

C1. Wave friction factor

$$f_{wi} = 0.00251 \exp \left[5.21 \left(\frac{(2T_{tu})^{c_1}}{T_i} \hat{a} \right)^{-0.19} \right] \text{ for } \frac{\hat{a}}{k_{sw}} > 1.587 \quad (21)$$

$$f_{wi} = 0.3 \text{ for } \frac{\hat{a}}{k_{sw}} \leq 1.587$$

$$f_w = 0.00251 \exp \left[5.21 \left(\frac{\hat{a}}{k_{sw}} \right)^{-0.19} \right] \text{ for } \frac{\hat{a}}{k_{sw}} > 1.587 \quad (A.4)$$

$$f_w = 0.3 \text{ for } \frac{\hat{a}}{k_{sw}} \leq 1.587.$$

C2. Current function factor

$$\langle |\theta| \rangle = \frac{\frac{1}{2} f_{\delta} u_{\delta}^2}{(s-1)gd_{50}} + \frac{\frac{1}{2} f_w \hat{u}^2}{(s-1)gd_{50}} \quad (A.3)$$

$$f_{\delta} = 2 \left[\frac{0.4}{\ln(30\delta/k_{s\delta})} \right]^2 \quad (20)$$

$$\alpha = \frac{|u_{\delta}|}{|u_{\delta}| + \hat{u}} \quad (19)$$

$$f_{w\delta i} = \alpha f_{\delta} + (1-\alpha)f_{wi} \quad (18)$$

$$\tau_{wRe} = \rho \frac{f_{w\delta}}{2c_w} \alpha_w \hat{u}^3 \quad (22)$$

$$\theta_{ix} = |\theta_i| \frac{u_{i,rx}}{|u_{i,r}|} + \frac{\tau_{wRe}}{(s-1)gd_{50}} \quad (15)$$

$$|\theta_i| = \frac{\frac{1}{2} f_{w\delta i} |u_{i,r}|^2}{(s-1)gd_{50}} \quad (17)$$

D. Ripple model

$$\mu = \begin{cases} 6 & \text{if } d_{50} \leq 0.15 \text{ mm} \\ 6 - \frac{5(d_{50}-0.15)}{(0.20-0.15)} & \text{if } 0.15 \text{ mm} < d_{50} < 0.20 \text{ mm} \\ 1 & \text{if } d_{50} \geq 0.20 \text{ mm} \end{cases} \quad (A.2)$$

$$k_{s\delta} = \max\{3d_{90}, d_{50}[\mu + 6(\langle |\theta| \rangle - 1)]\} + 0.4\eta^2/\lambda \quad (A.1)$$

$$k_{sw} = \max\{d_{50}, d_{50}[\mu + 6(\langle |\theta| \rangle - 1)]\} + 0.4\eta^2/\lambda. \quad (A.5)$$

A. Intra-wave velocity time-series

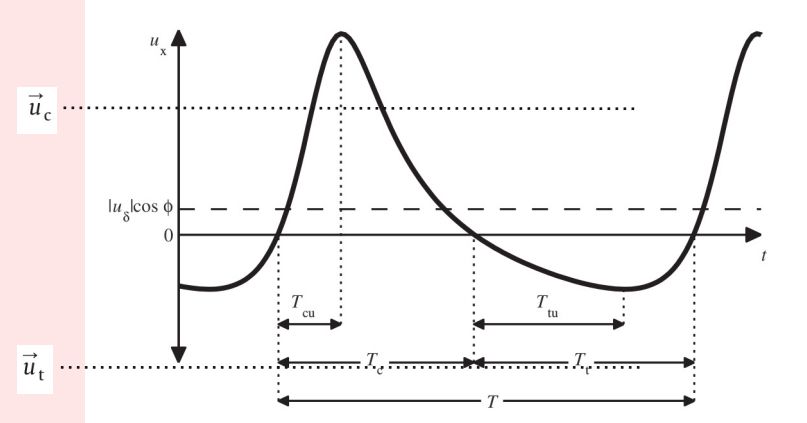


Fig. 1. Definition sketch of near-bed velocity time-series in wave direction. The parameters T_c and T_t are the positive (crest) and negative (trough) flow durations. Similarly, T_{cu} and T_{tu} are the durations of flow acceleration in positive and negative x -directions.

$$\hat{u} = \sqrt{\frac{2}{T} \int_0^T u_w^2(t) dt} \quad (8)$$

$$\hat{a} = \frac{\hat{u}T}{2\pi} \quad (9)$$

$$\tilde{u}_{c,r} = \frac{1}{2}\sqrt{2}\hat{u}_c \quad (10)$$

$$\tilde{u}_{t,r} = \frac{1}{2}\sqrt{2}\hat{u}_t \quad (11)$$

$$u_x(t) = u_w(t) + |u_{\delta}| \cos \varphi \quad (4)$$

$$u_y = |u_{\delta}| \sin \varphi \quad (5)$$

$$\vec{u}_{c,r} = \{u_{c,rx}, u_{c,ry}\} = \{\tilde{u}_{c,r} + |u_{\delta}| \cos \varphi, |u_{\delta}| \sin \varphi\} \quad (12)$$

$$\vec{u}_{t,r} = \{u_{t,rx}, u_{t,ry}\} = \{-\tilde{u}_{t,r} + |u_{\delta}| \cos \varphi, |u_{\delta}| \sin \varphi\}. \quad (13)$$

F. Sheet flow thickness

$$\hat{\theta}_i = \frac{\frac{1}{2} f_{w\delta i} \hat{u}_i^2}{(s-1)gd_{50}} \quad (C.2)$$

$$\frac{\delta_{si}}{d_{50}} = \begin{cases} 25\hat{\theta}_i & \text{if } d_{50} \leq 0.15 \text{ mm} \\ 25 - \frac{12(d_{50}-0.15)}{(0.20-0.15)} & \text{if } 0.15 \text{ mm} < d_{50} < 0.20 \text{ mm} \\ 13\hat{\theta}_i & \text{if } d_{50} \geq 0.20 \text{ mm} \end{cases} \quad (C.1)$$

B. Entrained sand load

$$\Omega_i = \begin{cases} 0 & \text{if } |\theta_i| \leq \theta_{cr} \\ m(|\theta_i| - \theta_{cr})^n & \text{if } |\theta_i| > \theta_{cr} \end{cases} \quad (2)$$

E. Phase lag

$$\Omega_{cc} = \begin{cases} \Omega_c & \text{if } P_c \leq 1 \\ \frac{1}{P_c} \Omega_c & \text{if } P_c > 1 \end{cases} \quad (23)$$

$$\Omega_{ct} = \begin{cases} 0 & \text{if } P_c \leq 1 \\ \left(1 - \frac{1}{P_c}\right) \Omega_c & \text{if } P_c > 1 \end{cases} \quad (24)$$

$$\Omega_{tt} = \begin{cases} \Omega_t & \text{if } P_t \leq 1 \\ \frac{1}{P_t} \Omega_t & \text{if } P_t > 1 \end{cases} \quad (25)$$

$$\Omega_{tc} = \begin{cases} 0 & \text{if } P_t \leq 1 \\ \left(1 - \frac{1}{P_t}\right) \Omega_t & \text{if } P_t > 1 \end{cases} \quad (26)$$

$$w_{sc} = w_s - w_{\min}(r_c) \quad (29)$$

$$w_{st} = \max(w_s - w_{\max}(r_t), 0) \quad (30)$$

$$P_c = \begin{cases} \alpha \left(\frac{1 - \xi \hat{u}_c}{c_w} \right) \frac{\eta}{2(T_c - T_{cu})w_{sc}} & \text{if } \eta > 0 \text{ (ripple regime)} \\ \alpha \left(\frac{1 - \xi \hat{u}_c}{c_w} \right) \frac{\delta_{sc}}{2(T_c - T_{cu})w_{sc}} & \text{if } \eta = 0 \text{ (sheet flow regime)} \end{cases} \quad (27)$$

$$P_t = \begin{cases} \alpha \left(\frac{1 + \xi \hat{u}_t}{c_w} \right) \frac{\eta}{2(T_t - T_{tu})w_{st}} & \text{if } \eta > 0 \text{ (ripple regime)} \\ \alpha \left(\frac{1 + \xi \hat{u}_t}{c_w} \right) \frac{\delta_{st}}{2(T_t - T_{tu})w_{st}} & \text{if } \eta = 0 \text{ (sheet flow regime)} \end{cases} \quad (28)$$

G. Main function

$$\vec{\phi} = \frac{\vec{q}_s}{\sqrt{(s-1)gd_{50}^3}} = \frac{\sqrt{|\theta_c|} T_c \left(\Omega_{cc} + \frac{T_c}{2T_{cu}} \Omega_{tc} \right) \frac{\vec{\theta}_c}{|\theta_c|} + \sqrt{|\theta_t|} T_t \left(\Omega_{tt} + \frac{T_t}{2T_{tu}} \Omega_{ct} \right) \frac{\vec{\theta}_t}{|\theta_t|}}{T} \quad (1)$$