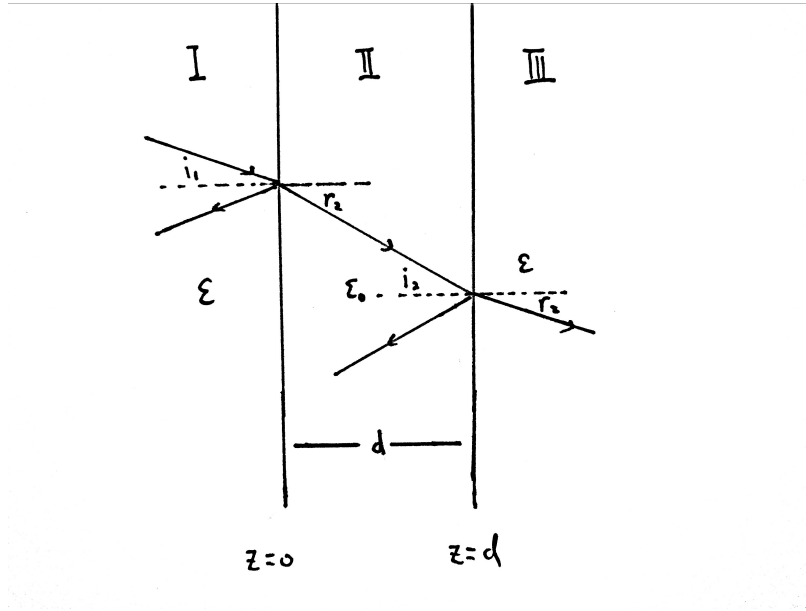


HW1, Electromagnetism II, Spring 2017

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Jackson 7.3 (a)



The path and symbols are shown as above. The waves in three regions are:

Region I:

$$\begin{aligned}\vec{E}_1 &= \vec{E}_1 e^{i\vec{k}_1 \cdot \vec{x} - i\omega t} & \vec{B}_1 &= \sqrt{\mu_0 \varepsilon} \frac{\vec{k}_1 \times \vec{E}_1}{k_1} \\ \vec{E}'_1 &= \vec{E}'_1 e^{i\vec{k}'_1 \cdot \vec{x} - i\omega t} & \vec{B}'_1 &= \sqrt{\mu_0 \varepsilon} \frac{\vec{k}'_1 \times \vec{E}'_1}{k'_1}\end{aligned}$$

Region II:

$$\begin{aligned}\vec{E}_2 &= \vec{E}_2 e^{i\vec{k}_2 \cdot \vec{x} - i\omega t} & \vec{B}_2 &= \sqrt{\mu_0 \varepsilon_0} \frac{\vec{k}_2 \times \vec{E}_2}{k_2} \\ \vec{E}'_2 &= \vec{E}'_2 e^{i\vec{k}'_2 \cdot \vec{x} - i\omega t} & \vec{B}'_2 &= \sqrt{\mu_0 \varepsilon_0} \frac{\vec{k}'_2 \times \vec{E}'_2}{k'_2}\end{aligned}$$

Region III:

$$\vec{E}_3 = \vec{E}_3 e^{i\vec{k}_3 \cdot \vec{x} - i\omega t} \quad \vec{B}_3 = \sqrt{\mu_0 \varepsilon} \frac{\vec{k}_3 \times \vec{E}_3}{k_3}$$

where $k_1 = k'_1 = k_3 = \omega\sqrt{\mu_0\varepsilon}$ and $k_2 = k'_2 = \omega\sqrt{\mu_0\varepsilon_0}$. The phases match on the plane at $z = 0$ and $z = d$,

$$k_1 \sin i_1 = k'_1 \sin i_1 = k_2 \sin r_1$$

$$k_2 \sin i_2 = k'_2 \sin i_2 = k_2 \sin r_2$$

$$r_1 = i_2$$

Next we consider the boundary conditions at $z = 0$ and $z = d$.

I-II:

$$\begin{aligned} [\varepsilon(\vec{E}_1 + \vec{E}'_1) - \varepsilon_0\vec{E}_2 - \varepsilon_0\vec{E}'_2] \cdot \vec{n} &= 0 \\ [\vec{k}_2 \times \vec{E}_1 + \vec{k}'_1 \times \vec{E}'_1 - \vec{k}_2 \times \vec{E}_2 - \vec{k}'_2 \times \vec{E}'_2] \cdot \vec{n} &= 0 \\ [\vec{E}_1 + \vec{E}'_1 - \vec{E}_2 - \vec{E}'_2] \times \vec{n} &= 0 \\ [\vec{k}_1 \times \vec{E}_1 + \vec{k}'_1 \times \vec{E}'_1 - \vec{k}_2 \times \vec{E}_2 - \vec{k}'_2 \times \vec{E}'_2] \times \vec{n} &= 0 \end{aligned}$$

II-III:

$$\begin{aligned} [\varepsilon_0(\vec{E}_2 + \vec{E}'_2) - \varepsilon\vec{E}_3] \cdot \vec{n} &= 0 \\ [\vec{k}_2 \times \vec{E}_2 + \vec{k}'_2 \times \vec{E}'_2 - \vec{k}_3 \times \vec{E}_3] \cdot \vec{n} &= 0 \\ [\vec{E}_2 + \vec{E}'_2 - \vec{E}_3] \times \vec{n} &= 0 \\ [\vec{k}_2 \times \vec{E}_2 + \vec{k}'_2 \times \vec{E}'_2 - \vec{k}_3 \times \vec{E}_3] \times \vec{n} &= 0 \end{aligned}$$

Let's discuss two different cases.

Case I

When the electric field perpendicular to the plane of incidence, the boundary conditions turn to,

$$\begin{bmatrix} 1 & -1 & -1 & 0 \\ -\sqrt{\varepsilon} \cos i_1 & -\sqrt{\varepsilon_0} \cos r_1 & \sqrt{\varepsilon_0} \cos r_1 & 0 \\ 0 & e^{i\phi} & e^{-i\phi} & -1 \\ 0 & \sqrt{\varepsilon_0} \cos i_2 e^{i\phi} & -\sqrt{\varepsilon_0} \cos i_2 e^{-i\phi} & -\sqrt{\varepsilon} \cos r_2 \end{bmatrix} \begin{bmatrix} E'_1 \\ E_2 \\ E'_2 \\ E_3 \end{bmatrix} = \begin{bmatrix} -E_1 \\ \sqrt{\varepsilon} E_1 \cos i_1 \\ 0 \\ 0 \end{bmatrix}$$

where the phase ϕ is given by $\phi = kd \cos r_1 = \frac{\omega d \sqrt{1-n^2 \sin^2 i_1}}{c}$. Our aim is to find,

$$\begin{aligned} \frac{E'_1}{E_1} &= \frac{i(1-\alpha^2) \sin \phi}{2\alpha \cos \phi - i(1+\alpha^2) \sin \phi} \\ \frac{E_3}{E_1} &= \frac{2\alpha}{2\alpha \cos \phi - i(1+\alpha^2) \sin \phi} \end{aligned}$$

where $\alpha = \frac{n \cos i_1}{\sqrt{1-n^2 \sin^2 i_1}}$. To calculate the transmission and reflection coefficients:

$$\begin{aligned} T &= \frac{|E_3|^2}{|E_1|^2} = \frac{4\alpha^2}{4\alpha^2 + (1-\alpha^2)^2 \sin^2 \phi} \\ R &= \frac{|E'_1|^2}{|E_1|^2} = \frac{(1-\alpha^2)^2 \sin^2 \phi}{4\alpha^2 + (1-\alpha^2)^2 \sin^2 \phi} \end{aligned}$$

Case II

Similarly, we can write the boundary condition in matrix when the electric field is parallel to the plane of incidence.

$$\begin{bmatrix} -\cos i_1 & -\cos r_1 & \cos r_1 & 0 \\ \sqrt{\varepsilon} & -\sqrt{\varepsilon_0} & -\sqrt{\varepsilon_0} & 0 \\ 0 & \cos i_2 e^{i\phi} & -\cos i_2 e^{-i\phi} & -\cos r_2 \\ 0 & \sqrt{\varepsilon_0} e^{i\phi} & \sqrt{\varepsilon_0} e^{-i\phi} & \sqrt{\varepsilon} \end{bmatrix} \begin{bmatrix} E'_1 \\ E_2 \\ E'_2 \\ E_3 \end{bmatrix} = \begin{bmatrix} -\cos i_1 E_1 \\ -\sqrt{\varepsilon} E_1 \\ 0 \\ 0 \end{bmatrix}$$

In this case,

$$T = \frac{|E_3|^2}{|E_1|^2} = \frac{4\beta^2}{4\beta^2 + (1 - \beta^2)^2 \sin^2 \phi}$$

$$R = \frac{|E'_1|^2}{|E_1|^2} = \frac{(1 - \beta^2)^2 \sin^2 \phi}{4\beta^2 + (1 - \beta^2)^2 \sin^2 \phi}$$

where $\beta = \frac{\cos i_1}{n\sqrt{1 - n^2 \sin^2 i_1}}$.

Jackson 7.12 (a)

In absence of external magnetic field, the equations are given as below:

$$\begin{aligned}\vec{J} &= \sigma(\omega)\vec{E} \\ \frac{\partial \rho}{\partial t} + \nabla \times \vec{J} &= 0 \\ \nabla \times \vec{E} &= \frac{\rho}{\varepsilon_0}\end{aligned}$$

Substitute the first and the third equations to the second one, we find

$$\frac{\partial \rho}{\partial t} + \frac{\sigma(\omega)}{\varepsilon_0} \rho = 0$$

The time-Fourier-transformed charge density is

$$\rho(\vec{x}, \omega) = \frac{1}{2\pi} \int_{-\infty}^{\infty} \rho(\vec{x}, t) e^{-i\omega t} dt$$

Inserting to the continuity equation, we can rewrite it as,

$$\boxed{[-i\omega + \frac{\sigma(\omega)}{\varepsilon_0}] \rho(\vec{x}, \omega) = 0}$$

Jackson 7.12 (b)

From the continuity equation above, we may write

$$\sigma(\omega) - i\omega\varepsilon_0 = 0$$

while $\sigma(\omega) = \sigma_0/(1 - i\omega\tau)$ and $\sigma_0 = \varepsilon_0\omega_p^2\tau$. The equation above can be rewrite as,

$$\tau\varepsilon_0\omega^2 - i\varepsilon_0\omega - \varepsilon_0 + 0\omega_p^2\tau$$

which can be solved in the form of

$$\omega = \frac{i\varepsilon_0 \pm \sqrt{-\varepsilon_0 + 4\varepsilon_0\omega_p^2\tau^2}}{2\tau\varepsilon_0}$$

In the approximation $\omega_p\tau \gg 1$,

$$\sqrt{-\varepsilon_0 + 4\varepsilon_0\omega_p^2\tau^2} \approx 2\varepsilon_0\omega_p\tau$$

The solutions for ω turn to

$$\omega = \frac{1}{2\tau} \pm \omega_p$$

This can be interpret as oscillations at the plasma frequency while decay with a factor $1/2\tau$.

Jackson 7.16 (a)

Write the electric field as,

$$\vec{E} = \vec{E}_0 e^{i\vec{k} \cdot \vec{x} - i\omega t}$$

Then calculate,

$$\nabla \times \vec{E} = i\vec{k} \times \vec{E}, \quad \frac{\partial}{\partial t} \vec{E} = -i\omega \vec{E}$$

From the Maxwell equations,

$$\nabla \times \vec{E} + \frac{\partial}{\partial t} \vec{B} = 0$$

$$\nabla \times \vec{H} - \frac{\partial}{\partial t} \vec{D} = 0$$

By taking the curl of the first equation and substitute the second one, we find

$$\nabla \times (\nabla \times \vec{E}) + \mu_0 \frac{\partial^2}{\partial t^2} \vec{D} = 0$$

Using the results above,

$$\boxed{\vec{k} \times (\vec{k} \times \vec{E}) + \mu_0 \omega^2 \vec{D} = 0}$$

Jackson 7.16 (b)

With $\vec{k} = k\vec{n}$ and $\vec{D} = \varepsilon\vec{E}$ (ε is a 3 by 3 matrix), we may write the result in part (a) as

$$k^2[\vec{n}(\vec{n} \cdot \vec{E}) - \vec{E}(\vec{n} \cdot \vec{n})] + \mu_0\omega^2\varepsilon\vec{E} = 0$$

When choosing the principle axes as the coordinate axes, the components of displacement can be written as $D_i = \varepsilon_i E_i$. Form the equation above in matrix,

$$\begin{bmatrix} n_1^2 - 1 & n_1 n_2 & n_1 n_3 \\ n_2 n_1 & n_2^2 - 1 & n_2 n_3 \\ n_3 n_1 & n_3 n_2 & n_3^2 - 1 \end{bmatrix} \vec{E} + v^2 \begin{bmatrix} 1/v_1^2 & & \\ & 1/v_2^2 & \\ & & 1/v_3^2 \end{bmatrix} \vec{E} = 0$$

where we used $v = \omega/k$ and $v_i = 1/\sqrt{\mu_0\varepsilon_0}$. The nontrivial solution exist only when the determinant is equal to zero.

$$\begin{aligned} & \begin{vmatrix} n_1^2 - 1 + \frac{v^2}{v_1^2} & n_1 n_2 & n_1 n_3 \\ n_2 n_1 & n_2^2 - 1 + \frac{v^2}{v_2^2} & n_2 n_3 \\ n_3 n_1 & n_3 n_2 & n_3^2 - 1 + \frac{v^2}{v_3^2} \end{vmatrix} \\ &= \frac{v^6}{v_1^2 v_2^2 v_3^2} - \left(\frac{n_1^2 + n_2^2}{v_1^2 v_2^2} + \frac{n_1^2 + n_3^2}{v_1^2 v_3^2} + \frac{n_2^2 + n_3^2}{v_2^2 v_3^2} \right) v^4 + \left(\frac{n_1^2}{v_1^2} + \frac{n_2^2}{v_2^2} + \frac{n_3^2}{v_3^2} \right) v^2 \\ &= \frac{v^2}{v_1^2 v_2^2 v_3^2} [n_1^2(v^2 - v_2^2)(v^2 - v_3^2) + n_2^2(v^2 - v_1^2)(v^2 - v_3^2) + n_3^2(v^2 - v_1^2)(v^2 - v_2^2)] \\ &= \frac{v^2}{v_1^2 v_2^2 v_3^2} \frac{1}{(v^2 - v_1^2)(v^2 - v_2^2)(v^2 - v_3^2)} \left[\frac{n_1^2}{v^2 - v_1^2} + \frac{n_2^2}{v^2 - v_2^2} + \frac{n_3^2}{v^2 - v_3^2} \right] = 0 \end{aligned}$$

Except for trivial solution $v = 0$, we have two distinct solutions for v , given by the quadratic equation. For each solution, the phase velocity satisfies the Fresnel equation,

$$\sum_{i=1}^3 \frac{n_i^2}{v^2 - v_i^2} = 0$$

Jackson 7.16 (c)

From the equation in part a, we have

$$\vec{n} \times (\vec{n} \times \vec{E}_a) = -\mu_0 v_a^2 \vec{D}_a$$

Hence the dot product of the two displacement can be written as,

$$\begin{aligned} \vec{D}_a \cdot \vec{D}_b &= -\frac{1}{\mu_0 v_a^2} (\vec{n} \times (\vec{n} \times \vec{E}_a)) \cdot \vec{D}_b \\ &= -\frac{1}{\mu_0 v_a^2} (\vec{n}(\vec{n} \cdot \vec{E}_a) - \vec{E}_a) \cdot \vec{D}_b \\ &= \frac{1}{\mu_0 v_a^2} \vec{E}_a \cdot \vec{D}_b \end{aligned}$$

Meanwhile we can also write the product as

$$\vec{D}_a \cdot \vec{D}_b = \frac{1}{\mu_0 v_b^2} \vec{D}_a \cdot \vec{E}_b$$

Thus,

$$\mu_0(v_a^2 - v_b^2) \vec{D}_a \cdot \vec{D}_b = \vec{E}_a \cdot \vec{D}_b - \vec{D}_a \cdot \vec{E}_b$$

where $\vec{E}_a \cdot \vec{D}_b - \vec{D}_a \cdot \vec{E}_b = E_i^a \varepsilon_i E_i^b - \varepsilon_i E_i^a E_i^b = 0$. Since v_a and v_b are distinct solution for the wave, $v_a^2 \neq v_b^2$. Hence,

$$\boxed{\vec{D}_a \cdot \vec{D}_b = 0}$$

Jackson 7.28

Since the wave is circularly polarized, we can write the electric field as

$$\vec{E}(x, y, z, t) \simeq [E_0(x, y)(\vec{e}_1 \pm i\vec{e}_2) + F(x, y)\vec{e}_3]e^{ikz-i\omega t}$$

The field needs to satisfy $\nabla \cdot \vec{E} = 0$,

$$\frac{\partial E_0}{\partial x} \pm i \frac{\partial E_0}{\partial y} + ikF(x, y) = 0$$

$$F(x, y) = \frac{i}{k} \left(\frac{\partial E_0}{\partial x} \pm i \frac{\partial E_0}{\partial y} \right)$$

Thus the electric field is given approximately by

$$\vec{E}(x, y, z, t) \simeq [E_0(x, y)(\vec{e}_1 \pm i\vec{e}_2) + \frac{i}{k} \left(\frac{\partial E_0}{\partial x} \pm i \frac{\partial E_0}{\partial y} \right) \vec{e}_3]e^{ikz-i\omega t}$$

For the magnetic field, we have

$$\nabla \times \vec{E} - i\omega \vec{B} = 0$$

Since the amplitude changes slowly, the second order derivative for E_0 can be neglected.

$$\begin{aligned} \vec{B} &\simeq \frac{1}{i\omega} \nabla \times E_0(\vec{e}_1 \pm i\vec{e}_2)e^{ikz-i\omega t} \\ &= \frac{k}{i\omega} [\pm iE_0\vec{e}_1 + E_0\vec{e}_2 + \left(\frac{\partial E_0}{\partial x} \pm i \frac{\partial E_0}{\partial y} \right) \vec{e}_3]e^{ikz-i\omega t} \\ &= \mp \frac{k}{\omega} \vec{E} \end{aligned}$$

where $k/\omega = \sqrt{\mu\varepsilon}$