

## Chapitre 9

19 g/K  
28 g/mol

### Exercice 13

$$(1) \chi_T = \frac{1}{V} \left( \frac{\partial V}{\partial P} \right)_T$$

$$\alpha = \frac{1}{V} \left( \frac{\partial V}{\partial T} \right)_P$$

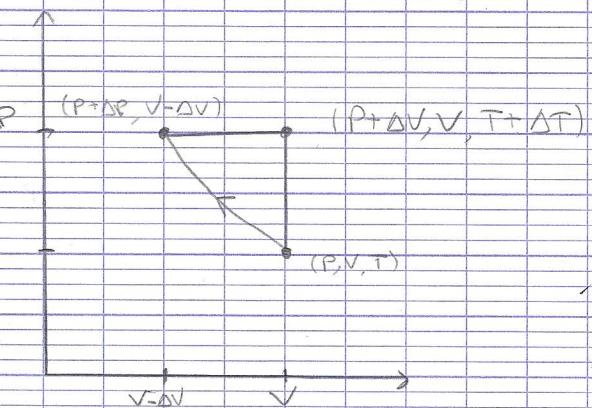
$$\beta = \frac{1}{P} \left( \frac{\partial P}{\partial T} \right)_V$$

$$PV = mRT \Leftrightarrow V = \frac{mRT}{P}$$

$$\chi_T = -\frac{1}{V} \left( -\frac{mRT}{P^2} \right) = \frac{1}{P} \quad P + \Delta P \quad (P + \Delta P, V - \Delta V)$$

$$\alpha = \frac{1}{T} \quad \beta = \frac{1}{T}$$

$$(2) \boxed{\frac{\alpha}{\beta \chi_T} = P}$$



(1) On applique une surpression  $\Delta P$  ( $\rightarrow T = \text{cte}$  donc avec des parois adiabatiques) et on mesure  $\Delta V$  diathermique.

On chauffe le gaz avec le piston libre ( $\Rightarrow P = \text{cte}$ ) (paroi adiabatique) ainsi. Le volume va augmenter

On rend les parois diathermiques, on bloque le piston

### Exercise 16

$$m = 0,01 \text{ kg}$$

$$T_0 = 250 \text{ K}$$

$$P_0 = 0,25 \text{ bar}$$

$$V = 8L \quad , \quad S = 0,05 \text{ m}^2$$

$$(1) P_0 V_0 = m R T_0 \Rightarrow V_0 = \frac{m R T_0}{P_0} = 1L = 10^{-3} \text{ m}^3$$

$$(2) (a) C_V = \frac{5}{2} m R$$

$$(b) C_P - C_V = R_m \quad C_P = \frac{7}{2} m R$$

$$(c) \gamma = C_P/C_V = 7/5 = 1.4$$

$$(d) \frac{C_P}{C_V} - 1 = \frac{m R}{C_V} = \gamma - 1$$

$$C_V = \frac{m R}{\gamma - 1}$$

$$(3) P_g, T_g, V_g = V$$

$$(a) dU = \delta W + \delta Q$$

$$\Delta U = W_{\text{ext}} + Q_{\text{ext}}$$

$$(b) Q = 0$$

$$(c) \delta W = -P_{\text{ext}} dV$$

$P_{\text{ext}}$  = pression contre laquelle il faut faire le système

$$\text{donc } P_{\text{ext}} = 0$$

$$(d) \Delta U = 0$$

$$\Delta U = C_V \Delta T$$

$$\Rightarrow \Delta T = 0 \Rightarrow T_g = T_0$$

$$4) a) \vec{F}_g = k_{\text{xc}} \vec{e}_x$$

$$\vec{F}_g = -P_g S \frac{\vec{e}_x}{x}$$

b) À l'équilibre  $\sum \vec{F} = \vec{0}$

$$k_{\text{xc}} = P_g S$$

$$P_g = \frac{k_{\text{xc}}}{S}$$

5) a)  $W_g = -W_R$   
 $\Delta U = -V_R = -\frac{1}{2} R \alpha^2 g$

b)  $\Delta U = C_v \Delta T = -\frac{1}{2} R \alpha^2 g$

c)  $\frac{mR}{\gamma-1} (\gamma - 1) = -\frac{1}{2} R \alpha^2 g$

$$T_g = T_0 - \frac{(\gamma-1)}{2mR} \frac{R \alpha^2 g}{k}$$

6)  $\gamma = 1.4409$   
 $\gamma^{\text{exp}}$  proche de  $\gamma^{\text{th}}$  ( $\approx 3\%$ )

$$P_g V_g = mRT_g$$

$$V_g = S \alpha_g + V_0$$

$$\frac{P_g}{mR} T_g = \frac{P_g V_g}{mR} = \frac{R \alpha_g (V_0 + S \alpha_g)}{mR}$$

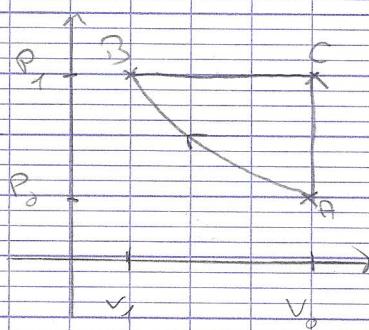
### Exercice 47

$$(1) m = m_1 + m_2 = \frac{P_1 V_1}{R T_1} + \frac{P_2 V_2}{R T_2} = 0,18 \text{ mol}$$

$$(2) P_0 = m R T_0 / V_0 = 64450 \text{ Pa} = 0,6445 \text{ bar}$$

$$(3) P_1 = 2 \text{ bar} \quad V_1 = \frac{m R T_0}{P_1} = 1,61 \text{ L}$$

$$T_1 = T_0$$



$$(4) V_1 = 1,61 \text{ L}$$

$$W_1 (0 \rightarrow 1)$$

$$T_2 = 1002 \text{ K}$$

$$\delta V = -P_{\text{ext}} dV$$

$$= -P_{\text{int}} dV$$

$$= -\frac{m R T_0}{V} dV$$

$$W_1 = \int \delta W = m R T_0 P_m \left[ \frac{V_0}{V_1} \right]$$

$$= 365,2 \text{ J}$$

$$W_2 (1 \rightarrow 2)$$

$$\delta W = -P_{\text{ext}} dV = -P_1 dV$$

$$W_2 = \int \delta W = \int_{V_1}^{V_0} -P_1 dV$$

$$= -P_1 \Delta V = -678 \text{ J}$$

$$W_3 (2 \rightarrow 0) = 0$$

$$\delta W = -P_{\text{ext}} dV = 0$$

$$(5) \Delta U = W + Q$$

$$Q_1 = -365,2 \text{ J}$$

$$\Delta U = \frac{1}{2} m R \Delta T$$

$$Q_2 = 1691,3 + 678 = 2369,3 \text{ J}$$

$$Q_3 = -1691,3 \text{ J}$$

$$(7) W = \sum_i W_i = -315,8 \text{ J}$$

$$Q = \sum_i Q_i = 315,8 \text{ J}$$

$$\Delta U = 0 \quad (\text{cycle})$$

$$(8) \gamma = C_p / C_v = 7/5$$

(9)  $0 \rightarrow 1$  adiabatique  
 $V_1' \text{ et } T_1' \quad , \quad P_1' \approx P_1$

$P_{\text{ext}}$  fixé de l'appareil

$$PV^\gamma = C$$

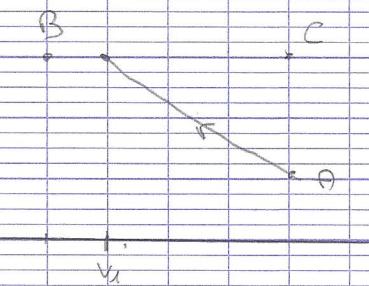
$$\frac{P_0 V_0}{V_1'} = \frac{P_1 (V_1')^\gamma}{P_1} \quad \Rightarrow \\ (V_1')^\gamma = \frac{P_0}{P_1} V_0^\gamma$$

$$V_1' = \left( \frac{P_0}{P_1} \right)^{\frac{1}{\gamma}} V_0 = 8,83 \text{ L}$$

$$T_1' = \frac{P_1 V_1'}{m R} = 496,4 \text{ K}$$

$$cte = P_0 V_0^\gamma = P_1 (V_1')^\gamma$$

(10)



(11)  $W_1'$

$$\delta W = -P_{\text{ext}} dV$$

$$= -P_1 f dV$$

$$= \frac{m R T}{V} dV \quad \triangle$$

$$= - \frac{cte}{\sqrt{\gamma}} dV$$

$$= -cte \left[ \frac{V}{\gamma-1} \right]_{V_0}^{V_1'} \quad \text{car } \gamma = \frac{C_p}{C_v}$$

$$= \frac{1}{\gamma-1} [P_1 V_1' - P_0 V_0]$$

$$W = 309,3 \text{ J}$$

(12)  $W_1'$  directement

$$\Delta U_1 = W_1' + Q_1' = W_1' \text{ car}$$

adiabatique

$$= \frac{1}{2} m R (T_1' - T_0)$$

$$= 307,8 \text{ J}$$

$$(13) W_1' = 307,8 \text{ J}$$

$$W_2' = \frac{W_1'}{2} - ?_1 \Delta V = -554 \Rightarrow \quad W_2' = 0 \quad W_3' = 266,8 \text{ J}$$

### Exercice 10

$$1) \quad T, V_m = \frac{V}{3}$$

$$\delta P = \frac{R}{V_m - b} dT - \left( \frac{RT}{(V_m - b)^2} + \frac{2a}{V_m^3} \right) dV_m$$

On va montrer que  $\delta P = dP$

$$\frac{\partial}{\partial V_m} \left( \frac{R}{V_m - b} \right) = \frac{\partial}{\partial T} \left( \frac{RT}{(V_m - b)^2} + \frac{2a}{V_m^3} \right)$$

$$\Leftrightarrow - \frac{R}{(V_m - b)^2} = - \frac{R}{(V_m - b)^2}$$

$$\text{donc } \delta P = dP = \left( \frac{\partial P}{\partial T} \right)_{V_m} dT + \left( \frac{\partial P}{\partial V_m} \right) dV_m$$

$$2) \quad \begin{cases} \frac{\partial P}{\partial T} = \frac{R}{V_m - b} \\ \frac{\partial P}{\partial V_m} = - \frac{RT}{(V_m - b)^2} + \frac{2a}{V_m^3} \end{cases} \quad \begin{matrix} (1) \\ (2) \end{matrix}$$

$$(1) \Leftrightarrow P(T, V_m) = \frac{RT}{V_m - b} + g(V_m)$$

$$\frac{\partial P}{\partial V_m} = - \frac{RT}{(V_m - b)^2} + \frac{dg}{dV_m}$$

$$= - \frac{RT}{(V_m - b)^2} + \frac{2a}{V_m^3}$$

$$\text{donc } \frac{dg}{dV_m} = \frac{2a}{V_m^3} \Rightarrow g(V_m) = - \frac{a}{V_m^2} + \text{cte}$$

$$\Rightarrow P(T, V_m) = \frac{RT}{V_m - b} - \frac{a}{V_m^2} + \text{cte}$$

$$\text{Si } V_m \rightarrow \infty \quad (\text{i.e. } T = \text{cte}) \quad , \quad P \rightarrow 0 \quad \Rightarrow \text{cte} = 0$$

$$P = \frac{RT}{V_m - b} - \frac{a}{V_m^2}$$

3)  $V_m = \frac{V}{n}$

$$P = \frac{mRT}{V-mb} - \frac{m^2a}{V^2}$$

$$\Leftrightarrow \left( P + \frac{m^2a}{V^2} \right) (V-mb) = mRT$$

Van der Waals

4)  $\beta, \chi_T, \alpha$

$$\beta \frac{\alpha}{\chi_T} = P$$

$$\beta = \frac{1}{P} \left( \frac{\partial P}{\partial T} \right)_V$$

$$\chi_T = - \frac{1}{V} \left( \frac{\partial V}{\partial P} \right)_T$$

$$\alpha = \frac{1}{V} \left( \frac{\partial V}{\partial T} \right)_P$$

$$\cdot \beta = \frac{1}{P} \left( \frac{\partial P}{\partial T} \right)$$

$$\frac{\partial P}{\partial T} = \frac{mR}{V-mb}, P = \frac{mRTV^2 - m^2a(V-mb)}{V^2(V-mb)}$$

$$\Rightarrow \beta = \frac{V^2(V-mb)}{mRTV^2 - m^2a(V-mb)} \times \frac{mR}{V-mb}$$

$$= \frac{RV^2}{RTV^2 - ma(V-mb)}$$

$$\rightarrow \frac{1}{1}$$

$$\cdot \chi_T = - \frac{1}{V} \left( \frac{\partial V}{\partial P} \right)_T = - \frac{1}{V} \left( - \frac{mRT}{(V-mb)^2} + \frac{2m^2a}{V^3} \right)$$

$$= - \frac{1}{V} \left( \frac{2m^2a(V-mb)^2 - mRTV^3}{V^3(V-mb)^2} \right)$$

$$= \frac{V^2(V-mb)^2}{2m^2a(V-mb)^2 - mRTV^3}$$

$$\text{Bi: } a = b \Rightarrow 0$$

$$\frac{P}{T} \rightarrow \frac{V'}{mRTV^3} = \frac{V}{mRT} = \frac{1}{P}$$

$$\frac{\alpha}{\beta \chi_T} = P \Leftrightarrow \alpha = P \beta \chi_T = \frac{dP}{dT} \chi_T$$

$$= \frac{mR}{V-mb} \frac{V^2(V-mb)^2}{mRTV^3 - 2m^2a(V-mb)^2}$$

$$= \frac{RV^2(V-mb)}{RTV^3 - 2ma(V-mb)^2}$$

$$\text{Bi: } a = b \Rightarrow 0$$

$$\alpha = \frac{1}{T}$$

5)  $\cancel{\alpha} U(T, V)$

$$dU = \left(\frac{\partial U}{\partial T}\right)_V dT + \left(\frac{\partial U}{\partial V}\right)_T dV$$

$$\text{Bi: } T = c^2$$

$$\cancel{dU = \left(\frac{\partial U}{\partial V}\right)_T dV}$$

$$\text{Ca: } dU = -pdV + TdS + \cancel{\nu dN}$$

$$\Leftrightarrow \left(\frac{\partial U}{\partial V}\right)_T dV = -pdV + TdS$$

$$\Leftrightarrow \left(\frac{\partial U}{\partial V}\right)_T = -p + T \frac{dS}{dV}$$

$$= -p + T \left(\frac{\partial S}{\partial V}\right)_T = p - p$$

$$dU = \left(\frac{\partial U}{\partial T}\right)_V dT + \cancel{\left(\frac{\partial U}{\partial V}\right)_T dV}$$

$$\text{Bi: } T$$

$$6) \quad F = U - TS \quad (\text{énergie libre})$$

$$dF = d(U - TS)$$

$$= dU - d(TS)$$

$$= dU - TdS - SdT$$

$$= -pdV + TdS - TdS - SdT$$

$$= -pdV - SdT$$

$$\text{Théorème de Schwarz : } \frac{\partial(-P)}{\partial T} = \frac{\partial(-S)}{\partial V} = \left(\frac{\partial P}{\partial T}\right)_V = \left(\frac{\partial S}{\partial V}\right)_T$$

$$\Rightarrow P = T \left( \frac{\partial S}{\partial V} \right)_T = T \left( \frac{\partial P}{\partial T} \right)_V = T \frac{mR}{V-mb} = P + \frac{m^2 a}{V^2}$$

$$\underline{\exists} \quad dU = \left( \frac{\partial U}{\partial T} \right)_V dT + \left( \frac{\partial U}{\partial V} \right)_T dV \Rightarrow \underline{\ell} = P + \frac{m^2 a}{V^2}$$

$$\left[ \left( \frac{\partial U}{\partial T} \right)_V = C_V \right] \text{ par déf} \Rightarrow \underline{\ell} = P + \frac{a}{V^2}$$

$$\left( \frac{\partial U}{\partial V} \right)_T = \underline{\ell} - P \Rightarrow dU = C_V dT + (\underline{\ell} - P) dV$$

$$C_V = C_V(T)$$

$$dU = C_V dT + (\underline{\ell} - P) dV$$

$$\text{Théo de Schwarz : } \left( \frac{\partial C_V}{\partial V} \right)_T = \left( \frac{\partial(\underline{\ell} - P)}{\partial T} \right)_V$$

$$\Rightarrow \frac{\partial}{\partial T} \left( \frac{m^2 a}{V^2} \right) = 0 \Rightarrow \frac{\partial C_V}{\partial V} = 0 \Rightarrow C_V(T)$$

$$\underline{\exists} \quad dU = C_V(T) dT + (\underline{\ell} - P) dV$$

$$= C_V(T) dT + \frac{m^2 a}{V^2} dV$$

$$\begin{cases} \frac{\partial U}{\partial T} = C_V \\ \frac{\partial U}{\partial V} = \frac{m^2 a}{V^2} \end{cases} \Rightarrow U = C_V T + g(V)$$

$$\frac{\partial U}{\partial V} = \frac{dg}{dV} = \frac{m^2 a}{V^2}$$

$$\Leftrightarrow g(V) = -\frac{m^2 a}{V} + cte$$

$$U = C_V T - \frac{m^2 c}{V} \text{ rcte}$$

Quand  $T \rightarrow 0$  et  $V \rightarrow \infty$

$$\bar{C}_V \rightarrow 0 \Rightarrow U \rightarrow 0$$

$$\bar{c}_p \rightarrow 0$$

$$\Rightarrow U \rightarrow 0$$

$$\Rightarrow C_V^{\text{rcte}} = 0$$

$$U(T, V) = C_V T - \frac{m^2 c}{V}$$

### Exercice 19

#### Partie 1

$$1) dW = -P_{\text{ext}} dV$$

$$\delta W = \delta W_1 + \delta W_2$$

$$= -P_{\text{ext}} dV = -P_1 dV$$

$$W_1 = \int_{V_1}^{V_2} -P_1 dV = -P_1 \Delta V = -P_1 (V_2 - V_1)$$

$$= P_1 V_1$$

$$W_2 = -P_2 \Delta V = -P_2 V_2$$

$$W = P_1 V_1 - P_2 V_2$$

$$2) \Delta H = 0$$

$$H = U + PV$$

$$H_1 = U_1 + P_1 V_1$$

$$H_2 = U_2 + P_2 V_2$$

$$\Delta H = H_2 - H_1 = U_2 - U_1 + P_2 V_2 - P_1 V_1$$

$$= \Delta U + P_2 V_2 - P_1 V_1$$

$$= W + P_2 V_2 - P_1 V_1 = 0$$

$$Q = 0$$

$$H = C_p T \Leftrightarrow \Delta H = C_p \Delta T$$

$$\Delta H = 0 \Rightarrow \Delta T = 0 \Rightarrow T = \text{cte}$$

$$\Delta U = C_v \Delta T = 0$$

$$= W + Q = W = 0$$

$$\Leftrightarrow P_1 V_1 = P_2 V_2$$

3)  $dH = 0$

$$H = U + PV$$

$$\begin{aligned} dH &= dU + PdV + VdP \\ &= -pdV + TdS + \nu dW + PdV + VdP \\ &= TdS + VdP = 0 \end{aligned}$$

$$\Leftrightarrow dS = -\frac{V}{T} dP \quad \text{or} \quad S \text{ est une variable d'état}$$

donc  $dS = -\frac{mR}{P} dP$

$$dS = mR P_m \left( \frac{P_1}{P_2} \right) > 0$$

ou

$$dU = -pdV + TdS$$

$$dS = \frac{P}{T} dV$$

$$= \frac{mR}{V} dV$$

$$dS = mR P_m \left( \frac{V_2}{V_1} \right) = mR P_m \left( \frac{P_1}{P_2} \right) > 0$$

## Partie 2

$$\underline{4)} \quad PV \approx mRT + m\rho b - \frac{m^2 a}{V}$$

$$V \approx \frac{mRT}{P}$$

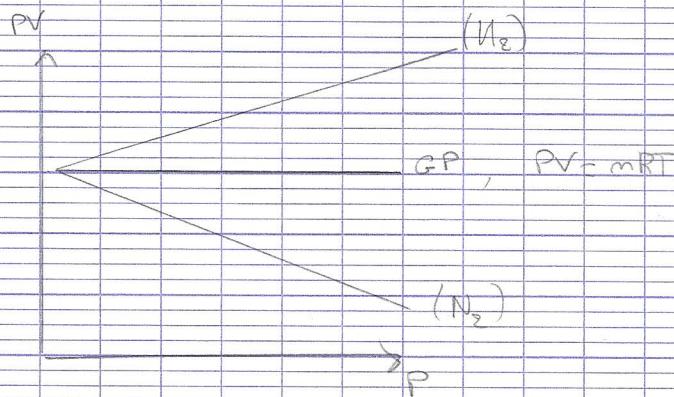
$$PV = mRT + m\rho \left( b - \frac{a}{RT} \right)$$

$$PV = nRT \quad \text{so} \quad T = T_m$$

$$\Leftrightarrow b - \frac{a}{RT} = 0$$

$$T_m = \frac{a}{bR}$$

5)



$$PV = mRT + mPb - m\cancel{P}b \frac{a}{RT}$$

$$= m \left( b - \frac{a}{RT} \right) P + mRT$$

$$T = cte \quad : m \left( b - \frac{a}{RT} \right) = \alpha$$

$$PV = \alpha P + cte$$

$$\text{so } T > T_m \Rightarrow T > \frac{a}{bR} \Leftrightarrow b > \frac{a}{RT} \Leftrightarrow \alpha > 0$$

$$\text{so } T < T_m, \alpha < 0$$

$$6) U(T, V) = C_V T - \frac{m^2 a}{V}$$

$$H = U + PV$$

$$= C_V T - \frac{m^2 a}{V} + mRT + mP \left( b - \frac{a}{RT} \right)$$

$$\underline{7) H = C_v T + mRT - \frac{m^2 a}{V} + mPb - \frac{maP}{RT}}$$

$$= C_v T + mRT + mPb - \frac{m^2 a}{V} - \frac{maP}{RT}$$

$$V \approx \frac{mRT}{P}$$

$$H = C_v T + mRT + mPb - \frac{m^2 a P}{mRT} - \frac{maP}{RT}$$

$$= C_v T + mRT + mPb - \frac{8maP}{RT}$$

$$\underline{8) dH = C_v dT + mRdT}$$

$$= \frac{\partial H}{\partial T} dT + \frac{\partial H}{\partial P} dP$$

$$= \left( C_v + mR + \frac{8maP}{RT^2} \right) dT + \left( mb - \frac{8ma}{RT} \right) dP$$

$$= (C_v + mR) dT + \left( mb - \frac{8ma}{RT} \right) dP$$

$$dH \approx C_p dT + m \left( b - \frac{8a}{RT} \right) dP$$

$$\underline{9) \beta_{ST} = \left( \frac{\partial T}{\partial P} \right)_H}$$

$$H = c_v T, \quad dH = 0$$

$$\Leftrightarrow C_p dT + m \left( b - \frac{8a}{RT} \right) dP = 0$$

$$\Leftrightarrow \frac{dT}{dP} = \frac{-m \left( b - \frac{8a}{RT} \right)}{C_p}$$

$$\underline{1a) M = C_p T + mP \left( b - \frac{8a}{RT} \right)}$$

$$\text{Si } H = C_p T \Leftrightarrow b - \frac{8a}{RT}$$

$$\Leftrightarrow T = T_c = \frac{2a}{bR} = 2T_m$$

ii) Si  $T < T_c$

$$\Leftrightarrow T < \frac{2a}{bR} \Leftrightarrow b < \frac{2a}{RT}$$

$$b - \frac{2a}{RT} < 0 \Leftrightarrow \beta_{ST} > 0$$

$$\Leftrightarrow \cancel{\beta_{ST}} = \frac{\partial T}{\partial P}$$

$$\text{comme } \beta_{ST} = \left( \frac{\partial T}{\partial P} \right)$$

Si  $\beta > 0$  alors les variations de  $T$  et  $P$  sont de même signe. Donc  $T \rightarrow s' \Rightarrow P \rightarrow$   
donc  $P$  se réduit.