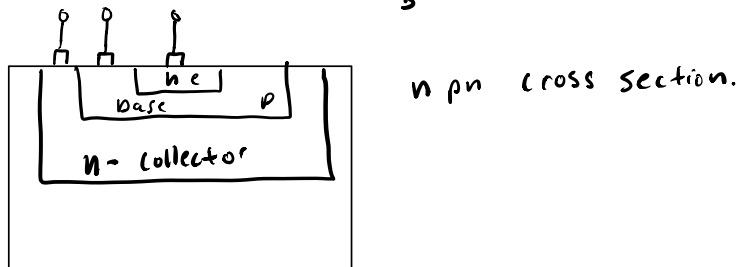
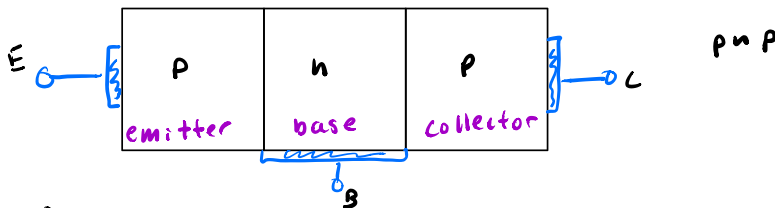
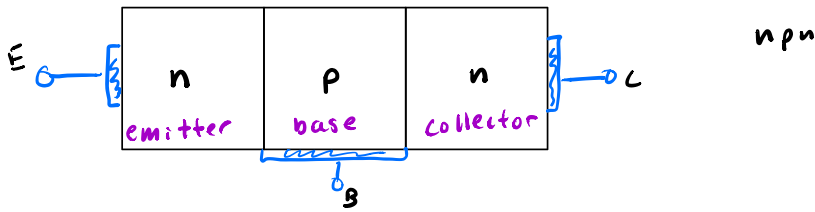


Bipolar Junction Transistors (BJTs)

BJT's were the transistor of choice but they were supplanted by mosfets in 1980s

↳ large, asymmetrical, higher power

↳ good for discrete circuits, for high power or high frequency application.



BJTs look like 2 pn junctions

emitter base junction EBJ } EB
collector base junction CBJ } CB or BC

modes of operation

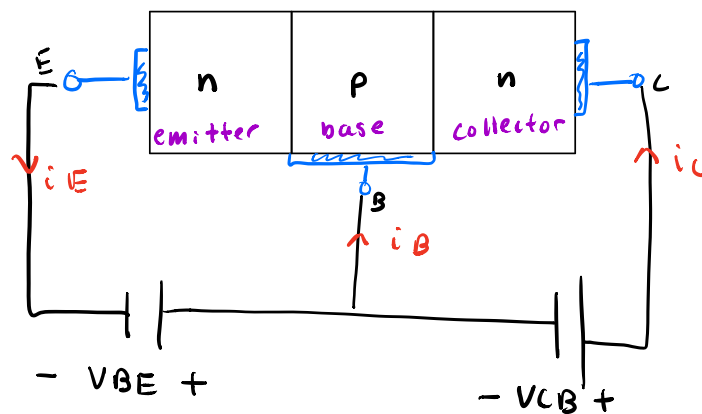
Active : amplifiers

Cutoff : } digital logic ckt's

Saturation :

↑ junctions * Both types of charge carrier participate in current conduction → Bipolar operation

Active Mode operation



$V_{BE} > 0$ (p) base is greater than the (n) emitter \Rightarrow Forward biased

$V_{CB} > 0$ (n) collector is greater than the (p) base \Rightarrow Reverse Biased.

$$i_C = I_S \exp(V_{BE}/V_T)$$

\nearrow
Saturation
current

\searrow Thermal
Voltage

i_C is independent of V_{CB} iff V_{CB} is at least greater than 0. (Reverse Biased)

$$i_B = \frac{i_C}{\beta}$$

$\beta \equiv$ common emitter current gain
 $\hookrightarrow 50 \rightarrow 200$

β unitless

related to width of base region and ratio of the doping levels to the emitter
high $\beta \rightarrow$ thin base lightly doped base heavily doped emitter.

$$i_B = \frac{I_S}{\beta} \exp(V_{BE}/V_T) \quad i_E = i_B + i_C$$

$$= \frac{I_S}{\beta} \exp(V_{BE}/V_T) + I_S \exp(V_{BE}/V_T)$$

$$i_E = \left(\frac{\beta + 1}{\beta} \right) i_C$$

$$i_C = \alpha i_E$$

$\alpha \equiv$ common base current gain
 α unitless

$$\alpha = \frac{\beta}{\beta + 1}$$

$\alpha < 1$ (.98-.99)

$$\beta = \frac{\alpha}{\alpha - 1}$$

$$I_S = \frac{A_E q D_n n_i^2}{N_A \cdot w}$$

A_E cross sectional area of emitter base junction

D_n diffusivity of electrons in the base

n_i intrinsic carrier concentration

N_A concentration of acceptor atoms in the base

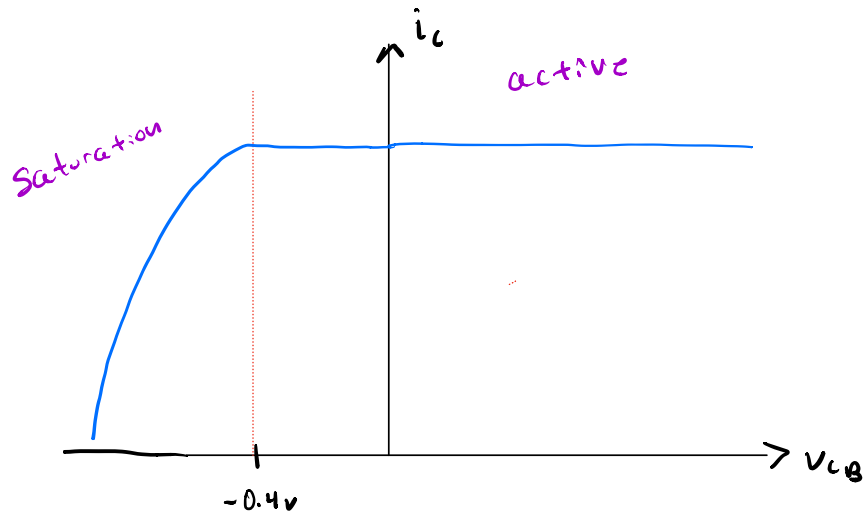
w base width

$$I_S \sim 10^{-12} \text{ to } 10^{-18} \text{ A}$$

↑ very dependent on temp.
 scale current

Saturation mode

To be active $V_{CB} > -0.4\text{V}$



$$V_{CE_{sat}} = V_{BE} - V_{BC}$$

V_{BC} is always smaller than V_{BE} by $.1\text{V} \rightarrow .3\text{V}$

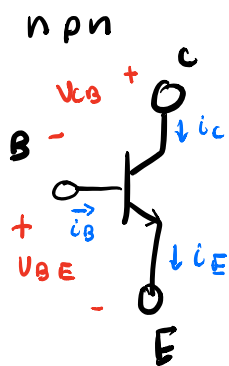
$\hookrightarrow C_{BJ} \text{ area} < EBJ$

$$V_{CE_{sat}} = 0.1 \text{ to } 0.3\text{V}$$

$$V_{CE_{sat}} (\text{edge}) = 0.3\text{V}$$

$$V_{CE_{sat}} (\text{deep}) = 0.2\text{V}$$

BJT operation / DC Biasing



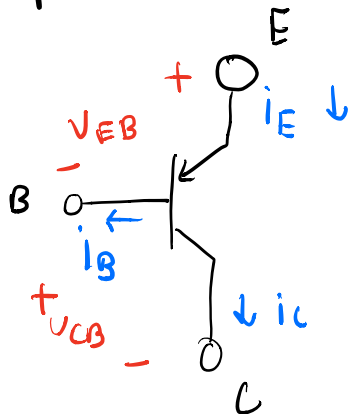
$$I_C = I_S \exp(V_{BE}/V_T)$$

$$i_B = \frac{i_C}{\beta} \quad \beta = \frac{\alpha}{\alpha - 1} \quad \alpha = \frac{\beta}{\beta + 1}$$

$$i_E = i_B + i_C$$

active: $V_{BE} > 0$ $V_{CB} > -0.4\text{V}$

p n p



$$I_C = I_S \exp(V_{EB}/V_T)$$

$$i_B = \frac{i_C}{\beta} \quad \beta = \frac{\alpha}{\alpha - 1} \quad \alpha = \frac{\beta}{\beta + 1}$$

$$i_E = i_C + i_B \quad i_C = \alpha i_E$$

active mode $V_{EB} > 0$ $V_{BC} > -0.4\text{V}$