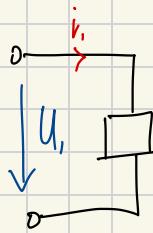
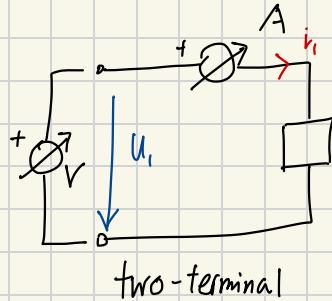


# Chapter 1

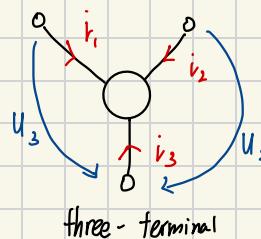
## 1.1 Reference Directions



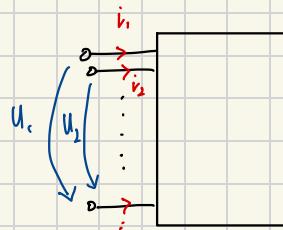
ASSOCIATED  
reference  
directions



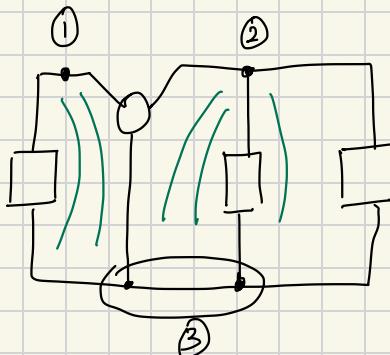
two-terminal



three-terminal



n-terminal

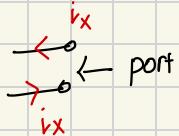


node is defined as a connection between 2 elements



3nodes  
5 branches

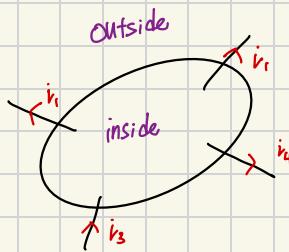
## 1.2 Ports



$i_x$  flowing into

first terminal  
and flowing out  
of second terminal

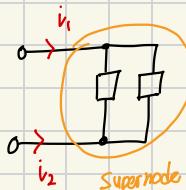
## 1.3 KCL



take into account the directions (out  $\oplus$ , in  $\ominus$ )

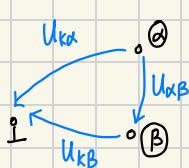
$$i_1 + i_2 + i_4 - i_3 = 0$$

KCL :  $\sum_{j \in \text{branches}} i_j = 0$   
Connected to node

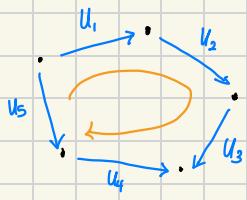


$$\text{KCL} : i_1 + i_2 = 0$$

## 1.4 KVL



$$\text{KVL} : U_{KA} - U_{KB} = U_{KA} - U_{KB}$$

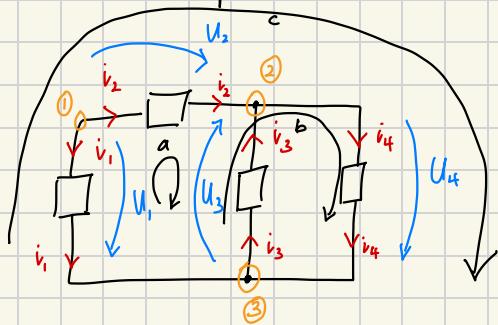


KVL :

$$U_1 + U_2 + U_3 - U_4 - U_5 = 0$$

KVL :

$$\sum_{\substack{j \in \text{branches} \\ \text{of loops}}} U_j = 0$$



$$KCL(1) : i_1 + i_2 = 0$$

$$\left. \begin{array}{l} \\ \end{array} \right\} + = i_1 - i_3 + i_4 = 0$$

$$KCL(2) : -i_3 + i_4 - i_2 = 0$$

$$KCL(3) : i_1 - i_3 + i_4 = 0$$

$$KVL(1) : -U_1 + U_2 - U_3 = 0 \quad \left. \begin{array}{l} \\ \end{array} \right\} + = -U_1 + U_2 + U_4 = 0$$

$$KVL(2) : U_3 + U_4 = 0$$

$$KVL(3) : U_2 + U_4 - U_1 = 0$$

## 1.5 Number of Linearly independent Kirchhoff's Eqns

$n$  nodes, e.g.,  $n=3$

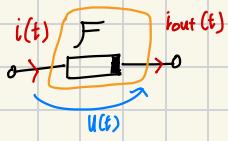
$n-1$  linearly KCL eqn, e.g.,  $n-1 = 2$  eqns

$b$  branches, e.g.,  $b=4$

$b-(n-1)$  linearly KVL eqns, e.g.,  $b-(n-1) = 4-(3-1) = 2$  eqns  
<sup>ind.</sup>  
 $\wedge$

## 2 Resistive One Ports

Characteristics



$$KCL: i(t) - i_{out}(t) = 0$$

$$i_{out}(t) = i(t)$$

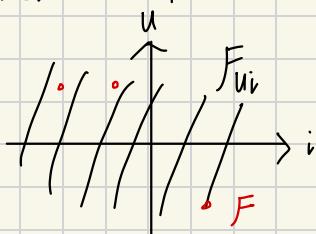
two-terminal = one-ports

$$\begin{aligned} \mathcal{F} &\subseteq \mathcal{F}_{ui} \\ \mathcal{F}_{ui} &= \{ (u, i) \mid \frac{u}{i_0} \in \mathbb{R}, \frac{i}{i_0} \in \mathbb{R} \} \end{aligned}$$

↓  
units

$$\mathcal{F} = \{ (u, i) \mid (u, i) \text{ is operating point of } \mathcal{F} \}$$

Every one port is  
a collection of points in  $\mathcal{F}_{ui}$  plane



### 2.1 Explicit Representation

$$\frac{i}{i_0} = \arctan \frac{u}{u_0} = \tan^{-1} \left( \frac{u}{u_0} \right) \quad \text{for } G$$

in general, one-port  $F$ :

Voltage-controlled repr.:

$$i = g_F(u)$$

$$G: i = g_G(u) = i_0 \arctan \frac{u}{u_0}$$

Current-controlled repr.:

$$u = r_F(i)$$

$$G: u = u_0 \tan \left( \frac{i}{i_0} \right)$$

$$i \in i_0 \left( -\frac{\pi}{2}, \frac{\pi}{2} \right)$$

## 2.2 Properties of One-Ports

### 2.2.1 Bilateral Property

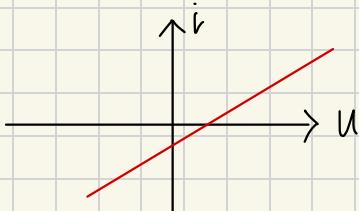
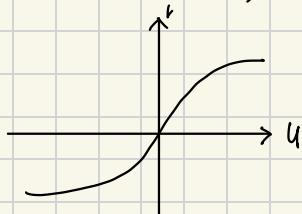
$$\forall (u, i) \in F : (-u, -i) \in F$$

$\Leftrightarrow$   
bilateral  $F$

$$i = g_F(u) : -i = g_F(-u)$$

$$i = -g_F(-u)$$

$$u = r_F(i) : u = -r_F(-i)$$



not-bilateral

## 2.2.2 Power

$$P(t) = U(t) \cdot i(t)$$

$$\exists (u, i) \in F : u_i < 0$$

$\Leftrightarrow$  active

$$\forall (u, i) \in F : u_i \geq 0$$

$\Leftrightarrow$  passive

$$\forall (u, i) \in F : u_i = 0$$

$\Leftrightarrow$  lossless

$$\exists (u, i) \in F : u_i \neq 0$$

$\Leftrightarrow$  lossy (opposite of lossless)

## 2.2.3 Source-Free

$$(0, 0) \in F : \text{source-free } F$$

## 2.2.4 Duality

duality constant :  $R_d$

$$(u, i) \in F :$$

$$u^d = R_d i \quad (u^d, i^d) \in F^d$$

$$i^d = \frac{1}{R_d} u$$

$$\text{e.g., } i = g_F(u)$$

$$\frac{1}{R_d} u^d = g_F(R_d i^d)$$

$$u^d = R_d g_F(R_d i^d)$$

$$u^d = r_F^d(i^d)$$

$$u = r_F(i) \rightarrow R_d$$

$$R_d i^d = r_F(\frac{1}{R_d} u^d)$$

$$i^d = \frac{1}{R_d} r_F(\frac{1}{R_d} u^d)$$

$$i^d = g_F^d(u^d)$$

## 2.3 Strictly linear one ports

$(u, i) \in F$ :

$$\forall k \in \mathbb{R} : (ku, ki) \in F$$

$\forall (u_1, i_1), (u_2, i_2) \in F$ :

$$(u_1 + u_2, i_1 + i_2) \in F$$

$k = -1$ :

$$\forall (u, i) \in F : (-u, -i) \in F$$

$\Leftrightarrow$  bilateral

$k = 0$

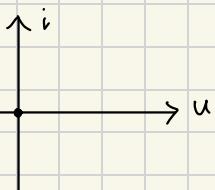
$(0, 0) \in F \Leftrightarrow$  source free

### 2.3.1 Nullator



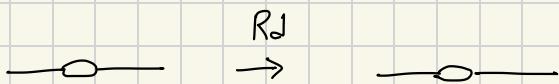
$$u = 0, i = 0$$

$$F_0 = \{(0, 0)\}$$

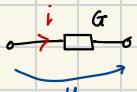


$$P = u \cdot i = 0 \Leftrightarrow \text{lossless}$$

$$U=0, i=0 \xrightarrow{R_d} U^d=0, i^d=0$$



### 2.3.2 Strictly linear Resistors



$$i = Gu$$

$$\downarrow R_d$$

$$\frac{1}{R_d} U^d = GR_d i^d$$

$$U^d = \frac{R_d^2 G}{R_d} i^d$$

$$i = Gu$$

$\downarrow$

conductance

$$G = \frac{i}{u} |_{u \neq 0}$$

$$= \frac{1A}{1V} = 1S$$

$$U = Ri$$

$\downarrow$

resistance

$$R = \frac{1}{G} \quad \frac{1V}{1A} = 1\Omega$$

#### 2.3.2.1 Open Circuits and short circuits

$$\begin{cases} i = GU \\ G = 0 \\ i = 0 \end{cases}$$

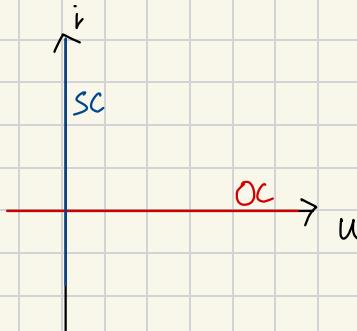
|

open  
circuit  
OC

$$\begin{cases} U = Ri \\ R = 0 \\ U = 0 \end{cases}$$

|

short circuit  
SC



OC, SC : lossless

define :

$$\frac{1}{0\Omega} = \infty \text{ s}$$

$$OC: G=0, R=\infty$$

$$SC: R=0, G=\infty$$

$$\frac{1}{0S} = \infty \Omega$$

### 2.3.2.2 Ohmic Resistors

$$0 \leq R \leq \infty \quad \text{or} \quad 0 \leq G \leq \infty$$

$$U = R \cdot i$$

$$P = R \cdot i \cdot i$$

$$= \underline{\underline{R}} \cdot i^2 \geq 0$$

$$\geq 0 \geq 0$$

$\Rightarrow$  passive

### 2.3.2.3 Negative Resistors

$$-\infty < R < 0$$

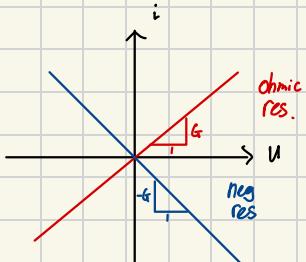
$$-\infty < G < 0$$

$$U = R_i$$

$$P = \underline{\underline{R}} \cdot i^2 \leq 0$$

$$\leq 0 \geq 0$$

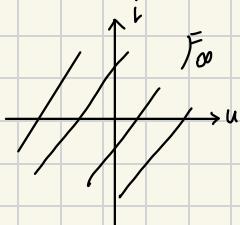
$\Rightarrow$  active



## 2.3.3 Norafor



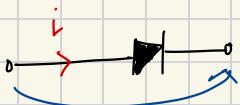
$$F_\infty = F_{ui}$$



no eqn.

$u$  arbitrary,  $i$  arbitrary

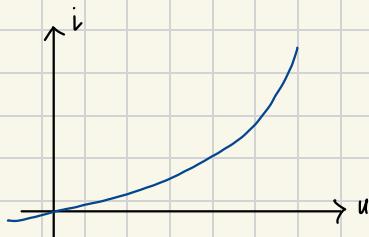
## 2.4 pn-Junction Diode



$$i = I_s (e^{\frac{u}{U_T}} - 1)$$

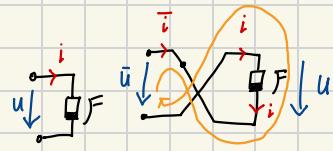
↓  
thermal  
voltage

$$u = U_T \ln\left(\frac{i}{I_s} + 1\right)$$



## 2.5 Basic One-Port Circuits

### 2.5.1 Polarity Reversal



$$KCL: i - 2i = 0$$

$$KVL: u - u = 0$$

$$\bar{u} = -u, \bar{i} = -i$$

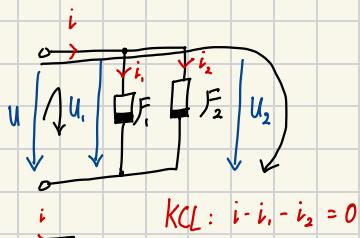


$$(u, i) \in \mathcal{F} : (\bar{u}, \bar{i}) = (-u, -i) \in \bar{\mathcal{F}}$$

$$i = g_F(u) : \bar{i} = -g_F(-\bar{u})$$

$= g_F(\bar{u})$  : bilateral

### 2.5.2 Parallel-Connection



$$KCL: i - i_1 - i_2 = 0$$

$$KVL: u - u_1 = 0 \\ u - u_2 = 0$$

$$i = i_1 + i_2$$

$$U = U_1$$

$$U = U_2$$

$$\rightarrow U = U_1 = U_2$$

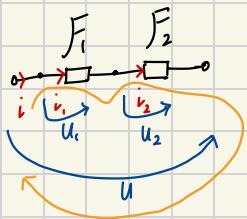
### Voltage-Control

$$i_1 = g_{F_1}(U_1)$$

$$i_2 = g_{F_2}(U_2)$$

$$i = g_{F_1}(U) + g_{F_2}(U) = g_G(U)$$

## 2.5.3 Series Connection



$$KCL: -i + i_1 = 0$$

$$-i_1 + i_2 = 0$$

$$KVL: u_1 + u_2 - u = 0$$

$$U = U_1 + U_2$$

$$i = i_1 = i_2$$

Series Connection is dual to parallel

$$U = r_{F_1}(i) + r_{F_2}(i)$$

## 2.5.4 Connection of Strictly linear Resistors

$$\text{Parallel sum: } \frac{1}{a \parallel b} = \frac{1}{a} + \frac{1}{b}$$

$$a \parallel b = \frac{ab}{a+b}$$

### 2.5.4.1 Parallel Connection



$$i = i_1 + i_2$$

$$\text{Ohm: } i = G_1 u + G_2 u$$

$$\begin{aligned} i &= (G_1 + G_2) u \\ &= G u \end{aligned}$$

$$G = G_1 + G_2$$

$$R = \frac{1}{G} = \frac{1}{\frac{1}{R_1} + \frac{1}{R_2}}$$

$$\frac{1}{R} = \frac{1}{R_1} + \frac{1}{R_2}$$

$$\Rightarrow R = R_1 \parallel R_2$$

$$i = Gu = (G_1 + G_2)u$$

$$i_1 = G_1 u$$

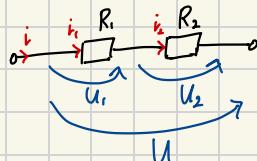
$$i_2 = G_2 u$$

$$\frac{i_1}{i} = \frac{G_1 u}{(G_1 + G_2)u} \quad \frac{i_2}{i_1} = \frac{G_2}{G_1}$$

$$= \frac{G_2}{G_1 + G_2}$$

Current divider rule

## 2.5.4.2 Series Connection



$$U = U_1 + U_2$$

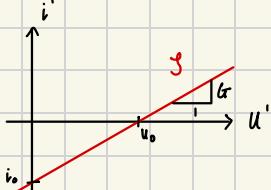
$$i = i_1 + i_2$$

$$R = R_1 + R_2$$

$$\frac{U_1}{U} = \frac{R_1}{R_1 + R_2}$$

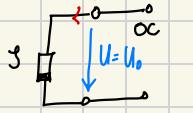
$$\frac{U_2}{U_1} = \frac{R_2}{R_1}$$

## 2.6 Linear sources

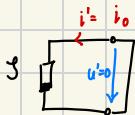


non-source free

$$U_0 : i = 0 \rightarrow OC$$



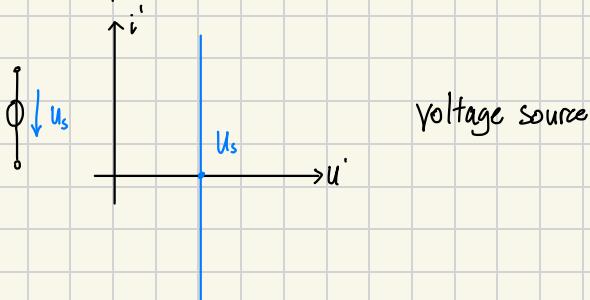
$$-i_0 : U' = 0 \rightarrow SC$$



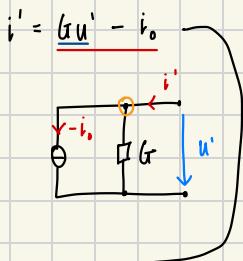
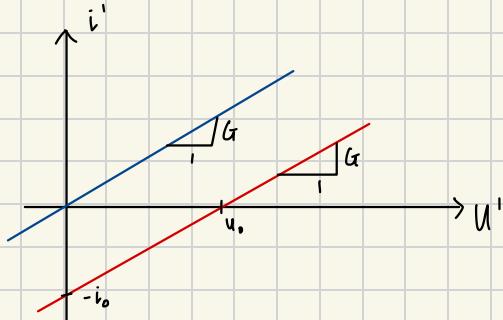
$$G = \frac{i_0}{U_0} \dots \text{internal Conductance}$$

$$R = \frac{U_0}{i_0} = \frac{1}{G} \dots \text{internal resistance}$$

### 2.6.1 Independent Sources



## 2.6.2 internal structure

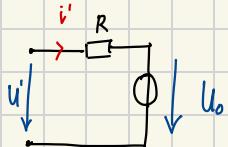


$$i' + i_0 = Gu'$$

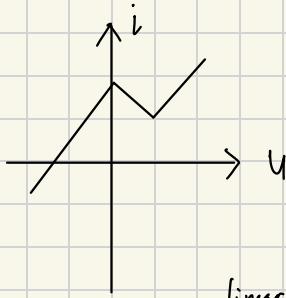
$$u' + \frac{1}{G}i' + \frac{1}{G}i_0$$

$$\frac{1}{G} = R, \quad G = \frac{i_0}{u_0}$$

$$u' = Ri' + U_0$$



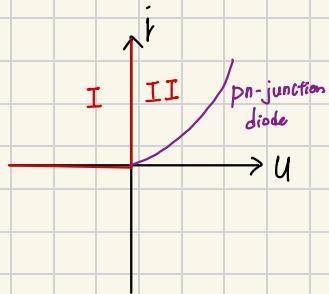
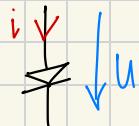
## 2.7 Piecewise linear One-Ports



Piecewise linear Diodes

2.7.1

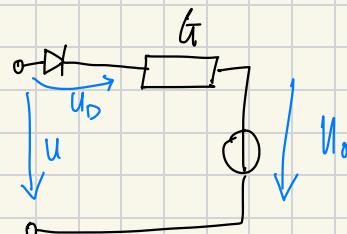
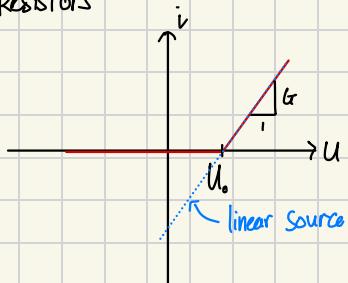
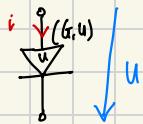
2.7.1.1 Ideal Diodes



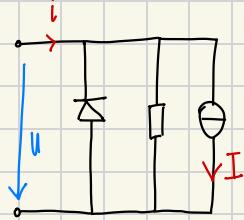
I:  $i=0$  for  $u \leq 0$

II:  $u=0$  for  $i \geq 0$

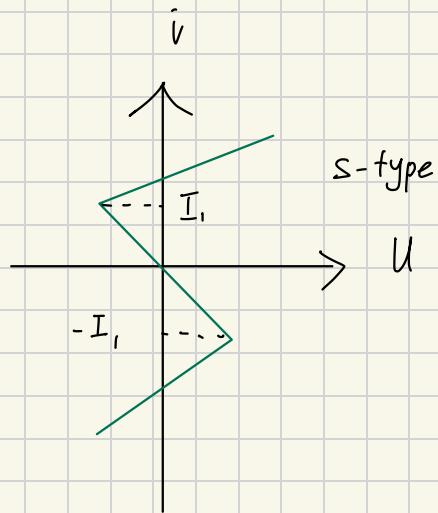
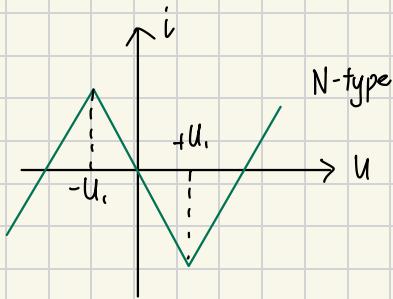
2.7.1.2 Concave Resistors



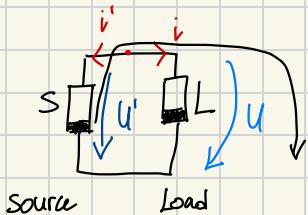
### 2.7.1.2 Convex resistor



### 2.7.2 Real Negative Resistors



### 2.8 one-Port Circuits



## 2.8.1 Operating Point

$$KCL : i' + i = 0$$

$$KVL : -U' + U = 0$$

Rearranging them

$$i' = -i$$

$$U' = U$$

$$(U', i') \in S$$

$$(U, i) \in L$$

$$\downarrow (U, -i) \in S$$

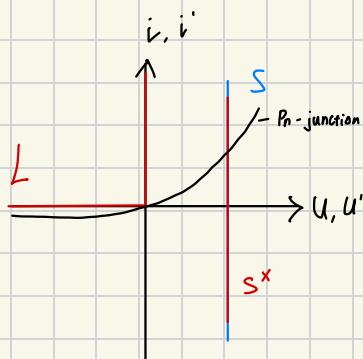
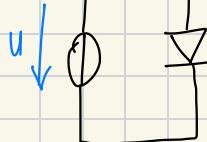
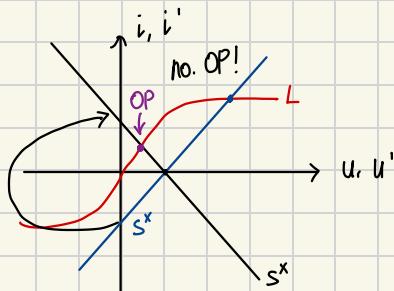
$$S = \{(U, i) / (U, -i) \in S\}$$

external source characteristic

$$(U, i) \in S^x \quad \& \quad (U, i) \in L$$

operating point

$$\emptyset' p = S^x \cap L$$

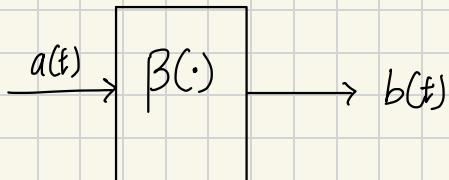


$$\emptyset' p = \{\} = \emptyset$$

## 2.8.2 Large Signal Analysis

system input:  $a(t)$

" output:  $b(t)$



$$b(t) = \textcircled{B}(a(t))$$

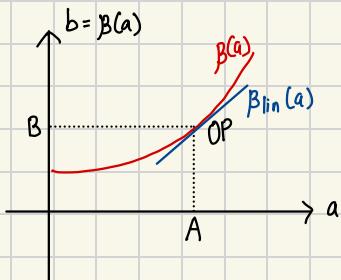
non-linear

## 2.8.3 Linearization

$$b(t) = B(a(t))$$

$$\approx k(a(t) - A) + B = B_{\text{lin}}(a(t))$$

$$\text{OP : } B = B(A)$$



$$k = \left. \frac{d B(a)}{d a} \right|_{a=A}$$

$B(a)$

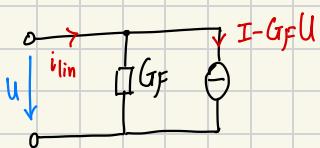
$$\rightarrow B_{\text{lin}}(a) = \left. \frac{d B(a)}{da} \right|_{a=A} \cdot (a - A) + B \rightarrow \text{impt. formula}$$

$$i = g_F(u), I = g_F(U) : \text{OP}$$

$$i_{\text{lin}} = \left. \frac{d g_F(u)}{du} \right|_{u=U} \cdot (u - U) + I$$

$$= G_F(u - U) + I$$

$$= G_F u + I - G_F U$$

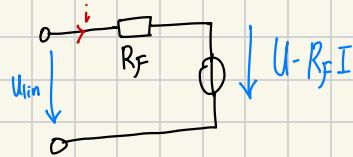


$$U = r_F(i), \text{ OP: } U = r_F(I)$$

$$U_{\text{lin}} = \left. \frac{d r_F(i)}{di} \right|_{i=I} \cdot (i - I) + U$$

$$R_F = \left. \frac{d r_F(i)}{di} \right|_{i=I}$$

$$U_{\text{lin}} = R_F i + U - R_F I$$



$g_F(\cdot)$  is the inverse function of  $r_F(\cdot)$

$$G_F = \frac{1}{R_F}$$

$$i_{\text{lin}} = G_F u + I - G_F U$$

$$\frac{1}{G_F} \cdot i_{\text{lin}} = u + \frac{1}{G_F} I - U$$

$$U = R_F \cdot i_{\text{lin}} + U - R_F \cdot I$$

## 2.8.4 Small Signal Analysis

$$\text{input } a(t) = A + \Delta a(t)$$

$$\text{output } b(t) = B + \Delta b(t)$$

$$b(t) = B(a(t))$$

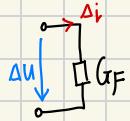
$$b_{\text{lin}}(t) = \left[ \frac{d B(a)}{a} \right]_{a=A} \cdot (a - A) + B$$

$$b_{\text{lin}}(t) - B = K(a(t) - A)$$

$$\Delta b(t) = K \Delta a(t)$$

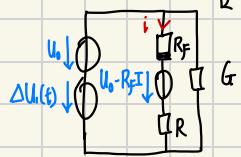
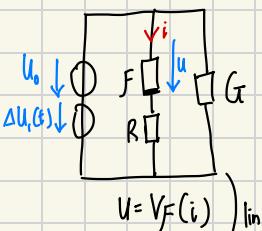
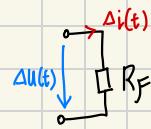
$$\stackrel{u(t)}{\overbrace{g_F}} \text{lin}(u) = I + G_F(u - U)$$

$$\Delta i(t) = G_F(\Delta u(t))$$

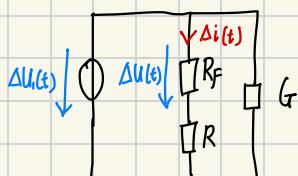


$$U_{\text{lin}}(t) = U + R_F(i - I)$$

$$\Delta U(t) = R_F \cdot \Delta i(t)$$



Small Signals:





Strictly linear two ports:

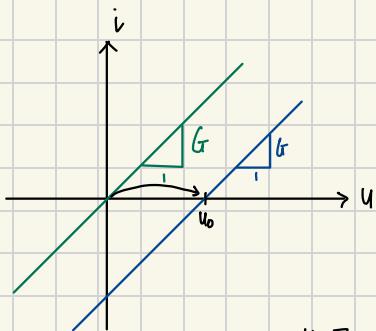
2 measurements:

$$\underline{U} = \begin{bmatrix} U^{(1)} & U^{(2)} \end{bmatrix}$$

$$\underline{I} = \begin{bmatrix} I^{(1)} & I^{(2)} \end{bmatrix}$$

$$\begin{bmatrix} \frac{U}{I} \end{bmatrix} = \begin{bmatrix} \frac{U}{I} \end{bmatrix} \subseteq \mathbb{C} \subseteq \mathbb{R}^2$$

### 3.3 Linear two ports



$$\begin{bmatrix} \frac{U}{I} \end{bmatrix} = \begin{bmatrix} \frac{U}{I} \end{bmatrix} \subseteq + \begin{bmatrix} \frac{U_0}{I_0} \end{bmatrix} \subseteq \mathbb{C} \subseteq \mathbb{R}^2$$

three measurements

$$\begin{bmatrix} \frac{U_0}{I_0} \end{bmatrix} = \begin{bmatrix} \frac{U^{(1)}}{I^{(1)}} \end{bmatrix} \quad \underline{U} = \begin{bmatrix} U^{(2)} - U^{(1)} & U^{(3)} - U^{(1)} \end{bmatrix}$$
$$\begin{bmatrix} \frac{U_0}{I_0} \end{bmatrix} = \begin{bmatrix} \frac{U^{(1)}}{I^{(1)}} & \frac{U^{(3)} - U^{(1)}}{I^{(3)} - I^{(1)}} \end{bmatrix}$$

$$\frac{U}{I} = \underline{\frac{U}{I}} \subseteq + U_0$$

$$\frac{U}{I} = \underline{\frac{I}{U}} \subseteq + I_0$$

$$U - U_0 = \underline{U} \subseteq$$

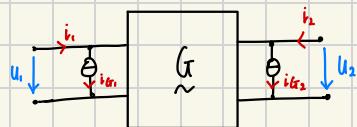
$$\subseteq = \underline{U}^*(U - U_0)$$

$$\underline{i} = \frac{1}{\omega} \underline{U}^{-1} (\underline{u} - \underline{u}_0) + \underline{i}_0$$

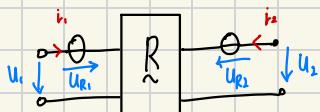
$$= \underbrace{\frac{1}{\omega} \underline{U}^{-1} \underline{u}}_{\underline{G}} - \underbrace{\frac{1}{\omega} \underline{U}^{-1} \underline{u}_0}_{\underline{G}} + \underline{i}_0$$

$\underline{i}_G$

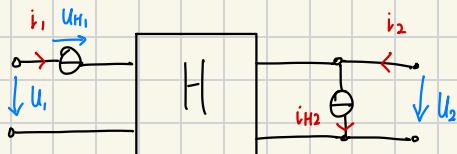
$$\underline{i} = \underline{G} \underline{u} + \underline{i}_G$$



$$\underline{U} = R \underline{i} + \underline{U}_R$$



$$\begin{bmatrix} u_1 \\ i_2 \end{bmatrix} = H \begin{bmatrix} i_1 \\ u_2 \end{bmatrix} + \begin{bmatrix} u_{H1} \\ i_{H2} \end{bmatrix}$$



### 3.4 Properties of two ports

#### 3.4.1 Power

$$P_1 = U_1 i_1$$

$$P_2 = U_2 i_2$$

$$P = P_1 + P_2$$

$$= U_1 i_1 + U_2 i_2$$

##### 3.4.1.1 losslessness

$$\forall \begin{bmatrix} \underline{U} \\ \underline{i} \end{bmatrix} \in F : P = U_1 i_1 + U_2 i_2 \\ = \underline{U}^T \underline{i} = 0$$

Strictly linear two port

$$\begin{bmatrix} \underline{U} \\ \underline{i} \end{bmatrix} = \begin{bmatrix} \underline{U} \\ \underline{I} \end{bmatrix} \subseteq \mathbb{C}^2, \quad \subseteq \in \mathbb{R}^2$$

$$\underline{U} = \underline{U} \subseteq, \quad \underline{i} = \underline{I} \subseteq$$

$$P = \underline{U}^T \underline{i} = (\underline{U} \subseteq)^T \underline{I} \subseteq \\ = \underline{\underline{C}}^T \underline{\underline{U}}^T \underline{\underline{I}} \subseteq = 0 \quad \forall \subseteq \in \mathbb{R}^2$$

$$= \frac{1}{2} \underline{\underline{C}}^T (\underline{\underline{U}}^T \underline{\underline{I}} + \underline{\underline{I}}^T \underline{\underline{U}}) \subseteq = 0$$

$$\underline{\underline{U}}^T \underline{\underline{I}} + \underline{\underline{I}}^T \underline{\underline{U}} = 0 \quad \Leftrightarrow \text{lossless}$$

losslessness :

$$\forall \begin{bmatrix} \underline{U} \\ \underline{i} \end{bmatrix} \in F : \underline{U}^T \underline{i} = 0$$

strictly linear two-port:

$$\begin{bmatrix} \underline{U} \\ \underline{i} \end{bmatrix}^T \begin{bmatrix} I \\ I \end{bmatrix} + \begin{bmatrix} I \\ I \end{bmatrix}^T \begin{bmatrix} \underline{U} \\ \underline{i} \end{bmatrix} = 0$$

### 3.4.1.2 Activity & Passive

passive:

$$\forall \begin{bmatrix} \underline{U} \\ \underline{i} \end{bmatrix} \in F : \underline{U}^T \underline{i} \geq 0$$

active:

$$\exists \begin{bmatrix} \underline{U} \\ \underline{i} \end{bmatrix} \in F : \underline{U}^T \underline{i} < 0$$

### 3.4.2 Duality

$$\underline{U} \xrightarrow{R_d} R_d \underline{i}^d$$

$$\underline{i} \xrightarrow{R_d} \frac{1}{R_d} \underline{U}^d$$

$$\begin{bmatrix} U_1 \\ i_2 \end{bmatrix} = H \begin{bmatrix} i_1 \\ U_2 \end{bmatrix}$$

↓  $R_d$

$$\begin{bmatrix} R_d i_1^d \\ \frac{1}{R_d} U_2^d \end{bmatrix} = H \begin{bmatrix} \frac{1}{R_d} U_1^d \\ R_d i_2^d \end{bmatrix}$$

$$\begin{bmatrix} i_1^d \\ U_2^d \end{bmatrix} = \underbrace{\begin{bmatrix} \frac{1}{R_d} & 0 \\ 0 & R_d \end{bmatrix}}_{H^d} H \begin{bmatrix} \frac{1}{R_d} & 0 \\ 0 & R_d \end{bmatrix} \begin{bmatrix} U_1^d \\ i_2^d \end{bmatrix}$$

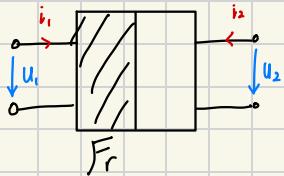
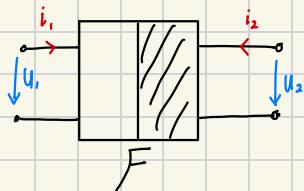
$$\underline{u} = \underline{\tilde{R}} \underline{i}$$

↓  $R_d$

$$R_d \underline{i}^d = \underline{\tilde{R}} \cdot \frac{1}{R_d} \underline{u}^d$$

$$\underline{i}^d = \underbrace{\frac{1}{R_d^2} \underline{\tilde{R}}}_{G^d} \cdot \underline{u}^d$$

### 3.4.3 Reversibility (Symmetry)



permutation matrix

$$\underline{\tilde{P}} = \begin{bmatrix} 0 & 1 \\ 1 & 0 \end{bmatrix}$$

$$\underline{\tilde{P}} \cdot \begin{bmatrix} a_1 \\ a_2 \end{bmatrix} = \begin{bmatrix} a_2 \\ a_1 \end{bmatrix}$$

$$\underline{u} \xrightarrow{\text{rev.}} \underline{\tilde{P}} \underline{u}$$

$$\underline{i} \xrightarrow{\text{rev.}} \underline{\tilde{P}} \underline{i}$$

$$\underline{\tilde{i}} = \underline{\tilde{G}} \underline{u}$$

↓ rev

$$\underline{\tilde{P}} \underline{i} = \underline{\tilde{G}} \underline{\tilde{P}} \underline{u}$$

$$\underline{\tilde{P}}^{-1} = \underline{\tilde{P}}$$

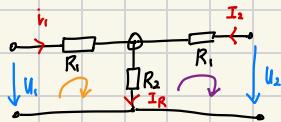
$$\underline{i} = \underbrace{P G P}_{\sim \sim \sim} \underline{U}$$

if  $\underline{G}$  is symmetric

if  $\underbrace{P R P}_{\sim \sim \sim} = R$ ,  $\underline{F}$  is symmetric

$$\Rightarrow \underline{R} = \begin{bmatrix} r_{11} & r_{12} \\ r_{21} & r_{22} \end{bmatrix}$$

$$\underline{A} = \underline{A}'$$



$$KCL: i_1 + i_2 - i_R = 0$$

$$KVL: -U_1 + R_1 i_1 + R_2 i_R = 0$$

$$KVL: -R_2 i_R - R_1 i_2 + U_2 = 0$$

$$i_R = i_1 + i_2$$

$$U_1 = R_1 i_1 + R_2 i_R = (R_1 + R_2) i_1 + R_2 i_2$$

$$U_2 = R_2 i_1 + (R_1 + R_2) i_2$$

$$\underline{R} = \begin{bmatrix} R_1 + R_2 & R_2 \\ R_2 & R_1 + R_2 \end{bmatrix}$$

### 3.4.4 Reciprocity & linear two ports

#### Symmetry of transfer Characteristics

$$\underline{R} = \begin{bmatrix} r_{11} & r_{12} \\ r_{21} & r_{22} \end{bmatrix}$$

$$U_1 = r_{11} i_1 + \boxed{r_{12} i_2}$$

$$U_2 = \boxed{r_{21}} i_1 + r_{22} i_2$$

Reciprocity:

$$r_{12} = r_{21}$$

$$g_{12} = g_{21}$$

page 42:

$$h_{12} = -h_{21}$$

$$h'_{12} = -h'_{21}$$

$$\det \tilde{A} = 1$$

$$\det \tilde{A}' = 1$$

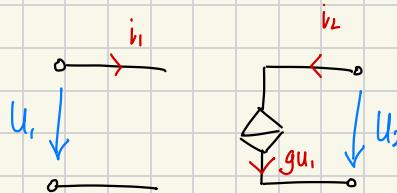
reciprocal two-port

$$\begin{matrix} U \\ \sim \end{matrix} \stackrel{\text{I}}{\stackrel{T}{\sim}} \ominus \stackrel{\text{I}}{\stackrel{T}{\sim}} \begin{matrix} U \\ \sim \end{matrix} = \begin{matrix} U \\ \sim \end{matrix}$$

↓ different from losslessness

## 3.5 Special two-ports

### 3.5.1 Controlled sources

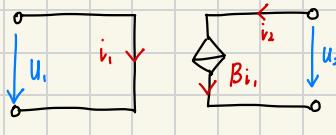


Voltage - Controlled  
Current source

$$\begin{aligned} i_1 &= 0 \\ i_2 &= gu_1 \end{aligned} \quad \begin{matrix} \tilde{G} = [0 & 0 \\ g & 0] \end{matrix}$$

Alternative

$$\begin{matrix} \tilde{A} = [0 & -\frac{1}{g} \\ 0 & 0] \end{matrix}$$



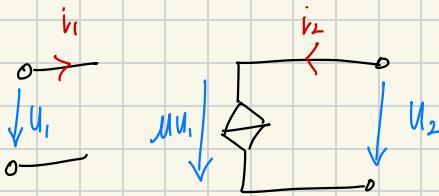
CCCS

$$U_1 = 0$$

$$i_2 = \beta i_1$$

$$\tilde{H} = \begin{bmatrix} 0 & 0 \\ \beta & 0 \end{bmatrix}$$

$$\tilde{A} = \begin{bmatrix} 0 & 0 \\ 0 & -\frac{1}{\beta} \end{bmatrix}$$



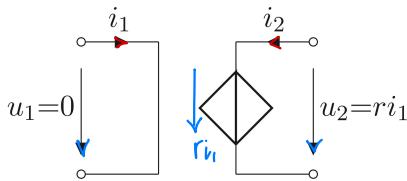
VCVS

$$i_1 = 0$$

$$\tilde{H}' = \begin{bmatrix} 0 & 0 \\ \mu & 0 \end{bmatrix}$$

$$U_2 = \mu U_1$$

$$\tilde{A} = \begin{bmatrix} \frac{1}{\mu} & 0 \\ 0 & 0 \end{bmatrix}$$



$$U_1 = 0$$

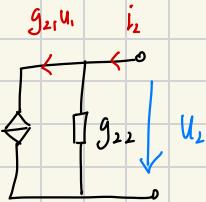
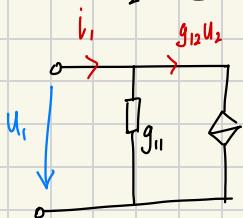
$$U_2 = r_i i_1$$

$$\tilde{R} = \begin{bmatrix} 0 & 0 \\ r & 0 \end{bmatrix}$$

$$\tilde{A} = \begin{bmatrix} 0 & 0 \\ \frac{1}{r} & 0 \end{bmatrix}$$

$$i_1 = g_{11} u_1 + g_{12} u_2$$

$$i_2 = g_{21} u_1 + g_{22} u_2$$

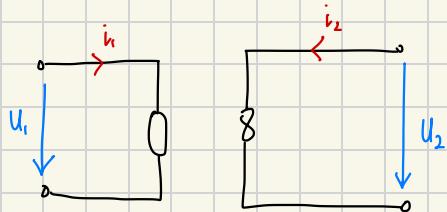


### 3.5.2 Nullor

$$\text{VCCS: } A_{\text{VCCS}} = \begin{bmatrix} 0 & -\frac{1}{g} \\ 0 & 0 \end{bmatrix}$$

$$\lim_{g \rightarrow \infty} A_{\text{VCCS}} = \begin{bmatrix} 0 & 0 \\ 0 & 0 \end{bmatrix} = 0$$

$$u_1 = 0, \quad i_1 = 0$$



### 3.5.3 Transformer

lossless & reciprocal

$$\left. \begin{aligned} \underbrace{\underline{U}^T \underline{I}}_{\sim} + \underbrace{\underline{I}^T \underline{U}}_{\sim} &= \underline{0} \\ \underbrace{\underline{U}^T \underline{I}}_{\sim} - \underbrace{\underline{I}^T \underline{U}}_{\sim} &= \underline{0} \end{aligned} \right\} \rightarrow \underline{U} = \underline{R} \underline{I}$$

$$\underline{I}^T \underline{R}^T \underline{I} + \underline{I}^T \underline{R} \underline{I}$$

$$\underline{R}^T + \underline{R} = \underline{0}$$

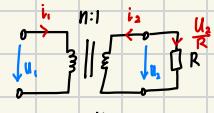
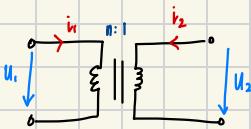
$$\left. \begin{aligned} \underline{R} &= -\underline{R}^T \\ \underline{R} &= \underline{R}^T \end{aligned} \right\} \underline{R} = \underline{0}$$

$$\underline{G} = \underline{0}$$

$$\left. \begin{aligned} \underline{H}_{\text{trans}} &= \begin{bmatrix} 0 & n \\ -n & 0 \end{bmatrix} \\ \underline{H}'_{\text{trans}} &= \begin{bmatrix} 0 & -\frac{1}{n} \\ \frac{1}{n} & 0 \end{bmatrix} \end{aligned} \right\}$$

$$U_1 = n U_2$$

$$i_2 = -ni_1$$



$$i_2 = -\frac{U_2}{R}$$

$$= -n i_1$$

$$i_1 = \frac{1}{n} \cdot \left( \frac{U_1}{R} \right)$$

$$U_2 = \frac{1}{n} \cdot U_1$$

$$i_1 = \frac{1}{n^2} \frac{U_1}{R}$$

=  $n^2 R$  at port 1

### 3.5.4 gyrator

lossless & not reciprocal

$$\begin{cases} \underbrace{U^T I}_{\sim \sim} + \underbrace{I^T U}_{\sim \sim} = 0 \\ \underbrace{U^T I}_{\sim \sim} - \underbrace{I^T U}_{\sim \sim} \neq 0 \\ \therefore R = -\underbrace{R^T}_{\sim} \end{cases}$$

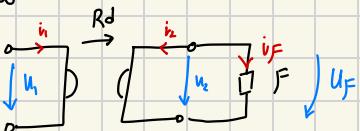
$$\Rightarrow R_{\text{gyr}} = \begin{bmatrix} 0 & -R_d \\ R_d & 0 \end{bmatrix}$$

$$U_1 = -R_d i_2$$

$$U_2 = R_d i_1$$

$$\therefore i_1 = \frac{1}{R_d} U_2$$

$$\text{Gyrator} = \begin{bmatrix} 0 & +G_d \\ -G_d & 0 \end{bmatrix}$$



$$i_2 = -i_F, \quad U_2 = U_F$$

$$(U_F, i_F) \in F$$

$$(R_d i_1, \frac{1}{R_d} U_1) \in F$$

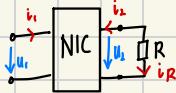
$$(U_1, i_1) \in F'$$

### 3.5.5 negative impedance converter (NIC)

$$U_1 = -k U_2$$

$$i_1 = -\frac{1}{k} i_2 \Rightarrow -i_2 = k i_1$$

$$\underline{A}_{\text{NIC}} = \begin{bmatrix} k & 0 \\ 0 & \frac{1}{k} \end{bmatrix}$$



Ohm:  $U_2 = R i_R \leftarrow i_R = -i_2$

$$U_2 = R(-i_2)$$

$$U_1 = -k U_2$$

$$= -k R(-i_2)$$

$$U_1 = -k R k i_1$$

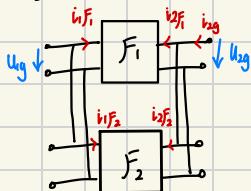
$$= \begin{bmatrix} -k^2 R \\ 0 \end{bmatrix} i_1$$

$\Rightarrow$  negative resistor at port 1

### 3.6 Connection of two ports

$F_1$  &  $F_2$

#### 3.6.1 Parallel Connection



parallel connection of ports 1:

$$U_{1g} = U_{1F_1} = U_{1F_2}$$

$$i_{1g} = i_{1F_1} + i_{1F_2}$$

part 2:  $U_{2g} = U_{2F_1} = U_{2F_2}$

$$i_{2g} = i_{2F_1} + i_{2F_2}$$

$$\underline{i}_g = \begin{bmatrix} i_{1g} \\ i_{2g} \end{bmatrix} \quad \underline{i}_{F_1} = \begin{bmatrix} i_{1F_1} \\ i_{2F_1} \end{bmatrix} \quad \underline{i}_{F_2} = \begin{bmatrix} i_{1F_2} \\ i_{2F_2} \end{bmatrix}$$

$$i_{F_1} = g_{F_1}(\underline{U}_{F_1}) = g_{F_1}(\underline{U}_g)$$

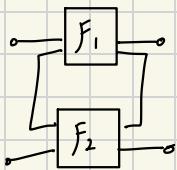
$$i_{F_2} = g_{F_2}(\underline{U}_{F_2}) = g_{F_2}(\underline{U}_g)$$

$$\begin{aligned} i_g &= i_{F_1} + i_{F_2} \\ &= g_{F_1}(\underline{U}_g) + g_{F_2}(\underline{U}_g) \\ &= g_F(\underline{U}_g) \end{aligned}$$

$$g_F = g_{F_1} + g_{F_2}$$

$$\underline{G}_F = \underline{G}_{F_1} + \underline{G}_{F_2}$$

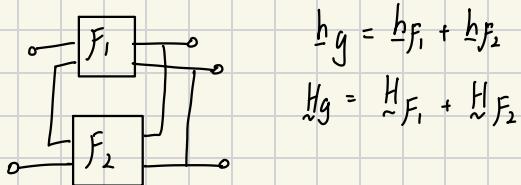
### 3.6.2 Series Connection



$$i_g = i_{F_1} + i_{F_2}$$

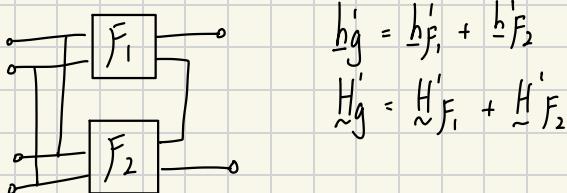
$$\underline{R}_g = \underline{R}_{F_1} + \underline{R}_{F_2}$$

### 3.6.3 Hybrid Connections



$$h_g = h_{F_1} + h_{F_2}$$

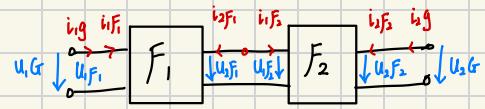
$$\underline{H}_g = \underline{H}_{F_1} + \underline{H}_{F_2}$$



$$h'_g = h'_{F_1} + h'_{F_2}$$

$$\underline{H}'_g = \underline{H}'_{F_1} + \underline{H}'_{F_2}$$

### 3.6.4 Cascade Connection



$$KCL: i_{1F_1} + i_{2F_2} = 0$$

$$\frac{i_{2F_2}}{u_{2F_2}} = -i_{1F_2}$$

$$\underline{u_{2F_2}} = \underline{u_{1F_2}}$$

$$\begin{bmatrix} \underline{u_{1F_2}} \\ \underline{i_{2F_2}} \end{bmatrix} = g_{F_2} \left( \begin{bmatrix} \underline{u_{2F_2}} \\ \underline{-i_{2F_2}} \end{bmatrix} \right)$$

$$= \begin{bmatrix} \underline{u_{2F_1}} \\ \underline{-i_{2F_1}} \end{bmatrix}$$

$$\begin{bmatrix} \underline{u_{1F_1}} \\ \underline{i_{1F_1}} \end{bmatrix} = \underline{a}_{F_1} \left( \begin{bmatrix} \underline{u_{2F_1}} \\ \underline{-i_{2F_1}} \end{bmatrix} \right)$$

$$= \underline{a}_{F_1} \left( \underline{a}_{F_2} \begin{bmatrix} \underline{u_{2g}} \\ \underline{-i_{2g}} \end{bmatrix} \right)$$

$$\begin{bmatrix} \underline{u_{1g}} \\ \underline{i_{1g}} \end{bmatrix} = \underline{a}_{F_1} \left( \underline{a}_{F_2} \begin{bmatrix} \underline{u_{2g}} \\ \underline{-i_{2g}} \end{bmatrix} \right)$$

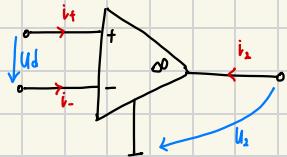
$$\begin{bmatrix} \underline{u_{1g}} \\ \underline{i_{1g}} \end{bmatrix} = \underline{A}_{F_1} \cdot \underline{A}_{F_2} \cdot \begin{bmatrix} \underline{u_{2g}} \\ \underline{-i_{2g}} \end{bmatrix}$$

# 4 Operational Amplifier

## 4.1 modelling

### 4.1.1 Idealized

#### Non-linear Model



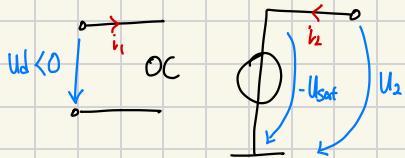
$$i_+ = i_- = 0$$

$$U_2 = \begin{cases} -U_{sat} & U_d < 0 \text{ (I)} \\ +U_{sat} & U_d > 0 \text{ (III)} \end{cases} \quad \text{Sat} \Rightarrow \text{saturation}$$

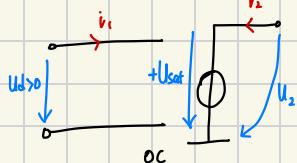
$$|U_2| \leq U_{sat} \text{ for } U_d = 0 \text{ (II)}$$

### 4.1.2 Saturation Regions

$$(I) : U_2 = -U_{sat} \text{ for } U_d < 0$$



$$(III) : U_2 = +U_{sat} \quad U_d > 0$$



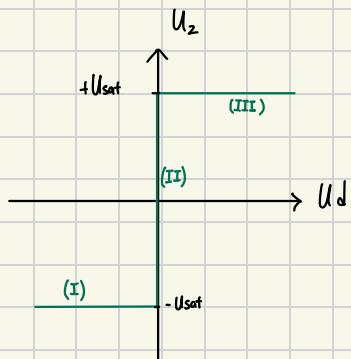
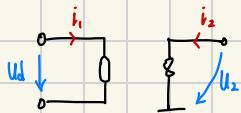
#### 4.1.3.1 Linear Region

(II) :  $U_d = 0, i_1 = 0$

$$|U_2| \leq U_{sat}$$

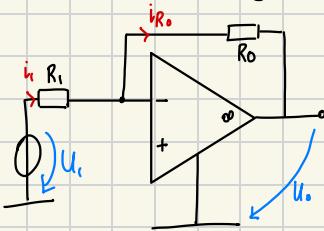
→ nullator

nullator at port 2

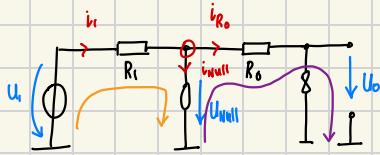


## 4.2 Op-Amp Circuits

### 4.2.1 Inverting Amplifier



(II) Linear region:



$$KVL: -U_1 + R_i i_1 + U_{\text{null}} = 0$$

$$U_1 = R_i i_1 \Rightarrow i_1 = \frac{1}{R_i} U_1$$

$$KCL: i_1 - i_{R_o} - i_{\text{null}} = 0$$

$$i_1 = i_{R_o} = \frac{1}{R_o} U_1$$

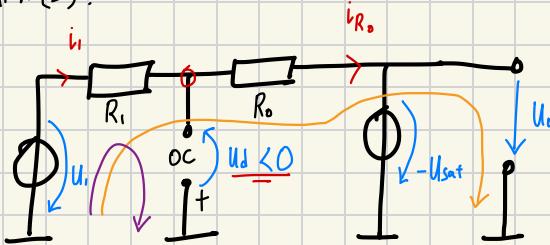
$$KVL: -U_{\text{null}} + R_o i_{R_o} + U_o = 0$$

$$U_o = -R_o i_{R_o} = -\frac{R_o}{R_i} U_1$$

$$\Rightarrow \text{gain} = -\frac{R_o}{R_i} < 0$$

inverting amplifier

Saturation (I) :



$$i_1 = i_{R_o}$$

$$\text{KVL: } -U_i + R_1 i_1 + R_o i_1 - U_{sat} = 0$$

$$i_1 = \frac{1}{R_o + R_1} (U_i + U_{sat})$$

$$\text{KVL: } -U_i + R_1 i_1 - U_d = 0$$

$$U_d = -U_i + R_1 i_1$$

$$= -U_i + R_1 \frac{1}{R_o + R_1} (U_i + U_{sat})$$

$$= -U_i + \frac{R_1}{R_o + R_1} \cdot U_i + \frac{R_1}{R_o + R_1} \cdot U_{sat}$$

$$= -\frac{R_o}{R_o + R_1} \cdot U_i + \frac{R_1}{R_o + R_1} U_{sat} \underset{< 0}{\underline{< 0}}$$

$$\frac{R_o}{R_o + R_1} U_i > \frac{R_1}{R_o + R_1} U_{sat}$$

$$U_i > \frac{R_1}{R_o} U_{sat}$$

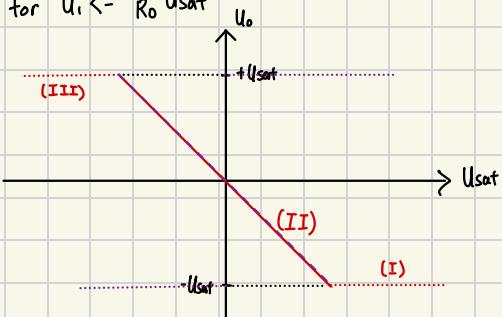
### Saturation (III)

$$-U_{sat} \rightarrow +U_{sat}$$

$$U_d < 0 \rightarrow U_d > 0$$

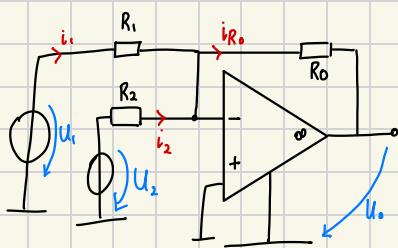
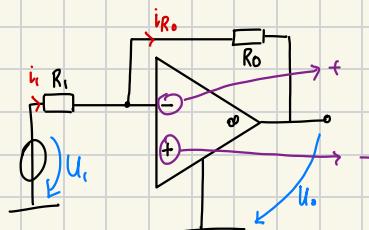
$$U_o = +U_{sat}$$

$$\text{for } U_i < -\frac{R_1}{R_0} U_{sat}$$

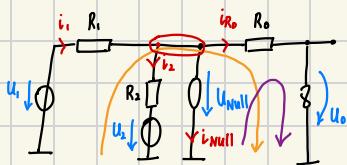


$$U_i < -\frac{R_1}{R_0} U_{sat}$$

$$U_i > \frac{R_1}{R_0} U_{sat}$$



linear region (II) :



$$\text{KVL: } -U_2 + R_2 i_2 + U_{null}^o = 0$$

$$i_2 = \frac{1}{R_2} U_2$$

$$i_1 = \frac{1}{R_1} U_1$$

$$\text{KCL: } i_1 + i_2 - i_{null}^o - i_{R_0} = 0$$

$$i_{R_0} = i_1 + i_2$$

$$KVL: -U_{\text{NULL}} + R_o i_{R_o} + U_o = 0$$

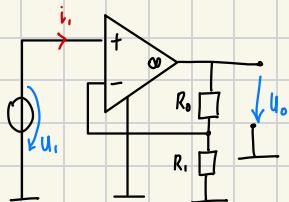
$$U_o = -R_o i_{R_o} = -R_o (i_1 + i_2)$$

$$U_o = -\frac{R_o}{R_i} U_i = \underbrace{-\frac{R_o}{R_i}}_{\alpha_1} U_1 - \underbrace{\frac{R_o}{R_i} U_2}_{\alpha_2}$$

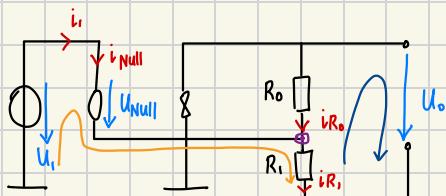
$$U_o = \alpha_1 U_1 + \alpha_2 U_2$$

$$= [\alpha_1, \alpha_2] \cdot \begin{bmatrix} U_1 \\ U_2 \end{bmatrix}$$

#### 4.2.2 Non-Inverting Amplifier



Linear region (II) :



$$KVL: -U_i + U_{\text{NULL}} + R_i i_{R_i} = 0$$

$$i_{R_i} = \frac{U_i}{R_i}$$

$$KCL: i_{\text{NULL}} + i_{R_o} - i_{R_i} = 0$$

$$i_{R_o} = i_{R_i} = \frac{U_i}{R_i}$$

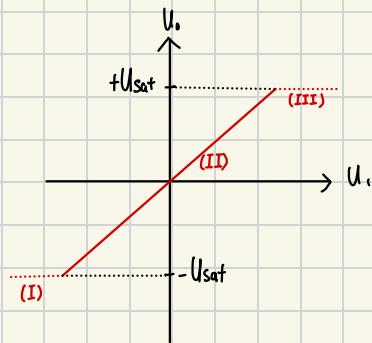
$$KVL: -R_i i_{R_i} - R_o i_{R_o} + U_o = 0$$

$$U_o = R_i i_{R_i} + R_o i_{R_o}$$

$$= \frac{R_o + R_i}{R_i} U_i$$

$$= \underbrace{\left(1 + \frac{R_o}{R_i}\right)}_{\geq 1} U_i$$

$$\text{gain} = 1 + \frac{R_o}{R_i}$$

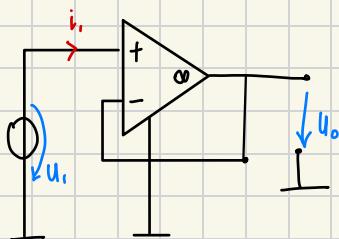


#### 4.2.2.1 Voltage Follower

$R_o$  : SC

$R_i$  : OC

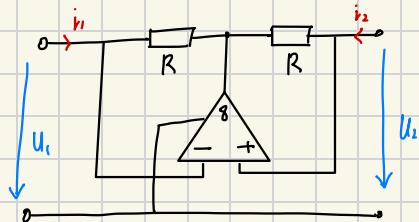
$$\Rightarrow \text{gain} = 1$$



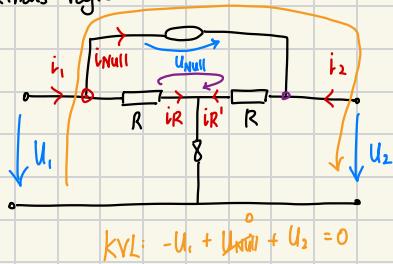
$$U_o = U_i$$

$$i_i = 0$$

#### 4.2.3 Negativire imittance converfer (NIC)



Linear region:



$$U_1 = U_2$$

$$\text{KCL: } i_1 - i_{R\text{null}} - i_R = 0$$

$$i_1 = i_R$$

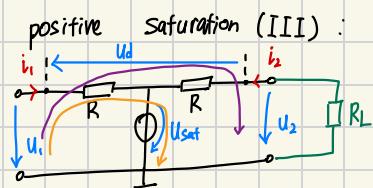
$$\text{KCL: } i_2 = i_{R'}$$

$$\text{KVL: } -Ri_R + U_{R\text{null}} + Ri_{R'} = 0$$

$$i_R = i_{R'}$$

$$\left. \begin{array}{l} i_1 = i_2 \\ U_1 = U_2 \end{array} \right\} \text{NIC with } K = -1$$

$\Rightarrow$  ability to build negative resistance



$$KVL: -U_1 + R_i_1 + U_{sat} = 0$$

$$U_1 = R_i_1 + U_{sat}$$

$$U_2 = R_i_2 + U_{sat}$$

$$KVL: -U_1 - U_d + U_2 = 0$$

$$U_d = U_2 - U_1 > 0$$

$$R_{i_2} + U_{sat} - R_{i_1} - U_{sat} > 0$$

$$i_2 - i_1 > 0$$

$$i_2 > i_1 \text{ for (III)}$$

due to  $R_L$ :

$$U_2 = R_2(-i_2)$$

Linear Region

$$i_1 = i_2$$

$$U_2 = U_1 = R_2(-i_2)$$

$$U_1 = -R_L i_1$$

neg.  
resistor

Saturated Region (III):

$$U_1 = R_{i_1} + U_{sat}$$

$$U_2 = -R_L i_2$$

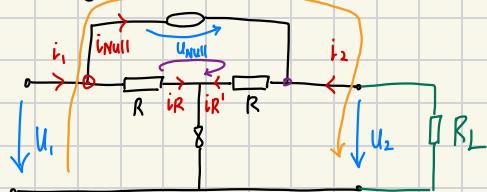
$$(= R_{i_2} + U_{sat})$$

$$-R_L i_2 = R_{i_2} + U_{sat}$$

$$(R + R_L) i_2 = U_{sat}$$

$$i_2 = -\frac{U_{sat}}{R + R_L}$$

Linear Region:



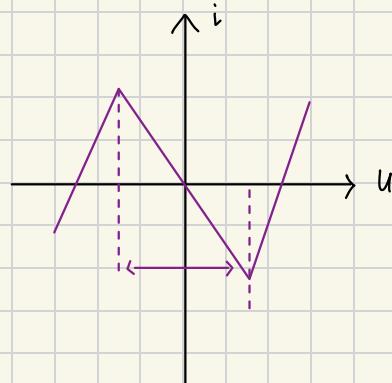
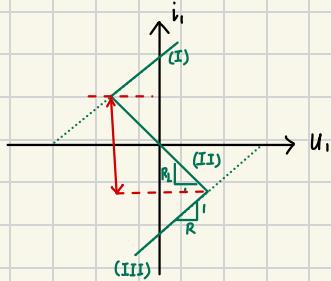
$$U_2 = \frac{R_L}{R+R_L} U_{sat}$$

$$U_d = U_2 - U_1$$

$$= \frac{R_L}{R+R_L} U_{sat} - R_{i_1} - U_{sat}$$

$$= -\frac{R}{R+R_L} U_{sat} - R_{i_1} > 0$$

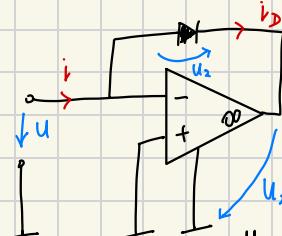
$$i_1 < \frac{-1}{R+R_L} U_{sat}$$



+ & - terminals  
exchanged

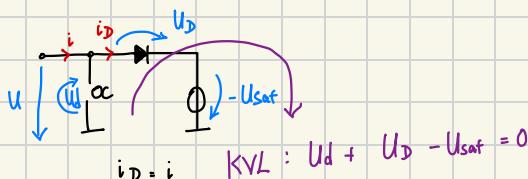
## 4.2.4 Piecewise Linear Resistors

### 4.2.4.1 Ideal Diode



$$i_D = I_s \left( e^{\frac{U_D}{U_T}} - 1 \right)$$

negative saturation (I):



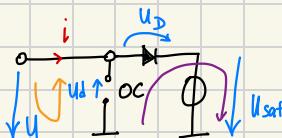
$$U_d = -U_D + U_{sat} < 0$$

$$U_D > U_{sat}$$

$$U_{sat} = 1.25V \quad I_s = 10^{-17}A, \quad U_T = 25mV$$

$$i_D \approx 10^{200} A \cdot e^{\frac{U_D}{U_T}} \rightarrow \text{impossible}$$

positive saturation (III)



$$KVL: U_d + U_D + U_{sat} = 0$$

$$U_d = -U_D - U_{sat} > 0$$

$$U_D < -U_{sat}$$

$$\Rightarrow i_D = 0$$

$$i = i_D = 0$$

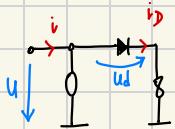
$$KVL: U + U_d = 0$$

$$U = -U_d, \quad U_d > 0$$

$$\Rightarrow U < 0$$

if voltage is negative, Current = 0 for ideal diode

linear region (II)



Null after:

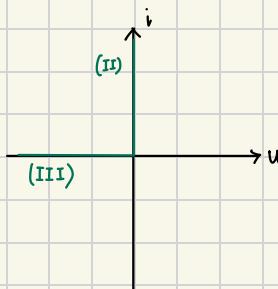
$$U = 0$$

$$i_D = 0$$

pn-junction diode:

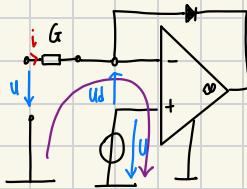
$$i_D \geq 0$$

$$i > 0, U = 0$$



ideal diode is connected to reference node

#### 4.2.4.2 Concave Resistors



$$KVL: -U + \frac{i}{G} - U_d + U = 0$$

$$U = U + \frac{i}{G} - U_d$$

linear region:  $U_d = 0$

$$U = U + \frac{i}{G}$$

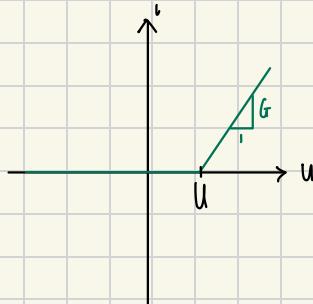
Sat. region (III):  $U_d > 0$

$$\rightarrow U_d = U - U + \frac{i}{G} > 0$$

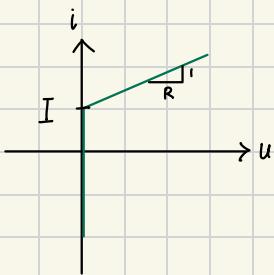
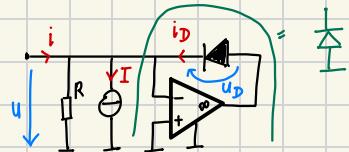
$i = 0$ :

$$U - u > 0$$

$$u < U$$



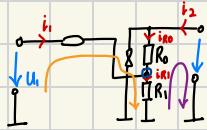
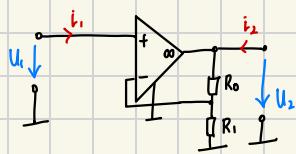
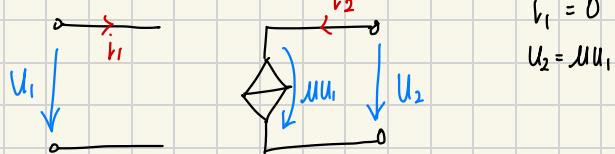
### 4.2.4.3 Convex Resistors



### 4.3 linear op- Amp Circuits

#### 4.3.1 Controlled sources

##### 4.3.1.1 voltage - Controlled Voltage Source



$$KVL: -U_1 + U_2 + R_i i_{R_i} = 0$$

$$U_1 = R_i i_{R_i}$$

$$KCL: i_{N\!U\!L\!L} + i_{R_o} - i_{R_i} = 0$$

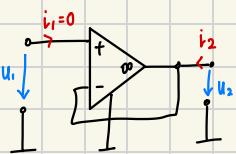
$$i_{R_o} = i_{R_i}$$

$$KVL: -U_2 + R_o i_{R_o} + R_i i_{R_i} = 0$$

$$U_2 = R_i i_{R_i} - R_o i_{R_o}$$

$$= \frac{R_o + R_i}{R_i} U_1$$

$$M = \frac{R_o + R_i}{R_i} \geq 1$$



$$U_2 = -\frac{R_o}{R_i} U_{in}$$

$$i_{in} = \frac{U_{in}}{R_i} \neq 0$$

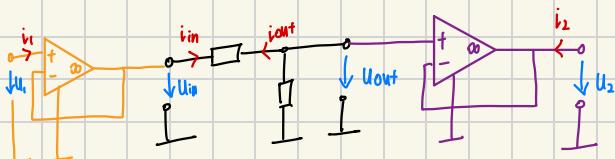
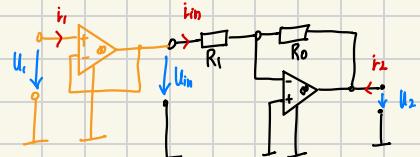
Voltage followers :

$$i_1 = 0$$

$$U_{in} = U_1$$

$$U_2 = -\frac{R_o}{R_i} U_1$$

$$\mu \leq 0$$



$$\text{for } i_{out}=0 : i_{in} = \frac{U_{in}}{R_o+R_i} \neq 0$$

Volt. foll:  $i_1 = 0, U_{in} = U_1$

Volt. foll2:  $i_{out} = 0, U_2 = U_{out}$

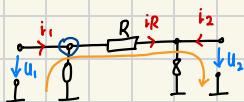
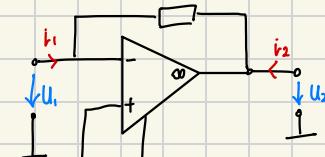
Volt. dir. rule :

$$\frac{U_{out}}{U_{in}} = \frac{R_o}{R_o+R_i}$$

$$U_2 = \frac{R_o}{R_o+R_i} U_1$$

$$0 \leq \mu \leq 1$$

#### 4.3.1.2 Current Controlled Voltage Source



$$U_1 = 0$$

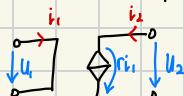
$$KCL: i_1 + i_R - i_{\text{out}} = 0$$

$$i_R = -i_1$$

$$KVL: -U_1 - R i_R + U_2 = 0$$

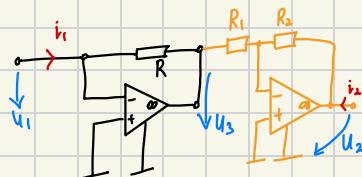
$$U_2 = R i_R$$

$$= -R i_1$$



$$U_1 = 0, \quad U_2 = r i_1$$

$$r = -R \leq 0$$



$$U_3 = -R i_1$$

$$\text{inv. ampl. : } U_3 = -\frac{R_2}{R_1} U_3$$

$$U_2 = \frac{R_2}{R_1} R i_1$$

$$r = \frac{R_2 \cdot R}{R_1} \geq 0$$

# 5 General Circuit Analysis

## 5.1 Incidence Matrices

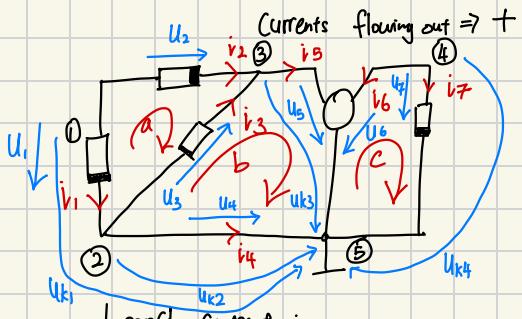
b branches

n nodes

Set up KCL eqns.

for all nodes except

reference node & Currents going in  $\Rightarrow -$



branch currents:

$$\underline{i} = [i_1, i_2, i_3, i_4, i_5, i_6, i_7]^T$$

$$(1) : i_1 + i_2 = 0$$

$$(2) : -i_1 + i_3 + i_4 = 0$$

$$(3) : i_5 - i_2 - i_3 = 0$$

$$(4) : i_6 + i_7 = 0$$

$$\begin{bmatrix} 1 & 1 & 0 & 0 & 0 & 0 & 0 \\ -1 & 0 & 1 & 1 & 0 & 0 & 0 \\ 0 & -1 & -1 & 0 & 1 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 1 & 1 \end{bmatrix} \cdot \underline{i} = \begin{bmatrix} 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \end{bmatrix}$$

$\underbrace{A}_{\text{A: node incidence matrix}}$

$$\text{KCL: } \underline{A} \underline{i} = 0$$

KVL

$$a: -U_1 + U_2 - U_3 = 0$$

$$b: U_3 + U_5 - U_4 = 0$$

$$c: -U_6 + U_7 = 0$$

$$\underline{U} = [U_1, U_2, U_3, U_4, U_5, U_6, U_7]$$

$$\underline{\underline{B}} \approx \begin{bmatrix} U_1 & U_2 & U_3 & U_4 & U_5 & U_6 & U_7 \\ -1 & 1 & -1 & & & & \\ & 1 & -1 & 1 & & & \\ 0 & 0 & 0 & 0 & 0 & -1 & 1 \end{bmatrix}$$

$$\underline{\underline{B}} \underline{U} = \underline{0}$$

$$\text{branches}(b) = 7$$

$$\text{nodes}(n) = 5$$

$$n-1 = 4 \text{ KCL eqns}$$

$$\underline{b} - (n-1) = 3 \text{ KVL eqn}$$

b. eqns.

$$\underline{U}_k = [U_{k1}, U_{k2}, U_{k3}, U_{k4}]^T$$

$$U_1 = U_{k1} - U_{k2}$$

$$U_2 = U_{k1} - U_{k3}$$

$$U_3 = U_{k2} - U_{k3}$$

$$U_4 = U_{k2} - U_{k5} = U_{k2}$$

↓  
ref. node = 0

$$U_5 = U_{k3}$$

$$U_6 = U_{k4}$$

$$U_7 = U_{k4}$$

$$\underline{U} = \begin{bmatrix} \underline{U}_{k1} & \underline{U}_{k2} & \underline{U}_{k3} & \underline{U}_{k4} \\ | & -1 & 0 & 0 \\ | & 0 & -1 & 0 \\ 0 & 1 & -1 & 0 \\ 0 & 1 & 0 & 0 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \\ 0 & 0 & 0 & 1 \end{bmatrix} \cdot \underline{U}_k$$

$\xrightarrow{\sim}$

$$\underline{U} = \underline{A}^T \underline{U}_k$$

$$\underline{A} \underline{i} = \underline{0}$$

### 5.5.1 Tellegen's Theorem

$$\underline{U}^T \underline{i} \stackrel{KVL}{=} (\underline{A}^T \underline{U}_k)^T \underline{i}$$

$$= \underline{U}_k^T \underline{A} \underline{i} \stackrel{KCL}{=} \underline{U}_k^T \underline{0} = 0$$

$$\underline{U}^T \underline{i} = 0 \quad \text{Tellegen's Theorem}$$

$$\underline{A} \underline{B}^T \stackrel{\sim}{=} \underline{0}$$

## 5.2 Tableau Equations

linear element S:

Strictly linear resistance, linear sources

$$\underbrace{M}_{\sim} \underline{u} + \underbrace{N}_{\sim} \underline{i} = \underline{e}$$

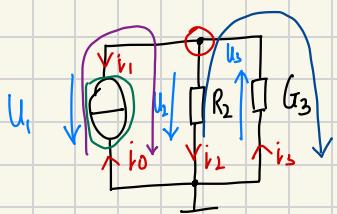
$$\underbrace{B}_{\sim} \underline{u} = \underline{0}$$

$$\underbrace{A}_{\sim} \underline{i} = \underline{0}$$

$$b \left\{ \underbrace{\begin{bmatrix} B & 0 \\ 0 & A \end{bmatrix}}_{2b \times 2b} \cdot \underbrace{\begin{bmatrix} \underline{u} \\ \underline{i} \end{bmatrix}}_{2b} \right\} = \begin{bmatrix} 0 \\ 0 \\ \underline{e} \end{bmatrix}$$

$$\underline{I} \cdot \begin{bmatrix} \underline{u} \\ \underline{i} \end{bmatrix} = \begin{bmatrix} 0 \\ 0 \\ \underline{e} \end{bmatrix}$$

$$\begin{bmatrix} \underline{u} \\ \underline{i} \end{bmatrix} = \underline{I}^{-1} \begin{bmatrix} 0 \\ 0 \\ \underline{e} \end{bmatrix}$$



$$KCL: i_1 + i_2 - i_3 = 0$$

$$KVL: -U_1 + U_2 = 0$$

$$KVL: -U_2 - U_3 = 0$$

$$\tilde{A} = \begin{bmatrix} 1 & 1 & -1 \end{bmatrix}$$

$$\tilde{B} = \begin{bmatrix} -1 & 1 & 0 \\ 0 & -1 & -1 \end{bmatrix}$$

$$\text{Tellegen: } \tilde{A} \cdot \tilde{B}^T = \begin{bmatrix} 1 & 1 & -1 \end{bmatrix} \cdot \begin{bmatrix} -1 & 0 \\ 1 & -1 \\ 0 & -1 \end{bmatrix} = \begin{bmatrix} 0 & 0 \end{bmatrix}$$

$$i_1 + i_0 = 0 \Rightarrow i_1 = -i_0$$

$$\text{Ohm: } U_2 = R_2 i_2$$

$$\underline{U_2 - R_2 i_2 = 0}$$

$$\text{Ohm: } i_3 = G_3 U_3$$

$$\underline{-G_3 U_3 + i_3 = 0}$$

$$\begin{array}{l}
 \text{KVL} \\
 \left[ \begin{array}{ccc|cc}
 u_1 & u_2 & u_3 & i_1 & i_2 & i_3 \\
 1 & 1 & 0 & 0 & 0 & 0 \\
 0 & -1 & -1 & 2 & 0 & 0 \\
 \hline
 0^T & 1 & 1 & -1 & 0 & 0 \\
 \end{array} \right] \\
 \text{KCL} \\
 \cdot \left[ \begin{array}{ccc|cc}
 0 & 0 & 0 & 1 & 0 & 0 \\
 0 & 1 & 0 & 0 & -R_2 & 0 \\
 0 & 0 & -R_3 & 0 & 0 & 1 \\
 \end{array} \right] = \left[ \begin{array}{c}
 \underline{u} \\
 \underline{i} \\
 \end{array} \right] = \left[ \begin{array}{c}
 0 \\
 0 \\
 0 \\
 -i_0 \\
 0 \\
 0 \\
 \end{array} \right]
 \end{array}$$

### 5.2.1 Node Analysis

$$\begin{aligned}
 \underline{\underline{A}} \underline{\underline{i}} &= \underline{\underline{0}} & \underline{\underline{u}} &= \underline{\underline{A}}^T \underline{\underline{u}}_k \\
 \underline{\underline{M}} \underline{\underline{u}} + \underline{\underline{N}} \underline{\underline{i}} &= \underline{\underline{e}} & \downarrow \underline{\underline{u}} - \underline{\underline{A}}^T \underline{\underline{u}}_k &= \underline{\underline{0}}
 \end{aligned}$$

$$\begin{array}{l}
 b \left\{ \begin{array}{c|c|c}
 -\underline{\underline{A}}^T & \underline{\underline{I}} & \underline{\underline{0}} \\
 \hline
 \underline{\underline{0}} & \underline{\underline{0}} & \underline{\underline{A}} \\
 \hline
 \underline{\underline{0}} & \underline{\underline{M}} & \underline{\underline{N}}
 \end{array} \right\} \\
 n-1 \left\{ \begin{array}{c|c|c}
 & & \\
 \hline
 & & \\
 \hline
 & &
 \end{array} \right\} \\
 b \left\{ \begin{array}{c|c|c}
 & & \\
 \hline
 & & \\
 \hline
 & &
 \end{array} \right\}
 \end{array} \cdot \left[ \begin{array}{c}
 \underline{\underline{u}}_k \\
 \underline{\underline{u}} \\
 \underline{\underline{i}}
 \end{array} \right] = \left[ \begin{array}{c}
 \underline{\underline{0}} \\
 \underline{\underline{0}} \\
 \underline{\underline{e}}
 \end{array} \right]$$

## 5.3 Nodal Analysis

$$\underline{U} = \underline{\Lambda}^T \underline{U}_K$$

$$\underline{\Lambda} \underline{i} = 0$$

$$\underline{\Lambda} \underline{U} + \underline{N} \underline{i} = \underline{e}$$

$$\underline{N} \underline{i} = -\underline{\Lambda} \underline{U} + \underline{e}$$

$\underline{N}^{-1}$  exists

Voltage-control elements

$$\underline{i} = -\underline{N}^{-1} \underline{\Lambda} \underline{U} + \underline{N}^{-1} \underline{e}$$

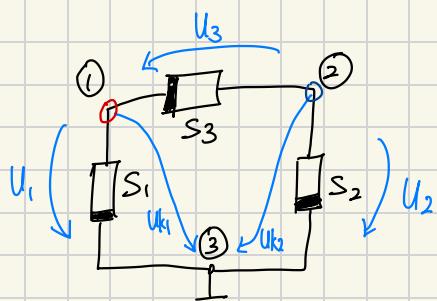
$$\underline{\Lambda} \underline{i} = 0$$

$$\underline{\Lambda} \underline{i} = -\underline{A} \underline{N}^{-1} \underline{\Lambda} \underline{U} + \underline{A} \underline{N}^{-1} \underline{e} = 0$$

$$-\underline{A} \underline{N}^{-1} \underline{\Lambda} \underline{\Lambda}^T \underline{U}_K + \underline{A} \underline{N}^{-1} \underline{e} = 0$$

$$\underbrace{-\underline{A} \underline{N}^{-1} \underline{\Lambda} \underline{\Lambda}^T \underline{U}_K}_{\text{Node Conductance matrix}} = -\underline{A} \underline{N}^{-1} \underline{e}$$

$$\begin{matrix} \uparrow \underline{G}_K \underline{U}_K \\ \text{Node Conductance matrix} \end{matrix} = \begin{matrix} \downarrow \underline{I}_q \\ \text{node Current source vector} \end{matrix}$$



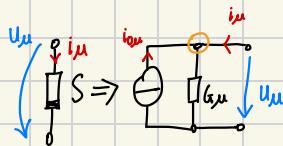
Arrow goes direction of bar

$$KCL(1): i_1 - i_2 = 0$$

$$KCL(2): i_2 + i_3 = 0$$

$$\tilde{A} = \begin{bmatrix} 1 & -1 & 0 \\ 0 & 1 & 1 \end{bmatrix}$$

$$\underline{U}_k = \begin{bmatrix} U_{k1} \\ U_{k2} \end{bmatrix}; \quad \begin{bmatrix} U_1 \\ U_2 \\ U_3 \end{bmatrix} = \begin{bmatrix} 1 & 0 \\ 0 & 1 \\ -1 & 1 \end{bmatrix} \cdot \begin{bmatrix} U_{k1} \\ U_{k2} \end{bmatrix}$$

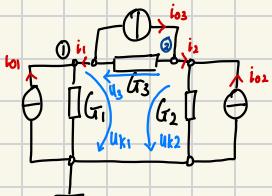


$$KCL: G_m \cdot U_{mu} - i_{mu} - i_{om} = 0$$

$$G_1 \cdot U_1 - i_1 = i_{o1}$$

$$G_2 \cdot U_2 - i_2 = i_{o2}$$

$$G_3 \cdot U_3 - i_3 = i_{o3}$$



$$\begin{bmatrix} -A^T & I & 0 \\ 0 & 0 & A \\ 0 & M & N \end{bmatrix} \cdot \begin{bmatrix} \underline{U_k} \\ \underline{U} \\ \underline{i} \end{bmatrix} = \begin{bmatrix} 0 \\ 0 \\ e \end{bmatrix}$$

$\underbrace{-A^T}_{\text{identity matrix}}$

$$\left[ \begin{array}{c|cc|ccc|c} -1 & 0 & 1 & 0 & 0 & 0 & 0 & U_{k1} \\ 0 & -1 & 0 & 1 & 0 & 0 & 0 & U_{k2} \\ 1 & -1 & 0 & 0 & 1 & 0 & 0 & U_1 \\ \hline 0 & 0 & 0 & 0 & 1 & 0 & -1 & U_2 \\ 0 & 0 & 0 & 0 & 0 & 1 & 1 & U_3 \end{array} \right] \cdot \begin{bmatrix} U_{k1} \\ U_{k2} \\ U_1 \\ U_2 \\ U_3 \\ i_1 \\ i_2 \\ i_3 \end{bmatrix} = \begin{bmatrix} 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ i_{01} \\ i_{02} \\ i_{03} \end{bmatrix}$$

M  $\quad \quad$  N

$$\underline{G}_k = -\underline{A} \underline{N}^{-1} \underline{M} \underline{A}^T$$

$$= \boxed{\begin{bmatrix} 1 & 0 & -1 \\ 0 & 1 & 1 \end{bmatrix}} \cdot \boxed{\begin{bmatrix} -1 & 0 & 0 \\ 0 & -1 & 0 \\ 0 & 0 & -1 \end{bmatrix}} \cdot \begin{bmatrix} G_1 \\ G_2 \\ G_3 \end{bmatrix} \cdot \begin{bmatrix} 1 & 0 \\ 0 & 1 \\ -1 & 1 \end{bmatrix}$$

$$= \begin{bmatrix} 1 & 0 & -1 \\ 0 & 1 & 1 \end{bmatrix} \cdot \begin{bmatrix} G_1 & 0 \\ 0 & G_2 \\ -G_3 & G_3 \end{bmatrix} = \begin{bmatrix} (G_1 + G_3) & -G_3 \\ -G_3 & (G_2 + G_3) \end{bmatrix}$$

if element lies between 4 node, it appears  $\underbrace{2}_{\text{times}}$  times  
it will be negative

$$\underline{i}_q = -\underline{A} \underline{N}^{-1} \underline{e} = -\begin{bmatrix} 1 & 0 & -1 \\ 0 & 1 & 1 \end{bmatrix} \cdot \begin{bmatrix} -1 & & \\ & -1 & \\ & & -1 \end{bmatrix} \cdot \begin{bmatrix} i_{01} \\ i_{02} \\ i_{03} \end{bmatrix}$$

$$= \begin{bmatrix} i_{01} - i_{03} \\ i_{02} + i_{03} \end{bmatrix} \Rightarrow \begin{bmatrix} G_1 + G_3 & -G_3 \\ -G_3 & G_2 + G_3 \end{bmatrix} \cdot \begin{bmatrix} u_{k1} \\ u_{k2} \end{bmatrix} = \begin{bmatrix} i_{01} - i_{03} \\ i_{02} + i_{03} \end{bmatrix}$$

## 5.4 Direct Formulation of Node Conductance Matrix

$$\underline{G}_k \cdot \underline{u}_k = \underline{i}_q$$

VCCS :

$$i_1 = 0, \quad i_2 = g u_1$$

$$\underline{G}_{VCCS} = \begin{bmatrix} 0 & 0 \\ g & 0 \end{bmatrix}$$

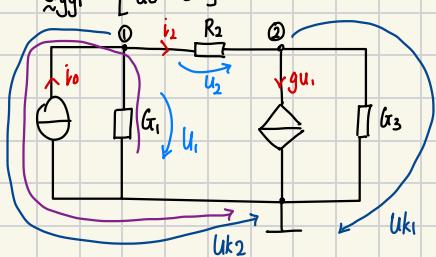
$$\begin{bmatrix} i_1 \\ i_2 \end{bmatrix} = \underline{G}_{VCCS} \begin{bmatrix} u_1 \\ u_2 \end{bmatrix}$$

Gyrator :

$$i_1 = G_d u_2$$

$$i_2 = -G_d u_1$$

$$\underline{G}_{gyr} = \begin{bmatrix} 0 & G_d \\ -G_d & 0 \end{bmatrix}$$



$$\text{Ohm: } U_2 = R_2 i_2$$

$$\Rightarrow i_2 = \frac{1}{R_2} U_2$$

$$\text{KVL: } -U_1 + U_{k1} = 0$$

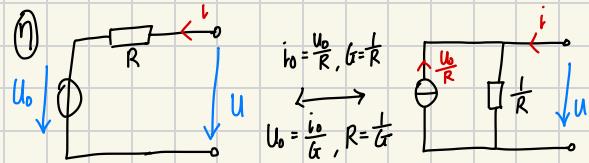
$$U_1 = U_{k1}$$

$$g_{U_1} = g_{U_{k1}}$$

$$\left[ \begin{array}{cc|c} G_1 + \frac{1}{R_2} & -\frac{1}{R_2} & \\ \hline -\frac{1}{R_2} + g & G_3 + \frac{1}{R_2} & \end{array} \right] \cdot \underbrace{\begin{bmatrix} U_{k1} \\ U_{k2} \\ \vdots \\ U_k \end{bmatrix}}_{\underline{U_k}} = \underbrace{\begin{bmatrix} i_0 \\ \vdots \\ 0 \\ \vdots \\ i_q \end{bmatrix}}_{\underline{i_q}}$$

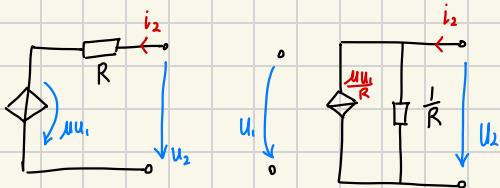
## 5.5 Non-Voltage Controlled Element

### 5.5.1 Source Transform



node between the resistor and source

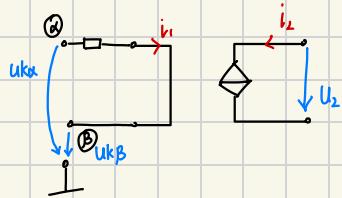
no ①!



## 5.5.2 Ohm's Law



CCCS:

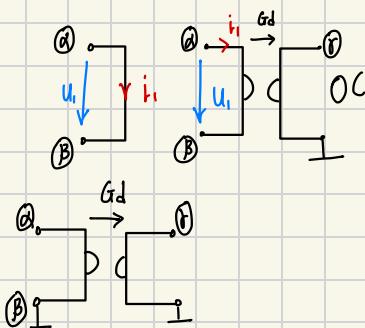
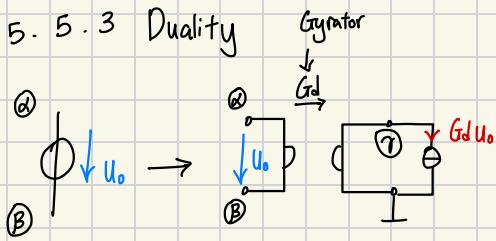


$$i_1 = G(U_{k\alpha} - U_{k\beta})$$

$$i_2 = \beta i_1$$

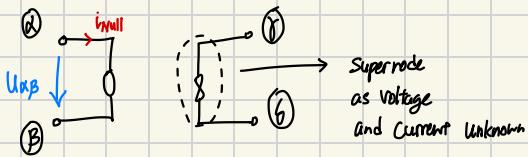
$$= \beta G(U_{k\alpha} - U_{k\beta})$$

## 5.5.3 Duality



$$\begin{bmatrix} G_d \\ -G_d \end{bmatrix} \begin{bmatrix} U_{k\alpha} & U_{k\beta} \end{bmatrix} = \begin{bmatrix} G_d \\ G_d \end{bmatrix} \begin{bmatrix} \alpha & \gamma \end{bmatrix}$$

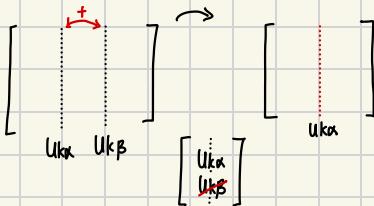
## 5.5.4 Nullors



$$KCL \textcircled{1} + KCL \textcircled{5}$$

$$U_{AB} = 0, i_{Null} = 0$$

$$\downarrow U_{KA} = U_{KB}$$



Nullator reduce Columns

Norators reduce rows

## 6. Reactive elements

Charge:

$$q(t) = \int_{-\infty}^t i(t') dt' \\ = q(t_0) + \int_{t_0}^t i(t') dt'$$

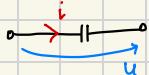
flux:

$$\Phi(t) = \Phi(t_0) + \int_{t_0}^t u(t') dt'$$

$$i(t) = \frac{dq(t)}{dt} = \underline{\underline{\dot{q}(t)}}$$

$$u(t) = \frac{d\Phi(t)}{dt} = \underline{\underline{\dot{\Phi}(t)}}$$

Capacitors:



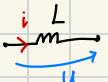
$$q(t) = \int_{-\infty}^t i(t') dt'$$

$$q(t) = C \cdot u(t)$$

C: Capacitance

$$i(t) = \dot{q}(t) = C \dot{u}(t)$$

inductor:



$$\Phi(t) = \int_{-\infty}^t u(t') dt'$$

$$\underline{\Phi}(t) = L i(t)$$

$L$ : inductance

$$U(t) = \frac{d}{dt} \underline{\Phi}(t)$$

$$= L \dot{i}(t)$$

## 6.1 Duality

$$U \xrightarrow{R_d} R_d i^d ; \quad i \xrightarrow{R_d} \frac{1}{R_d} U^d$$

$$q(t) = \int_{-\infty}^t i(t') dt'$$

$\downarrow R_d$

$$\int_{-\infty}^t \frac{1}{R_d} U^d(t') dt' = \frac{1}{R_d} \int_{-\infty}^t U^d(t') dt'$$

$$= \frac{1}{R_d} \underline{\Phi}^d(t)$$

$$\underline{\Phi}(t) \xrightarrow{R_d} R_d q^d(t)$$



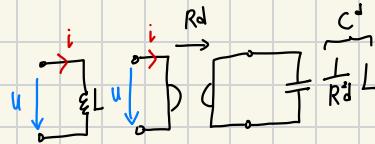
$$q(t) = C U(t)$$

$\downarrow R_d$

$$\frac{1}{R_d} \underline{\Phi}^d(t) = C R_d i^d(t)$$

$$\underline{\Phi}^d(t) = \frac{R_d^2 C}{L^d} i^d(t)$$





## 6.2 Properties of reactances

### 6.2.1 Continuity

State Variables :

$U, q$  Capacitors

$i, \Phi$  inductors

do not jump

### 6.2.2 Energy

$$\text{power : } P(t) = U(t) \cdot i(t)$$

$$W_c(t_1, t_2) = \int_{t_1}^{t_2} P(t) dt$$

$$= \int_{t_1}^{t_2} U(t) i(t) dt$$

$$i(t) = C \dot{u}(t)$$

$$W_c(t_1, t_2) = \int_{t_1}^{t_2} U(t) (C \dot{u}(t)) dt$$

$$= \int_{u(t_1)}^{u(t_2)} C \cdot U du = \frac{C}{2} (u^2(t_2) - u^2(t_1))$$

$$W_c(u_1, u_2) = \frac{C}{2} (u_2^2 - u_1^2)$$

$$W_c(q_1, q_2) = \frac{1}{2C} (q_2^2 - q_1^2)$$

for  $u_1 = 0$ ,  $u_2 = u$

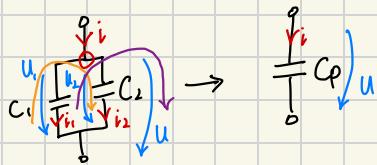
$$E(u) = W_c(0, u)$$

$$= \frac{C}{2} u^2$$

$$W_L(i_1, i_2) = \frac{L}{2} (i_2^2 - i_1^2)$$

$$E_L(i) = \frac{L}{2} i^2$$

### 6.3 Connection of Reactances



$$KCL: -i + i_1 + i_2 = 0$$

$$\begin{cases} i = i_1 + i_2 \\ \int dt \end{cases}$$

$$q(t) = q_1(t) + q_2(t)$$

$$C_p u(t) = C_1 u_1(t) + C_2 u_2(t)$$

$$KVL: -U_1 + U = 0$$

$$KVL: -U_2 + U = 0$$

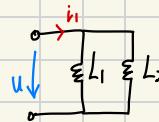
$$U = U_1 = U_2$$

$$C_p u = C_1 u + C_2 u$$

$$C_p = C_1 + C_2$$

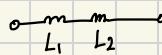


$Rd$



$$C_S = C_1 \parallel C_2$$

$$L_P = L_1 \parallel L_2$$



$$L_S = L_1 + L_2$$

$$U = U_1 + U_2$$

$$i = i_1 + i_2$$

$$q = q_1 = q_2$$

$$q = C_S U$$

series

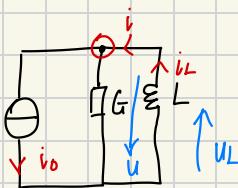
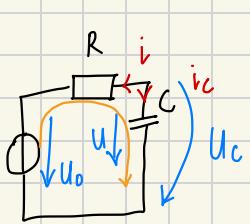
$$U = \frac{1}{C_S} q$$

$$\frac{1}{C_S} i = \frac{1}{C_1} i_1 + \frac{1}{C_2} i_2$$

$$\frac{1}{C_S} = \frac{1}{C_1} + \frac{1}{C_2}$$

$$C_S = C_1 \parallel C_2$$

# 7. linear first order Circuits



$$KCL: i_o - G U_L - i_L = 0$$

$$KVL: -U_o + R i_c + U_c = 0$$

$$i_c = C \dot{U}_c$$

$$-U_o + R(C \dot{U}_c) + U_c = 0$$

$$\dot{U}_c = -\frac{1}{RC} U_c + \frac{1}{RC} U_o$$

$$\begin{aligned} T &= RC \\ X &= U_c, v = U_o \end{aligned}$$

$$U_L = L \dot{i}_L$$

$$i_o - G(L \dot{i}_L) - i_L = 0$$

$$\dot{i}_L = -\frac{1}{GL} i_L + \frac{1}{GL} i_o$$

$$\begin{aligned} T &= GL \\ x &= i_L, v = i_o \end{aligned}$$

## 7.1 General Excitation

$$\dot{x} = -\frac{1}{T} x + \frac{1}{T} v$$

homogeneous Case

$$\dot{x} = -\frac{1}{T} x$$

$$\frac{dx}{dt} = -\frac{1}{T} x$$

$$\frac{dx}{x} = -\frac{dt}{T}$$

$$\int \frac{dx}{x} = -\int \frac{dt}{T} \quad \text{integr. const.}$$

$$\ln(x_{hom}) = -\frac{t}{T} + C_{int}$$

$$x_{hom}(t) = e^{-\frac{t}{T}} \cdot C$$

$$\left. \begin{aligned} X(t) &= X_0 e^{-\frac{t-t_0}{\tau}} + \int_{t_0}^t \frac{1}{\tau} e^{-\frac{t-t'}{\tau}} v(t') dt' \\ U_C(t) &= U_{C0} e^{-\frac{t-t_0}{RC}} + \int_{t_0}^t \frac{1}{RC} e^{-\frac{t-t'}{RC}} U_o(t') dt' \end{aligned} \right.$$

or

$$i_L(t) = i_L(t_0) e^{-\frac{t-t_0}{RL}} + \int_{t_0}^t \frac{1}{RL} e^{-\frac{t-t'}{RL}} i_o(t') dt'$$

## 7.2 Constant Excitation

$$v(t) \rightarrow X\omega$$

$$\begin{aligned} \overset{o}{X}(t) &= -\frac{1}{\tau} X(t) + \frac{1}{\tau} X_\infty \\ X(t) &= X_0 e^{-\frac{t-t_0}{\tau}} + \int_{t_0}^t \frac{1}{\tau} e^{-\frac{t-t'}{\tau}} X_\infty dt' \\ &= X_0 e^{-\frac{t-t_0}{\tau}} + \left[ \frac{1}{\tau} e^{-\frac{t-t'}{\tau}} (T) X_\infty \right]_{t_0}^t \\ &= X_0 e^{-\frac{t-t_0}{\tau}} + X_\infty - e^{-\frac{t-t_0}{\tau}} X_\infty \\ &= X_\infty + (X_0 - X_\infty) e^{-\frac{t-t_0}{\tau}} \end{aligned}$$

Stable Case:  $\tau > 0$ 

$$e^{-1} \text{ approx} = 0.37 \approx \frac{1}{3}$$

$$t \rightarrow \infty : X(t) \rightarrow X_\infty$$

$$\begin{aligned} X(t_0 + T) &= X_\infty + (X_0 - X_\infty) \underbrace{e^{-\frac{t_0 + \tau - t_0}{\tau}}}_{\frac{1}{3}} \\ &\approx X_\infty + (X_0 - X_\infty) \frac{1}{3} = 1 - \frac{2}{3} \end{aligned}$$

$$= X_\infty + X_0 \left(1 - \frac{2}{3}\right) - X_\infty \left(1 - \frac{2}{3}\right)$$

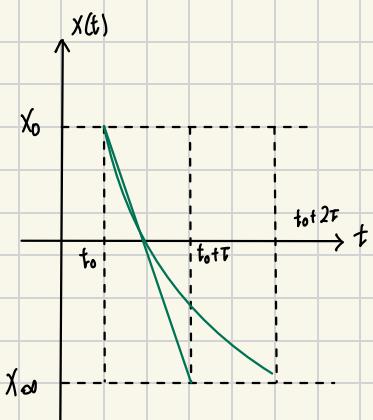
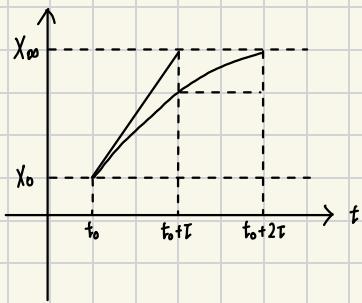
$$= X_0 + (X_\infty - X_0) \frac{2}{3}$$

↓  
moved  $\frac{2}{3}$  of distance from  $X_\infty$  to  $X_0$   
towards  $X_\infty$

· Linearization

$$\begin{aligned}X_{lin}(t) &= X(t_0) + \frac{dx(t)}{dt} \Big|_{t=t_0} (t - t_0) \\&= X_0 + \left(-\frac{1}{\tau}\right) (X_0 - X_\infty) (t - t_0) \\&= X_0 + \frac{X_0 - X_\infty}{\tau} (t - t_0)\end{aligned}$$

$$X_{lin}(t_0 + \tau) = X_\infty$$



Unstable Case:  $\tau < 0$

$$X(t) = X_\infty + (X_0 - X_\infty) e^{\frac{t-t_0}{|\tau|}}$$

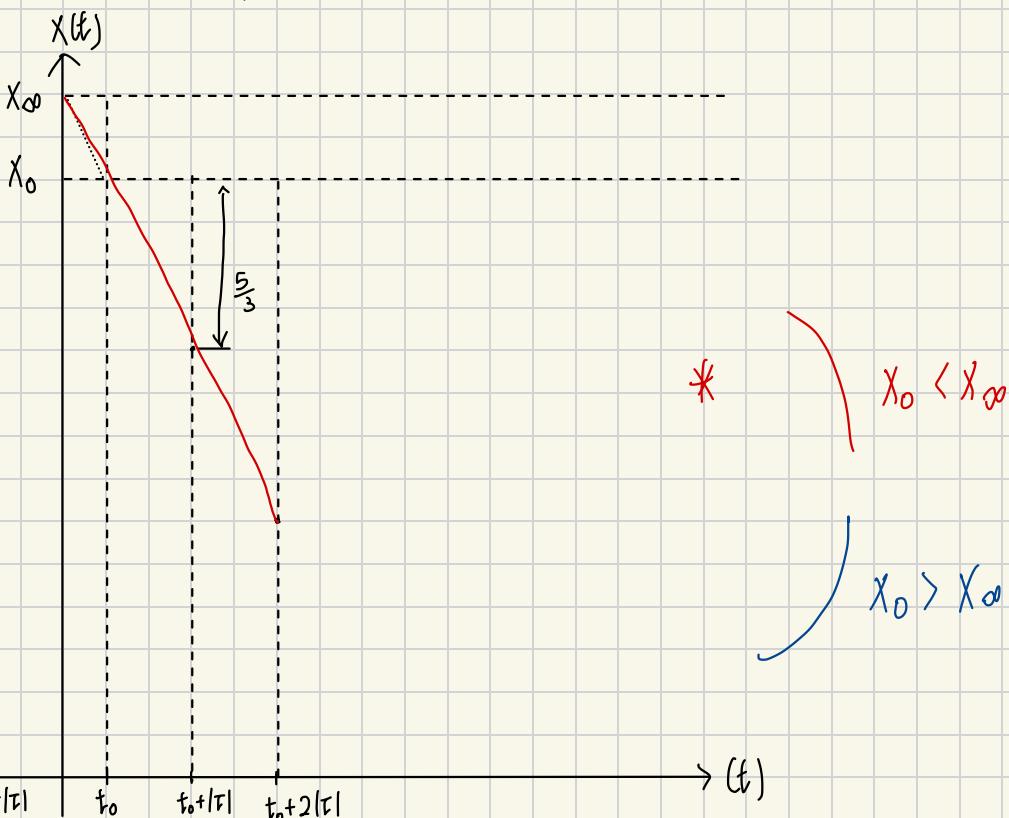
$$X(t_0 + |\tau|) \cong X_0 + (X_0 - X_\infty) \frac{5}{3}$$

$X_{lin}(t) \Rightarrow$

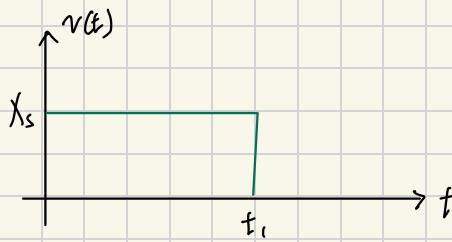
tangent:  $(t_0, X_0) - (t_0 - |\tau|, X_\infty)$

$t \rightarrow \infty : X(t) \rightarrow +\infty$  for  $X_0 > X_\infty$

$X(t) \rightarrow -\infty$  for  $X_0 < X_\infty$



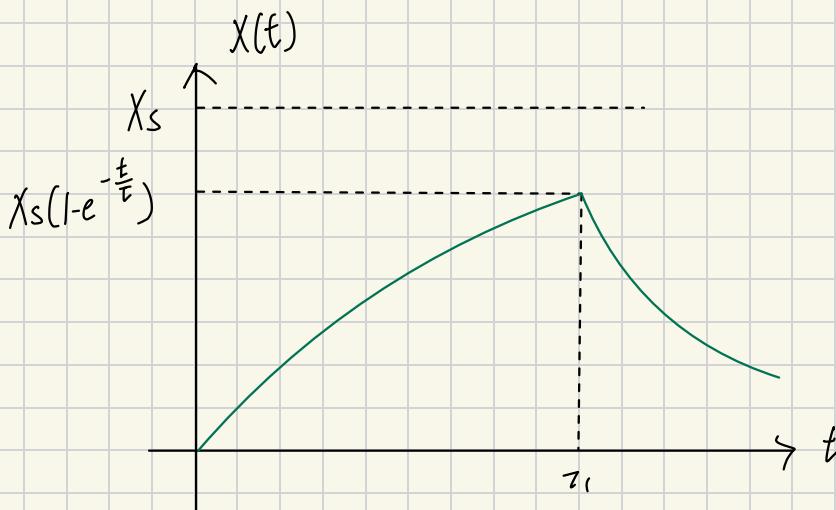
### 7.3 Piecewise Constant Exc.



$$v(t) = \begin{cases} v_s & 0 \leq t \leq t_1 \\ 0 & \text{else} \end{cases}$$

$$t \geq 0 : X(t) = X_0 + (X_0 - X_\infty) e^{-\frac{t-t_0}{\tau}}$$

$$\begin{aligned} X_0 &= X(0) = 0 \\ &= X_s - X_s e^{-\frac{t_0}{\tau}} \end{aligned}$$



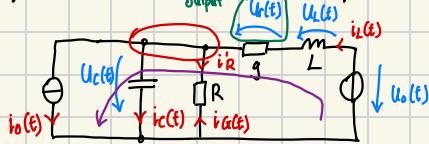
$$t \geq t_1 : X_0 = X(t_1)$$

$$= X_s - X_s e^{-\frac{t_1}{\tau}}$$

$$X(t) = \left( X_s - X_s e^{-\frac{t_1}{\tau}} \right) e^{-\frac{t-t_1}{\tau}}$$

## 8 second order Circuits

### 9.1 Formulation of State Eqn



$$KCL: i_o + i_C - i_L - i_R = 0$$

$$KVL: -U_o + U_L + U_R + U_C = 0$$

$$\text{Ohm: } U_C = R i_R = -R i_G$$

$$i_G = -\frac{1}{R} U_C$$

$$\text{Ohm: } i_L = g U_R$$

$$U_R = \frac{1}{g} i_L$$

$$i_o + i_C - i_L + \frac{1}{R} U_C = 0$$

$$-U_o + U_L + \frac{1}{g} i_L + U_C = 0$$

$$\text{Reactances: } i_C = C U_C$$

$$U_L = L i_L$$

$$i_o + C U_C - i_L + \frac{1}{R} U_C = 0$$

$$-U_o + L i_L + \frac{1}{g} i_L + U_C = 0$$

$$\dot{U}_C = -\frac{1}{RC} U_C + \frac{1}{C} i_L - \frac{1}{C} i_o$$

Xincheng

$$\dot{i}_L = -\frac{1}{L} U_C - \frac{1}{gL} i_L + \frac{1}{L} U_o$$

$$\underline{x}(t) = \begin{bmatrix} U_C(t) \\ i_L(t) \end{bmatrix}$$

$$\underline{y}(t) = \begin{bmatrix} U_o(t) \\ i_o(t) \end{bmatrix}$$

$$\dot{\underline{x}} = A \underline{x} + B \underline{y}$$

$$\tilde{A} = \begin{bmatrix} -\frac{1}{RC} & \frac{1}{C} \\ -\frac{1}{L} & -\frac{1}{gL} \end{bmatrix}$$

$$\tilde{B} = \begin{bmatrix} 0 & -\frac{1}{C} \\ \frac{1}{L} & 0 \end{bmatrix}$$

$$y(t) = u_r(t)$$

$$= \frac{1}{g} i_L(t)$$

$$y(t) = \underline{C}^T \underline{x}(t) + \underline{d}^T v(t)$$

$$\underline{C}^T = [0, \frac{1}{g}]$$

$$\underline{d}^T = [0, 0]$$

## 8.2 Solution of State Eqn

### 8.2.1 General Solution

$$\dot{X} = -\frac{1}{T}X + \frac{1}{T}V$$

$$X(t) = e^{-\frac{t-t_0}{T}} X(t_0) + \int_{t_0}^t e^{-\frac{t-t'}{T}} \frac{1}{T} V(t') dt' \quad \dots \text{ 1st order}$$

$$\text{2nd order : } X(t) = \exp(A(t-t_0)) X(t_0) + \int_{t_0}^t \exp(A(t-t')) B V(t') dt'$$

Taylor series :

$$e^{at} = 1 + at + \frac{1}{2}(at)^2 + \frac{1}{6}(at)^3 + \dots$$

$$= \sum_{j=0}^{\infty} \frac{1}{j!} (at)^j$$

$$\frac{de^{at}}{dt} = ae^{at}$$

$$\exp(At) = \sum_{j=0}^{\infty} \underbrace{\frac{1}{j!} (At)^j}_{A^j \cdot t^j}$$

$$\int \exp(At) dt = A^{-1} \exp(At)$$

$$\frac{d\exp(At)}{dt} = \underbrace{A \exp(At)}_{= \exp(At)A}$$

#

## 8.2.2 Autonomous Case

$$\underline{v}(t) \rightarrow \underline{v}_0$$

$$\underline{x}(t) = \exp(\underline{A}(t-t_0)) \underline{x}(t_0) + \int_{t_0}^t \exp(\underline{A}(t-t')) \underline{B} \underline{v}_0 dt'$$

$$\underline{x}(t) = \exp(\underline{A}(t-t_0)) \underline{x}(t_0) + \left[ \exp(\underline{A}(t-t')) \cdot \underline{A}^{-1} \underline{B} \underline{v}_0 \right]_{t_0}^t$$

$$= \exp(\underline{A}(t-t_0)) \underline{x}(t_0) + \left[ -\underline{A}^{-1} \underline{B} \underline{v}_0 + \exp(\underline{A}(t-t_0)) \underline{A}^{-1} \underline{B} \underline{v}_0 \right]$$

$$= -\underline{A}^{-1} \underline{B} \underline{v}_0 + \exp(\underline{A}(t-t_0)) (\underline{x}(t_0) + \underline{A}^{-1} \underline{B} \underline{v}_0)$$

autonomous:

$$\dot{\underline{x}} = \underline{A} \underline{x} + \underline{B} \underline{v}_0 \longrightarrow$$

$$\text{Substitute } \underline{x} = \underline{x}' + \underline{x}_\infty$$

$$\begin{aligned}\dot{\underline{x}} &= \dot{\underline{x}'} \\ \dot{\underline{x}'} &= \underline{A}(\underline{x}' + \underline{x}_\infty) + \underline{B} \underline{v}_0\end{aligned}$$

$$\begin{aligned}\dot{\underline{x}'} &= \underline{A} \underline{x}' ; \quad \underline{x}'(t_0) = \underline{x}(t_0) - \underline{x}_\infty \\ \underline{x}'(t) &= \exp(\underline{A}(t-t_0)) \underline{x}'(t_0)\end{aligned}$$

$$\underline{x}(t) - \underline{x}_\infty = \exp(\underline{A}(t-t_0))(\underline{x}(t_0) - \underline{x}_\infty)$$

$$\underline{x}(t) = \underline{x}_\infty + \exp(\underline{A}(t-t_0))(\underline{x}_0 - \underline{x}_\infty)$$

$$\underline{x}_\infty = -\underline{A}^{-1} \underline{B} \underline{v}_0$$

$$\underline{x}(t) = \underline{x}_\infty + \exp(\underline{A}(t-t_0))(\underline{x}_0 - \underline{x}_\infty)$$

$$\underline{x}_0 = \underline{x}(t_0)$$

### 8.2.3 Homogeneous State eqn

$$\dot{\underline{X}} = \underline{A} \underline{X}$$

$$\underline{X}(t) = \exp(\underline{A}(t-t_0)) \underline{X}(t_0)$$

eigenvalues :

$$\det(\underline{A} - \lambda \underline{I}) = 0$$

$$\begin{aligned} \det \begin{bmatrix} a_{11} - \lambda & a_{12} \\ a_{21} & a_{22} - \lambda \end{bmatrix} &= (a_{11} - \lambda)(a_{22} - \lambda) - a_{12}a_{21} \\ &= \lambda^2 - (a_{11} + a_{22})\lambda + (a_{11}a_{22} - a_{12}a_{21}) \\ &\quad \downarrow \text{tr}(\underline{A}) \\ T = \text{trace}(\underline{A}) \end{aligned}$$

$$\Delta = \det(\underline{A})$$

$$\lambda^2 - T\lambda + \Delta = 0$$

$$\lambda_{1/2} = \frac{T}{2} \pm \sqrt{\left(\frac{T}{2}\right)^2 - \Delta}$$

$$\text{(I)} : \left(\frac{T}{2}\right)^2 > \Delta : \lambda_1, \lambda_2 \in \mathbb{R}$$

$$\text{(II)} : \left(\frac{T}{2}\right)^2 = \Delta : \lambda_1 = \lambda_2 \in \mathbb{R}$$

$$\text{(III)} : \left(\frac{T}{2}\right)^2 < \Delta : \lambda_1 = \lambda_2^* \in \mathbb{C}$$

↓  
complex conjugate

$\lambda_i$  : Eigenvalues

## 8.2.4 Normal Form

$$\lambda_1 \neq \lambda_2 \in \mathbb{R}$$

$$\tilde{A} \tilde{q}_k = \lambda_k \tilde{q}_k \quad q_k: \text{eigenvectors}$$

$$\tilde{A} \tilde{q}_1 = \lambda_1 \tilde{q}_1$$

$$\tilde{A} \tilde{q}_2 = \lambda_2 \tilde{q}_2$$

$$[\tilde{A} \tilde{q}_1, \tilde{A} \tilde{q}_2] = [\lambda_1 \tilde{q}_1, \lambda_2 \tilde{q}_2]$$

$$\tilde{A} \underbrace{[\tilde{q}_1, \tilde{q}_2]}_{\tilde{Q}} = \underbrace{[\tilde{q}_1, \tilde{q}_2]}_{\tilde{Q}} \underbrace{\begin{bmatrix} \lambda_1 & 0 \\ 0 & \lambda_2 \end{bmatrix}}_{\tilde{\Lambda}}$$

$$\tilde{A} \tilde{Q} = \tilde{Q} \tilde{\Lambda}$$

$$\tilde{A} = \tilde{Q} \tilde{\Lambda} \tilde{Q}^{-1}$$

eigenvalue decomposition (EVD)

$$\overset{\circ}{X} = \tilde{A} X$$

$$\text{EVD: } \overset{\circ}{X} = \tilde{Q} \tilde{\Lambda} \tilde{Q}^{-1} X$$

$$\underbrace{\tilde{Q}^{-1} \overset{\circ}{X}}_{\tilde{S}} = \tilde{\Lambda} \underbrace{\tilde{Q}^{-1} X}_{\tilde{S}}$$

$$\tilde{s} = \tilde{\Lambda} \tilde{s} \leftarrow x_i$$

$$\text{diagonalized: } \tilde{s}_1 = \lambda_1 s_1$$

$$\tilde{s}_2 = \lambda_2 s_2$$

$$\xi_1(t) = e^{\lambda_1(t-t_0)} \cdot \xi_1(t_0)$$

$$\xi_2(t) = e^{\lambda_2(t-t_0)} \cdot \xi_2(t_0)$$

$$\xi(t) = \underbrace{\begin{bmatrix} e^{\lambda_1(t-t_0)} & 0 \\ 0 & e^{\lambda_2(t-t_0)} \end{bmatrix}}_{\exp(\Delta(t-t_0))} \cdot \xi(t_0)$$

$$\underbrace{Q^{-1}}_{\sim} X(t) = \exp(\Delta(t-t_0)) \underbrace{Q^{-1}}_{\sim} X(t_0)$$

$$X(t) = \underbrace{Q \exp(\Delta(t-t_0))}_{\exp(A(t-t_0))} \underbrace{Q^{-1} X(t_0)}_{\xi(t_0)}$$

$$= \begin{bmatrix} q_1, q_2 \end{bmatrix} \cdot \begin{bmatrix} e^{\lambda_1(t-t_0)} & 0 \\ 0 & e^{\lambda_2(t-t_0)} \end{bmatrix} \begin{bmatrix} \xi_1(t_0) \\ \xi_2(t_0) \end{bmatrix}$$

$$= \xi_1(t_0) e^{\lambda_1(t-t_0)} \cdot q_1 + \xi_2(t_0) e^{\lambda_2(t-t_0)} \cdot q_2$$

$$= \exp(A(t-t_0)) \xi(t_0)$$

$$A q_k = \lambda_k q_k$$

$$(A - \lambda_k I) q_k = 0$$

$$\Rightarrow \det(A - \lambda_k I) = 0$$

$$\begin{bmatrix} a_{11} - \lambda_k & a_{12} \\ a_{21} & a_{22} - \lambda_k \end{bmatrix} \cdot \begin{bmatrix} q_{k1} \\ q_{k2} \end{bmatrix} = \begin{bmatrix} 0 \\ 0 \end{bmatrix}$$

non-zero

$$(a_{11} - \lambda_k) q_{k1} + a_{12} q_{k2} = 0$$

$$q_k = \begin{bmatrix} -a_{12} \\ a_{11} - \lambda_k \end{bmatrix}$$

## 8.2.5 Jordan Normal form

$$\lambda_1 = \lambda_2 \in \mathbb{R}$$

Special case:

$$\tilde{A} = \begin{bmatrix} \lambda & 0 \\ 0 & \lambda \end{bmatrix}$$

$$\tilde{A}: \text{non-diagonal} : \det(\tilde{A} - \lambda \tilde{I}) = 0$$

$$\tilde{A} q = \lambda q \rightarrow \begin{matrix} \text{eigenvector} \\ q \end{matrix}$$

only one  $q$

$$\tilde{J} = \begin{bmatrix} \lambda & 1 \\ 0 & \lambda \end{bmatrix}$$

$\uparrow$   
Jordan matrix

$$\tilde{A} \tilde{Q}^{-1} = \tilde{Q}' \cdot \tilde{J}$$

$$\tilde{Q}' = \begin{bmatrix} q & q' \\ 0 & 1 \end{bmatrix}$$

$$\tilde{A} q = \lambda q$$

$$\tilde{A} q' = q + \lambda q'$$

$$(\tilde{A} - \lambda \tilde{I}) q' = q$$

$$\tilde{A} = \tilde{Q}' \tilde{J} \tilde{Q}'^{-1}$$

$$\dot{\underline{x}} = \tilde{A} \underline{x}$$

$$\dot{\underline{x}} = \tilde{Q}' \tilde{J} \tilde{Q}'^{-1} \underline{x}$$

$$\tilde{Q}^{-1} \tilde{\underline{X}} = \tilde{\underline{J}} \tilde{Q}^{-1} \tilde{\underline{X}}$$

$$\tilde{\underline{\xi}}' = \tilde{\underline{\xi}}'$$

$$\tilde{\underline{\xi}}' = \tilde{\underline{J}} \tilde{\underline{\xi}}' \quad \tilde{\underline{\xi}}' = \begin{bmatrix} \tilde{\xi}_1' \\ \tilde{\xi}_2' \end{bmatrix}$$

$$\dot{\tilde{\xi}}_1' = \lambda \tilde{\xi}_1' + \tilde{\xi}_2'$$

$$\boxed{\dot{\tilde{\xi}}_2' = \lambda \tilde{\xi}_2'} \quad \tilde{\xi}_2'(t) = e^{\lambda(t-t_0)} \tilde{\xi}_2'(t_0)$$

$$\tilde{\xi}_1' = \lambda \tilde{\xi}_1' + e^{\lambda(t-t_0)} \tilde{\xi}_2'(t_0)$$

$$\tilde{\xi}_1'(t) = e^{\lambda(t-t_0)} \tilde{\xi}_1'(t_0) + (t-t_0) e^{\lambda(t-t_0)} \tilde{\xi}_2'(t_0)$$

$$\begin{aligned} \tilde{\xi}_1' &= \underbrace{\lambda e^{\lambda(t-t_0)} \tilde{\xi}_1'(t_0)}_{\lambda \tilde{\xi}_1'} + e^{\lambda(t-t_0)} \tilde{\xi}_2'(t_0) + \underbrace{\lambda(t-t_0) e^{\lambda(t-t_0)} \tilde{\xi}_2'(t_0)}_{\tilde{\xi}_2'(t)} \\ &= \lambda \tilde{\xi}_1' + e^{\lambda(t-t_0)} \tilde{\xi}_2'(t_0) \end{aligned}$$

$$\underline{X}(t) = (\tilde{\xi}_1'(t_0) + (t-t_0) \tilde{\xi}_2'(t_0)) e^{\lambda(t-t_0)} \underline{x} + \tilde{\xi}_2'(t_0) e^{\lambda(t-t_0)} \underline{x}'$$

Recap:

$$\dot{\underline{X}} = \underline{A} \underline{X} + \underline{B} \underline{V}$$

$$\underline{X}(t) = \exp(\underline{A}(t-t_0)) \underline{X}(t_0) + \int_{t_0}^t \exp(\underline{A}(t-t')) \underline{B} \underline{v}(t') dt'$$

$$\underline{V}(t) = \underline{V}_0$$

$$\dot{\underline{X}} = \underline{A} \underline{X} + \underline{B} \underline{V}_0$$

$$= \underline{A} \underline{X} + \underline{B} \underline{V}_0$$

$$\text{equilibrium : } \dot{\underline{X}} = 0 ; 0 = \underline{A} \underline{X}_{\infty} + \underline{B} \underline{V}_0$$

$$\underline{X}_{\infty} = - \underline{A}^{-1} \underline{B} \underline{V}_0$$

$$\underline{X} + \underline{X}' + \underline{X}_{\infty}$$

$$\overset{\circ}{\underline{X}} = \overset{\circ}{A} \underline{X}$$

$$\underline{X}'(t) = \exp(\overset{\circ}{A}(t-t_0)) \underline{X}'(t_0)$$

$$\underline{X}(t) = \underline{X}'(t) + \underline{X}_\infty$$

$$\overset{\circ}{\underline{X}} = \overset{\circ}{A} \underline{X}$$

$$\det(\overset{\circ}{A} - \lambda I) = 0 \Rightarrow \lambda_{1,2}$$

$$\text{I)} \quad \lambda_1 \neq \lambda_2 \in \mathbb{R}$$

$$\overset{\circ}{A} = \overset{\circ}{Q} \overset{\circ}{\Lambda} \overset{\circ}{Q}^{-1}$$

$$\overset{\circ}{\Lambda} = \text{diag}(\lambda_1, \lambda_2)$$

$$\begin{aligned}\underline{X}(t) &= \overset{\circ}{Q} \exp(\overset{\circ}{\Lambda}(t-t_0)) \overset{\circ}{Q}^{-1} \underline{X}(t_0) \\ &= \overset{\circ}{Q} \begin{bmatrix} e^{\lambda_1(t-t_0)} & 0 \\ 0 & e^{\lambda_2(t-t_0)} \end{bmatrix} \overset{\circ}{Q}^{-1} \underline{X}(t_0) \\ &= \zeta_1(t_0) e^{\lambda_1(t-t_0)} \cdot q_1 + \zeta_2(t_0) e^{\lambda_2(t-t_0)} q_2\end{aligned}$$

$$\text{II)} \quad \lambda_1 = \lambda_2 \in \mathbb{R} :$$

$$\overset{\circ}{A} = \overset{\circ}{Q} \overset{\circ}{J} \overset{\circ}{Q}^{-1} \quad \overset{\circ}{J} = \begin{bmatrix} \lambda & 1 \\ 0 & \lambda \end{bmatrix}$$

### 8.2.6 Real-valued Normal form

$$\lambda_1 = \alpha + j\beta \in \mathbb{C} \quad j = \sqrt{-1}$$

$$\lambda_2 = \alpha - j\beta = \lambda_1^* \in \mathbb{C}$$

$$\begin{array}{l} \overset{\circ}{\underline{X}} = \overset{\circ}{A} \underline{X} \\ \downarrow \end{array}$$

$$\overset{\circ}{\underline{X}} = \overset{\circ}{Q}_{\text{real}} \overset{\circ}{\Lambda}_{\text{real}} \overset{\circ}{Q}_{\text{real}}^{-1} \underline{X}$$

$$\zeta_{\text{real}} = \overset{\circ}{\Lambda}_{\text{real}} \zeta_{\text{real}}$$

$$\zeta_{\text{real}} = \overset{\circ}{Q}_{\text{real}}^{-1} \underline{X}$$

$$(\tilde{A} - \lambda_1 \tilde{I}) \tilde{q}_1 = \underline{0}$$

$$\tilde{q}_1 = q_r + j q_i$$

$$\tilde{Q}_{\text{real}} = [q_r, -q_i]$$

$$\tilde{\Lambda}_{\text{real}} = \begin{bmatrix} \alpha & -\beta \\ \beta & \alpha \end{bmatrix}$$

$$\text{EVD: } \tilde{A} = \tilde{Q} \tilde{\Lambda} \tilde{Q}^{-1}$$

$$\tilde{g}(t) = \tilde{Q}^{-1} \tilde{x}(t)$$

$$\tilde{g}_{\text{real}} = \begin{bmatrix} 1 & 1 \\ -j & j \end{bmatrix} \tilde{g}$$

$$= \begin{bmatrix} 2 \operatorname{Re}\{\tilde{g}_1\} \\ 2 \operatorname{Im}\{\tilde{g}_2\} \end{bmatrix}$$

$$\overset{\circ}{g} = \tilde{\Lambda} \tilde{g}$$

$$g_1(t) = e^{\lambda_1(t-t_0)} g_1(t_0)$$

$$= e^{\alpha(t-t_0)} e^{j\beta(t-t_0)} g_1(t_0)$$

$$g_1(t_0) = k e^{j\theta} \leftarrow \text{angle of complex value}$$

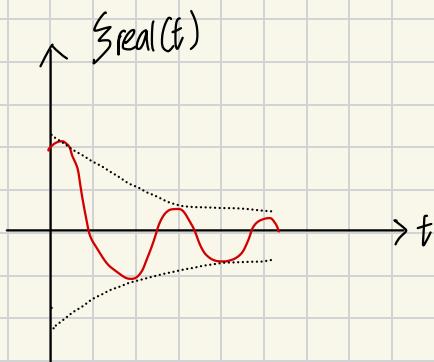
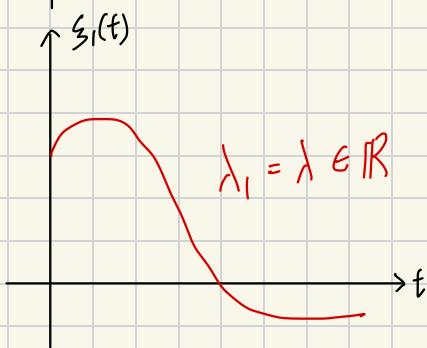
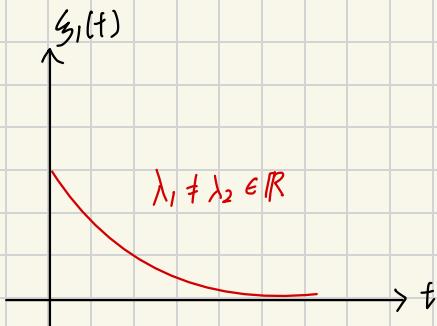
$$g_1(t) = e^{\alpha(t-t_0)} e^{j(\beta(t-t_0) + \theta)} \cdot k$$

Euler's rule:  $e^{j\varphi} = \cos \varphi + j \sin \varphi$

$$g_1(t) = e^{\alpha(t-t_0)} k [\cos(\beta(t-t_0) + \theta) + j \sin(\beta(t-t_0) + \theta)]$$

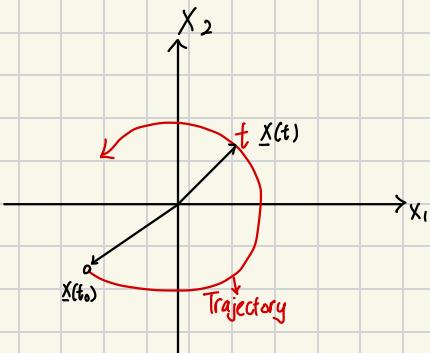
$$g_{\text{real}}(t) = \begin{bmatrix} 2 \operatorname{Re}\{g_1\} \\ 2 \operatorname{Im}\{g_1\} \end{bmatrix}$$

$$g_{\text{real}}(t) = 2k e^{\alpha(t-t_0)} \cdot \begin{bmatrix} \cos(\beta(t-t_0) + \theta) \\ \sin(\beta(t-t_0) + \theta) \end{bmatrix}$$



## 8.3 Phase Portrait (qualitative properties)

### 8.3.1 Trajectory



### 8.3.2 Focii Case I & III

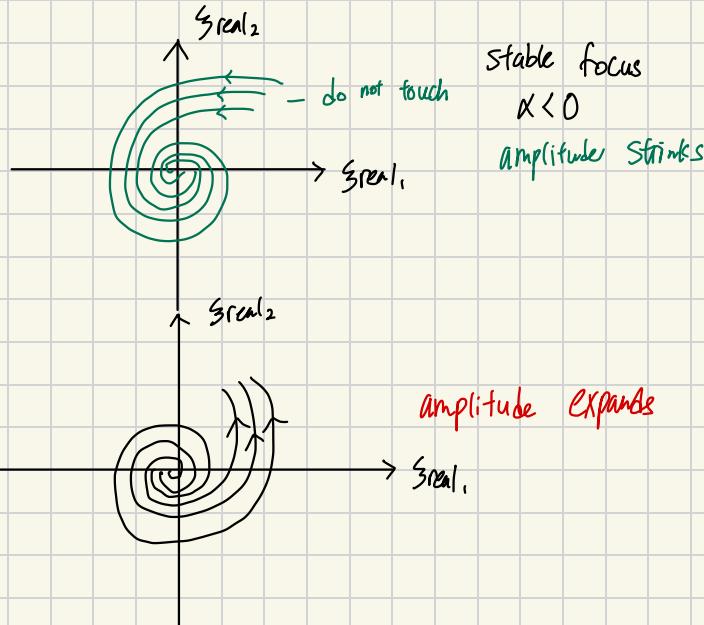
$$\lambda_1 = \alpha + j\beta$$

$$\alpha \neq 0, \beta > 0$$

for  $t_0 = 0$ :

$$s_{\text{real}_1}(t) = k e^{\alpha t} \cos(\beta t + \theta)$$

$$s_{\text{real}_2}(t) = k e^{\alpha t} \sin(\beta t + \theta)$$



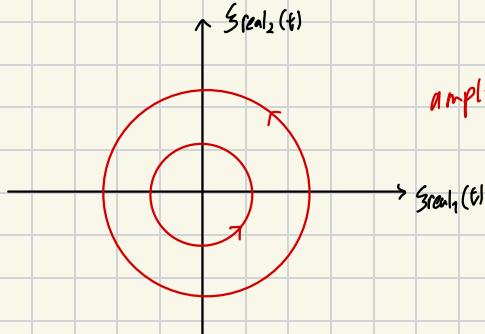
### 8.3.3 Center

$$\lambda_1 = j\beta$$

$$\alpha = 0, \beta > 0$$

$$\xi_{\text{real}_1}(t) = k \cos(\beta t + \theta)$$

$$\xi_{\text{real}_2}(t) = k \sin(\beta t + \theta)$$



amplitude Constant, Centers are Unstable

### 8.3.4 Nodes

$$\lambda_1 \neq \lambda_2 \in \mathbb{R}$$

$$\lambda_1 \cdot \lambda_2 > 0$$

normal forms :

$$\xi_1(t) = e^{\lambda_1 t} \xi_1(0)$$

$$\xi_2(t) = e^{\lambda_2 t} \xi_2(0)$$

$$\rightarrow \frac{\xi_1(t)}{\xi_0(t)} = e^{\lambda_1 t}$$

$$\ln \frac{\xi_1(t)}{\xi_0(t)} = \lambda_1 t$$

$$\Rightarrow t = \frac{1}{\lambda_1} \ln \frac{\xi_1}{\xi_{01}}$$

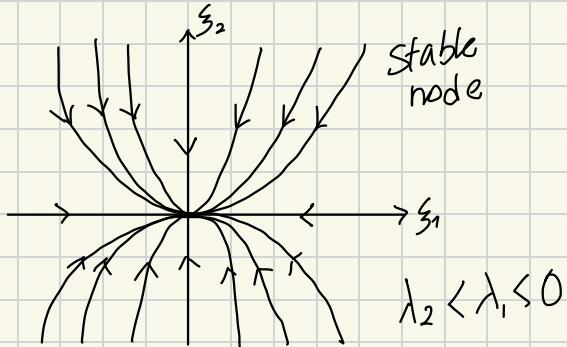
$$\xi_2 = e^{\lambda_2 \frac{t}{\lambda_1} \ln \frac{\xi_1}{\xi_{01}}} \cdot \xi_{02} \leftarrow$$

$$d \ln b = \ln b^{\alpha}$$

$$\xi_2 = e^{\ln \left( \frac{\xi_1}{\xi_{01}} \right) \frac{\lambda_2}{\lambda_1}} \xi_{02}$$

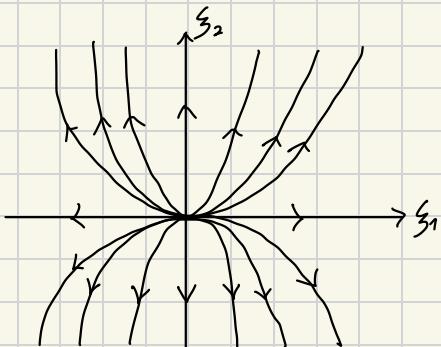
$$= \left( \frac{\xi_1}{\xi_{01}} \right)^{\frac{\lambda_2}{\lambda_1}} \xi_{02}$$

↓  
parabola



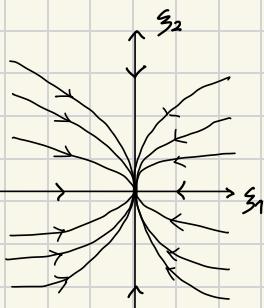
stable  
node

$$\lambda_2 < \lambda_1 < 0$$



unstable  
node

$$\lambda_2 > \lambda_1 > 0$$



stable node     $\lambda_1 < \lambda_2 < 0$

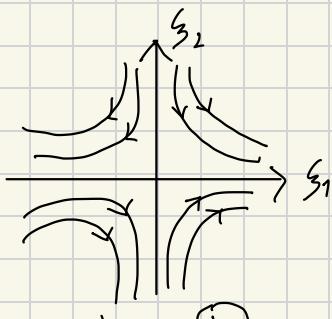
### 8.3.5 Saddle point

$$\lambda_1 \neq \lambda_2 \in \mathbb{R}$$

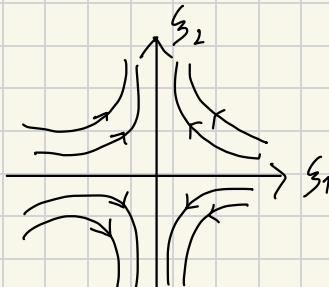
$$\lambda_1 \cdot \lambda_2 < 0$$

$$\xi_2 = \left( \frac{\xi_1}{\xi_{01}} \right) \frac{\lambda_2}{\lambda_1} \xi_{02}$$

→ hyperbola



$$\lambda_2 < 0 < (\lambda_1)$$



$$\lambda_1 < 0 < (\lambda_2)$$

saddle points are unstable

Stability :  $\operatorname{Re} \sum \lambda_i \xi < 0$

$$\operatorname{Re} \sum \lambda_i \xi < 0$$

$$\begin{matrix} \downarrow \\ \text{Real} \end{matrix}$$

# 9 Complex Phasor Analysis

## Linear Circuits

f

## Sinusoidal Excitations

### 9.1 Sinusoidal input and steady state

$$v(t) = A_m \cos(\omega t + \alpha)$$

↑      ↑      ↑  
amplitude      angular frequency      phase angle  
 $\omega = 2\pi f$

$u(t) \xrightarrow{R} i(t)$

$$i(t) = I_m \cos(\omega t + \beta)$$
$$u(t) = R \underbrace{I_m}_{U_m} \cos(\omega t + \beta)$$

$$\dot{v}(t) = \frac{d}{dt} A_m \cos(\omega t + \alpha)$$

$$= A_m (-\sin(\omega t + \alpha) \cdot \omega)$$

$$= -\omega A_m \sin(\omega t + \alpha)$$

$$= -\omega A_m \cos(\omega t + \alpha - \frac{\pi}{2})$$

$$= \omega A_m \cos(\omega t + \alpha + \frac{\pi}{2})$$

Series Connection :

$$U_{\text{tot}}(t) = U_1(t) + U_2(t)$$

$$U_1(t) = U_{1m} \cos(\omega t)$$

$$U_2(t) = U_{2m} \cos(\omega t + \delta)$$

$$\begin{aligned} U_{\text{tot}}(t) &= U_{1m} \cos(\omega t) + U_{2m} \cos(\omega t + \delta) \\ &= U_{\text{totm}} \cos(\omega t + \varphi) \end{aligned}$$

$$\cos(\alpha + \beta) = \cos \alpha \cos \beta - \sin \alpha \sin \beta$$

$$\begin{aligned} U_{1m} \cos(\omega t) + U_{2m} \cos(\omega t) \cos(\delta) - U_{2m} \sin(\omega t) \sin(\delta) \\ = U_{\text{totm}} \cos(\omega t) \cos \varphi - U_{\text{totm}} \sin(\omega t) \sin \varphi \end{aligned}$$

$$\underline{U_{1m} \cos(\omega t) + U_{2m} \cos(\omega t) \cos \delta} = \underline{U_{\text{totm}} \cos(\omega t) \cos \varphi}$$

$$\underline{U_{1m} + U_{2m} \cos \delta} = \underline{U_{\text{totm}} \cos \varphi}$$

$$\cancel{\pm U_{2m} \sin(\omega t) \sin \delta} = \cancel{\mp U_{\text{totm}} \sin(\omega t) \sin \varphi}$$

$$\underline{U_{2m} \sin \delta} = \underline{U_{\text{totm}} \sin \varphi}$$

$$\frac{U_{\text{totm}} \sin \varphi}{U_{\text{totm}} \cos \varphi} = \tan \varphi = \frac{U_{2m} \sin \delta}{U_{1m} + U_{2m} \cos \delta}$$

$$\sin^2 \varphi + \cos^2 \varphi = 1$$

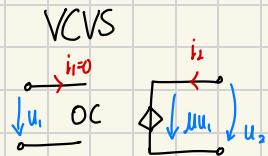
$$\underline{U_{\text{totm}}^2 (\cos^2 \varphi + \sin^2 \varphi)} = \underline{U_{\text{totm}}^2}$$

$$= (U_{1m} + U_{2m} \cos \delta)^2 + (U_{2m} \sin \delta)^2$$

$$= U_{1m}^2 + U_{2m}^2 + 2U_{1m}U_{2m} \cos \delta$$

for one frequency

if  $\omega$  angular frequency must find one  
by one and add together



$$i_1 = 0, \quad u_2 = mu_1$$

$$\tilde{H} = \begin{bmatrix} 0 & 0 \\ m & 0 \end{bmatrix}$$

## 9.2 Complex Phasors

$$a(t) = A_m \cos(\omega t + \alpha)$$

define phasor:

$$A = A_m e^{j\alpha}$$

then,

$$a(t) = \operatorname{Re} \{ A e^{j\omega t} \}$$

$$\operatorname{Re} \{ A e^{j\omega t} \} = \operatorname{Re} \{ A_m e^{j\alpha} \cdot e^{j\omega t} \}$$

$$= \operatorname{Re} \{ A_m e^{j(\omega t + \alpha)} \}$$

$$= A_m \cos(\omega t + \alpha)$$

Euler's rule:  $e^{j\varphi} = \cos \varphi + j \sin \varphi$

3 Lemmas

Lemma 1 : Uniqueness

$$\forall t : a(t) = b(t) \Leftrightarrow A = B$$

Lemma 2: Linearity

$$y(t) = \sum_{k=1}^L a_k \cdot x_k(t) \Leftrightarrow Y = \sum_{k=1}^L a_k X_k$$

Lemma 3: Differentiation

$$b(t) = \dot{a}(t) = \frac{da(t)}{dt} \Leftrightarrow b(t) = \overset{\circ}{a}(t) = \frac{d}{dt} \operatorname{Re} \{ A e^{j\omega t} \}$$
$$= \operatorname{Re} \{ A \cdot \frac{d}{dt} e^{j\omega t} \}$$
$$= \operatorname{Re} \{ j\omega A \cdot e^{j\omega t} \}$$

$$B = \boxed{j\omega A}$$

$$\overset{\circ}{a}_3 \ddot{X}(t) + \overset{\circ}{a}_2 \ddot{X}(t) + \overset{\circ}{a}_1 \dot{X}(t) + \overset{\circ}{a}_0 X(t) = w(t) \Leftrightarrow a_3(j\omega)^3 X + a_2(j\omega)^2 X + a_1(j\omega) X + a_0 X = W$$

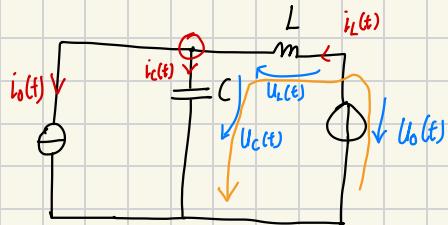
$$\begin{array}{c} \text{R} \\ | \\ \text{---} \\ | \\ \text{U}_R(t) \end{array} \quad i_R(t)$$
$$U_R(t) = R i_R(t) \stackrel{L_1, L_2}{\Leftrightarrow} U_R = R I_R$$
$$U_R(t) = \operatorname{Re} \{ U_R e^{j\omega t} \}$$
$$i_R(t) = \operatorname{Re} \{ I_R e^{j\omega t} \}$$

$$\begin{array}{c} G \\ | \\ \text{---} \\ | \\ \text{U}_G(t) \end{array} \quad i_G(t)$$
$$i_G(t) = G U_G(t) \stackrel{L_1, L_2}{\Leftrightarrow} I_G = G U_G$$

$$\begin{array}{c} C \\ | \\ \text{---} \\ | \\ \text{U}_C(t) \end{array} \quad i_C(t)$$
$$i_C = C \cdot \dot{U}_C(t) \stackrel{L_1, L_2, L_3}{\Leftrightarrow} I_C = j\omega C U_C$$

$$\begin{array}{c} L \\ | \\ \text{---} \\ | \\ \text{U}_L(t) \end{array} \quad i_L(t)$$
$$U_L(t) = L \cdot \ddot{i}_L(t) \stackrel{L_1, L_2, L_3}{\Leftrightarrow} U_L = j\omega L I_L$$

## 9.2.1 Reactive Simple Circuit



$$KCL: i_o(t) + i_C(t) - i_L(t) = 0$$

$$KVL: -U_o(t) + U_L(t) + U_C(t) = 0$$

$$i_C(t) = i_L(t) - i_o(t)$$

$$U_L(t) = U_o(t) - U_C(t)$$

$$C_i(t) = i_L(t) - i_o(t)$$

$$L_i(t) = U_o(t) - U_C(t)$$

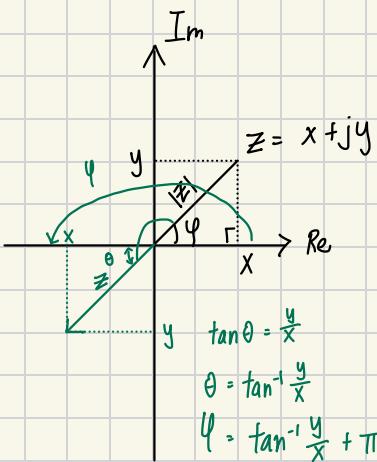
$$\begin{aligned} & \stackrel{L_1, L_2, L_3}{\Leftrightarrow} j\omega C U_C = I_L - I_o \\ & j\omega L I_L = U_o - U_C \\ & j\omega C U_o - j\omega C U_C = j\omega^2 L C I_L \\ & j\omega C U_o = I_L - I_o + (j\omega)^2 L C I_L \\ & j\omega C U_o + I_o = (1 + (j\omega)^2 L C) I_L \end{aligned}$$

$$I_L = \frac{I_o + j\omega C U_o}{1 + (j\omega)^2 L C}$$

$$j\omega L \cdot \frac{I_o + j\omega C U_o}{1 + (j\omega)^2 L C} = U_o - U_C$$

$$U_C = U_o - \frac{j\omega L I_o + (j\omega)^2 C U_o}{1 + (j\omega)^2 L C}$$

$$= \frac{U_o - j\omega L I_o}{1 + (j\omega)^2 L C}$$



Pythagoras :

$$|z|^2 = x^2 + y^2 \\ = (x + jy)(x - jy)$$

$$= z \cdot z^*$$

$$\tan \psi = \frac{y}{x} \\ = \frac{\operatorname{Im}\{z\}}{\operatorname{Re}\{z\}}$$

$$U_{C,m} = |U_C| = \sqrt{|U_C \cdot U_C^*|}$$

$$= \frac{|U_0 - j\omega L I_0|}{|1 - \omega^2 LC|}$$

$$I_{L,m} = \frac{|I_0 - j\omega C U_0|}{|1 - \omega^2 LC|}$$

$$\beta_u = \tan^{-1} \left( \frac{\operatorname{Im}\{U_C\}}{\operatorname{Re}\{U_C\}} \right)$$

$$U_0, I_0 \in \mathbb{R}$$

$$\beta_u = \tan^{-1} \left( \frac{-j\omega L I_0}{U_0} \right)$$

$$\beta_i = \tan^{-1} \left( \frac{\omega C U_0}{I_0} \right)$$

$$U_C = U_{C,m} e^{j\beta_u}$$

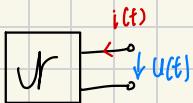
$$I_L = I_{L,m} e^{j\beta_i}$$

$$U_C(t) = \operatorname{Re} \{ U_C e^{j\omega t} \}$$

$$= U_{C,m} \cos(\omega t + \beta_u)$$

$$i_L(t) = I_{L,m} \cos(\omega t + \beta_i)$$

## 9.4 Network Functions



### 9.4.1 Two terminal function

$$U(t) = \operatorname{Re} \{ U e^{j\omega t} \}$$

$$i(t) = \operatorname{Re} \{ I e^{j\omega t} \}$$

impedance :

$$Z(j\omega) = \frac{U(j\omega)}{I(j\omega)}$$

admittance :

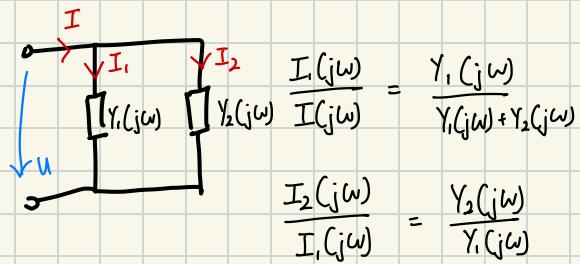
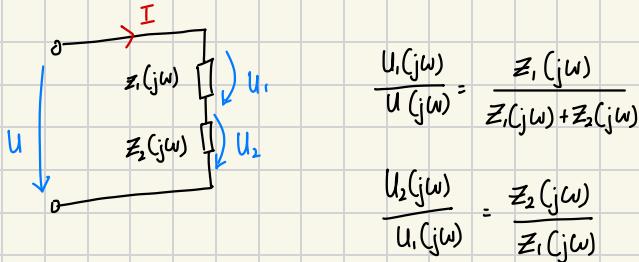
$$Y(j\omega) = \frac{I}{U(j\omega)} = \frac{I(j\omega)}{U(j\omega)}$$

$$Z_R = R, \quad Y_R = \frac{1}{R}$$

$$Z_G = \frac{1}{G}, \quad Y_G = G$$

$$Z_C = \frac{1}{j\omega C}, \quad Y_C = j\omega C$$

$$Z_L = j\omega L, \quad Y_L = \frac{1}{j\omega L}$$



## 9.4.2 Transfer functions

Relate quantities at different ports

$$\text{e.g.: } H(jw) = \frac{U_{\text{out}}(jw)}{U_{\text{in}}(jw)}$$

$$U_{\text{out}} = H(jw) \cdot U_{\text{in}}(jw)$$

$$U_{\text{out}}(t) = \operatorname{Re} \left\{ H(jw) U_{\text{in}}(jw) e^{j\omega t} \right\}$$

## 9.5 Energy & Power

$$P(t) = U(t) \cdot i(t)$$

$$E = \int_0^T P(t) dt$$

$$T = \frac{2\pi}{\omega}$$

average power

$$P_{\text{av}} = \frac{E}{T} = \frac{1}{T} \int_0^T P(t) dt$$

Complex power

$$P = \frac{1}{2} \cdot U \cdot I^* \rightarrow \text{complex Conjugate}$$

$$= P_{\text{av}} + j P_B$$

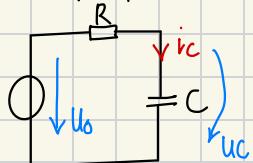
$$P_w = \operatorname{Re} \{ P \}$$

$$P_B = I_m \sum P \rightarrow \text{blind power}$$

apparent power:

$$S = |P|$$

Wrap up first order Circuits



$$\text{KVL: } -U_o + R i_{rc} + U_c = 0$$

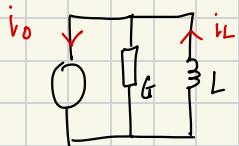
$$R i_{rc} = -U_c + U_o$$

$$i_{rc} = C \dot{U}_c$$

$$RC \dot{U}_c = -U_c + U_o$$

$$\dot{U}_c = -\frac{1}{RC} U_c + \frac{1}{RC} U_o$$

$$U_c(t) = U_c(t_0) e^{-\frac{t-t_0}{RC}} + \int_{t_0}^t \frac{1}{RC} e^{-\frac{t-t'}{RC}} (U_o(t') dt'$$



$$\dot{i}_L = -\frac{1}{GL} i_L + \frac{1}{GL} i_o$$

$$i_L(t) = i_L(t_0) e^{-\frac{t-t_0}{GL}} + \int_{t_0}^t \frac{1}{GL} e^{-\frac{t-t'}{GL}} i_o(t') dt'$$

$$\text{for } U_o(t) = U_\infty \quad \text{or} \quad i_o(t) = i_\infty$$

$$U_c(t) = U_\infty + (U_c(t_0) - U_\infty) e^{-\frac{t-t_0}{RC}}$$

$$i_L(t) = i_\infty + (i_L(t_0) - i_\infty) e^{-\frac{t-t_0}{GL}}$$

if  $RC$  or  $GL$  is  $\oplus$ , circuit is stable

## Second order Circuits

$$\underline{X} = \begin{bmatrix} U_{C1} \\ U_{C2} \end{bmatrix}, \begin{bmatrix} i_{L1} \\ i_{L2} \end{bmatrix}, \begin{bmatrix} U_C \\ i_L \end{bmatrix}$$

$$\dot{\underline{X}} = \underline{A} \underline{X} + \underline{b} \underline{v}$$

↓  
input vector

find this

$$i_C = C U_C \quad \text{depending on which you need, find these}$$
$$U_L = L i_L$$

$$\text{eigenvalues: } \det(\underline{A} - \lambda \underline{I}) = 0$$

I)  $\lambda_1 \neq \lambda_2 \in \mathbb{R}$

II)  $\lambda_1 = \lambda_2 \in \mathbb{R} \rightarrow \text{Jordan Normal form (won't be exam)}$

III)  $\lambda_1 = \lambda_2^* \in \mathbb{C}$

$$\dot{\xi}_1 = \lambda_1 \xi_1$$

$$\dot{\xi}_2 = \lambda_2 \xi_2$$