



Spacecraft Attitude Dynamics

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Attitude kinematics

Direction cosines - kinematics

Evolution with time of kinematics powerers — Because s/c is rotation with a given another velocity. How attitude parameters change with time, and how they are related to the angular velocity expressed in body frame

Evolution with time of kinematics powerers — Because s/c is rotation from the application of the contraction of the

Rule for sequence of rotations
in terms of time pooring the vociotion of phrihole
poorinters is represented by fl =0 direction conine.

 $A(t + \Delta t) = A'A(t)$

notation in su interval St - so of

$$A' = I \cos \phi + (1 - \cos \phi) \underline{e} \underline{e}^{T} - \sin \phi [\underline{e} \wedge]$$

$$\downarrow f \quad \phi \leftarrow I \qquad \qquad \phi$$

$$A' = I - \phi [\underline{e} \wedge]$$

short time intervals, φ small

$$\phi = \omega \Delta t \qquad \underline{\omega} = \omega \underline{e} \qquad \text{The direction of the enter axis and the radiation on the same this is true for instruction and the same this is true for
$$\phi[\underline{e} \wedge] = \omega \Delta t \qquad \underline{e} \qquad 0 \qquad -e_w \qquad e_v \\ \underline{e}_w \qquad 0 \qquad -e_u \\ \underline{-e}_v \qquad e_u \qquad 0 \qquad \underline{e} \qquad 0 \qquad -\omega_u \\ \underline{-\omega}_v \qquad \omega_u \qquad 0 \qquad \Delta t = \underline{[\underline{\omega} \wedge] \Delta t} = \underline{\phi}[\underline{e} \wedge]$$$$

Direction cosines - kinematics

$$A' = I - [\underline{\omega} \wedge] \Delta t$$
$$A(t + \Delta t) = A(t) - \Delta t [\underline{\omega} \wedge] A(t)$$

$$\frac{dA}{dt} = -\big[\underline{\omega} \wedge \big] A(t)$$

$$\frac{dA}{dt} = \lim_{\Delta t \to 0} \frac{A(t + \Delta t) - A(t)}{\Delta t} = \lim_{\Delta t \to 0} - \frac{\Delta t \big[\underline{\omega} \land \big] A(t)}{\Delta t} = - \big[\underline{\omega} \land \big] A(t)$$

Need to preserve the structure -> Use a standard numerical integration scheme

and orthonormalize the matrix at every time step using: - This is important to previous

If we find that the results of the integration is no larger a actualized matrix $A_{k+1}(t) = A_k(t)*3/2 - A_k(t)*A_k^T(t)*A_k(t)/2$ To orch the result reaching the closest possible anthogonal matrix we could see this Iterative approach. The preferming this at a constant the result reaching the closest possible anthogonal matrix we could see this Iterative approach.

If performing this at every time step a single iteration is normally enough:

evolytime step of the integration

$$A(t) = A_0(t) * 3/2 - A_0(t) * A_0^T(t) * A_0(t)/2$$

Euler axis / angle - kinematics

No rule for sequence of rotations -> no rule for kinematics

They are usefull for roppresering on or bit but it is not possible to find the evalution of exis and on the in time.

High he refull for evaluating the rues the.

Quaternion - kinematics

- s some logic of the direction wine water approach.

$$q(t + \Delta t) = \begin{bmatrix} q'_4 & q'_3 & -q'_2 & q'_1 \\ -q'_3 & q'_4 & q'_1 & q'_2 \\ q'_2 & -q'_1 & q'_4 & q'_3 \\ -q'_1 & -q'_2 & -q'_3 & q'_4 \end{bmatrix} q(t)$$
 with
$$\begin{cases} q'_1 = e_u \sin \frac{\phi}{2} \\ q'_2 = e_v \sin \frac{\phi}{2} \\ q'_3 = e_w \sin \frac{\phi}{2} \\ q'_4 = \cos \frac{\phi}{2} \end{cases}$$

$$q(t+\Delta t) = \left\{ I\cos\frac{\phi}{2} + \begin{bmatrix} 0 & e_w & -e_v & e_u \\ -e_w & 0 & e_u & e_v \\ e_v & -e_u & 0 & e_w \\ -e_u & -e_v & -e_w & 0 \end{bmatrix} \sin\frac{\phi}{2} \right\} q(t)$$

Quaternion - kinematics

short intervals
$$\Delta t$$

$$\qquad \Longrightarrow \qquad$$

$$\phi = \omega \Delta t$$

$$cos \frac{\phi}{2} = 1$$

$$\phi = \omega \Delta t$$
 $\cos \frac{\phi}{2} = 1$ $\sin \frac{\phi}{2} = \frac{\phi}{2} = \frac{\omega \Delta t}{2}$

evaluate e_{uv} , e_{vv} , e_{wv} , as a function of $\underline{\omega} = \omega \underline{e}$

$$q(t + \Delta t) = \left[I + \frac{1}{2} \Omega \Delta t\right] q(t)$$

$$\Omega = \begin{bmatrix} 0 & \omega_w & -\omega_v & \omega_u \\ -\omega_w & 0 & \omega_u & \omega_v \\ \omega_v & -\omega_u & 0 & \omega_w \\ -\omega_u & -\omega_v & -\omega_w & 0 \end{bmatrix}$$

limit for $t \rightarrow 0$

$$\frac{dq}{dt} = \lim_{\Delta t \to 0} \frac{q(t + \Delta t) - q(t)}{\Delta t} = \frac{1}{2} \Omega q(t)$$

Gibbs vector - kinematics

$$g(t + \Delta t) = \frac{\underline{g}(t) + \underline{g}' - \underline{g}' \wedge \underline{g}(t)}{1 - \underline{g}(t) \cdot \underline{g}'}$$

$$\underline{g}' = \underline{e} \tan \frac{\phi}{2} = \xrightarrow{small \ \Delta t} = \frac{1}{2} \underline{\omega} \Delta t$$

$$\frac{dg}{dt} = \frac{1}{2} \Big[\underline{\omega} - \underline{\omega} \wedge \underline{g}(t) + \Big(\underline{g}(t) \cdot \underline{\omega} \Big) \underline{g}(t) \Big]$$

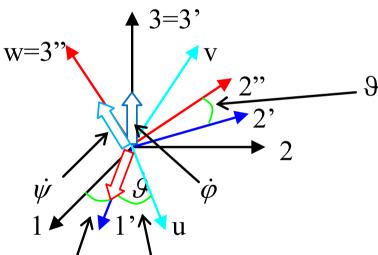
Euler angles - kinematics

no convenient rule for combining two consecutive rotations

consider the sequence 313 (ϕ, θ, ψ)

This directions one maturally orthogonal but we can something to be before the rector w

 $\underline{\omega} = \dot{\phi}\underline{3} + \dot{\vartheta}\underline{1}' + \dot{\psi}\underline{w}$



Euler angles - kinematics

$$\underline{\omega} = \dot{\phi}\underline{3} + \dot{\vartheta}\underline{1}' + \dot{\psi}\underline{w} \qquad \qquad \qquad \begin{cases} \omega_{u} = \underline{\omega} \cdot \underline{u} = \dot{\phi}\underline{3} \cdot \underline{u} + \dot{\vartheta}\underline{1}' \cdot \underline{u} + \dot{\psi}\underline{w} \cdot \underline{u} = \dot{\phi}\underline{3} \cdot \underline{u} + \dot{\vartheta}\underline{1}' \cdot \underline{u} \\ \omega_{v} = \underline{\omega} \cdot \underline{v} = \dot{\phi}\underline{3} \cdot \underline{v} + \dot{\vartheta}\underline{1}' \cdot \underline{v} + \dot{\psi}\underline{w} \cdot \underline{v} = \dot{\phi}\underline{3} \cdot \underline{v} + \dot{\vartheta}\underline{1}' \cdot \underline{v} \\ \omega_{w} = \underline{\omega} \cdot \underline{w} = \dot{\phi}\underline{3} \cdot \underline{w} + \dot{\vartheta}\underline{1}' \cdot \underline{w} + \dot{\psi}\underline{w} \cdot \underline{w} \end{cases}$$

$$\underline{3} \underline{u}, \underline{3} \underline{v}, \underline{3} \underline{w}$$
 third column of matrix A_{313}

$$\underline{1}$$
' \underline{u} , $\underline{1}$ ' \underline{v} , $\underline{1}$ ' \underline{w} first column of matrix A_{313} if $\varphi = 0$

Euler angles - kinematics

Direct Cosine Matrices (DCM)

Advantages

- Singularity free.
- Uniquely defines every possible rotation.
- Intuitive.

Disadvantages

- 9 components to evaluate.
- Requires orthonormalization during integration.

Euler axis / angle ? Quaternion ? Gibbs vector ? Euler angles ?