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Spacecraft Attitude Dynamics

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Attitude sensors

Sun sensor

feature: - horizon sensor could detect the body of a celestial body with a big angular dimension such as it is possible to detect the position and the dimensions of a celestial body.

- Sun sensor will detect only a point source (first approx)

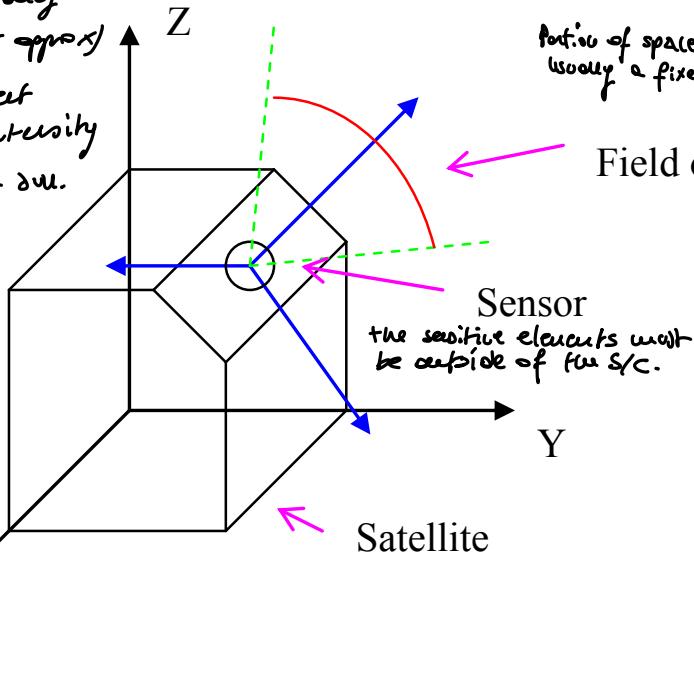
- Sun sensor will detect star with a light intensity much lower than the sun. Star as point source

- magnetic field sensor depend on the accuracy of the model are greatly useful

- Inertial sensor gyroscope, raid sensor

more general

-(gps, Galileo, GLONASS, BEIDOU) GNSS → allows receiver to detect it's own position
↳ not diff, problem with accuracy.

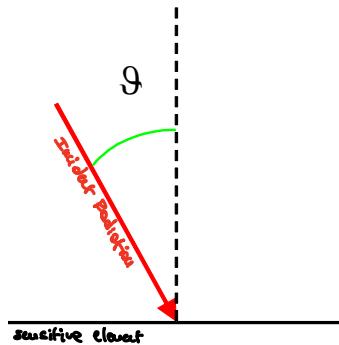


portion of space seen by the sensor →
usually a fixed characteristic $\Rightarrow \Omega < 180^\circ$
↑ because there is the S/C on
the other end.
Field of View

Some of the feature of
the sun sensor are common
between sensor that need
to identify celestial body.



Sun sensor \rightarrow work on the basis of photoelectric effect



constant that depends on the surface

$$I = I_0 \cos \theta = \alpha S W \cos \theta$$

Photo electric effect

The sensor becomes less and less accurate as the angle of viewing θ grows \rightarrow The cosine law is valid for an angle up to $\pm 60^\circ$ and then it is not accurate enough beyond that. That is still sufficient because they can give us a field of view of 120° .

On the base of this sensor we can design and build different kind of sensor.

Solar presence sensor

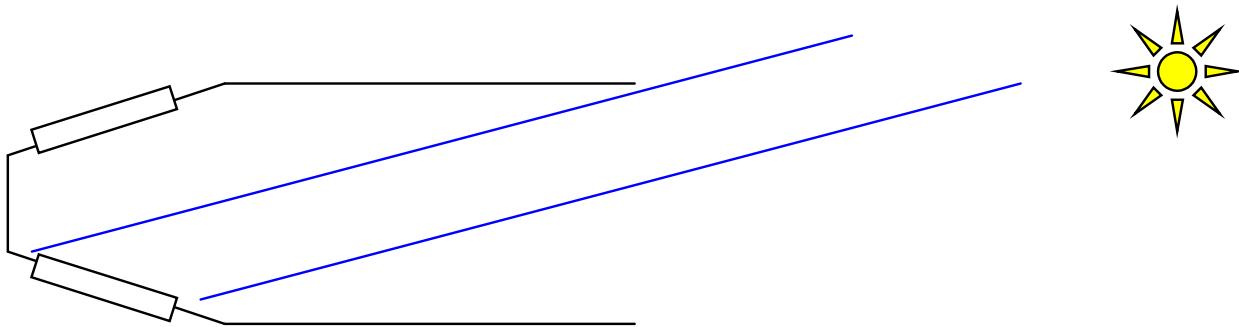
and

Sun sensor

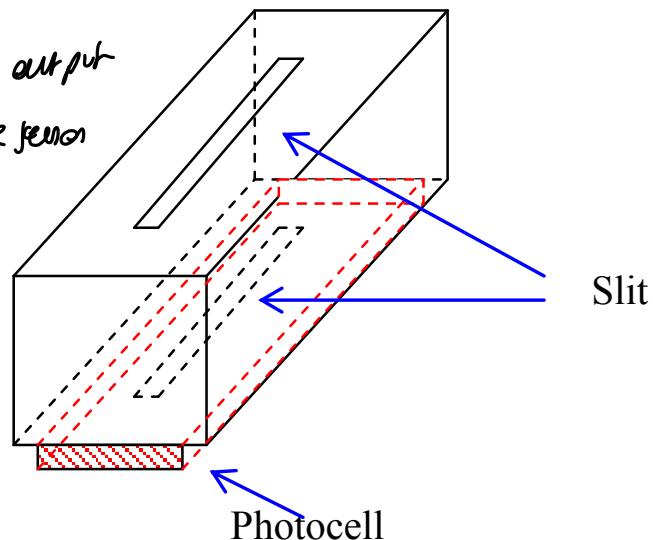
are narrow for and they
give the information of the
presence of the sun in the
narrow field of view.



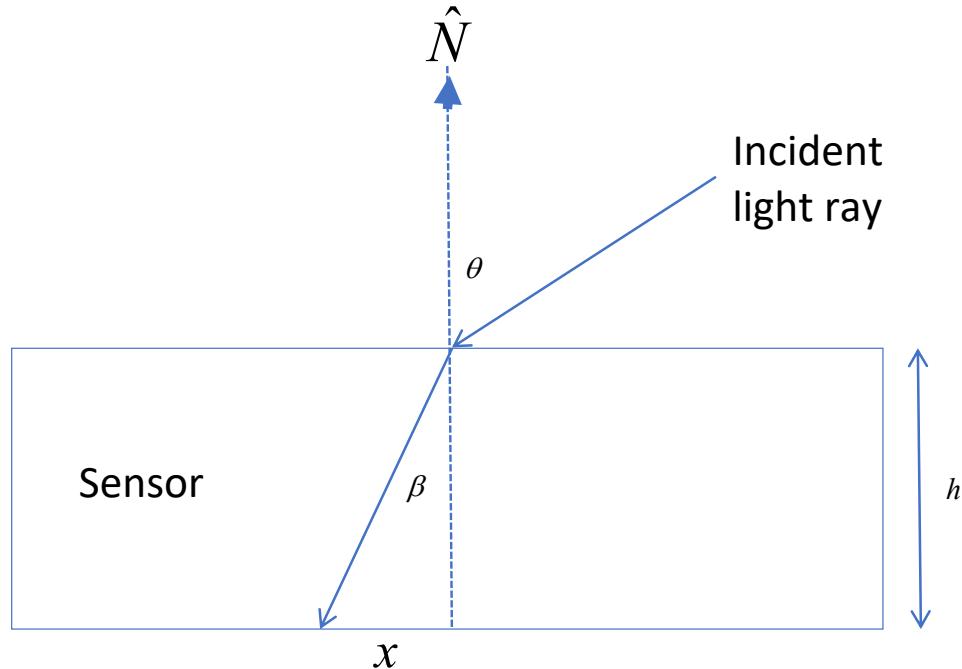
Sun presence sensor



We used to need a precise measurement of the output of the cell \rightarrow we need to know only if the sensor see the Sun.



Sun sensor



Snell's law

Need to take into account that
to interpret correctly the output
of the photodiode

$$n \sin \beta = \sin \theta$$

direction of the incoming radiation

n is the refractive index
La Keckle

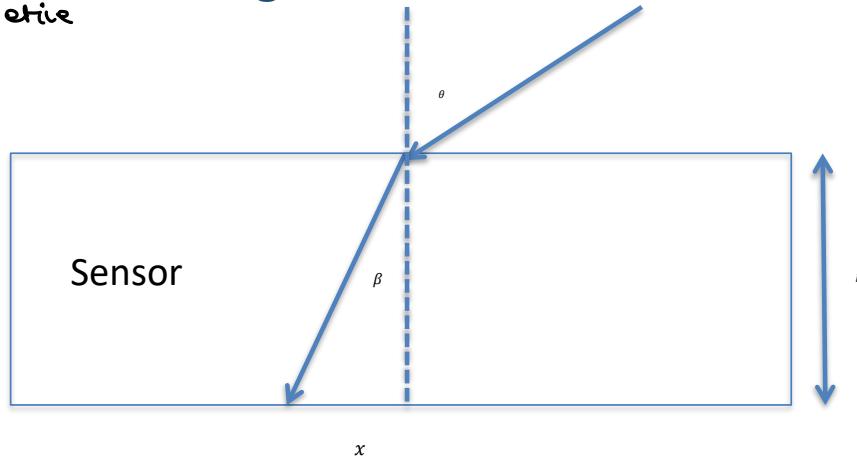


Sun Sensors for computing the Sun angle

we do not know if θ is positive or negative

$$\hat{N}_i \cdot \underline{s} = \cos \theta_i$$

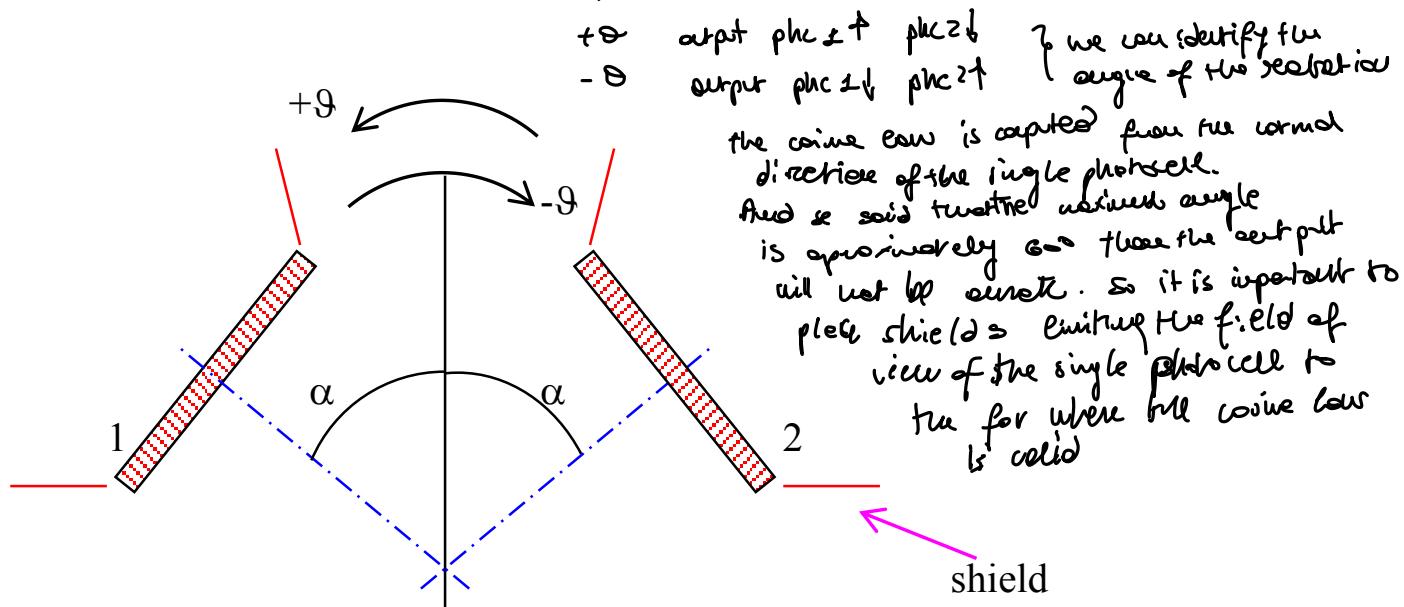
$$\begin{bmatrix} \cos \theta_1 \\ \cos \theta_2 \\ \cos \theta_3 \end{bmatrix} = \begin{bmatrix} \hat{N}_1 \cdot \underline{s} \\ \hat{N}_2 \cdot \underline{s} \\ \hat{N}_3 \cdot \underline{s} \end{bmatrix} = \begin{bmatrix} \hat{N}_1^T \\ \hat{N}_2^T \\ \hat{N}_3^T \end{bmatrix} \underline{s}$$



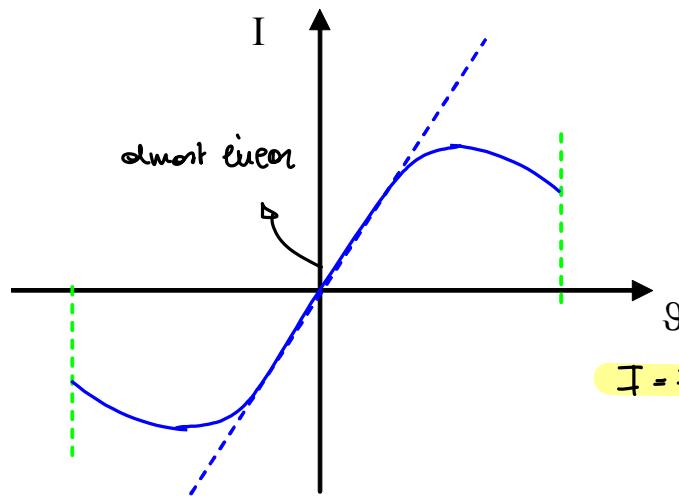
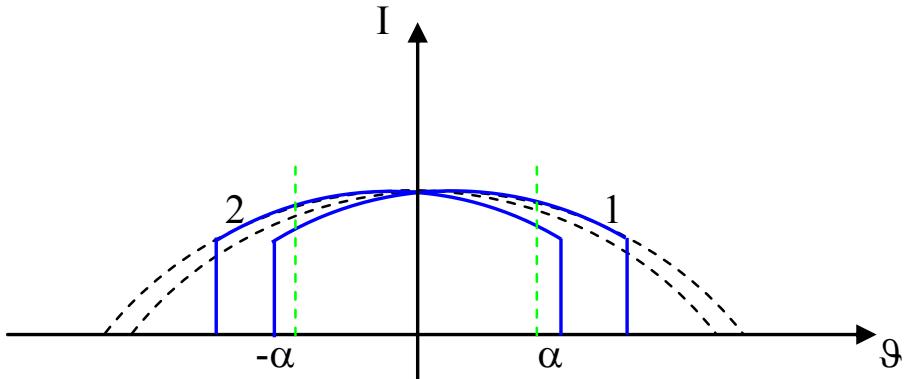
$$\underline{s} = \begin{bmatrix} \hat{N}_j^T \\ \hat{N}_k^T \\ \hat{N}_l^T \end{bmatrix}^{-1} \begin{bmatrix} \cos \sqrt{3} x_j / h \\ \cos \sqrt{3} x_k / h \\ \cos \sqrt{3} x_l / h \end{bmatrix}$$



Analog Sun Sensors \rightarrow if we place two photodiodes inclined w.r.t to one another we will see that



Analog Sun Sensors

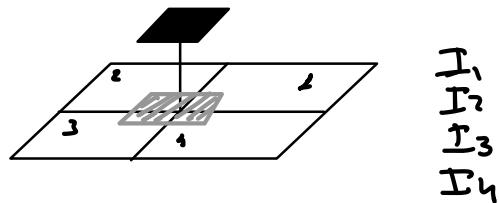
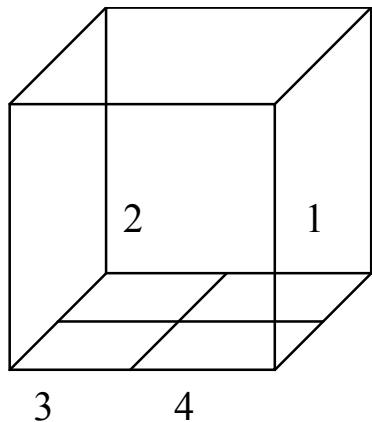


$$\begin{aligned}I &= \cos(\vartheta - \alpha) - \cos(\vartheta + \alpha) \\&= \cos \vartheta \cos \alpha + \sin \vartheta \sin \alpha - \cos \vartheta \cos \alpha \\&\quad + \sin \vartheta \sin \alpha = 2 \sin \vartheta \sin \alpha = k \cdot \sin \vartheta\end{aligned}$$

$$I = I_1 + I_2$$



Analog Sun Sensors \rightarrow Another type of sensor, using a photodiode element
 we can calculate the position of the sun.
 The sun position depends on the position of the
 shadow that will reduce the intensity
 output of the four cells.



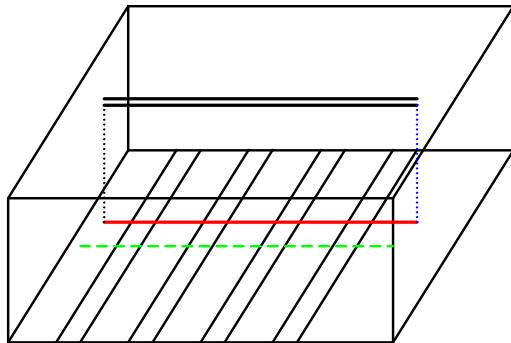
$$I = cA_0 \cdot i \cdot nA_0 = f(\vartheta, \phi) \rightarrow \text{then we will need to calculate the direct reflection from the direct function.}$$

$$(\vartheta, \phi) \rightarrow I \text{ direct}$$

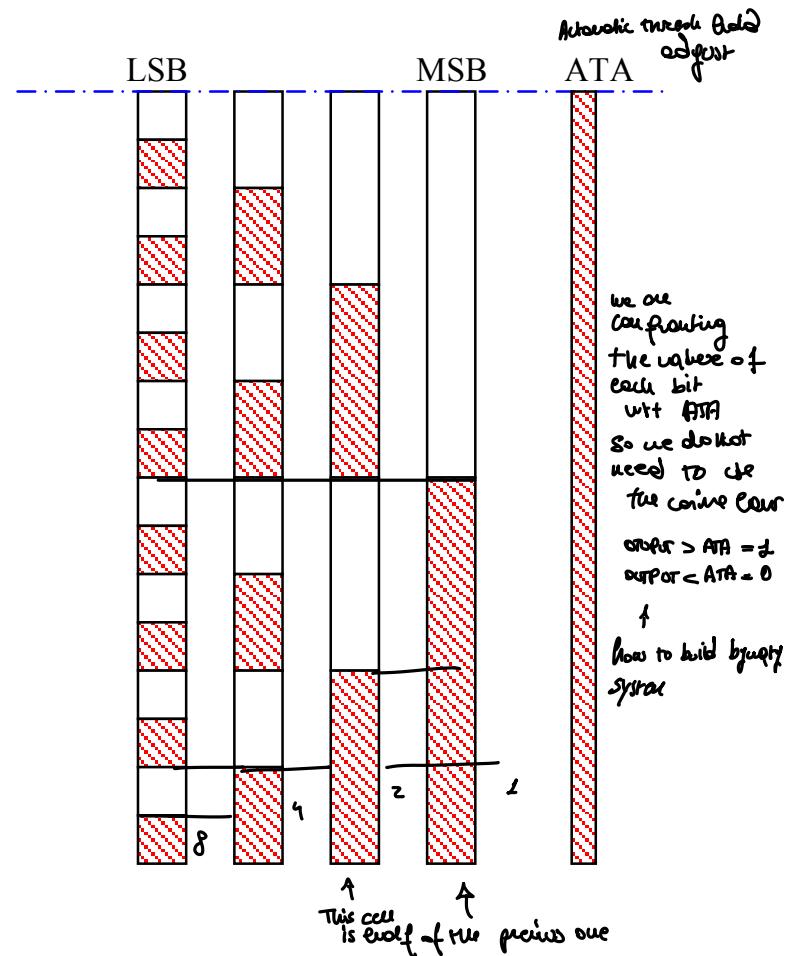
$$I \rightarrow \vartheta, \phi \text{ direct.}$$



Digital Sun Sensors



The main drawback of this method is when the Sun is in a middle position - between a cover part and not cover part \Rightarrow transitional shade. This is a problem because we have uncertainty due to some random noise that it is added.

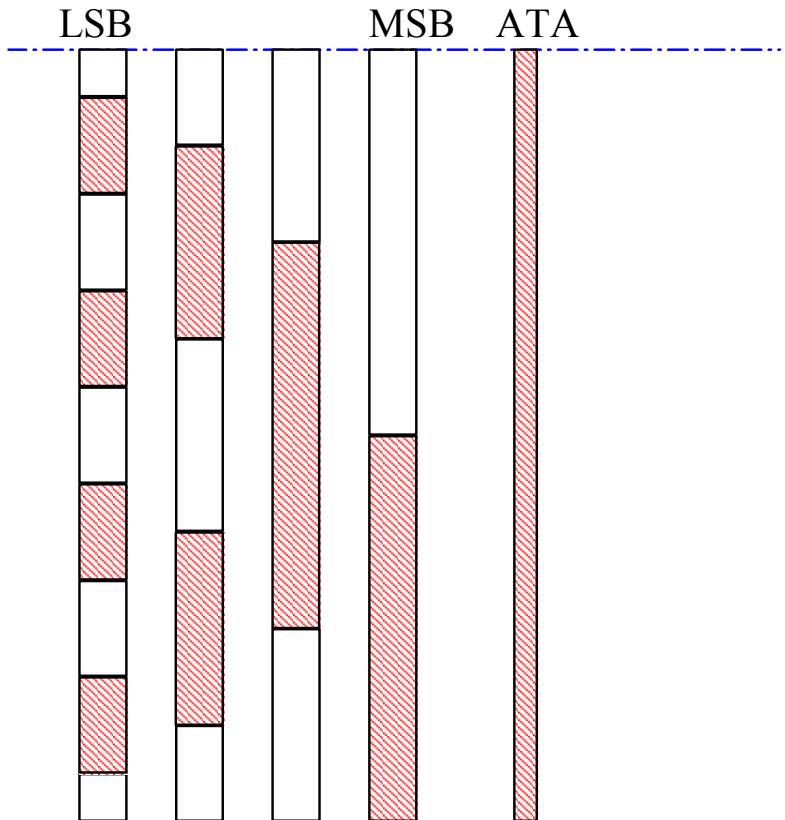


Digital Sun Sensors

⇒ Autometric threshold adjust does not depends
on the cosine law!

| Analog | Binary | Gray |
|--------|--------|------|
| 0 | 0000 | 0000 |
| 1 | 0001 | 0001 |
| 2 | 0010 | 0011 |
| 3 | 0011 | 0010 |
| 4 | 0100 | 0110 |
| 5 | 0101 | 0111 |
| 6 | 0110 | 0101 |
| 7 | 0111 | 0100 |
| 8 | 1000 | 1100 |

↳ Rule to convert binary value to a
integer

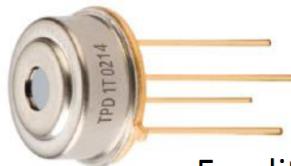


With 7 bits we have 64 degrees FOV, with 8 bits 128 degrees FOV.



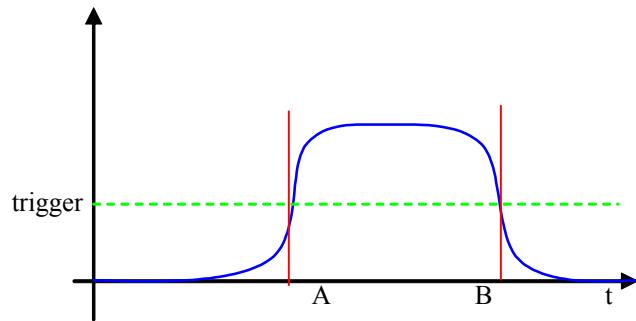
Earth horizon sensors – thermopile detector

The earth could cover up to 40% of the celestial sphere \rightarrow so we need to find the horizon of the sphere to determine its position.



Excelitas thermopile detector

TPD 1T 0214 G9 / 3850



- Thermopiles convert thermal energy into electrical energy \rightarrow Infrared wave \rightarrow emitted by the earth even during day
- Detect Earth's IR spectrum \hookrightarrow such that the ratio of Emissivity Sun / Emissivity Earth
- Two types of sensors (i) Scanning sensor FOV 7-10 deg (ii) Fixed pointing to Earth 60-70 deg
- IR sensors still work in an eclipse
so it is easier to find the edges of a planet.

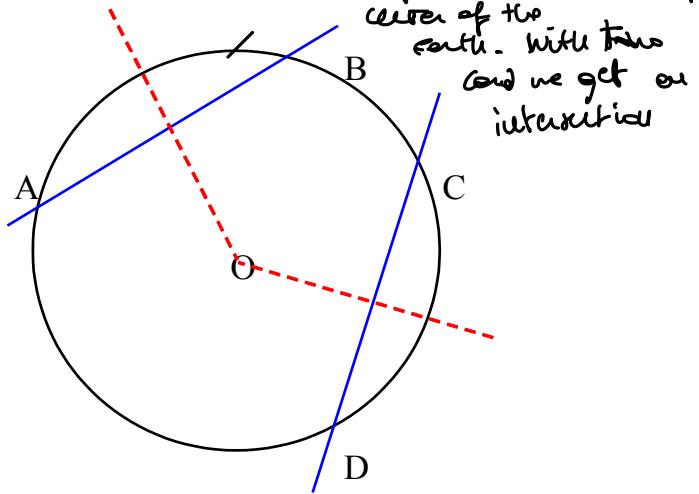
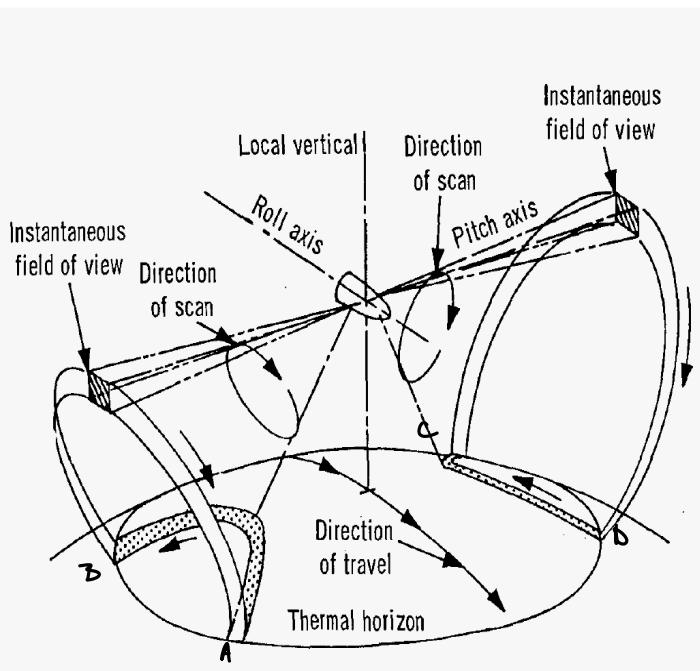


Scanning EH sensor

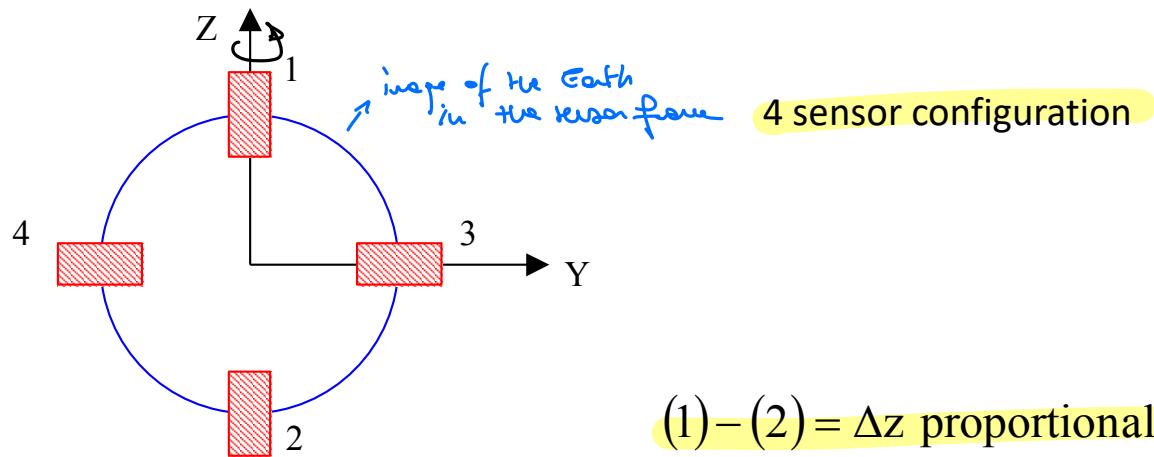
There are two types of sensor to detect horizons of celestial body -

Scanning EH sensors have a very narrow field of view → when we are detecting something for the first time or last time we are looking

→ detecting points. These four points given by two sensor tell us two cords → the angle between cords is the direction of the middle point center of the earth. With these and we get an intersection

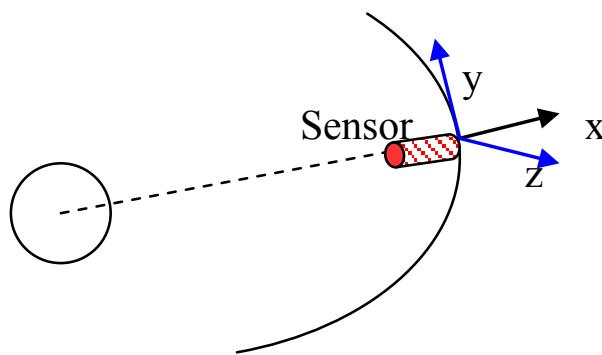


Horizon Sensors



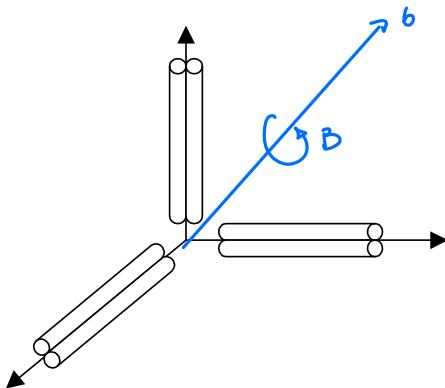
$$(1) - (2) = \Delta z \text{ proportional to } \alpha_y$$

$$(3) - (4) = \Delta y \text{ proportional to } \alpha_z$$



Attitude determination with a magnetometer

Using three pairs of nuclei, as shown below, we can measure the components of the magnetic field along three orthogonal directions, so the \mathbf{B} vector.



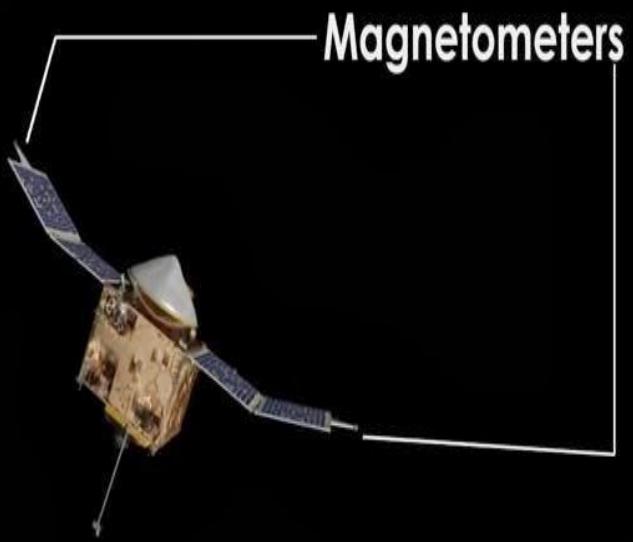
Provides a vector measurement of the local B-field

$$\|\underline{b}_B - A_{B/N} \underline{b}_N\| = 0$$

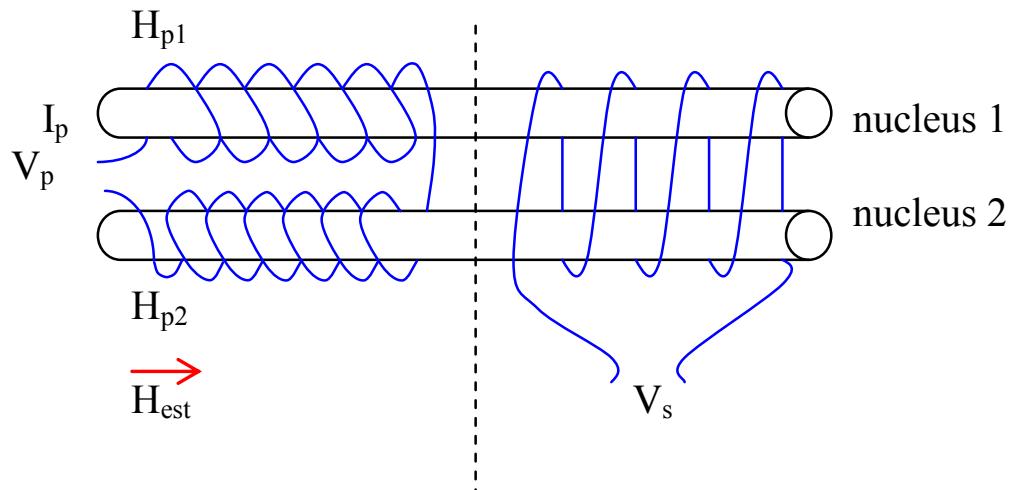
Minimize $J = \|\underline{b}_B - A_{B/N} \underline{b}_N\|^2$

Design requests derive from the first stage concept. If we have a fixed chart we can identify the component of the \mathbf{b} vector along its axis. With three stereoview elements we can identify any generic direction and intensity of the \mathbf{b} vector in space.





Fluxgate magnetometer

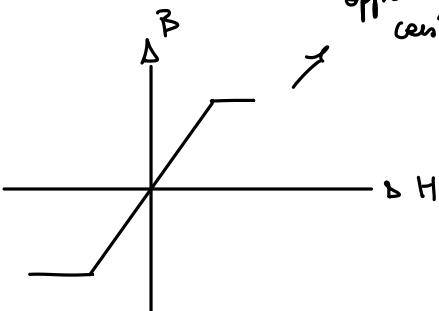
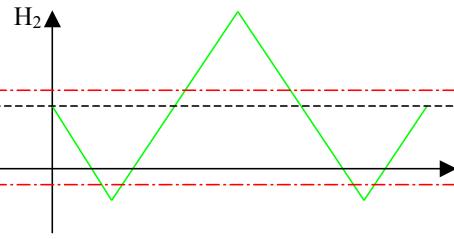
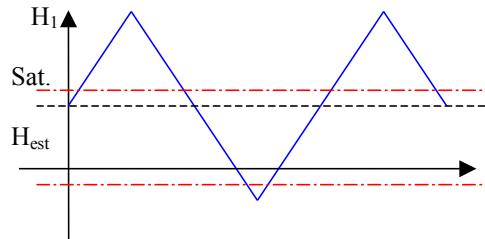
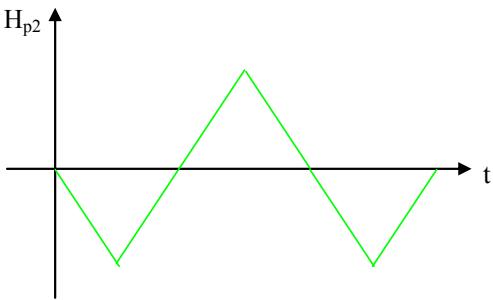
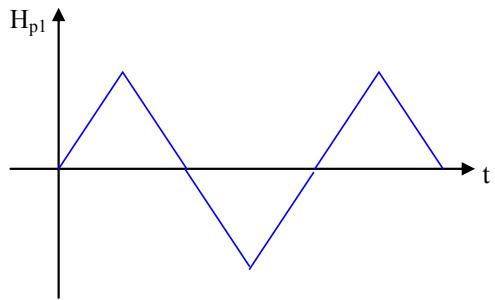
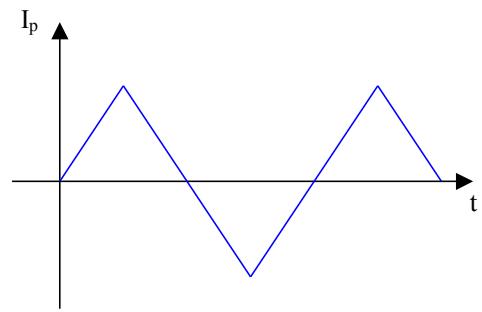


The magnetic field is not proportional to the variation due to the saturation behaviour.

$$V_s = -\frac{d\varphi(B_1 + B_2)}{dt}$$



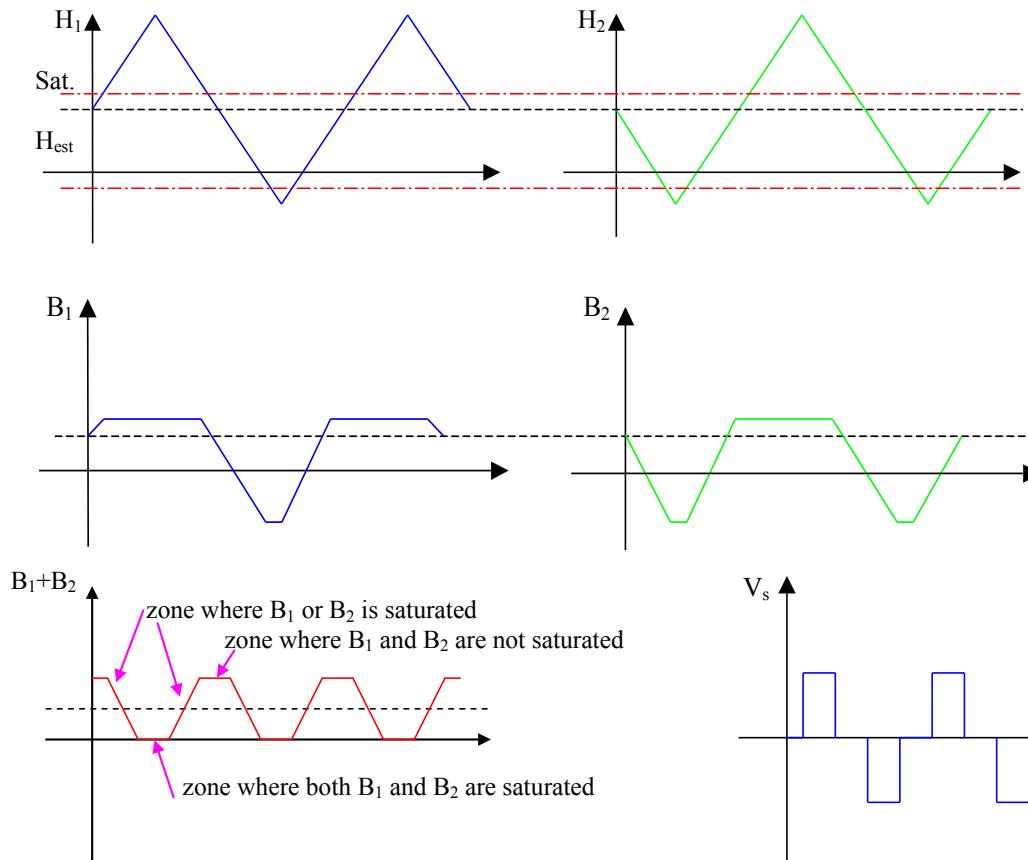
Fluxgate magnetometer



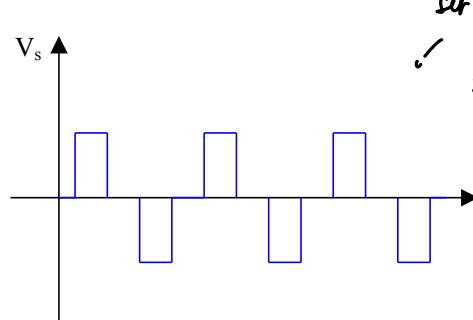
approximation, we are not
considering hysteresis.
please note



Fluxgate magnetometer



Magnetic field sensor can be made really small easily.
What we are measuring is the local magnetic field but we want to measure really magnetic field of the Earth depending the magnetic state of the space craft.
So usually the magnetometers are placed as far as possible from the body of the space craft.



set of impulses

- ✓ we can combine B from the separation of tree impulses.
- $B \uparrow$ low separation
- $B \downarrow$ high separation of impulses

