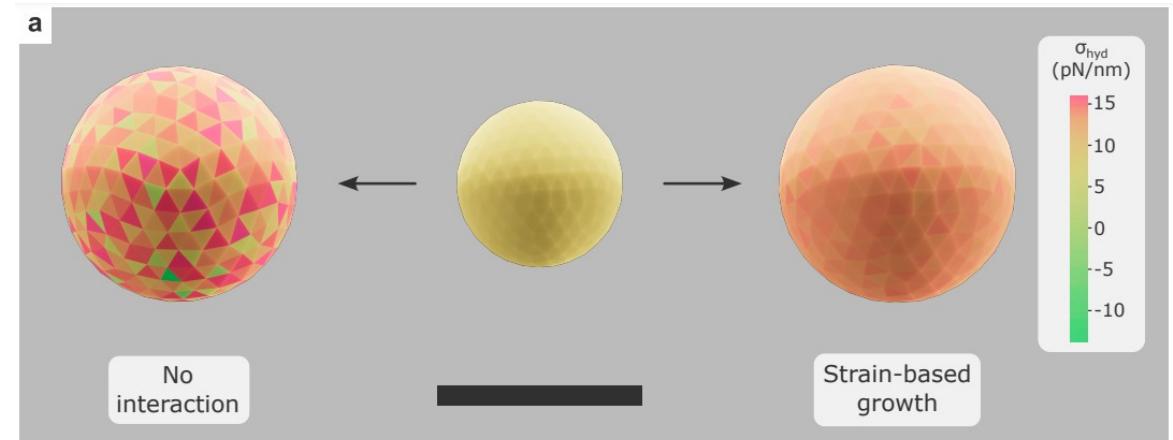
Size mismatch of elements

- High **compressive** and **tensile** stresses
- Affects mechanical stability

# Random vs. strain-based growth

Strain-based growth rates:

$$\lambda^{(e)} = -\lambda_0 + \lambda_1 \varepsilon_h^{(e)}$$

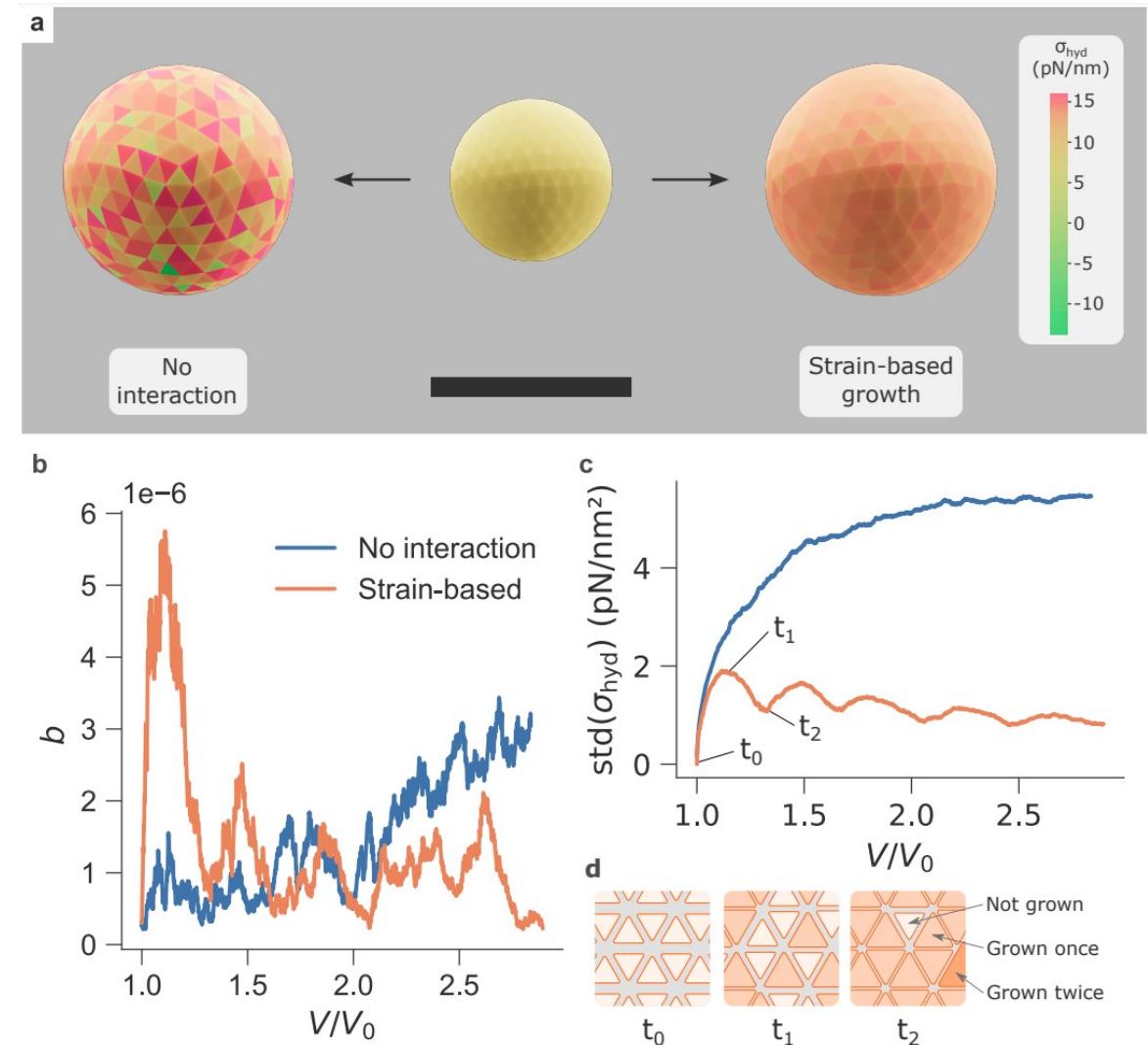


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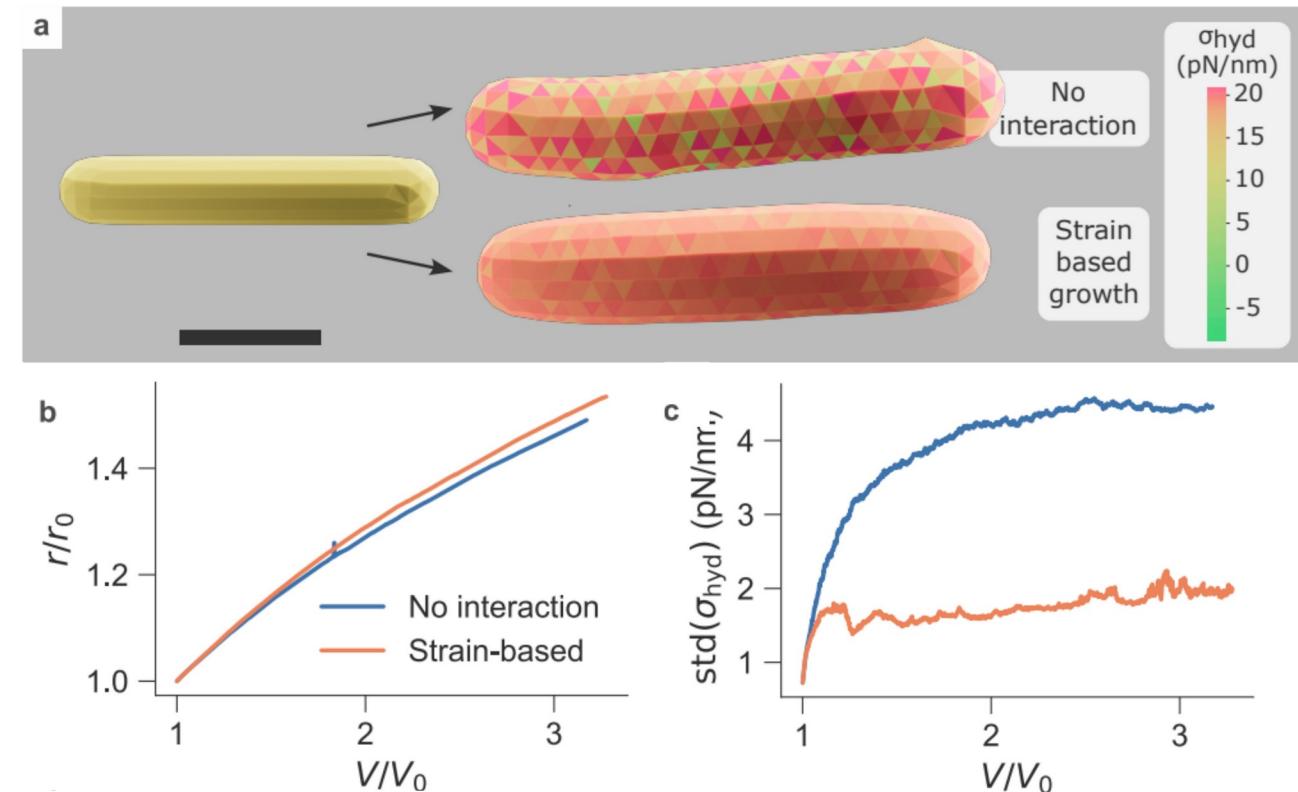
- Random
  - Spherical shape
  - **High** surface stresses
  
- Strain-based
  - Spherical shape
  - **Moderate** surface stresses



# Random vs. strain-based growth

Strain-based growth rates:

$$\lambda^{(e)} = -\lambda_0 + \lambda_1 \varepsilon_h^{(e)}$$



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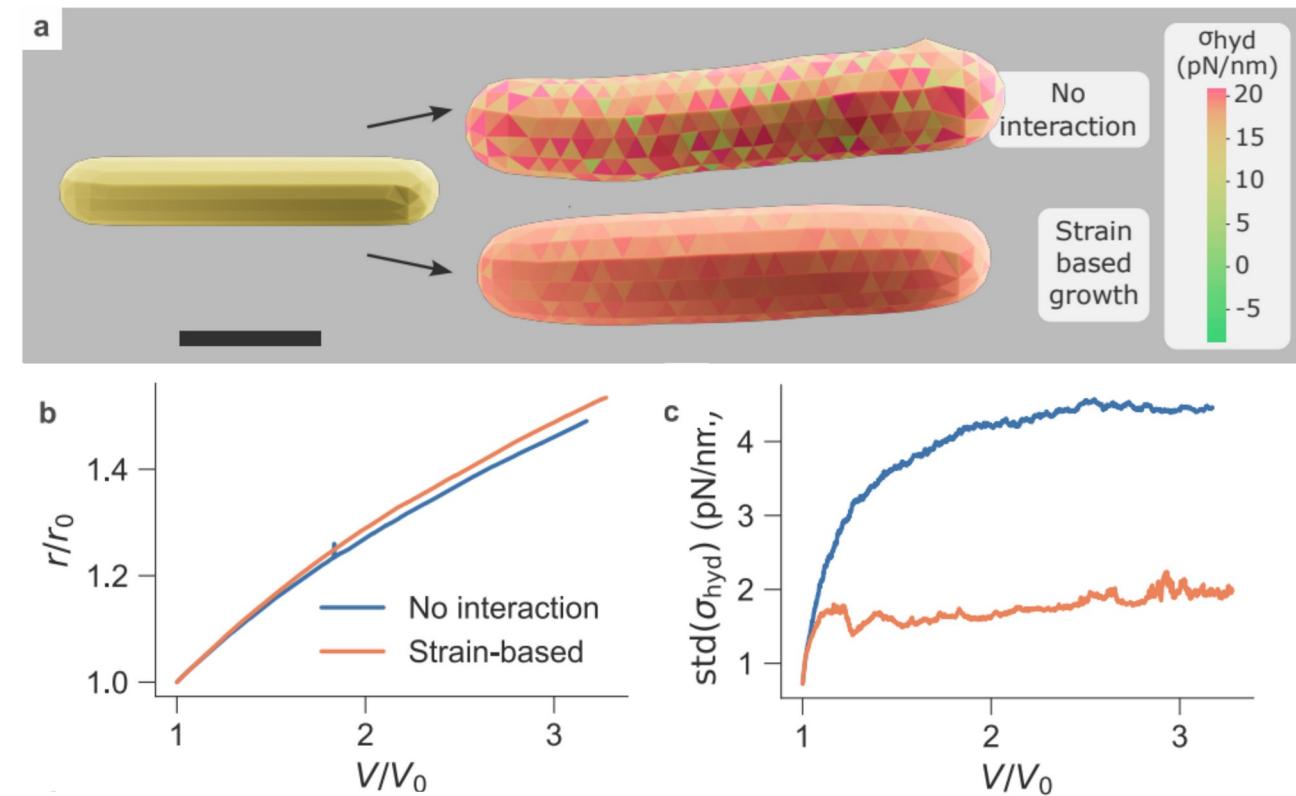
Random

- Spherical shape
- **High** stresses

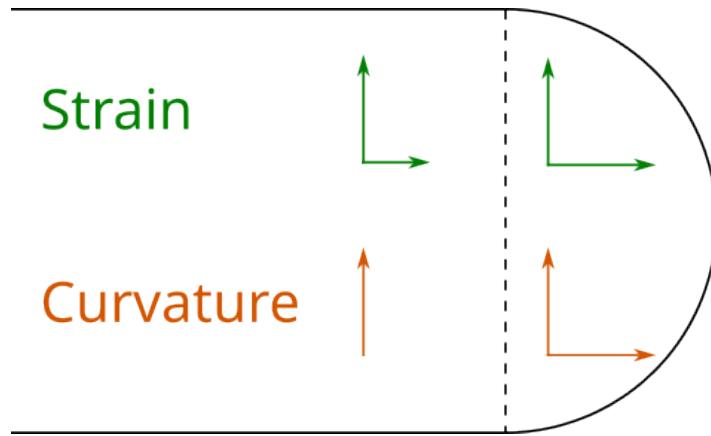
Strain-based

- Spherical shape
- **Moderate** stresses

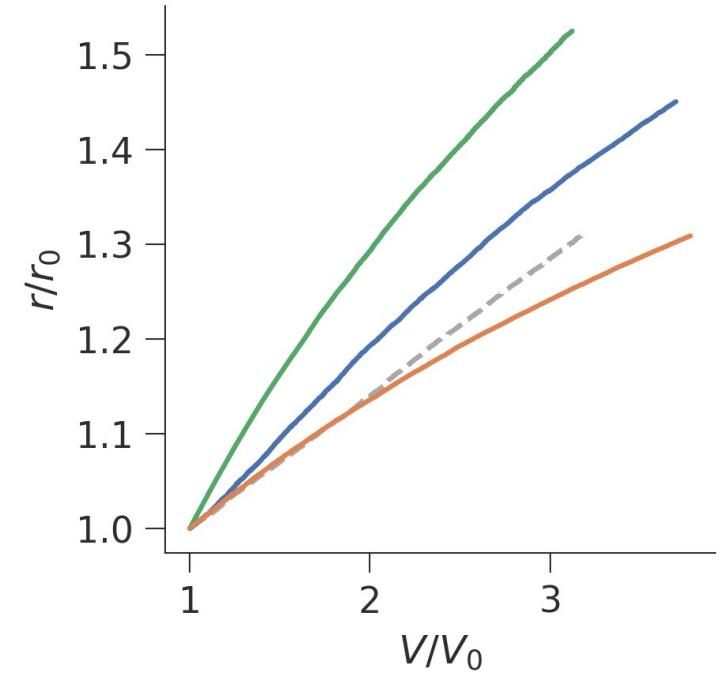
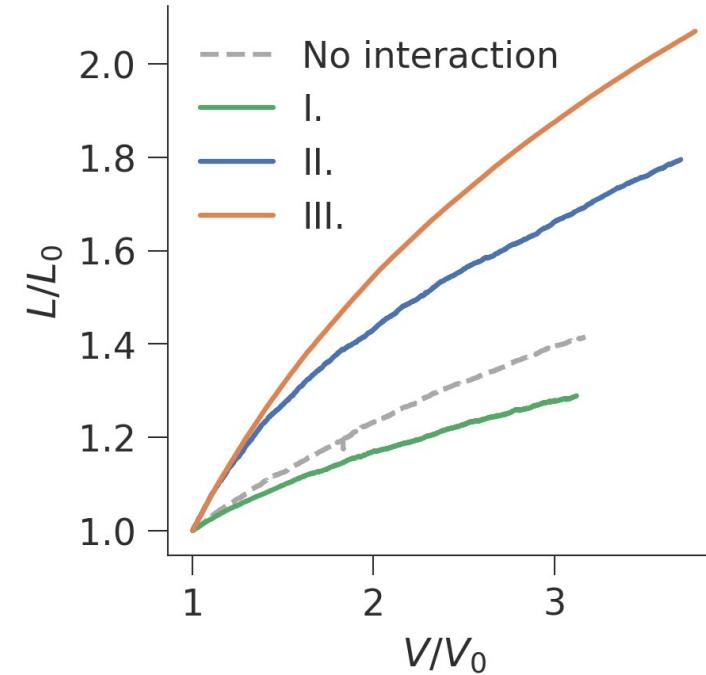
⇒ Radius is not conserved



# Directional Growth: Strain / Curvature



	Location	Direction
I.	Strain	Strain
II.	Curvature	Strain
III.	Curvature	Curvature

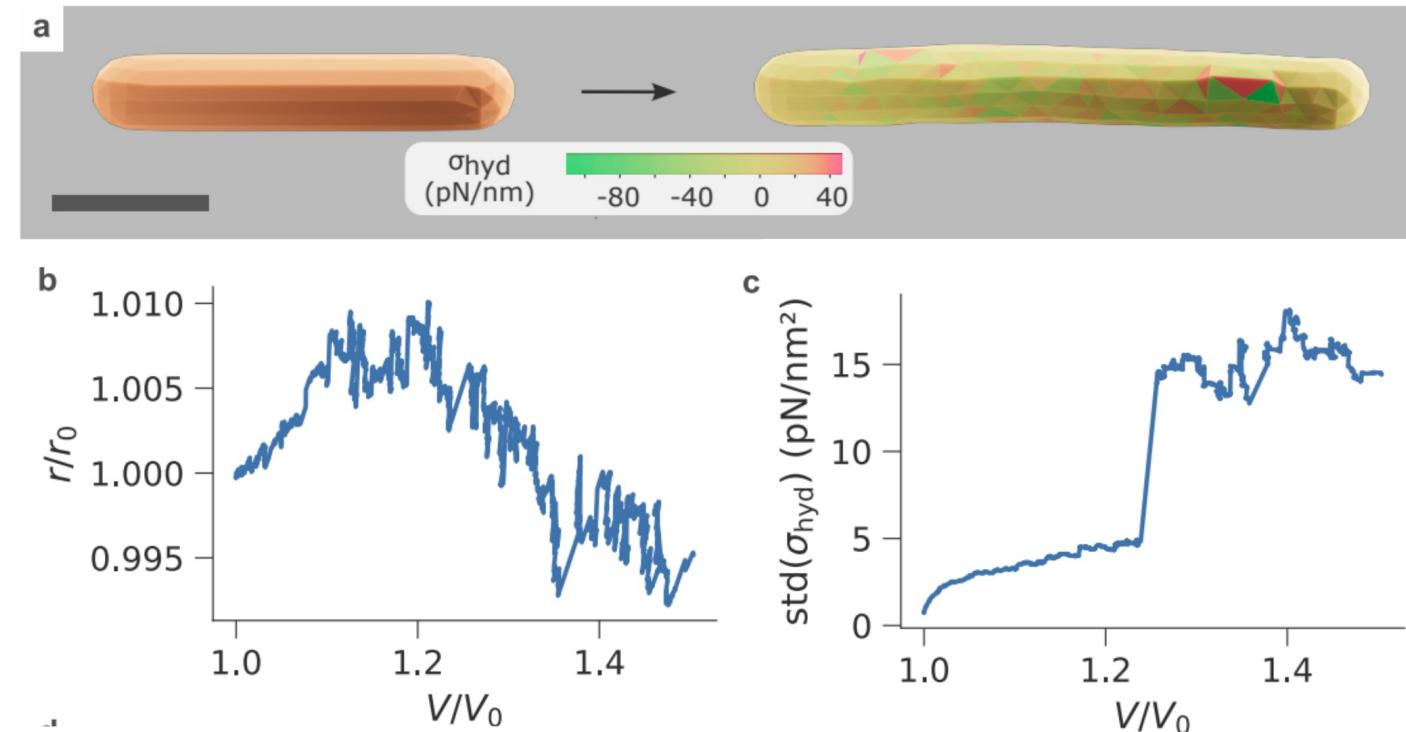


# Correction mechanism

## Combination

longitudinal: +  
circumferential: -

- Elongation
- Radius is conserved
- Problem: Large stresses



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# Summary

- Implemented two physical models of the bacterial shell
- Limitations of the spring-based model
- Solved with finite-element-based model
- Strain-based growth improved the mechanical stability
- Importance of a correction mechanism

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# Outlook

- Understanding high stresses
- Explore the parameter space
  - Gram-positive bacteria: Higher pressures, thicker cell wall
  - Pressure changes during growth
- Explore other geometries

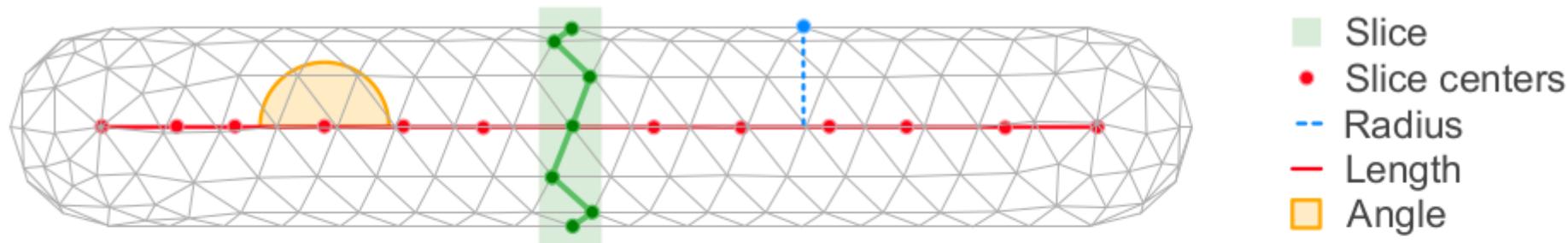
Thank you

# Appendix

$$Y=\frac{2}{\sqrt{3}}k_s,$$

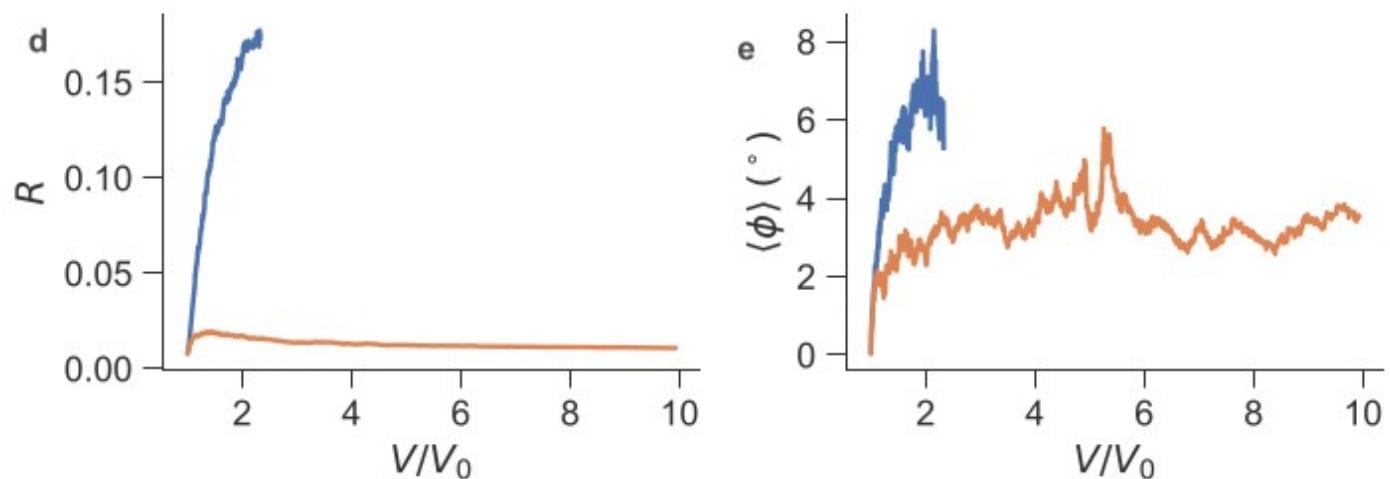
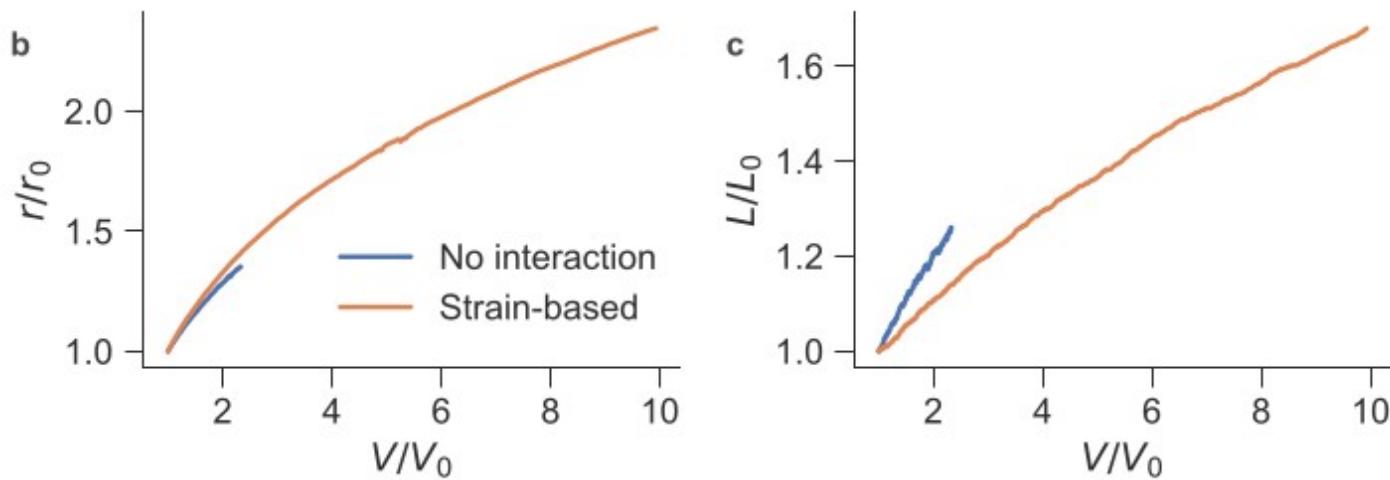
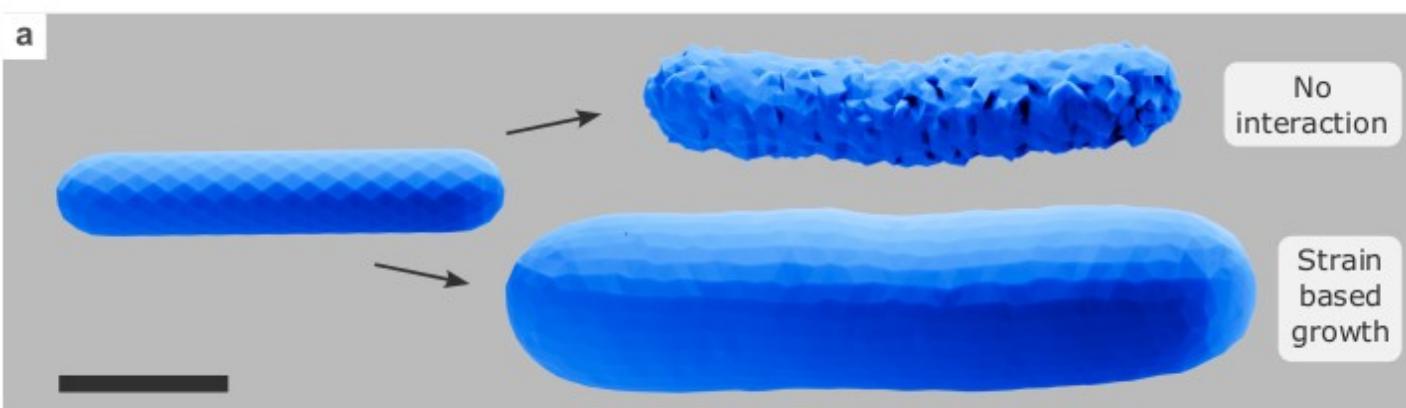
$$\kappa_{\rm b} = \frac{\sqrt{3}}{2} k_{\rm b},$$

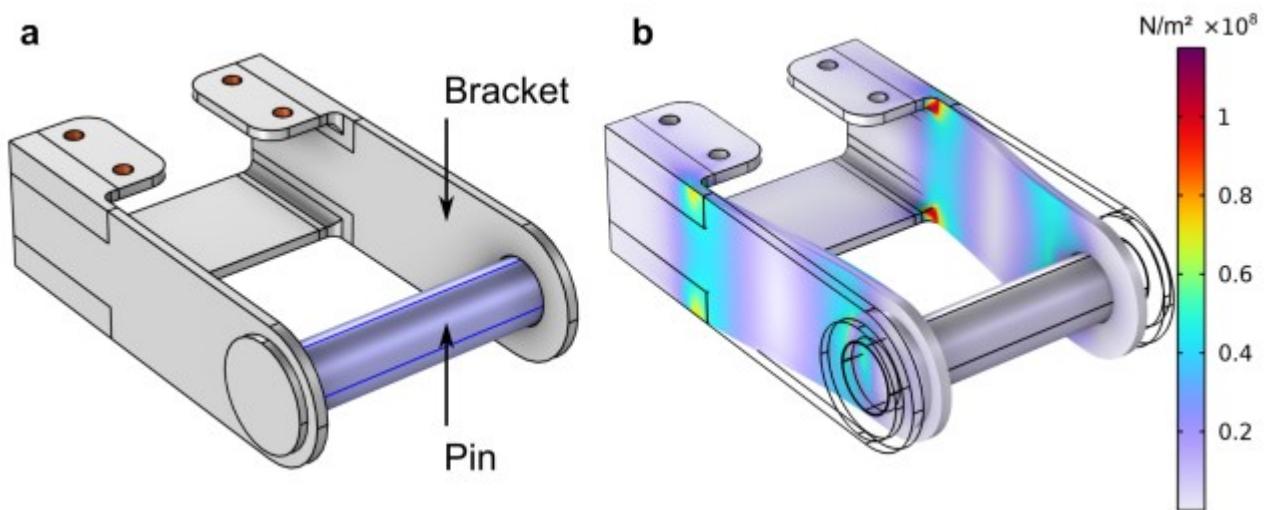
$$\kappa_b=\frac{Et^3}{12(1-\nu)}$$

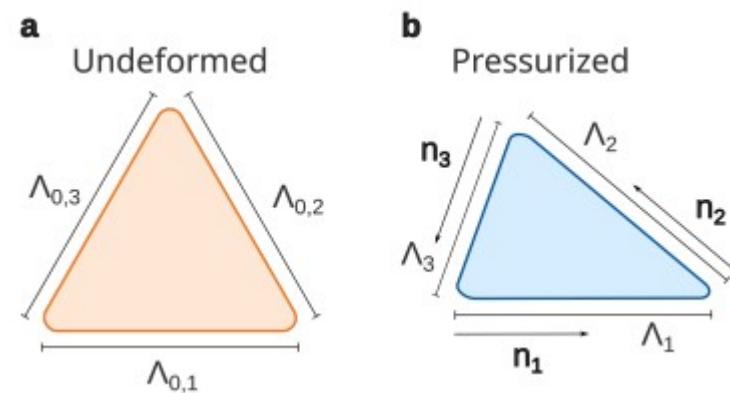


**Figure 2.3.4: Computing length, radius and bending angle of the rod-shaped shell.**

The shell is divided into slices (green) along its length. At initialization, each vertex is assigned a slice. The gravitational centers of the slices (red dots) can be computed at any point in the simulation. Radius, length and bending angles are computed from the line connecting the slice centers.



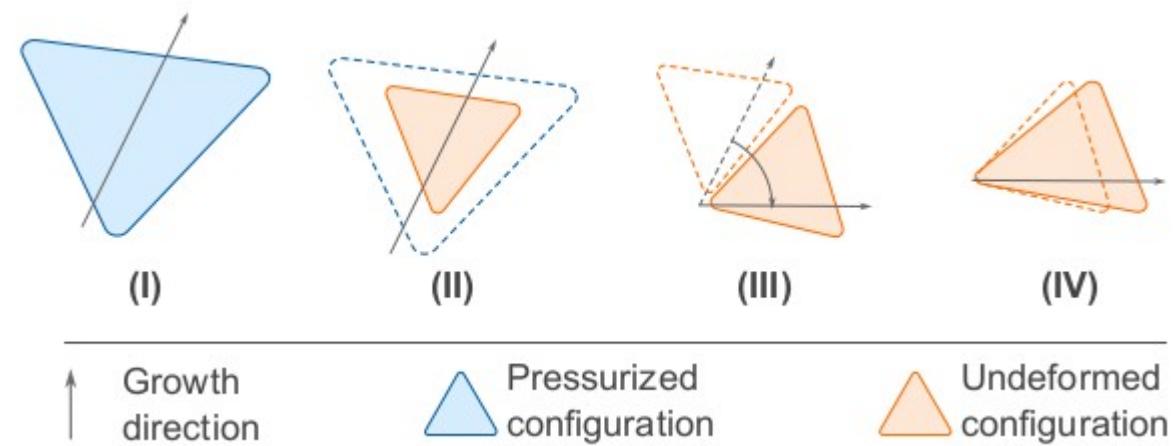


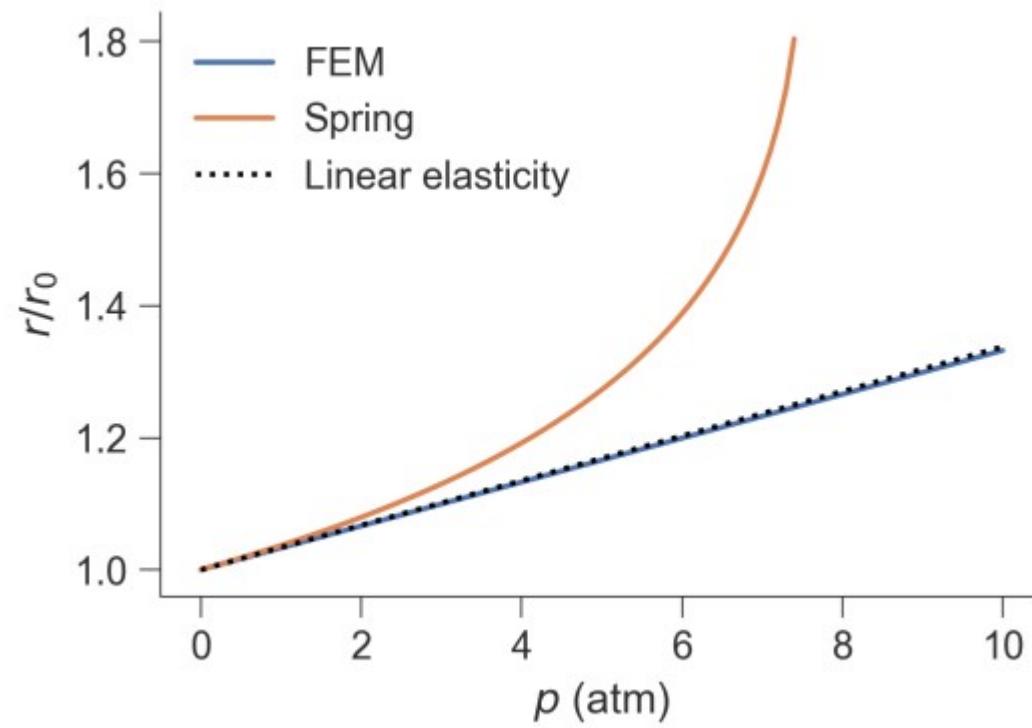


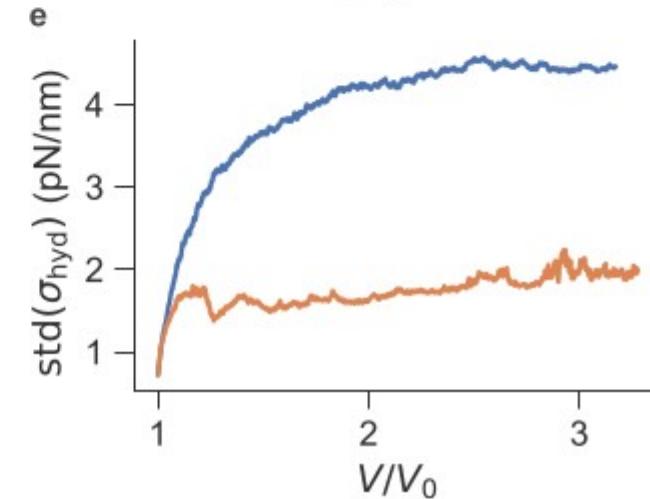
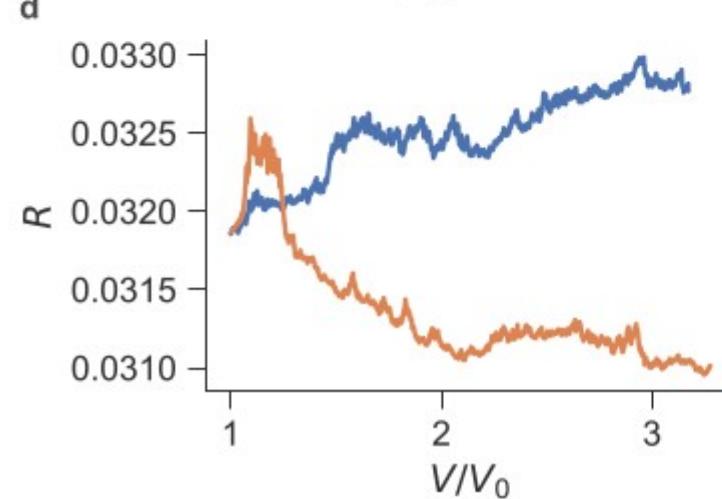
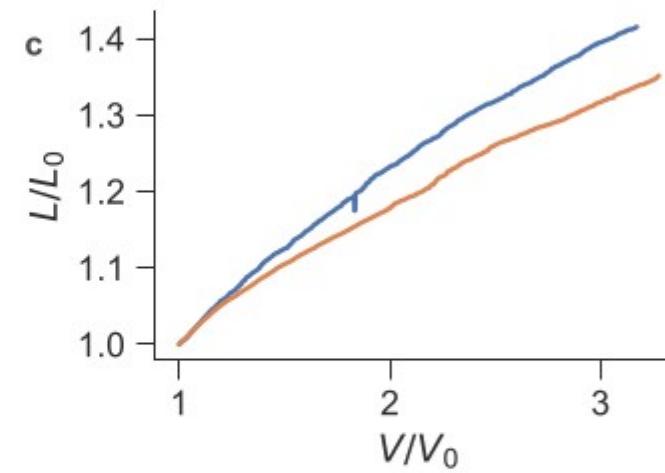
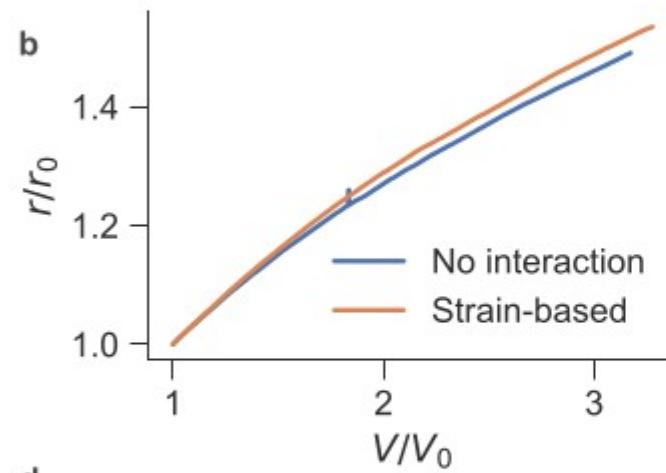
$$\varepsilon(\vec{n}^{(i)}) = \frac{\Lambda_i - \Lambda_{i,0}}{\Lambda_i}$$

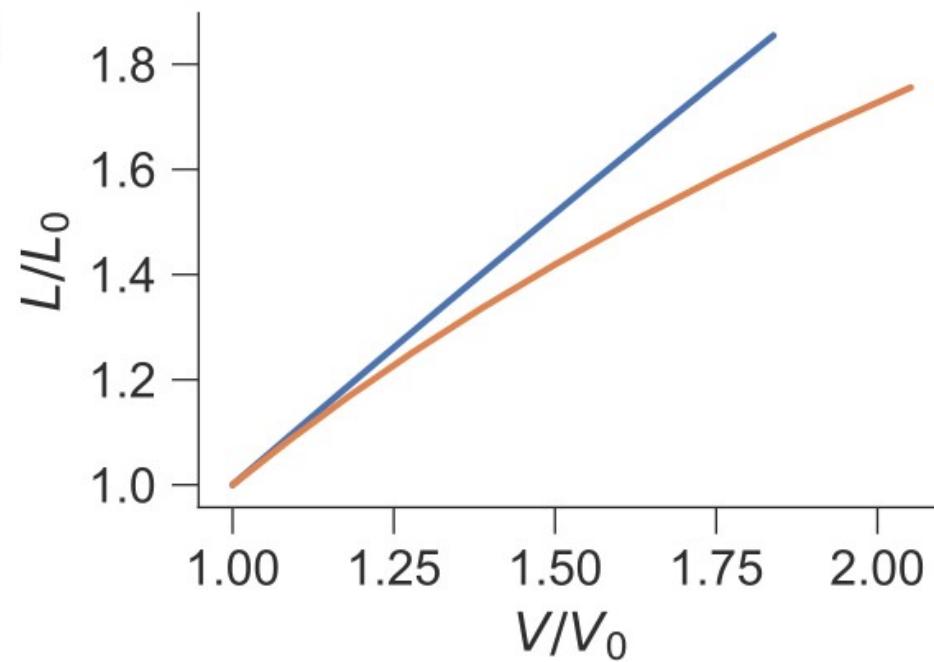
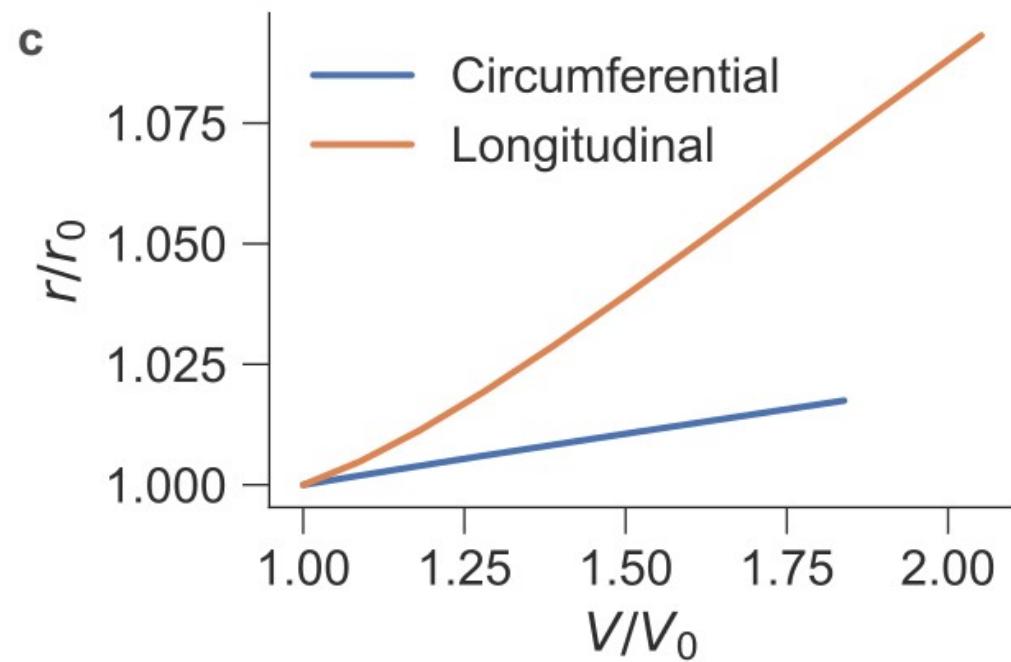
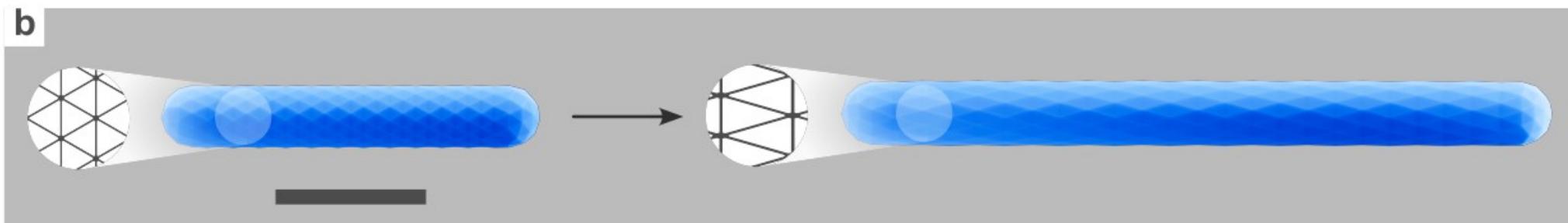
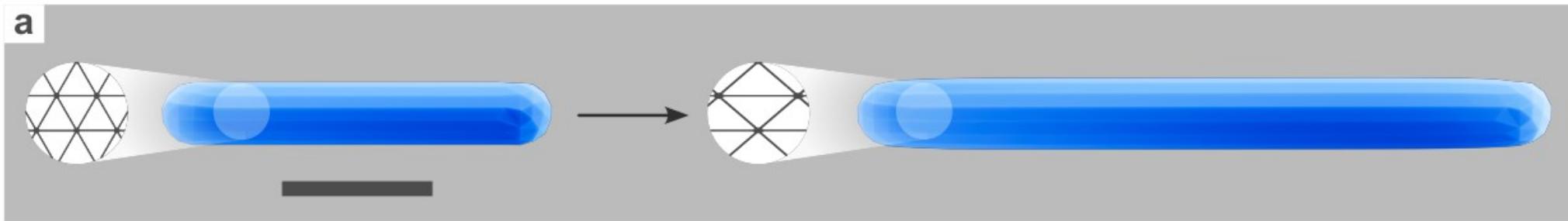
$$\varepsilon_{\text{direction}}(\vec{n}^{(i)}) = \varepsilon_{kl} n_k^{(i)} n_l^{(i)},$$

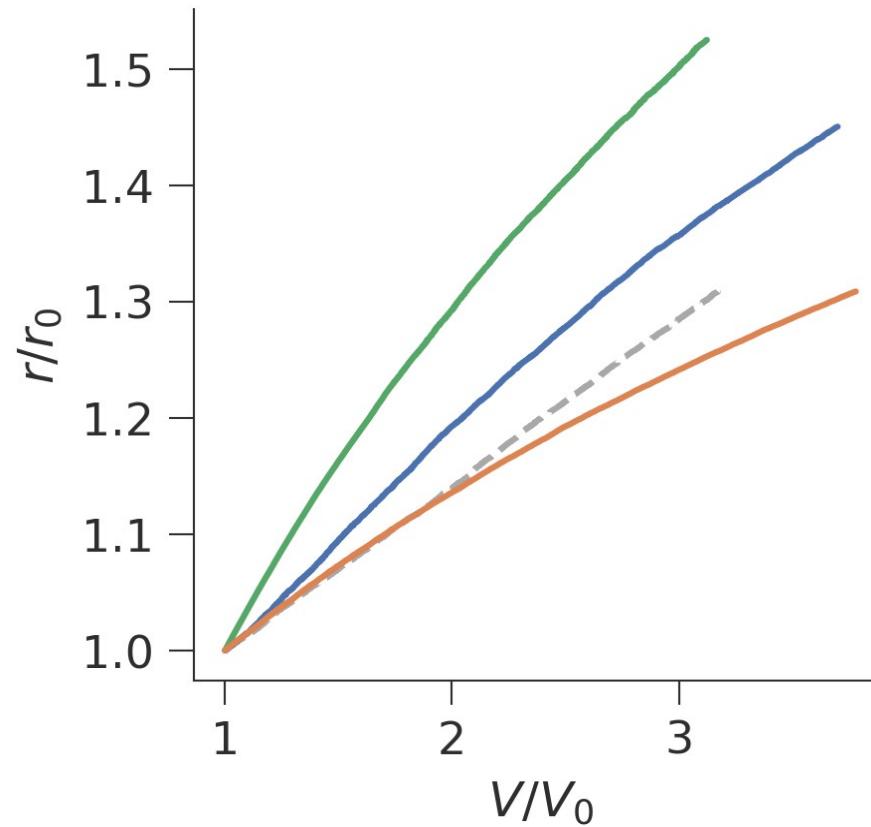
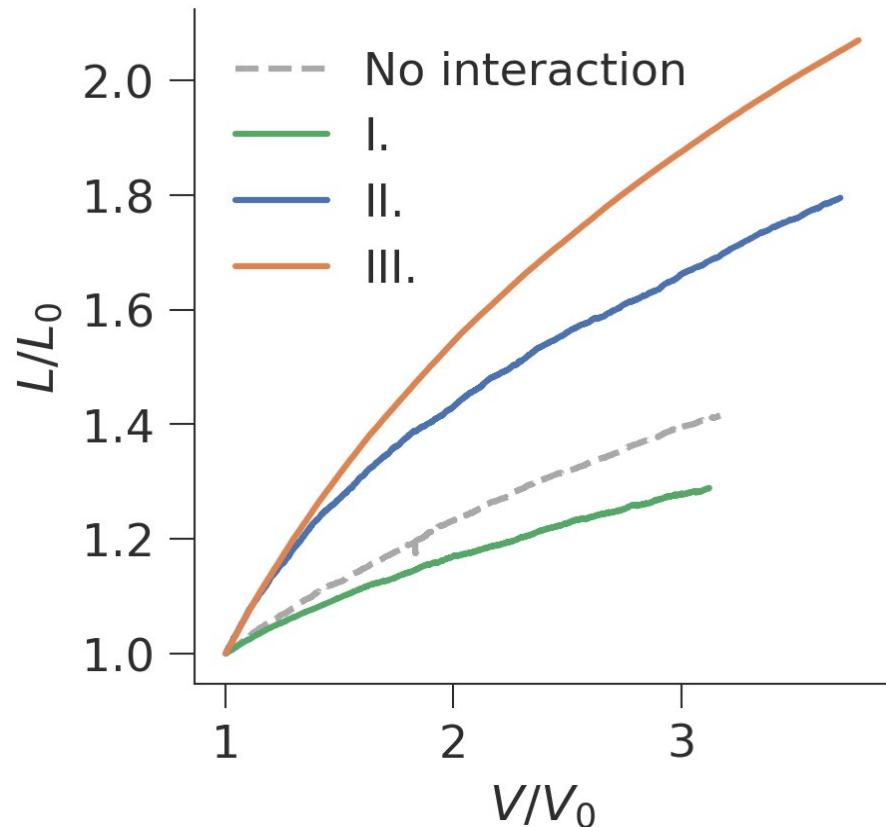
$$\begin{bmatrix} \varepsilon_{\text{direction}}(\vec{n}^{(1)}) \\ \varepsilon_{\text{direction}}(\vec{n}^{(2)}) \\ \varepsilon_{\text{direction}}(\vec{n}^{(3)}) \end{bmatrix} = \begin{bmatrix} n_1^{(1)} n_1^{(1)} & n_1^{(1)} n_2^{(1)} & n_2^{(1)} n_2^{(1)} \\ n_1^{(2)} n_1^{(2)} & n_1^{(2)} n_2^{(2)} & n_2^{(2)} n_2^{(2)} \\ n_1^{(3)} n_1^{(3)} & n_1^{(3)} n_2^{(3)} & n_2^{(3)} n_2^{(3)} \end{bmatrix} \cdot \begin{bmatrix} \varepsilon_{11} \\ 2\varepsilon_{12} \\ \varepsilon_{22} \end{bmatrix}$$



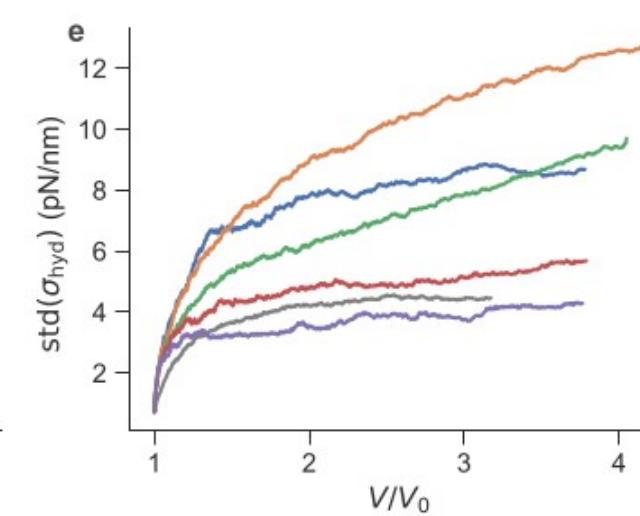
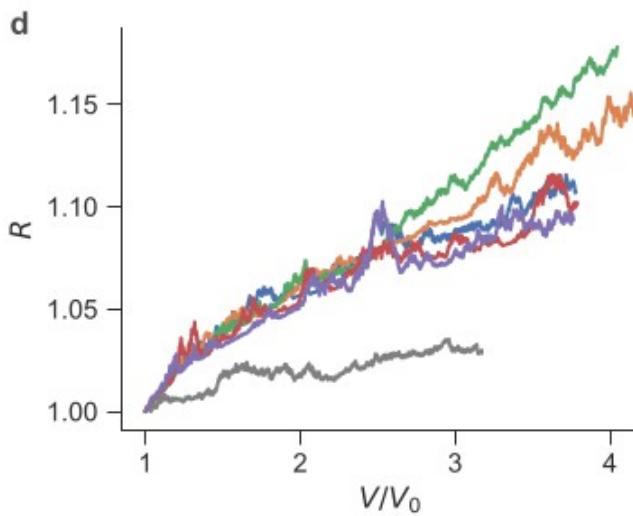
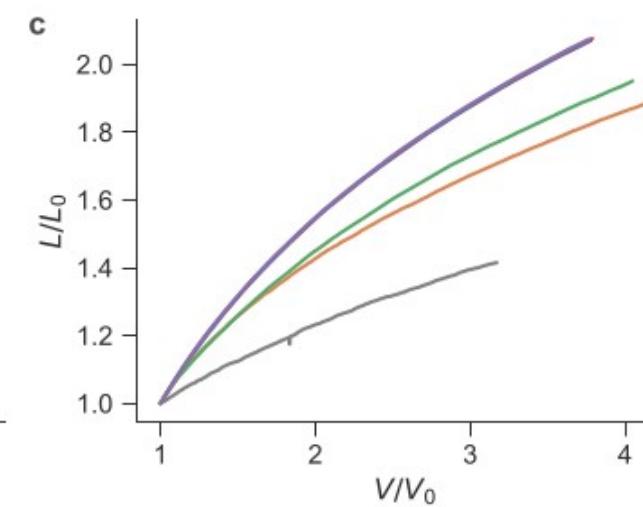
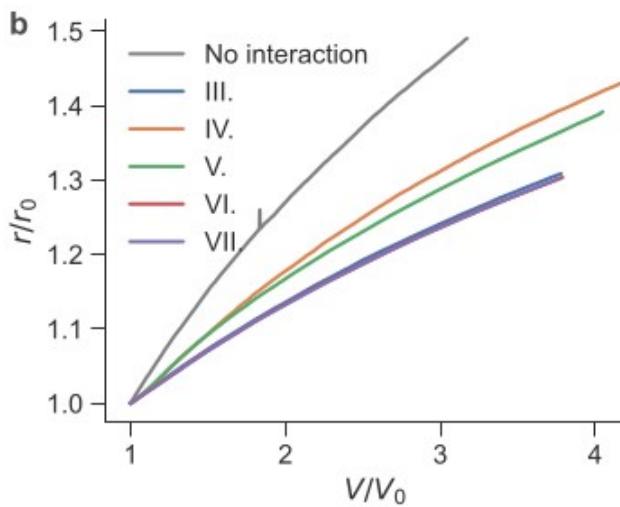
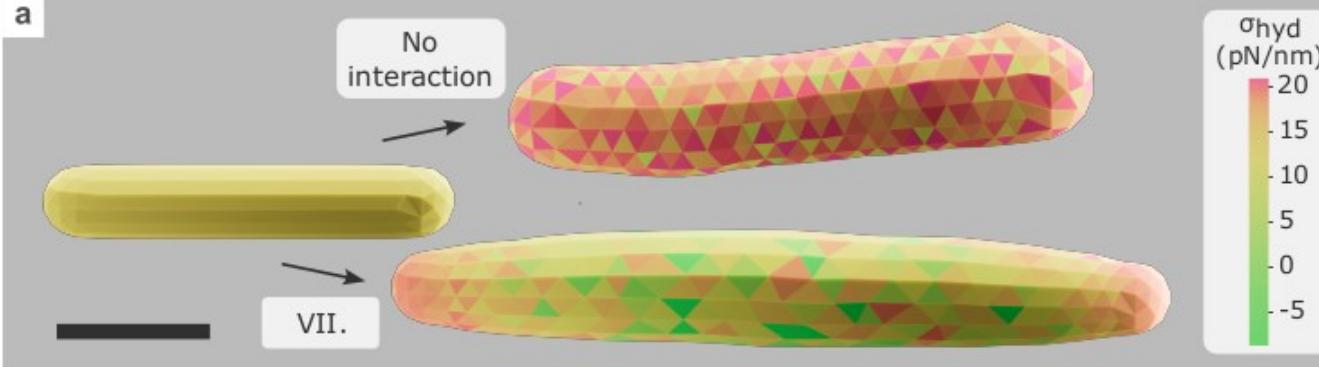








Growth reaction rates		Growth direction
I.	$\lambda_0 + \lambda_1 \varepsilon_{\min} - \lambda_2 \varepsilon_{\max}$	$\varepsilon_{\min}$
II.	$\lambda_0 + \lambda_1 K_{\min}$	$\varepsilon_{\min}$
III.	$\lambda_0 + \lambda_1 K_{\min}$	$K_{\min}$

**a**

	Growth reaction rates	Growth direction
IV.	$-\lambda_0 + \lambda_1 K_{\min} + \lambda_2 \varepsilon_{\text{hyd}}$	$\varepsilon_{\min}$
V.	$-\lambda_0 + \lambda_1 K_{\min} + \lambda_2 \varepsilon_{\min}$	$\varepsilon_{\min}$
VI.	$-\lambda_0 + \lambda_1 K_{\min} + \lambda_2 \varepsilon_{\text{hyd}}$	$K_{\min}$
VII.	$-\lambda_0 + \lambda_1 K_{\min} + \lambda_2 \varepsilon_{\min}$	$K_{\min}$

