Multiple Input Transfer Function Modelling for Streamflow Data

by

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Abstract

Developing a working multiple input transfer function model of streamflow data is a difficult task due both to the natural processes that generate the data and because of the inaccuracies of the data collection process. Still, much useful information can be gathered from applying ARIMA transfer function modelling to small, representative time periods. It is possible to develop reasonably well-behaved and accurate models even while seriously limiting the amount of data cleaning that is done.

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Chapter 1

Introduction

The Congaree River is formed by the confluence of the Saluda and Broad Rivers near Columbia, SC. Both the Saluda and the Broad Rivers are dam controlled with the Saluda being managed by the Lake Murray Dam 7 miles above the Congaree, and the Broad managed by Parr Shoals Dam which is about 20 miles above the confluence of the two rivers. There is much interest over the effect of the control

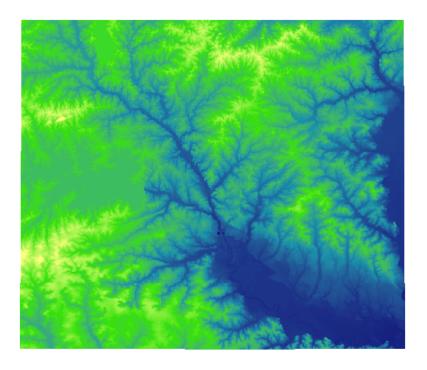


Figure 1.1: Congaree Confluence Zone - Columbia, SC

of these two rivers upon the Congaree National Park area that is roughly 25 miles from the confluence of the two rivers. The Broad has over two times the streamflow of the Saluda, but the Lake Murray dam is much closer to the confluence zone and therefore gets much more attention. In both rivers, streamflow is more dependent on dam release than any other factor except for high flows on the Broad River.

The Saluda is a popular river and is highly utilized by sportsmen and those looking for a cool place to swim during the hot summers in Columbia. The very low temperature (16-18 C) is due to the draft of the water from the bottom and middle layers of Lake Murray. The depth of the draft of the water also has an effect on dissolved oxygen content of the upper Saluda, but this effect will not be considered in this paper.

The Broad River is overlooked by many due to its more remote location and relatively few recreational areas developed for public use. It is possible that this lack of attention contributes to the lack of attention it has received in the complaints over the management of the Saluda in respect to the Congaree Swamp and recreation areas downstream of the confluence zone. It is clearly apparent from looking at streamflow data that the Broad River does have considerably more streamflow during all conditions, whether drought or flood. For example, during the summer of 2001, the Saluda consistently ran about 290 CFS (cubic feet per second) while the Broad ran in the vicinity of 2000 CFS. The Broad also appears to be just as highly managed as the Saluda, both being highly tied to power generation.

The effect of both dams on the Congaree National Park is attenuated by the distance between measuring stations and possibly the natural smoothing of the flow by obstructions, deepening and shallowing, and tributaries and runoff from precipitation events. The Lake Murray dam is closer, so it may have a more direct effect on the flow of the Congaree as long as the Broad remains relatively quiet, but the volume of the Broad probably gives it the upper hand.

What is the relationship between the Saluda and the Broad Rivers in terms of their combined effect on the Congaree River? How is this effect attenuated by the Congaree River's 25 mile reach above the Congaree Swamp?

The primary method that will be used in determining the relationship between these rivers will be the multiple input transfer function model. In Chapter 2 and Chapter 3 it will be shown how we will apply transfer function modelling to streamflow and river stage data. We will discuss three specific models in Chapter 4 and analyze some more sophisticated techniques for model determination in Chapter 5.

Chapter 2

ARIMA Transfer Function

Modelling

In dynamic systems such as these rivers, it would be ideal to have continuous information but instead we have hourly measurements. For the continuous case, we can visualize river segments between measuring stations as a system of interconnected reservoirs with the measurements at the upstream and downstream stations being the measurement of the level of water in the reservoirs as described in Box, Jenkins and Reinsel.

With river flows the system becomes a bit more complicated. The flow between measurement points is unidirectional in a non-tidal system. Also, equilibrium indicates complete absence of water in the system. If we consider the flows from both of the input rivers to be fixed, then the management of the rivers by changing the amount of water flowing over or through the dam yields a forcing function-the transfer function. By interpreting how the changes in the input flows correspond to the output flow we can determine the transfer function. From analyzing the transfer function we can see how the management of the river affects downstream river conditions.

Unfortunately, the profiles of both of the input rivers change wildly over time.

This is due to many effects, but mostly to large precipitation events upstream and

the effect of power production during dry times. Small time frames are chosen from the data when the river flows are fairly stable.

Once suitable time frames are selected, a Box-Jenkins transfer function ARIMA model is fitted to the system. Then once the input data has been transformed, ARIMA models are fitted for each input series. The diagnostics used to determine model accuracy are the Autocorrelation Function (ACF) and the Partial Autocorrelation Function (PACF)—both obtained on the residuals of each series. It is also necessary to check for cross correlation between the input series.

Once acceptable ARIMA models for the input series have been fitted, the output series is filtered against both of the input series. This is done to de-trend the output series based upon what effect the input series will have on it. At this point the Cross Correlation Function (CCF) for the system is calculated and examined. The delay parameter can be usually judged from the graph of this function as well as the parameters of the transfer function. Sometimes the cross-spectrum of the input and output series can be more useful in determining the delay parameter.

Using the delay, denominator and numerator transfer function parameters, the transfer function is fitted against the system. The ACF and PACF of the system residual series is checked and forecasts are generated. The model autocorrelation of residuals and cross correlation between input series should not be significant, and the forecasts should look stable and should be accurate against hold-out data.

2.1 The Box-Jenkins ARIMA Model

Autoregressive Processes

A regression model can be written

$$\tilde{y} = \beta_1 \tilde{x}_1 + \beta_2 \tilde{x}_2 + \beta_3 \tilde{x}_3 + \dots + \beta_p \tilde{x}_p + \epsilon \tag{2.1}$$

The time correlated counterpart to the regression model is the autoregressive model, or AR model. In the autoregressive model, the value z_t is regressed on its previous values using a time index. The general autoregressive model looks like

$$\tilde{z} = \phi_1 \tilde{z}_{t-1} + \phi_2 \tilde{z}_{t-2} + \phi_3 \tilde{z}_{t-3} + \dots + \phi_p \tilde{z}_{t-p} + a_t$$
(2.2)

representing an AR(p) model. The autoregressive operator ϕ can be described

$$\phi(B) = 1 - \phi_1 B - \phi_2 B^2 - \dots - \phi_p B^p \tag{2.3}$$

or $\phi(B)\tilde{z}_t=a_t$ where B=t-1 and $B^p=t-p$ on the time index t. This model has p+2 unknown parameters which must be estimated from the data: $\mu,\phi_1,\phi_2,\ldots,\phi_p$. The variance σ_a^2 of the white noise process a_t is the other parameter.

Moving Average Processes

The difference between the autoregressive and moving average models is that a autoregressive model constitutes a finite weighted sum of p previous deviations of the process plus the error term a while a moving average relates the process to the error term itself.

$$\tilde{z} = a_t - \theta_1 a_{t-1} - \theta_2 a_{t-2} - \dots - \theta_q a_{t-q}$$
 (2.4)

The moving average operator θ of order q is denoted by

$$\theta(B) = 1 - \theta_1 B - \theta_2 B^2 - \dots - \theta_q B^q \tag{2.5}$$

So then the autoregressive operator uses the previous values of the series, while the moving average operator works on the previous error terms. A combination of the

AR and MA operators is possible, resulting in an ARMA model which has the form

$$\tilde{z} = \phi_1 \tilde{z}_{t-1} + \phi_2 \tilde{z}_{t-2} + \phi_3 \tilde{z}_{t-3} + \dots + \phi_p \tilde{z}_{t-p} + a_t + a_t - \theta_1 a_{t-1} - \theta_2 a_{t-2} - \dots - \theta_q a_{t-q}$$
 (2.6)

The I in the ARIMA model results from differencing, a procedure that subtracts observed time series values one from another in some defined scheme. This operation helps to deal with nonstationarity and seasonal and unspecified periodicity. Differencing can be very useful in achieving an appropriate model, but can make explanation of the model difficult.

2.1.1 Transfer Function Models

A transfer function model is a time series model in which one or more input variables are used to determine the future state of an output variable. The transfer function essentially maps the change in the inputs to the output.

The transfer function transfers the effect of the input variables using what is called an *impulse response function*. The impulse response function waits a certain period of time (delay) before starting, then applies the input variable in a specific pattern.

If we consider the continuous case, the first order differential equation representing a single input X and a single output Y is:

$$(1 + T_1 D)Y_1(t) = g_1 X(t - \tau)$$
(2.7)

where τ is the delay, and g_1 is the gain (a scaling factor). T_1D indicates that the rate of change in Y depends on the difference between X and Y.

If higher order models reflect additional dependencies of Y on X:

$$(1 + \Xi_1 D + \dots + \Xi_R D^R) Y(t) = g(1 + H_1 D + \dots + H_S D^S) X(t - \tau)$$
(2.8)

In this equation the Ξ terms result from intermediate reservoir effects. The H terms represent increasing complexity in the relationship between the rate of change and the behavior of X.

The continuous model can be represented as a discrete system by the difference equation:

$$(1 + \delta_1 B + \dots + \delta_r B^r) Y_t = g(\omega_1 - \omega_2 B - \dots - \omega_R^s) X_{t-b}$$
(2.9)

or

$$\delta(B)Y_t = \omega(B)X_{t-b} \tag{2.10}$$

The standard form of the transfer function with output variable Y_t and input variable X_t can be written

$$Y_t = \frac{\omega(B)}{\delta(B)} X_{t-b} + N_t \tag{2.11}$$

The ω 's are analogous to the autoregressive part of a time series while the δ 's are analogous to the moving average part. The b's represent the general delay in the impulse response function, or the amount of time before the impulse response function "activates." This becomes more obvious if equation (2.11) is written

$$\delta(B)Y_t = \omega(B)X_{t-b} + N_t \tag{2.12}$$

 N_t is the noise series of the model and effectively describes the stochastic part of the dynamic time series model:

$$N_t = \frac{\theta(B)}{\varphi(B)} a_t \tag{2.13}$$

2.1.2 Fitting Transfer Function Models

To estimate an appropriate transfer function model the input time series must be analyzed, and appropriate ARIMA models identified. These models are first used to prewhiten the output series. Prewhitening involves filtering the output series with the model of the input series; both series are assumed to have no trend. This de-trending could be also accomplished by differencing. Prewhitening removes the direct influence of autocorrelation in the input series while preserving the important features of the transfer function model.

The cross correlation function yields a good bit of information about the delay in the system. It is not always a good indicator of the r and s components, but tentative orders for the $\omega(B)$ and $\delta(B)$ can be identified. If the cross correlation function is not helpful in determining delay, then the cross spectrum of the input with the output series might help.

Following the prewhitening step, the cross correlation function is fitted and examined for system wide lags in effect. In other words, the delay in the first series that affects the second series is identified.

Once the orders of the input series have been identified, a tentative ARIMA transfer function model is fit. This tentative model may or may not be a good fit, but the results can be used to identify the delays, and the r and s orders that will yield a good model fit.

At this point, the error is assumed to be due to an unidentified process, and an ARIMA model is fitted to the residuals it so that it can be combined into a systemwide model. This model, if accurate enough, can then be used for a variety of purposes. Forecasting of future output values based on past and current values of the input series is often the goal.

2.1.3 Model Diagnostic Procedures

In theory, the diagnostic procedures for transfer function models are rather straightforward. The residuals should be uncorrelated with the input series and should look like white noise. They should also not be cross-correlated with the input time series. If the residuals have any structure at this point, they should be modelled into a noise series, such that the remaining residuals look like white noise.

All this is important, but let us consider the random shock $a_t = N(0, 1)$ in reverse of what is usually done. This is the building block of our data and is the stochastic part of everything that follows. From this we assume that there are patterned inputs, functions that affect the output. These are applied to the a_t resulting in a patterned behavior based on a fixed interval of time, a Time Series.

Now, consider the variables that are available in streamflow modelling: Precipitation, power generation, the shape of the stream bed, tributary influence, stream bed absorption, evaporation and any other unconsidered notion. Chances are that most of these variables have a very small influence such that the influence cannot be distinguished statistically from white noise. In the case of this analysis, we have streamflow data in the form of flow and stage for four monitoring stations, each with a different subset of precipitation basins, river bed profile, average temperatures etc. The bottom line is that there is probably a lot of variation in the variable that we are trying to model, whether it be flow or stage.

But the goal is not to develop a specific model for each of the variables (which we do not know exactly) but to develop a predictive model that can shed some light onto the characteristics of this system of rivers. For this reason, great care must be taken when interpreting the diagnostic results. As usual, an attempt will be made to ensure that the diagnostic statistics are as reasonable as possible, but I employ a practical method as well. For each sequence, the forecast is compared against a period of "hold out" values to determine how well the model holds up for a short

duration. Another indication of model specificity is the 90% confidence bands that are produced by PROC ARIMA. This is a visual inspection only at this point, but the more stable the prediction interval the better.

Chapter 3

Multiple Input Transfer Function Models for River Data

3.1 The Broad-Saluda-Congaree River System

The Congaree River is formed by the confluence of the Broad and Saluda Rivers in the vicinity of downtown Columbia, South Carolina. The confluence zone is located between the I-126 bridges and the Jarvis Klapman Bridge, or SC 12, west of Columbia, South Carolina.

The Broad has the larger flow of the two, usually being three to five times higher in cubic feet per second (cf/s or cfs). The Broad, at this point, is managed by the Parr Shoals Dam which is located roughly 24 miles upstream near Peak, South Carolina and falls almost 98 vertical feet.

The part of the Saluda River of interest starts at the Lake Murray Dam, approximately 10 miles from the confluence zone, covering about 45 vertical feet over that distance. The streamflow of this part of the Saluda is a tightly controlled since the Lake Murray Dam's purpose is power production.

There are four measuring stations of interest to this analysis displayed in the following table:

River	Station Name	Station	Altitude	Drainage Area
Broad	Alston	02161000	211.91 ft.	4790 mi^2
Saluda	Below LM Dam	02168504	170 ft.	2420 mi^2
Saluda	Above Columbia	02169000	149.46 ft.	2520 mi^2
Congaree	Columbia	02169500	113.02 ft.	7850 mi^2
Congaree	Congaree Swamp NP	02169625	90.84 ft.	8290 mi^2

Table 3.1: Streamflow Monitoring Stations

3.1.1 General Analytical Concepts

It is desired to determine whether or not it is possible to develop a predictive dynamic forecasting model of the flow (or stage) of the Congaree River at the Congaree River at Columbia and the Congaree National Park site. The twist to this analysis is that the input series (Saluda and Broad Rivers) are usually quite correlated. This violates one of the primary assumptions of the transfer function model, but a good predictive model may still be possible if careful attention is given to choices of parameters.

Casual observation of the data shows that there are vast differences in the streamflow of both feeding rivers (Saluda and Broad). It is extremely unlikely that an all purpose model is possible for modelling all situations of streamflow of these two rivers.

We have identified five different macroscopic views of the flow of this riverine system for analysis purposes:

Streamflow	Definition			
Flood Conditions	Highly erratic flow where overbank conditions apply			
High flow	Large precipitation events or dam discharge on both rivers			
Normal Flow	Moderately managed situation on both rivers			
Low Flow	Highly managed situation on both rivers			
Drought Conditions	Flow is dependent on dam release only			

Table 3.2: Defined Streamflow Levels

There are a vast number of combinations that would need to be fit to accommodate every scenario, and the quality of the data is such that fitting a few well-behaved sequences of data are desired.

3.1.2 Dealing With The Data

The data that was used for this analysis was provided by the United States Geological Survey for the State of South Carolina. The data range for the entire input dataset is January 1, 1995 through October 1, 2002. This range was further filtered into three time periods

Date	Features			
September 5-10, 1996	Management of both the Broad and Saluda Rivers			
July 21-23, 1995	Management of the Saluda River while the Broad River is stable			
April 28 - May 7, 1999	Management of the Broad River while the Saluda River is stable			

Table 3.3: Data Analysis Time Periods

Making the Data Analyzable

The data were received in individual sets organized by streamflow monitoring station. Each of these files contained hourly observations of streamflow, stage, date, hour and minute. Each of these files were transformed to contain the following columns: DATETIME, STREAMFLOW, STAGE, LN(STREAMFLOW), and LN(STAGE). These files were then merged by DATETIME, which is a SASDATE datatype.

Imputation of Missing Values

Time sequences were chosen to avoid the missing value problem. Early on, missing values were replaced with the mean for the time sequence. This is a rather poor technique for imputing missing values so series were chosen to avoid this problem altogether¹

¹PROC EXPAND in SAS is an ideal choice for imputing missing time series data.

Datasets

The data originated from the US Geological Survey of South Carolina's streamflow monitoring system. This system is comprised of several hundred remote sensors that record the stage of the river or body of water.

3.2 Subsystems

The analysis of this river system has been divided into two sections for convenience. The first section has the Broad and Saluda Rivers as input series to the Congaree River at Columbia. The second has Congaree at Columbia as the input and Congaree Swamp National Park as the output. It makes sense to divide the system up in this way because of the natural configuration and the distances involved between measuring stations.

3.2.1 Stage 1: Saluda Broad Congaree System

For the purposes of this analysis, the Saluda River will begin at the base of Lake Murray Dam. This is a large impediment to natural flow and the flow of the river. Lake Murray also has a great reservoir capacity. Natural flow rarely occurs on the river below Lake Murray.

The Broad River is likewise controlled by the Parr Shoals Dam, but the upstream flow of the Broad is much higher, and the reservoir capacity of Parr Shoals Reservoir is fairly small. It is apparent from the flow diagrams that the Parr Shoals Dam is pretty good at controlling the flow of the Broad River below the dam until the river reaches moderate flood conditions.

3.3 Delays

One of the problems with ARIMA transfer function model determination for streamflow data is that the delay parameter is likely to change for different streamflow patterns. It was hypothesized using empirical knowledge that the amount of delay from station 1 to station 2 would decrease with increased volume. This makes physical sense due to the fact that the stream velocity will increase when the volume increases.

The figures (3.1) and (3.2) show the delays of the Broad and Saluda Rivers, against the Congaree at Columbia. These are not the raw cross correlation functions but a prewhitened fit taking all inputs into account. The crosscorrelation function was calculated on consecutive 7 day intervals starting on January 1, 1996 and going through the end of the data.

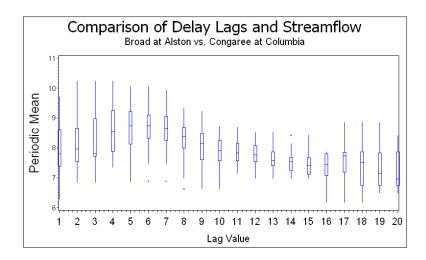


Figure 3.1: Comprehensive Delays of Lags vs. Streamflow for Broad River

This data, like all streamflow data, is rather messy. There is not much information to be gained from an in depth study of the results of this analysis, but it can be seen that the bulk of the results for the Broad River lie between lags 5 and 14. The lag is negatively correlated with the log of the streamflow in this vicinity. For the Broad, the river distance between the Alston and Columbia stations is roughly 20 miles. It

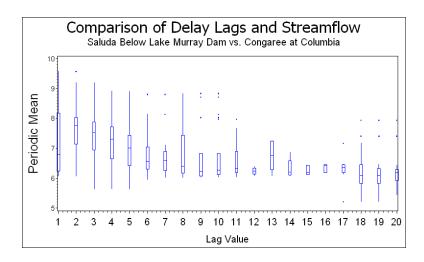


Figure 3.2: Comprehensive Delays of Lags vs. Streamflow for Saluda River

is unlikely that the average current velocity would be more than 5 miles per hour so lags of 0-4 are most likely representative of noise or aliasing in the data.

Performing the same analysis on the Saluda River yields results that are similar in nature. The lag again is negatively correlated with the log of streamflow. A lag of 1 is unlikely, but lags of 2 through 5 are physically possible. Lags 8 or larger are also unlikely and are probably a result of aliasing. We will see that lags near 3 build good models.

3.4 Description of the Data

3.4.1 Rivers

The analysis is divided into two parts: a multiple input transfer function model comprising the Saluda-Broad-Upper Congaree and a single input transfer function model made up of the Upper Congaree-Congaree Swamp.

When references are made to the Saluda River, the data was recorded at the United States Geological Survey Streamflow Monitoring Station 02168504 which is located just below Lake Murray Dam. The Broad River means SC-USGS station

02161000 at Alston, or Peak, SC. The Upper Congaree, Congaree at Columbia, or simply Congaree, is station 02169500. The Congaree Swamp National Park station is 02169625, and is located near Congaree National Park.

For the analysis of the multiple input system upstream, streamflow is used as the variable. The single input system below Congaree and Congaree Swamp utilizes the Stage variable since streamflow was unavailable for most of the dates in the dataset.

Streamflow is measured in cubic feet of water per second passing a specified point, and is often derived from the stage data mathematically.

Stage is the familiar height of the river above or below some datum. Stage is measured in feet for all of the gauges used in this report.

3.4.2 Methods of Analysis

All of the following analysis was performed using SAS/ETS software, primarily PROC ARIMA. Target time periods were selected by visually inspecting monthly profile graphs of the data from all of the stations. The time periods were further refined using trial and error to sections of data that could be modelled with reasonable accuracy. As mentioned in the section on data imputation, time periods were also selected where missing values did not occur.

It was decided early on not to difference the data. Since river related data is notoriously hard to model, this made finding representative timeframes fairly difficult.

Prewhitening of Inputs

For all analyzed time periods, a visual inspection of the input ACF, PACF, and CCF graphs was done in an attempt to identify model parameters. Since differencing was not a primary focus, this did not lead to a very good estimation of the p and q components of the model. Both the Saluda and Broad Rivers were subjected to a trial and error approach using a SAS/AF application (B) that was developed to

expedite the trial and error process. The idea behind the trial and error process is to pick AR and MA components such that the autocorrelation of residuals and the cross correlation between the inputs and the white noise of the residuals is negligible.

The primary method of determining input p and q parameters was using the output from the SCAN option of PROC ARIMA's IDENTIFY option. SCAN (Smallest Canonical correlation) analyzes the eigenvalues of the correlation matrix of an ARMA process and returns a matrix of possible autoregressive and moving average parameters. This criterion usually produced the best models, and saved time during the trial and error step.

Delay Parameters

The delay between each input and the output was also investigated at this time. This was done by looking at the largest absolute value of the cross correlation function over a lag spread of -24 to 24. There is no physical reason why the lag should ever exceed these parameters. This was a tricky part of the analysis since the delays were often aliased, or correlated with larger or smaller multiples of themselves. It is also possible that interference patterns caused the CCF analysis to be non-specific. A good bit of common sense went into picking the most appropriate lag for each prewhitening input.

Chapter 4

Data Analysis

Targets of opportunity for analysis were selected by looking at monthly flow and stage profiles at the four selected monitoring stations. Acceptable targets were time periods with a low incidence of missing data, visible stationarity, and situations where it was obvious that river management was occurring. Even with hourly data for seven years, this was an easy exercise.

4.1 September 5-10, 1996 - High Management On Both Rivers

4.1.1 Logged Streamflow Modelling

A quick look at the logged streamflow profile for this period shows a well-behaved system. The five days of hourly data should give enough data to generate a good model.

The ACF of the Saluda River (Figure 4.2) data shows that the series may benefit from differencing the data before analysis. The PACF of the Saluda data (Figure 4.2) shows that this river might be modelled using an AR(2) component.

The ACF of the Broad River data shows that the series could also benefit from

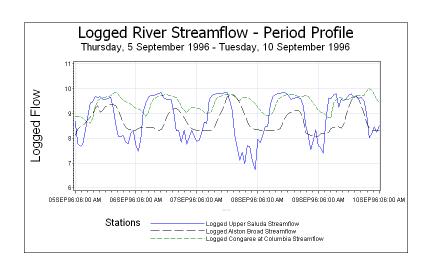


Figure 4.1: Flow Profile Plot for September 5-10, 1996

differencing the data before analysis. The PACF of this data shows that this river might be modelled using an AR(2) or an AR(3) component.

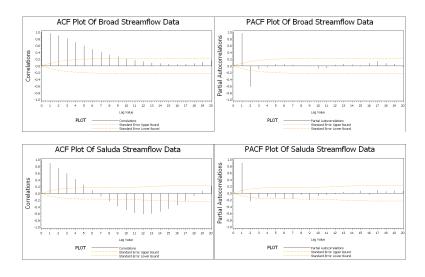


Figure 4.2: Input Series ACF and PACF Plots for September 5-10, 1996

The cross-correlation function for this period (Figure 4.3) shows that the Saluda delay is about three hours. This holds well with other observations and historical averages. The delay for the Broad River looks to be 10 hours. Again, this holds well with observational evidence.

There is a stronger negative correlation for the Broad River at 11 hours and a

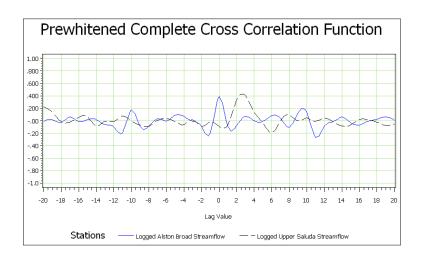


Figure 4.3: Streamflow Cross-Correlation Plot for September 5-10, 1996

very strong positive correlation at 0 hours. The 0 hour value probably is indicative of the correlation between the input series and is obviously false based on the physical nature of water and the distances between these two monitoring stations. The 11 hour correlation is interesting. Note that in most of the examples shown, the maximum absolute correlation will occur among a range of nearby lag values. Here it is 8, 10 and 11. The method for determining the best delay to use for the model was based upon the model fit diagnostics.

A quick look at the ACF and PACF(Figure 4.2) graphs for the input variables and the pre-whitened, system-wide data shows some valuable information for model building. All of the ACF's show a slow tail-off, usually indicating the need for differencing of the data. The data is not differenced in this analysis because it is desired to see if reasonably accurate models can be built without differencing. The one-step-ahead forecasts are of particular interest. Obviously, some of the assumptions of the ARIMA model will be violated. This does not mean that a fairly accurate predictive model cannot be created.

The forecast for this period is fairly stable. Often with transfer function models the forecast standard errors diverge quickly from the forecast itself. In this case it is

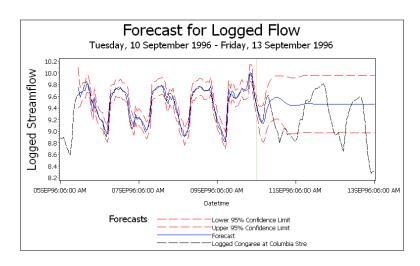


Figure 4.4: Streamflow Forecast Plot for September 5-10, 1996

obvious that the actual flow changed from the pattern that was used to create the model. The one step ahead forecasts for the series follow the data very well.

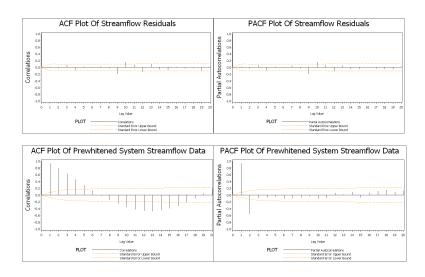


Table 4.1: System Diagnostics for September 5-10, 1996

The transfer function model, modelled as an ARMA(2,1) follows:

River	$\mathbf{A}\mathbf{R}$	MA	Delay
Broad	2	0	10
Saluda	2	1	3
Congaree (model)	2	1	_

Table 4.2: Streamflow Model Parameters for September 5-10 1996

$$CAC_{t} = 4.53 + \frac{0.11246 + 0.01779B^{1}}{1 - 0.55418B^{1}}SAL_{t-3} + \frac{0.09085 - 0.0852B^{1}}{1 - 0.97935B^{1}}BRD_{t-10} + \frac{1 + 0.01546B^{1}}{1 - 1.29681B^{1} + 0.49662B^{2}}\eta_{t}$$

$$(4.1)$$

Diagnostics

Using the Basic fit diagnostics involves making sure that the residuals are not autocorrelated, nor are cross correlated with the input data. It is clear from A.1 that this model passes the residual checks. The fact that the χ^2 test p-values are large for the cross-correlation of the residuals with the input series indicates that the transfer function model is correctly specified. The χ^2 test p-values for the autocorrelation of the residuals being large indicates that the input ARIMA model for the output series is correctly specified.

Finally, the residual series is again considered to determine if any structure still exists. If so, then it may be possible to further refine the model. The chi^2 test p-values (Figure 4.1) are quite large for the test that the residual series has structure remaining. It is safe to say that no appreciable structure remains in the residuals and the model is adequately specified.

4.1.2 Stage Modelling

The profile for this period looks like a good candidate for dynamic transfer function modelling. There does seem to be some linear trend, and the ACF (4.7) of the input

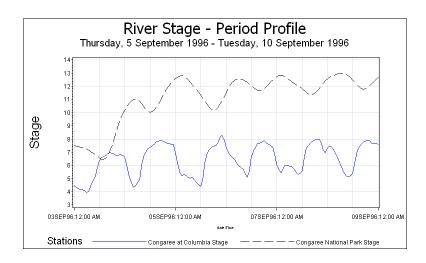


Figure 4.5: Stage Profile Plot for September 5-10, 1996

shows the classic pattern of slow alternating decay that suggests differencing the data. Again, it was chosen not to difference the data to determine if model building is possible under this limitation. The PACF for this period hints at the input Congaree at Columbia being satisfactorily specified using an AR(2) component.

Using a trial and error approach via the SAS/AF modelling application developed for this purpose (B) a ARMA(2,1) model was chosen for the input variable. This model is used to pre-whiten both the input and output series and then these pre-whitened series are analyzed to determine the model parameters. The pre-whitening filter is:

$$CAC_t = 1 - 1.52924B + 0.61964B^2 (4.2)$$

The pre-whitened model ACF (Figure 4.7) again shows the possible need for differencing. The PACF is a little more useful, showing a possible AR(3) component to the model.

The cross-correlation function of the Congaree at Columbia vs. Congaree Swamp 4.6 shows a difficult situation where there is no real indication of the delay in the system. It may be explained by looking at the profile plot itself. The offset of

the series are almost completely in interference with each other—making the cross-correlation function misleading for this series. The greatest absolute values for the CCF as-is yields a delay of one or two hours, both of which are physically improbable. The span of lags 6 to 12, corresponding with 6 to 12 hours, are much more feasible, and the CCF does hint that there may be something there. In the end, trial and error was used to determine the delay within this range that yielded the best diagnostic values. A delay of 9 hours and an ARMA(3,2) appears to be the best fit for the model

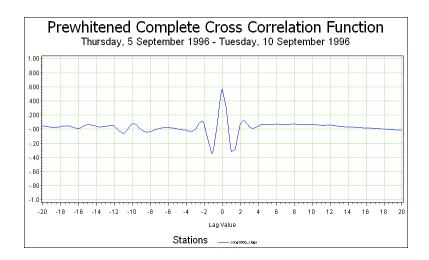


Figure 4.6: Stage Cross-Correlation Plot for September 5-10, 1996

using the trial and error approach through the SAS/AF application.

Even with the unknown factors, and the difficulty in deciding upon a delay, the forecast was very good. In the forecast plot, the vertical line represents the last data point used in the calculation of the forecast. The 95% confidence limits may not be very useful since they grow to such a large span so fast, but the actual forecast holds very true to the hold-out data. The forecast successfully predicts the trend for three days and very accurately predicts the actual stage for an entire day.

The stage model estimated to be an ARMA(3,2) for 5-10 September becomes:

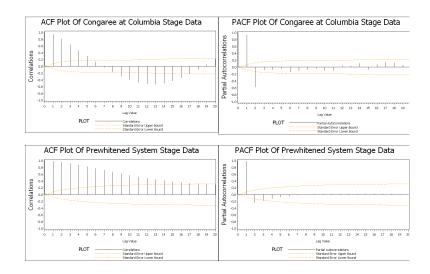


Figure 4.7: System Stage ACF and PACF for September 5-10, 1996

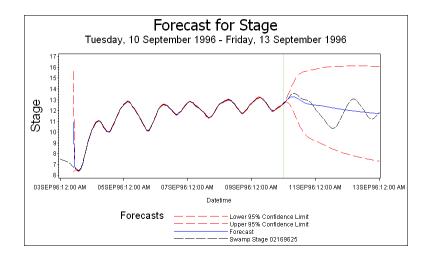


Figure 4.8: Stage Forecast Plot for September 5-10, 1996

$$CSNM_{t} = 10.951 + \frac{0.00143 + 0.00329B}{1 + 0.98073B}CAC_{t-9} + \frac{1 - 0.1747B + 0.48465B^{2}}{1 - 2.70765B + 2.49887B^{2} - 0.78999B^{3}}\eta_{t}$$

$$(4.3)$$

The diagnostics for this model show some of the problems that are associated with the cross-correlation function problem. The autocorrelation of the residuals (Figure A.3) shows a marginal problem out to lag 6, but no problem whatsoever thereafter.

River		MA	Delay
Congaree at Columbia	2	1	9
Congaree at Congaree Swamp (model)	3	2	-

Table 4.3: Stage Model Parameters for September 5-10, 1995

Furthermore, there is no reason to assume that the residual series is anything more than white noise (Figure A.4).

Again, the system χ^2 test p-values are large enough for both the cross correlation with the input series and autocorrelation of the residuals that we can be comfortable with the model and transfer function specifications.

The test for white noise of the residual series is likewise affirmative in that the χ^2 test p-values are large. This again indicates that the residual series does not have any autocorrelation structure and appears like white noise.

4.2 July 21-23, 1995 - High Management on Saluda,Constant Flow on the Broad River

4.2.1 Logged Streamflow Modelling

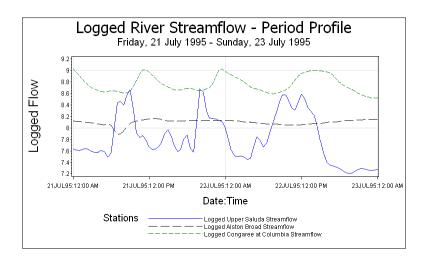


Figure 4.9: Flow Profile for July 21-23, 1995

The time period taken for study is July 21-23, 1995. This period was selected because the Saluda River was under heavy management as evidenced by the regular periodicity in stream flow. This periodicity relates to the regular afternoon water release by the Lake Murray Dam. It is assumed with a very high level of confidence that this is directly related to increased power need in the mid-afternoon. The Saluda was also flowing at roughly a 2800 cubic feet per second streamflow average representing a moderately high flow pattern. The monitoring station for this data is located less than one mile below the Lake Murray Dam, so will not suffer much from attenuation effects of tributaries and rainfall. Accurate precipitation records for the local drainage area were not available so this is not considered.

During the same time period, the Broad River streamflow remains at a fairly constant 3000 cubic feet per second. This combination makes this time period a

good one for studying the effect of the Saluda River when the Broad River remains constant. In other words, attenuation effects can be studied without interference of the Broad River.

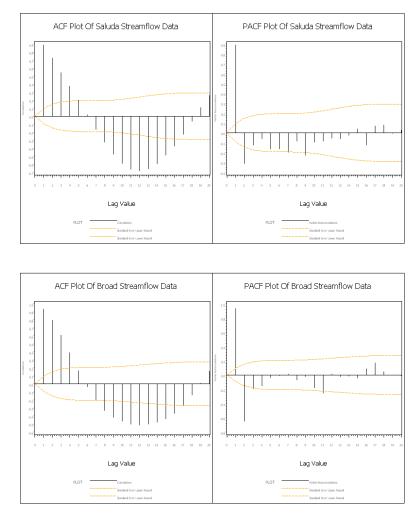


Figure 4.10: Saluda and Broad River Streamflow ACF/PACF July 21-23, 1995

The pre-whitened cross correlation function shows strong evidence for lags of three and seven hours for the Saluda and Broad River respectively.

In this time period, a delay of four hours for the Saluda River and seven hours for the Broad is consistent with most observations. It is interesting to note that good fitting models can be generated using multiples, or near multiples of this value. Notably, using a delay of four for the Broad River extent yields a model that would

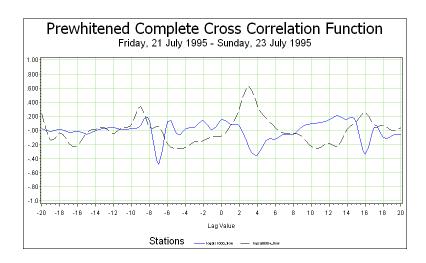


Figure 4.11: Flow Cross Correlation Plot for July 21-23, 1995

pass the rudimentary criteria that are used here for model selection. Furthermore, the CCF for the Broad River shows strongly negative peaks at -7, 4 and 16 lags.

Forecasts for this model are typical for transfer functions:

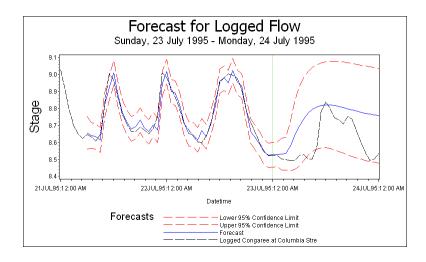
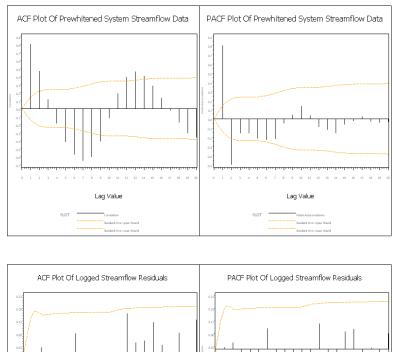


Figure 4.12: Flow Forecast Plot for July 21-23, 1995

The forecast for this time period looks like transfer function model forecasts usually do. The actual values are plotted along with the predicted values and the 90% confidence intervals for the ARIMA transfer function model. The forecast remains fairly accurate for an entire 24 hour period after the last data point, even though the



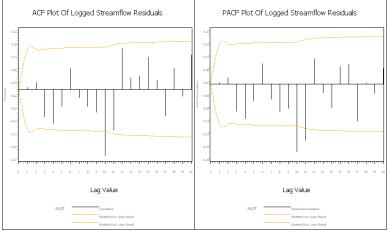


Figure 4.13: System Streamflow Diagnostics July 21-23, 1995 series seems to be deviating from the pattern used to forecast it.

River	$\mathbf{A}\mathbf{R}$	MA	Delay
Broad	0	2	7
Saluda	1	1	3
Congaree (model)	1	1	_

Table 4.4: Streamflow Model Parameters for July 21-23, 1995

The estimated model is then:

$$CAC_{t} = 6.88163 + \frac{0.19344 + 0.09706B}{1 - 0.20714B} SAL_{t-3} + \frac{-0.0328 - 0.11652B}{1 + 0.19723B} BRD_{t-7} + \frac{1 + 0.33188B}{1 - 0.33745B} \eta_{t}$$

$$(4.4)$$

The model diagnostics (shown in Appendix A Figure A.5) within PROC ARIMA show that the probability of the residual series not being white noise is very low. We can say with confidence that the residual series does not maintain characteristics of the model itself, and is fairly random. This may not be the best fitting model as residual diagnostics go, but it is well defined and very appropriate for the needs of this analysis.

4.2.2 Stage Modelling

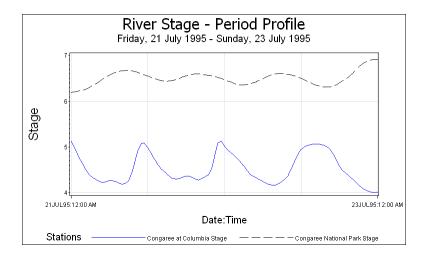


Figure 4.14: Stage Profile Plot for July 21-23, 1995

The stage values during this period were analyzed since reliable flow values were not available. The profile plot shows a good deal of attenuation between the Columbia and Congaree Swamp monitoring stations. It is also possible to discern the delay between these two stations.

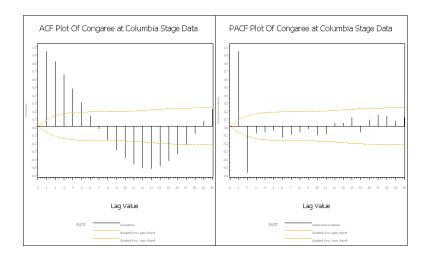


Figure 4.15: Congaree River at Columbia Stage ACF/PACF July 21-23, 1995

The CCF shows a common problem that was encountered during this analysis; the greatest correlation is negative and at b = 0. A quick look at the profile plot

may show why this is occurring. On the profile plot, the maxima for the Congaree at Columbia occur very near the minima for Congaree Swamp. This corresponds with a strong negative correlation at zero, and can account for the fairly strong positive correlations at -1 and 1. There is no way that any perturbation of flow can travel the 25 miles between these two stations within an hour or so. In this case it is necessary to use some common sense. If we look at the positive lag values, a maximum occurs at 8. If the delay was 8 hours as this peak hints, this would correspond with a streamflow rate of around 3 miles per hour. This not only makes sense, but is also a good estimate for the river at this point.

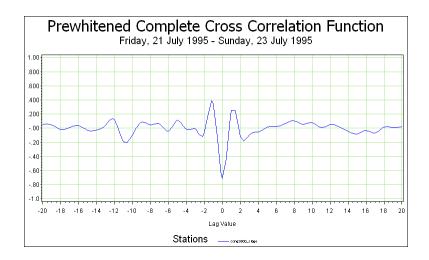


Figure 4.16: Stage Cross-Correlation Plot for July 21-23, 1995

There is also a strong negative correlation that occurs around the -11 lag. This is very interesting, but is also almost certainly due to aliasing in the data. This lag was also ignored based on empirical knowledge, and for the purposes of this analysis.

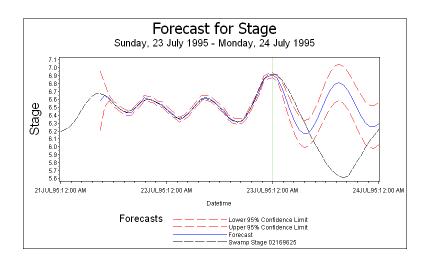


Figure 4.17: Stage Forecast Plot for July 21-23, 1995

As can be seen from the forecast plot, a precise model was created. The forecast deviated strongly from the actual values, but this appears to be a change in the profile itself.

River	AR	MA	Delay
Congaree at Columbia	2	0	8
Congaree at Congaree Swamp (model)	2	0	_

Table 4.5: Stage Model Parameters for July 21-23, 1995

$$CNSM_{t} = 6.012219 + \frac{0.02055 + 0.000006B}{1 - 0.81546B}CAC_{t-8} + \frac{1}{1 - 1.81268B + 0.97588B^{2}}\eta_{t}$$

$$(4.5)$$

One of the difficulties in modelling this type of data is knowing when the profile changes. In the case of managed rivers, the profile changes are related to both manmade (power generation requirements) and natural (precipitation or lack thereof) sources. Both of these sources are very difficult to account for. For example, power generation can be directly proportional to regional temperature, but can also be related to lack of power in other parts of the country. Precipitation can be related to local precipitation or precipitation upstream. Sometimes dams release water due to flooding instead of primarily power generation.

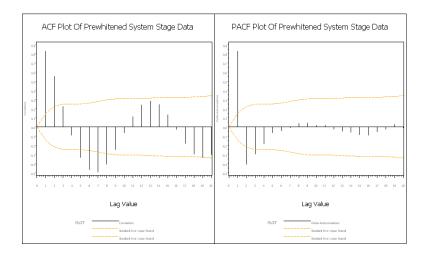


Figure 4.18: System Stage Diagnostics for July 21-23, 1995

4.3 April 28 - May 5 1999 - High Management Constant Flow on the Saluda River

4.3.1 Logged Streamflow Modelling

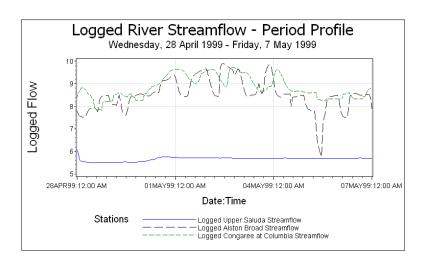


Figure 4.19: Flow Profile Plot for April 28 - May 5, 1999

This profile looks quite different from the others in that the Saluda input is quite monotone and flat. There is a good bit of variation in both the Broad River and the Congaree River at Columbia flow profiles. There is a large dip in the flow of the Congaree at Columbia around May 6.

The CCF for this time sequence is again problematic. In fact, the aliasing is so bad that a decision on delays was made using knowledge rather than the data. The Broad River station shows a strong positive correlation at 6 hours. This is almost half of the delay parameter that was seen in previous models for the Broad River. It is very possible that the stream velocity could double due to the increased flow during this period.

The Saluda, since it did not change much over the period, produced an unusual CCF. This pattern may well be due to the single large value at the start of the series. For this analysis the standard 3 hour delay is used even though the cross correlation

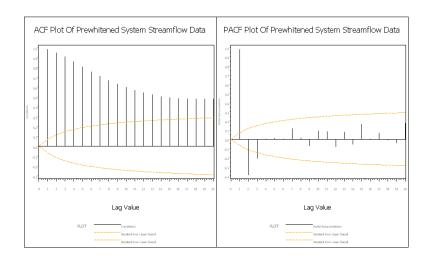


Figure 4.20: Pre-whitened System Streamflow ACF/PACF April 28-May 5, 1999

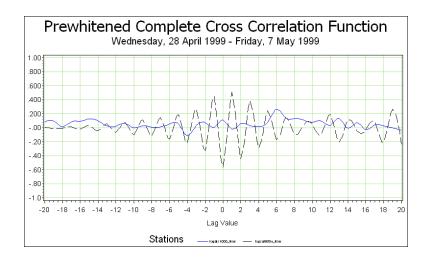


Figure 4.21: Streamflow Cross-Correlation Plot for April 28 - May 5, 1999

function does not necessarily specify this.

The ACF and PACF for this period seem to indicate an AR(2) model for both the Saluda and Broad inputs. After applying trial and error to the analysis the following parameters were determined to yield the best model for this time period:

The model is:

River	AR	MA	Delay
Broad	4	2	6
Saluda	1	1	3
Congaree (model)	5	2	_

Table 4.6: Streamflow Model Parameters for April 28-May 5, 1999

$$CAC_{t} = -7.86145 + \frac{0.3354 + 1.2452B}{1 - 0.27738B}SAL_{t-3} + \frac{0.11023 + 0.11878B}{1 + 0.18196B - 0.73073B^{2}}BRD_{t-6} + \frac{1 + 0.86116B + 0.9998B^{2}}{1 - 0.40928B + 0.05219B^{2} - 0.78709B^{3} + 0.2729B^{4} + 0.12169B^{5}}\eta_{t}$$

$$(4.6)$$

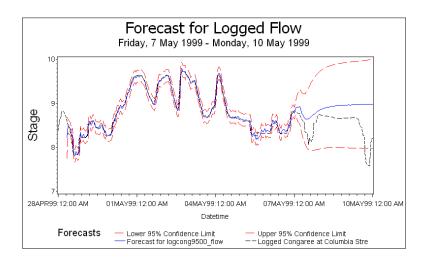


Figure 4.22: Streamflow Forecast Plot for April 28 - May 5, 1999

The forecast is relatively stable for the first part of the forecasting period.

4.3.2 Stage Modelling

The profile plot for this section shows the regular periodicity expected of this stretch of the Congaree River and it seems to attenuate the increase in streamflow seen in the streamflow profile.

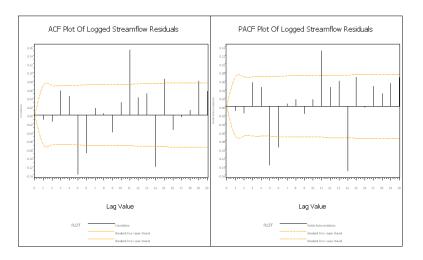


Figure 4.23: System Streamflow Diagnostics April 28-May 5, 1999

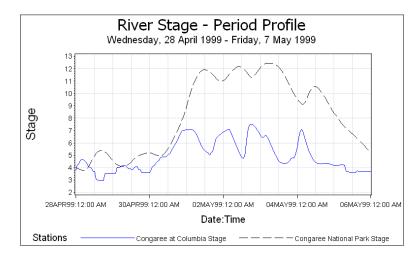


Figure 4.24: Stage Profile Plot for April 28 - May 5, 1999

The CCF for this period is again not particularly helpful. A value of 7 for the delay was used. This value was arrived upon by starting with the knowledge that delays in the range of 6-9 have been used in successful models on this stretch of river. The actual value of 7 was arrived at through trial and error.

The estimated model for stage is:

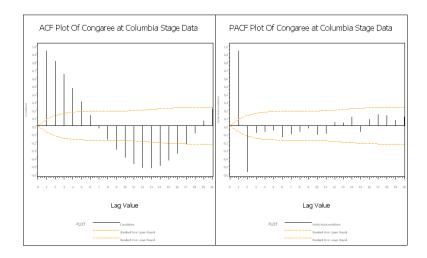


Figure 4.25: Stage ACF April 28 - May 5, 1999

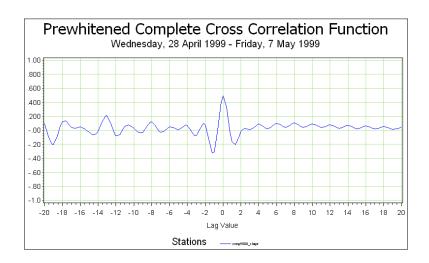


Figure 4.26: Stage Cross-Correlation Plot for April 28 - May 5, 1999

$$CSNM_{t} = 6.593664 + \frac{-0.0002 + 0.00562B * *(1)}{1 + 0.89108B * *(1)}CAC_{t-7} + \frac{1 - 0.19199B + 0.46371B^{2}}{1 - 2.67269B + 2.40008B^{2} - 0.72665B^{3}}\eta_{t}$$

$$(4.7)$$

The forecasts for the stage are fairly good. The deviation between the one step ahead forecasts and the actual values are fairly small and the long term forecast sticks very close to the hold out data.

River	AR	MA	Delay
Congaree at Columbia	3	3	7
Congaree at Congaree Swamp (model)	3	2	-

Table 4.7: Stage Model Parameters for April 28-May 5, 1999

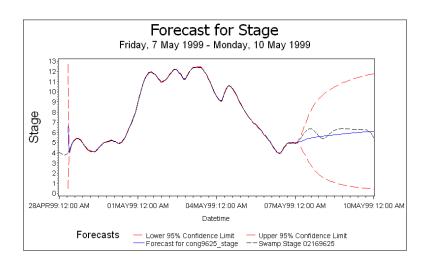


Figure 4.27: Stage Forecast Plot for April 28 - May 5, 1999

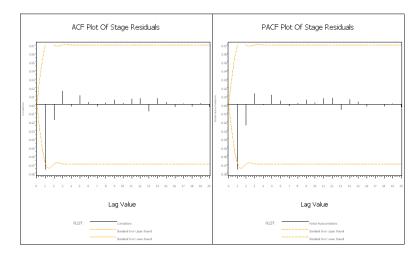


Figure 4.28: Stage Diagnostics for April 28 - May 5, 1999

4.4 Delay Determination Using Spectral Analysis

Although the cross correlation function was useful in determining the delay between the change in an input and the output, there was often a discrepancy in what the CCF suggested and what was logical and what yields a good model.

The cross correlation function for the July 21-23 stage analysis between the Congaree at Columbia and Congaree at Congaree Swamp National Park (4.16) is difficult to interpret. If we calculate the cross-spectra (4.29) of the river stage without transformation more information is possible.

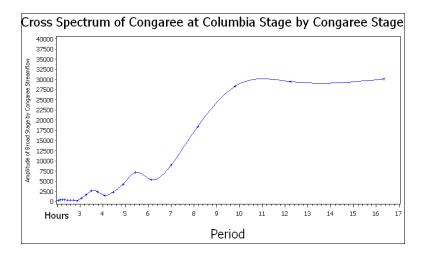


Figure 4.29: Spectrum Example 1

It is clear that there does appear to be a maximum around 11 hours, which is consistent with what is expected. Using a delay of 11 hours yielded a reasonably good model fit as well.

The cross-spectra plot does not always provide a good indicator of the delay parameter however.

Sometimes aliasing, or the superimposition of smaller periods, can lead to misleading results as in figure 4.30. Here the maximum occurs around 23 hours. This length of time indicates daily patterns, so in this case it might be necessary to investigate some of the smaller components of this peak to study delay. In figure 4.31 the

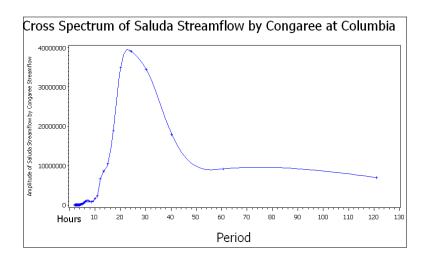


Figure 4.30: Spectrum Example 2

spectrum is zoomed in to periods less than 4. The common pattern of a maximum in the vicinity of 3 or 4 arises. It turns out that a delay of 3 yielded a good model fit.

In this case, the cross correlation plot showed a peak at 3 hours for the Saluda River (Figure 4.3).

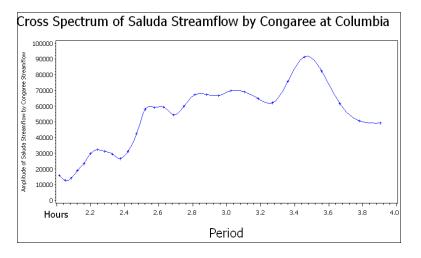


Figure 4.31: Spectrum Example 3

Using both the cross correlation function and the cross spectrum can lead to the delay parameter, but trial and error might still be necessary to develop a good model.

Chapter 5

Conclusions

It is possible to develop decent predictive models for multiple input ARIMA models for streamflow data. There will be no "silver bullet" for such models although it may be possible to categorize flow periods into a finite set of patterns which may then be modelled. It may even be possible to construct a piecewise ARIMA model for putting these together in a meaningful way.

Using the multiple input transfer function method we were able to discover details about the delays between the monitoring stations, and discovered how the delay is not necessarily constant but changes with flow. This will be a serious complication to any attempt to develop a comprehensive model.

Good predictive models were attainable without differencing. These usually corresponded to time sequences of three to five days and contained data that varied in complexity. Both the one step ahead and the long term forecasts can be fairly accurate when river management is consistent from day to day.

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Appendix A

Model Diagnostic Results

ARIMA Model Identification, Estimation, and Forecast Thursday, 5 September 1996 - Tuesday, 10 September 1996

The ARIMA Procedure

Crosscorrelation Check of Residuals with Input logsaluda_flow

10	CIII		rı /						
Lag	Square	DF	ChiSq			Crosscor	relations-		
5	5.14	4	0.2734	-0.028	-0.048	-0.082	-0.143	0.133	0.010
11	9.25	10	0.5088	-0.107	0.078	-0.101	0.086	0.016	-0.055
17	9.96	16	0.8688	-0.033	0.036	0.002	0.013	-0.021	0.060
23	13.25	22	0.9259	0.002	-0.028	0.034	-0.038	0.146	0.078
	Cro	osscorr	elation Ch	eck of Res	iduals wit	h Input lo	gbroad_flo	υW	

To Lag	Chi- Square	DF	Pr > ChiSq						
5	3.49	4	0.4787	0.066	-0.127	0.082	-0.074	0.047	0.004
11	9.04	10	0.5284	-0.083	-0.072	-0.040	0.125	0.145	-0.070
17	9.96	16	0.8687	0.073	0.042	-0.027	-0.010	0.035	-0.003
23	13.98	22	0.9024	-0.076	-0.133	-0.123	-0.018	0.036	-0.007

Autocorrelation Check of Residuals

To Lag	Chi- Square	DF	Pr > ChiSq			Autocorr	elations		
6	1.28	3	0.7334	-0.001	-0.023	0.075	-0.064	0.028	0.007
12	10.69	9	0.2974	0.028	-0.006	-0.183	0.142	0.073	-0.128
18	13.53	15	0.5618	0.098	-0.059	-0.085	0.013	-0.040	0.001
24	17.31	21	0.6919	-0.093	0.014	-0.013	-0.078	0.074	-0.081

Table A.1: Model Diagnostics for 5-10 September 1996 Streamflow

Streamflow Diagnostics for Residual Series

Thursday, 5 September 1996 - Tuesday, 10 September 1996

The ARIMA Procedure

Autocorrelation Check for White Noise

To	Chi-		Pr >						
Lag	Square	DF	ChiSq			Autocorr	elations		
6	1.45	6	0.9625	-0.011	-0.026	0.073	-0.077	0.021	0.011
12	12.06	12	0.4406	0.035	-0.015	-0.197	0.159	0.068	-0.126
18	14.65	18	0.6861	0.098	-0.059	-0.077	0.019	-0.025	-0.012

Table A.2: Streamflow Residual White Noise Check, September 1996

Autocorrelation Check of Stage Residuals

Thursday, 5 September 1996 - Tuesday, 10 September 1996

To Lag	Chi- Square	DF	Pr > ChiSq			Autocorr	elations		
6	3.34	1	0.0676	0.001	-0.037	-0.012	-0.107	0.006	-0.085
12	6.66	7	0.4650	0.068	-0.046	-0.012	0.016	0.102	-0.041
18	14.13	13	0.3647	-0.013	-0.085	-0.169	0.000	-0.055	0.056
24	25.22	19	0.1534	0.051	-0.061	0.158	0.050	0.088	0.134
30	29.49	25	0.2441	-0.005	-0.043	-0.098	0.032	0.028	0.092
	Cı	rosscor	relation (Check of Re	siduals wi	th Input c	ongaree_co	lumbia_sta	ge
То	Chi-		Pr >						
Lag	Square	DF	${\tt ChiSq}$			Crosscor	relations-		
5	1.73	4	0.7855	0.004	0.032	-0.037	-0.086	-0.005	0.042
11	7.54	10	0.6732	-0.025	-0.110	0.005	-0.147	-0.050	-0.044

-0.067

0.135

0.147

-0.055

17

23

29

35

18.63

22.81

26.43

33.57

16

22

28

34

0.2885

0.4124

0.5495

0.4884

Table A.3: Stage Model Diagnostics, September 1996

0.059

0.007

-0.029

0.010

0.006

-0.025

0.027

-0.070

-0.064

0.000

0.027

-0.182

0.014

-0.083

0.005

-0.033

0.248

0.045

-0.017

0.074

Stage Diagnostics for Residual Series

Thursday, 5 September 1996 - Tuesday, 10 September 1996

The ARIMA Procedure

Autocorrelation Check for White Noise

To	Chi-		Pr >						
Lag	Square	DF	${\tt ChiSq}$			Autocorr	elations		
6	0.20	6	0.9998	0.030	0.007	-0.002	-0.011	-0.007	-0.011
12	0.25	12	1.0000	-0.011	0.004	-0.003	0.004	0.003	-0.011
18	0.28	18	1.0000	-0.000	0.001	-0.012	-0.002	0.005	0.002

Table A.4: Stage Residual White Noise Check, September 1996

ARIMA Model Identification, Estimation, and Forecast Friday, 21 July 1995 - Sunday, 23 July 1995

Crosscorrelation Check of Residuals with Input logsal8504_flow

To Lag	Chi- Square	DF	Pr > ChiSq			Crosscor	relations-		
5	3.28	4	0.5122	-0.038	-0.123	0.180	-0.077	0.088	0.153
11	6.77	10	0.7473	-0.046	-0.045	0.100	-0.211	-0.045	0.177
17	9.20	16	0.9048	0.114	-0.047	0.032	-0.039	-0.124	0.176
23	9.76	22	0.9883	-0.043	0.009	0.108	-0.018	-0.013	0.027
	Cro	osscorr	elation Ch	neck of Res	iduals wit	h Input lo	gals1000_f	low	
То	Chi-		Pr >						
Lag	Square	DF	ChiSq			Crosscor	relations-		
5	7.52	4	0.1109	-0.223	-0.323	-0.234	-0.096	-0.006	0.056
11	14.19	10	0.1644	0.171	0.324	0.185	-0.122	0.106	-0.043
17	17.66	16	0.3444	-0.093	-0.001	0.025	-0.056	-0.186	-0.234
23	19.85	22	0.5925	0.062	0.106	0.137	0.031	0.046	0.166
			Autoc	correlation	Check of	Residuals			
То	Chi-		Pr >						
Lag	Square	DF	ChiSq			Autocorr	elations		
6	2.02	4	0.7314	0.010	0.026	-0.096	-0.147	-0.068	0.079
12	9.93	10	0.4469	-0.036	-0.069	-0.093	-0.265	-0.164	0.159
18	12.97	16	0.6749	0.043	0.065	0.138	0.030	-0.103	0.082
24	15.92	22	0.8200	-0.031	0.136	0.033	0.042	-0.090	0.052

Table A.5: Streamflow Model Diagnostics for 21-23 July, 1995

Diagnostics for Residual Series Friday, 21 July 1995 - Sunday, 23 July 1995

The ARIMA Procedure

Autocorrelation Check of Residuals

To	Chi-		Pr >						
Lag	Square	DF	ChiSq			Autocorr	elations		
6	5.28	4	0.2594	0.181	0.213	0.174	0.010	-0.083	0.056
12	11.93	10	0.2896	-0.062	-0.249	-0.073	-0.222	-0.046	-0.026
18	12.63	16	0.6999	0.031	0.057	-0.006	-0.055	-0.035	0.039
24	21.53	22	0.4884	-0.166	-0.043	-0.149	-0.164	-0.049	-0.132
30	27.95	28	0.4669	-0.054	-0.061	0.104	0.018	0.156	0.055
			Autoco	rrelation	Check for	White Nois	е		
То	Chi-		Pr >						
Lag	Square	DF	ChiSq			Autocorr	elations		
6	1.96	6	0.9230	0.007	0.025	-0.106	-0.134	-0.068	0.082
12	9.51	12	0.6593	-0.032	-0.067	-0.090	-0.258	-0.161	0.158
18	12.30	18	0.8315	0.045	0.053	0.124	0.036	-0.106	0.083

Table A.6: Streamflow Residual Diagnostics for 21-23 July, 1995

${\tt Crosscorrelation~Check~of~Residuals~with~Input~cong} 9500_{\tt stage}$

То	Chi-		Pr >							
Lag	Square	DF	ChiSq	Crosscorrelations						
5	0.87	4	0.9293	0.089	-0.004	0.008	-0.093	0.052	0.087	
11	5.92	10	0.8220	-0.204	-0.220	-0.042	-0.107	0.037	0.231	
17	11.05	16	0.8064	0.007	-0.130	0.343	-0.150	0.005	0.057	
23	12.57	22	0.9445	-0.126	-0.061	-0.040	-0.134	-0.074	0.052	
29	15.59	28	0.9715	-0.037	-0.160	0.200	0.139	-0.031	0.084	

Table A.7: Stage Model Diagnostics for 21-23 July, 1995

ARIMA Model Identification, Estimation, and Forecast Wednesday, 28 April 1999 - Friday, 7 May 1999

The ARIMA Procedure

Crosscorrelation Check of Residuals with Input logsal8504_flow

To Lag	Chi- Square	DF	Pr > ChiSq			Crosscor	relations-		
5	3.88	4	0.4227	0.093	0.007	0.078	0.057	-0.020	0.018
11	5.20	10	0.8774	0.050	0.029	-0.004	0.052	0.016	-0.008
17	7.21	16	0.9689	0.080	-0.027	0.025	0.025	-0.025	-0.027
23	9.67	22	0.9891	0.057	-0.054	0.052	-0.036	0.011	0.041
29	10.38	28	0.9990	-0.050	0.018	-0.009	0.007	0.018	0.013
35	11.53	34	0.9999	0.015	0.008	0.057	-0.001	0.042	0.018
41	16.32	40	0.9997	-0.004	-0.021	0.031	-0.102	0.057	-0.090
	Cro	osscorr	elation Ch	neck of Res	iduals wit	h Input lo	gals1000_f	low	
То	Chi-		Pr >						
Lag	Square	DF	ChiSq			Crosscor	relations-		
5	2.39	3	0.4961	0.064	-0.019	-0.033	-0.071	0.018	0.028
11	4.70	9	0.8593	0.037	0.054	-0.009	0.061	-0.039	-0.042
17	11.16	15	0.7413	-0.011	0.119	-0.132	0.005	0.015	-0.004
23	11.81	21	0.9446	-0.022	0.029	-0.035	0.009	0.006	0.023
29	18.95	27	0.8719	0.107	-0.060	0.111	0.075	0.022	-0.042
35	22.45	33	0.9170	-0.003	-0.053	-0.114	-0.023	0.029	0.011
			Autoc	correlation	Check of	Residuals			
To	Chi-		Pr >						
Lag	Square	DF	ChiSq			Autocorr	elations		
6	0.00	0	<.0001	-0.014	-0.026	0.084	0.030	-0.066	-0.105
12	8.86	5	0.1149	0.003	0.016	-0.034	0.035	0.092	0.073
18	16.71	11	0.1167	0.062	-0.129	0.112	-0.033	-0.003	0.021
24	22.33	17	0.1724	0.025	0.081	0.060	0.046	0.081	-0.066
30	26.38	23	0.2831	0.002	-0.006	-0.021	0.057	0.009	0.113

Table A.8: Streamflow Residual Diagnostics, May 1999

-0.013

0.091

0.008

0.080

0.056

-0.040

Diagnostics for Residual Series Wednesday, 28 April 1999 - Friday, 7 May 1999

31.33

29

0.3502

36

The ARIMA Procedure

Autocorrelation Check for White Noise

To Lag	Chi- Square	DF	Pr > ChiSq	Autocorrelations					
6	7.04	6	0.3175	-0.010	-0.015	0.056	0.044	-0.139	-0.089
12	13.14	12	0.3588	0.016	0.003	-0.040	0.029	0.152	0.040
18	18.92	18	0.3966	0.050	-0.121	0.084	-0.035	-0.004	0.011

Table A.9: Streamflow Residual White Noise Check, May 1999

The ARIMA Procedure

Crosscorrelation Check of Residuals with Input cong9500_stage

To Lag	Chi- Square	DF	Pr > ChiSq			Crosscor	relations-		
5	1.99	4	0.7369	-0.031	0.020	-0.015	0.042	0.028	-0.076
11	3.90	10	0.9516	-0.044	0.059	-0.022	0.051	0.012	-0.029
17	6.23	16	0.9854	-0.057	0.001	0.036	-0.081	-0.015	-0.006
23	9.73	22	0.9886	0.059	0.068	0.042	0.021	-0.064	-0.053
29	13.69	28	0.9892	0.085	-0.013	-0.019	0.064	-0.043	-0.077
35	26.57	34	0.8142	0.119	0.152	0.073	-0.061	-0.089	-0.098
			Autoc	correlation	Check of	Residuals			
To	Chi-		Pr >						
Lag	Square	DF	ChiSq			Autocorr	elations		
6	5.69	1	0.0170	0.020	-0.076	0.092	-0.080	0.039	0.063
12	10.29	7	0.1726	0.013	-0.053	-0.039	0.004	0.116	0.053
18	19.37	13	0.1119	-0.044	0.019	-0.053	-0.036	0.181	0.017
24	31.50	19	0.0355	-0.168	0.038	0.065	0.003	0.133	0.019
30	33.04	25	0.1301	0.001	-0.015	0.013	0.047	0.059	-0.017
36	43.82	31	0.0632	-0.021	-0.013	0.025	0.183	0.087	-0.025

Table A.10: Stage Residual Diagnostics, May 1999

Stage Diagnostics for Residual Series Wednesday, 28 April 1999 - Friday, 7 May 1999

The ARIMA Procedure

Autocorrelation Check for White Noise

To Lag	Chi- Square	DF	Pr > ChiSq	Autocorrelations						
6	1.38	6	0.9673	-0.076	-0.018	0.016	-0.002	0.010	0.003	
12	1.40	12	0.9999	-0.002	0.002	0.005	0.001	0.007	0.007	
18	1.43	18	1.0000	-0.008	0.007	0.003	-0.003	0.001	-0.002	

Table A.11: Stage Residual White Noise Check, May 1999

Appendix B

SAS/AF Modelling Application

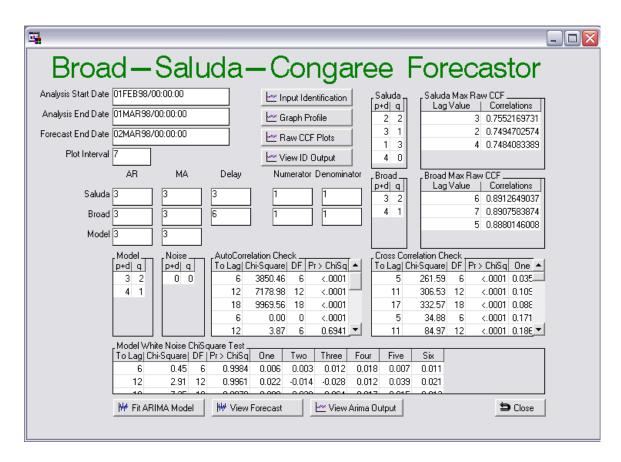


Figure B.1: Flow Model Fit Application