

# SLP

## Kinematic Analysis of Harmonic Drives

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May 7, 2025

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# **Introduction**

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# Introduction

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Gears play a crucial role in mechanical engineering as they are fundamental components used for transmitting power and motion between rotating shafts. There is a huge variety of gears; spur, helical, bevel, worm, and planetary gears, each offering unique advantages in terms of efficiency, torque transmission, and design complexity.



Figure: *Planetary gear*



Figure: *Spur gear*



Figure: *Worm Gear*



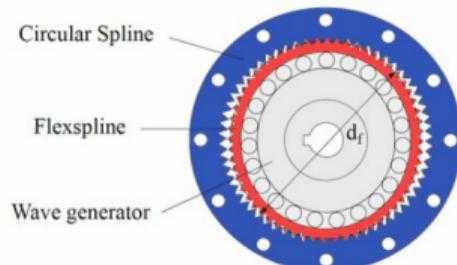
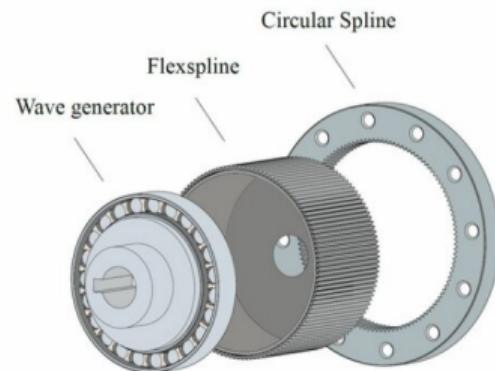
Figure: *Bevel gear*

# Harmonic Drive

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- **Wave Generator (WG):** An elliptical cam that deforms the flexspline as it rotates. It is the input element of the harmonic drive.
- **Flexspline (FS):** A thin, flexible cylindrical cup with external teeth, it deforms under loading and acts as output
- **Circular Spline (CS):** A rigid circular ring with internal teeth. It has two more teeth than the flexspline and remains fixed
- **Working Principle:** As the wave generator rotates, it continuously deforms the flexspline, causing its teeth to engage progressively with those of the CS.

[Harmonic Drive Animation – Wikipedia](#)



# Harmonic Drive

## Five coordinate systems

- $S(O,X,Y)$ : Global coordinate system
- $S_W$ : Attached to the wave generator
- $S_C$ : Attached to the circular spline
- $S_F$ : Attached to the closed end of the cup
- $S_f$ : Attached to the referred tooth on the FS,  $O_f$  is the origin

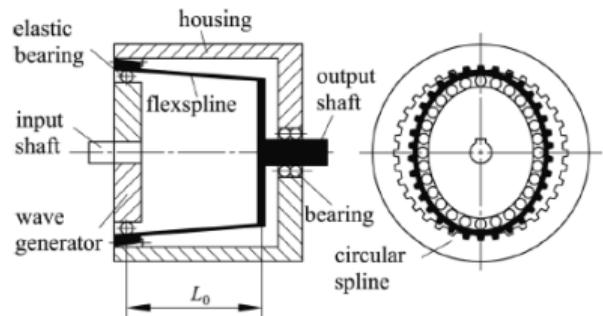


Figure: Structural diagram of a HD

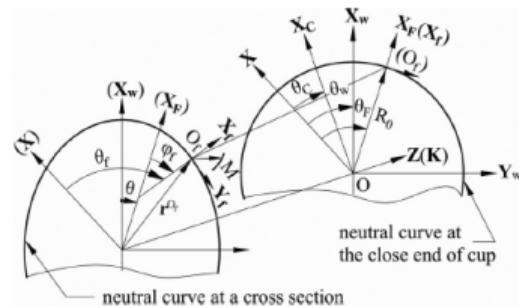


Figure: Coordinate systems of HDs

# Harmonic Drive

- $\theta_W$ : Angular displacement of the wave generator
- $\theta_f$ : Angular displacement of the flex spline tooth
- $\theta_F$ : Angular displacement of the flex spline's output end
- $\theta_C$ : Angular displacement of the circular spline
- $O_f$ : Point on the neutral layer of the referred cross section of the FS (open end)

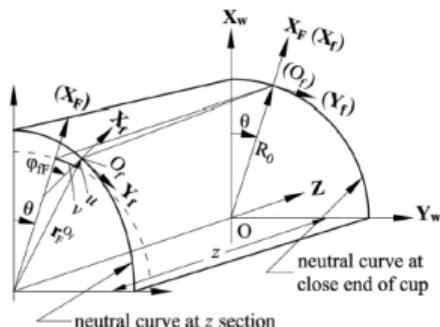


Figure: *Relative motion of  $S_f$  to  $S_F$  system*

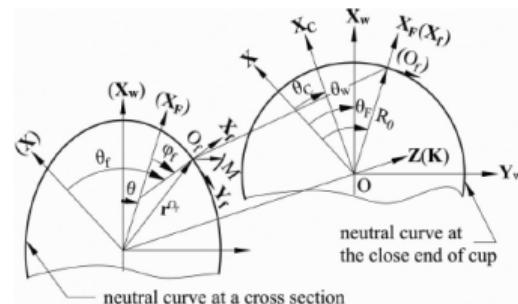


Figure: *Coordinate systems of HDs*

# Harmonic Drive

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- The images below show the 2-D sketches of the HD for reference

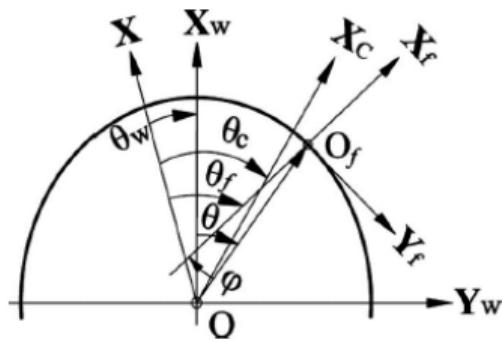


Figure: Relative position between the HD components

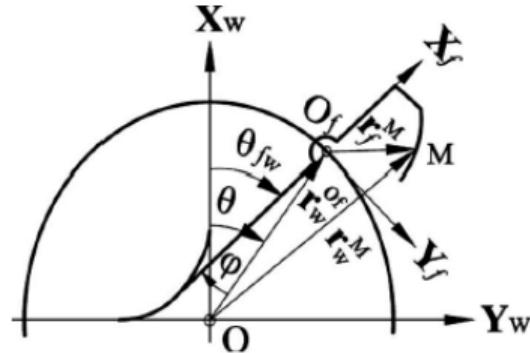


Figure: A point on the FS tooth curve

# Why Harmonic Drives?

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- **High Precision and Zero Backlash:** Harmonic drives offer extremely accurate motion control, making them ideal for robotics, aerospace, and medical devices.
- **Compact and Lightweight:** They provide high reduction ratios in a small footprint, crucial where space and weight constraints exist.
- **High Torque Capacity:** Despite their size, they can transmit large torques, which is valuable in applications like robotic arms and satellite actuators.
- **Smooth and Silent Operation:** The compliant flexspline ensures smooth transmission with minimal noise and vibration.
- **Widely Used in Cutting-Edge Technology:** Found in NASA space missions, surgical robots, humanoid joints, and precision automation, studying them opens doors to high-impact engineering fields.

# Our Objective

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**Goal:** To study and verify the kinematic mathematical model formulated by Prof. Huimin Dong in his paper "Kinematic Fundamentals of Planar Harmonic Drives"

## Steps:

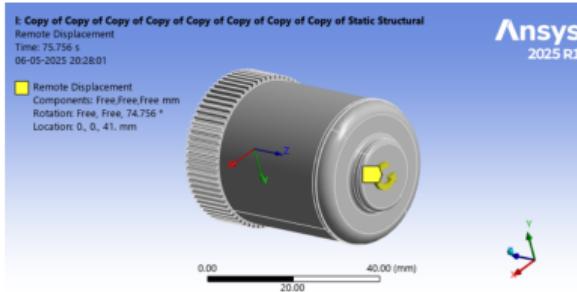
- To observe how motion of a point on flexspline (base of a tooth, point  $O_f$ ) changes if we give a constant angular velocity at the cup output end through Ansys simulations
- To test the above given point using analytical approach in MATLAB for verification
- This gives a function between the  $\theta_f$  and  $\theta_F$
- Now we use the mathematical model given in the paper to compute  $\theta_f$ , and using the function found above, we can find  $\theta_F$
- If the angular speed at the output (cup end) comes out to be constant, the model proposed in the paper is correct!

## **Methodology**

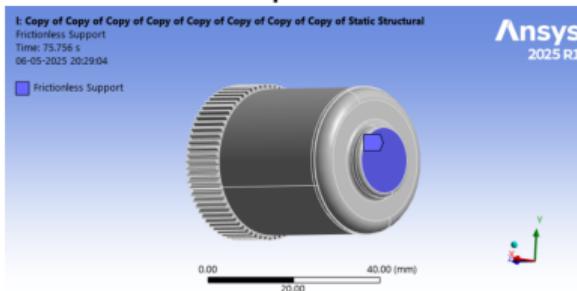
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# FEA Setup

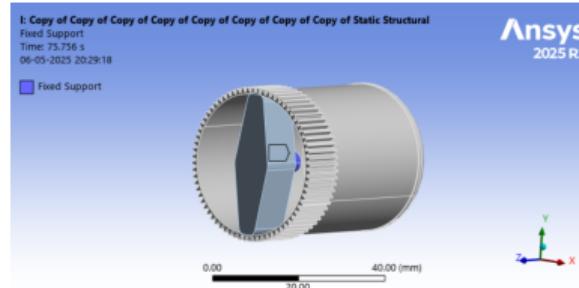
## Boundary Conditions



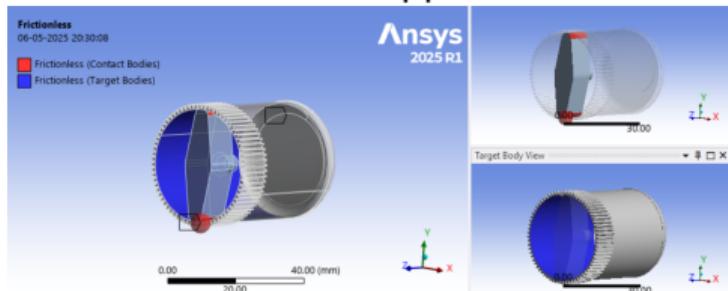
Remote Displacement  $90^\circ$



Frictionless support



Fixed Support



Frictionless Contact

# FEA Setup

A convergence study was attempted, but due to device limitation, had to restrict to element size of 0.6 mm

## Mesh Statistics

- **Elements:** 51,555
- **Nodes:** 94,226

A sphere of influence was added to get a finer mesh near the contact points

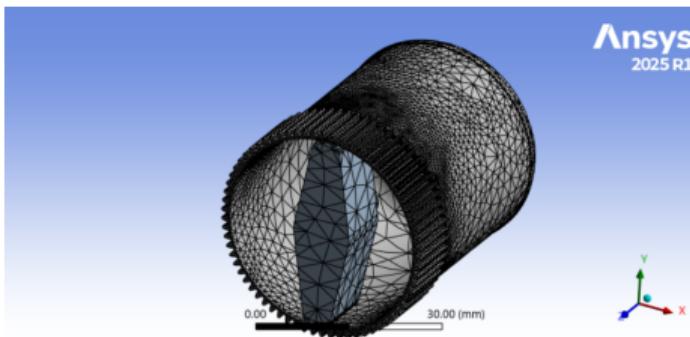


Figure: Meshed Geometry

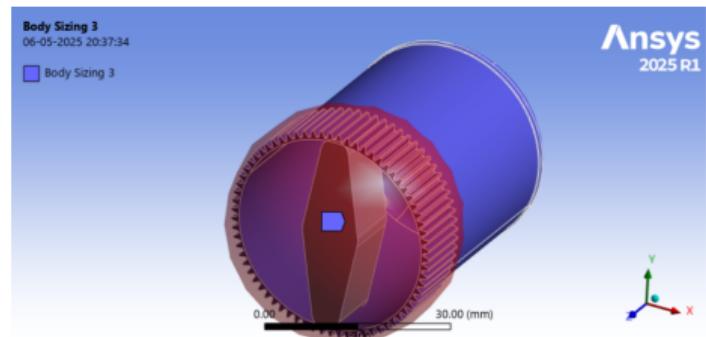


Figure: Sphere of influence

# FEA Setup

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## Named selections

Two nodes were selected as named selections, and their x,y and z displacements were noted

- **Node 1:** This is at front, placed on the tooth base, initially aligning with the y-axis ( $\theta = 0$ )
- **Node 2:** This node is the back, at the cup end

A sphere of influence was added to get a finer mesh near the contact points

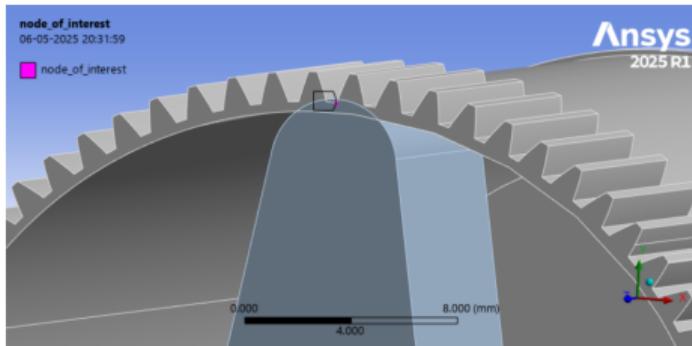


Figure: Node 1

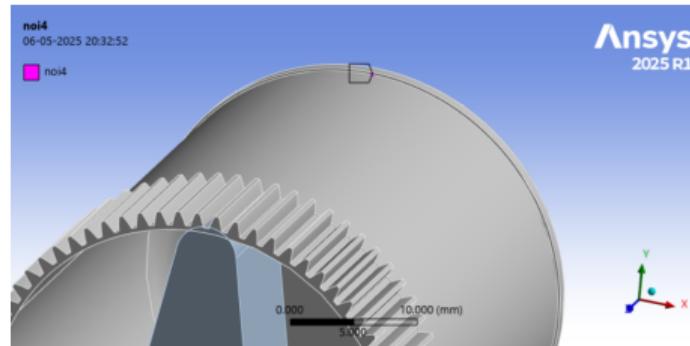


Figure: Node 2

# Analytical Formulation

The following equation is used to find the arc length of a polar curve  $R(\theta)$ :

$$\sigma = \int_0^\theta \sqrt{R^2 + \dot{R}^2} d\theta$$

Since the arc length remains the same before and after deformation, as mentioned in *Kondo, 1990*, we can write:

$$\sigma = R_0 \theta_F$$

where,  $R_0$  is the radius at the cup end and  $\theta_F$  is the angle at the cup end.

Using these two equations, we can find  $\theta$ . Now a comparison plot can be made between  $\theta$  and  $\theta_F$ , which can be used to validate the FEA results.

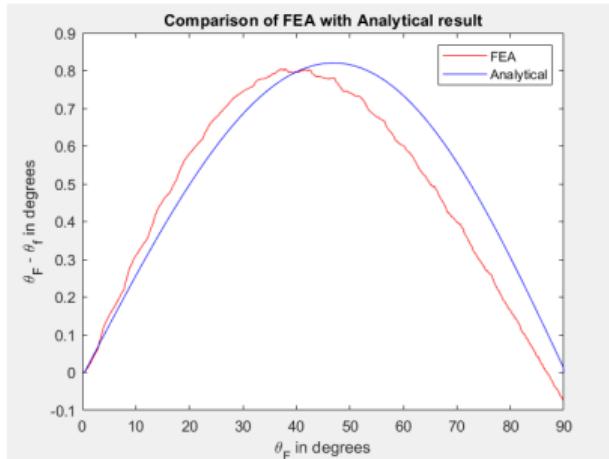


Figure:  $\theta_F - \theta_f$  comparison from FEA and Analytical formulation

# Kinematic Model

- Since HD is compliant mechanism, hard to predict kinematics
- The paper proposes a combination of disk cams with a translating knife-edge follower and an oscillating flat face follower to make a kinematic model of HD

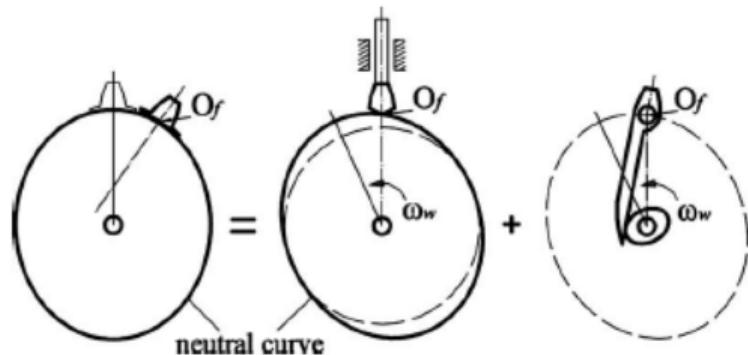


Figure: The analogy to the combination of disk cams with a translating knife-edge follower and an oscillating flat face follower

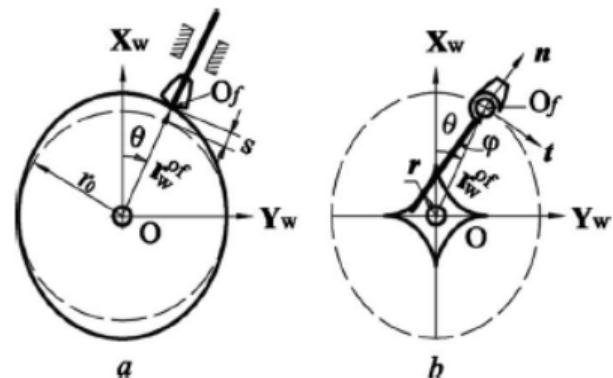


Figure: Modeling a FS tooth and the WG: (a) the translating knife-edge follower model and (b) the oscillating flat-face follower model

# Kinematic Model

## Major Assumptions

- The FS tooth is considered rigid
- CS and WG are completely rigid
- There is no load at the output

The images below show the 2-D sketches of the HD for reference

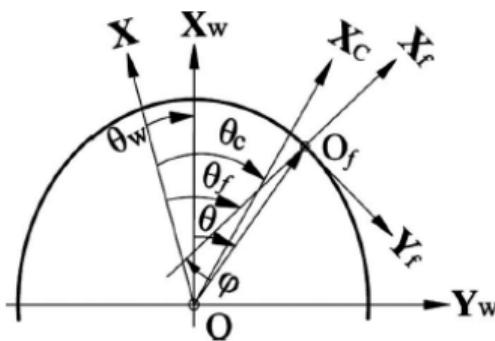


Figure: Relative position between the HD components

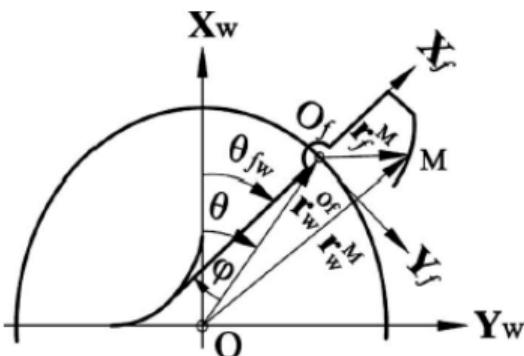


Figure: A point on the FS tooth curve

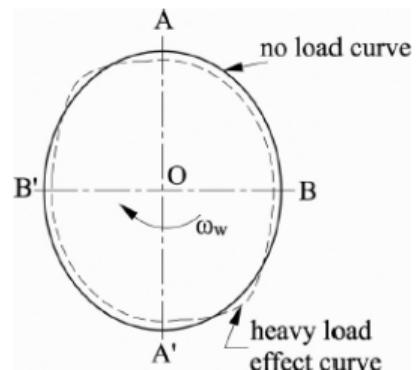
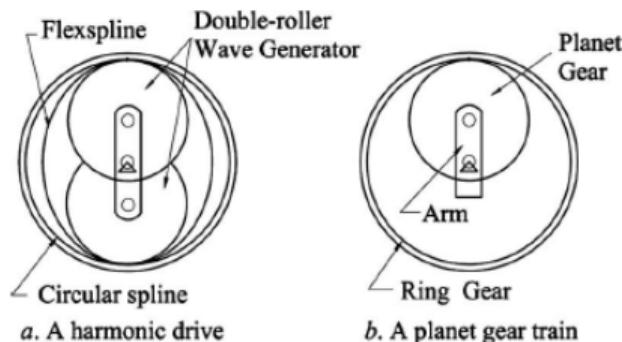


Figure: The FS neutral curve on the WG transverse section

# Kinematic Model

## Comparison with Planetary Gear Train

- The subscripts  $C$ ,  $W$ , and  $F$  refer to the Circular Spline (CS), Wave Generator (WG), and Flexspline (FS), respectively.
- Similar to planetary gear systems, if angular velocities of any two components are known, the third can be determined using the kinematic relation.



$$\frac{\bar{\omega}_F - \omega_W}{\omega_C - \omega_W} = \frac{N_C}{N_F}$$

where:

- $\omega_C$ : Angular speed of the circular spline (analogous to the ring gear)
- $\omega_W$ : Angular speed of the wave generator (analogous to the carrier)
- $\bar{\omega}_F$ : Average angular speed of the flexspline (analogous to the planet gear)

Figure: Kinematic diagrams of HD and PGT

# Kinematic Model

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$$R(\theta) = r_0 + w_0(1 + \cos 2\theta)$$

$$\varphi = \cos^{-1} \left( \frac{R}{\sqrt{R^2 + \dot{R}^2}} \right)$$

$$\theta_C = \theta_W + \theta_{CW}$$

$$\theta_{CW} = \frac{2N_F}{D_{F0}N_C} \int_0^\theta \sqrt{R^2 + \dot{R}^2} d\theta$$

$$\theta_f = \theta_w + \theta_{fw} = \theta_W + \theta + \varphi$$

## Variable Definitions:

- $R(\theta)$ : Radial position of the flexspline
- $r_0$ : Radius of the prime circle of cam FS
- $w_0$ : Amplitude of deformation
- $\varphi$ : Oscillating angle of tooth (follower)
- $N_F(N_C)$ : Number of teeth on the FS (CS)
- $D_{F0}$ : Initial pitch diameter of flexspline
- $\theta$ : Angular position on flexspline
- $\theta_W$ : Angular position of the WG
- $\theta_{CW}$ : Angular pos. of CS relative to WG
- $\theta_{fw}$ : Rel. angular pos. of tooth normal from WG
- $\theta_f$ : Final angular position of the joint
- $\theta_C$ : Final angular position of the CS

# Methodology

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- $r_0$  and  $w_0$  are known;  $R$  is a function of  $\theta$ , so compute  $\dot{R}$
- Find  $\varphi$  using the analytical expression
- The input is given to the wave generator and the circular spline is fixed, so  $\theta_{CW} = \theta_C - \theta_W = -\theta_W$
- Using equation 3, compute  $\theta$
- Compute  $\theta_f$  from equation 4
- Now that  $\theta_f$  is known, from the previous analytical formulation,  $\theta_F$  can be found
- Compute  $\omega_f$  and  $\omega_F$ , and plot them

## **Results**

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# HD Animation

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- The kinematic model was used to generate a sample animation. The tooth profiles for both CS and FS was known
- A harmonic drive has  $N_F = 240$ ,  $N_C = 242$ ,  $D_{F0} = 121.46$  mm, and  $r_0 = 60.31$  mm, with the neutral curve prescribed using  $w_0 = 0.42$  mm

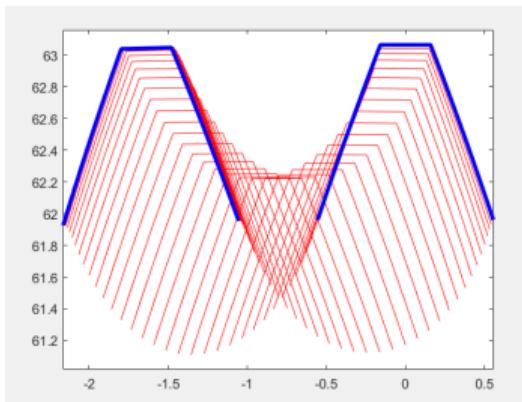


Figure: Our animation

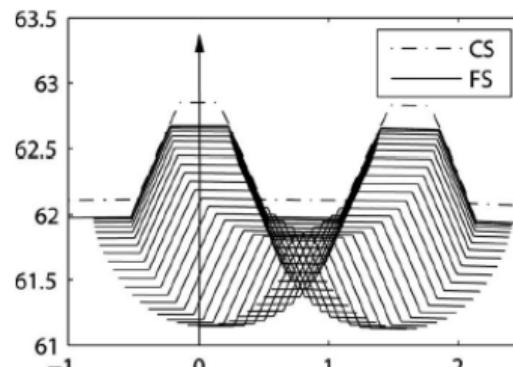
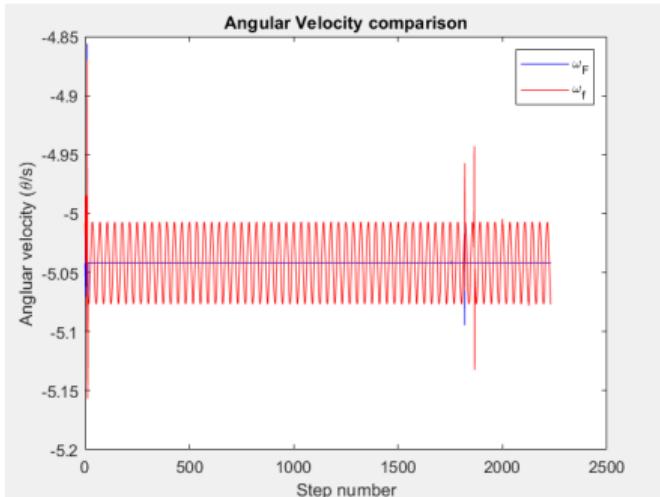


Figure: Animation from paper

# HD Animation

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- As mentioned earlier, our goal is to see the variation of  $\omega_F$  and  $\omega_f$
- It can be clearly observed that  $\omega_f$  shows a periodic variation, while  $\omega_F$  remains constant
- This proves the validity of the kinematic model proposed in the paper



## **Conclusions**

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# Final Thoughts

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- An analytical formulation was done to find relation between  $\theta_f$  and  $\theta_F$
- This analytical formulation was verified with Ansys simulation
- The kinematic model from the paper was then used to compute  $\theta_f$
- $\theta_F$  was computed from  $\theta_f$  using the analytical formulation, and consequently,  $\omega_F$  was found
- $\omega_F$  turns out to be constant, which means we get a constant output, thus proving the validity of the model

# Acknowledgement

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I would like to express my sincere gratitude to my project advisor, Prof. Prasanna Gandhi, for their constant guidance, encouragement, and insightful feedback throughout the course of this work.

# Thank you!

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# References

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-  Huimin Dong, *Kinematic Fundamentals of Planar Harmonic Drives*, 2011.
-  Huimin Dong, *Kinematic Effect of the Compliant Cup in Harmonic Drives*, 2011.
-  K. Kondo & J. Takada 1990, *Study on Tooth Profiles of the Harmonic Drive*, 131-137.