Stress Drop Reading Group

Week 2

August 7th, 2024

Corner frequency (f_c) and stress drop $(\Delta \sigma)$

- (Moment-based) stress drop ← source dimension (radius)
- Most popular approach is to estimate radius (a) from corner frequency (f_c) .

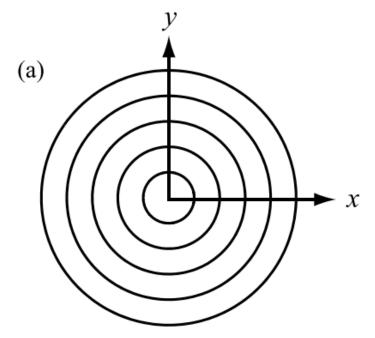
$$\Delta \sigma = C(a, b, v) \frac{M_0}{bS}$$
 (Eshelby, 1957) – (1)
 $\Delta \sigma = \frac{7}{16} \frac{M_0}{a^3}$ ($a = b; v = 0.25$) – (2)

$$\overline{f_c} = k \frac{\beta}{a}$$
 (Brune, 1970; Madariaga, 1976) – (3)

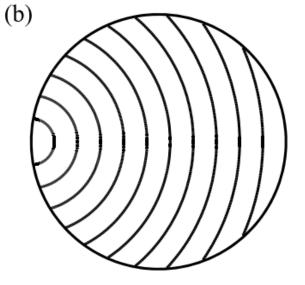
(2) & (3)
$$\rightarrow \Delta \sigma = \frac{7}{16} \left(\frac{\bar{f}_c}{k\beta} \right)^3 M_0 - (4)$$

Q) How is k affected by different assumptions about seismic source?

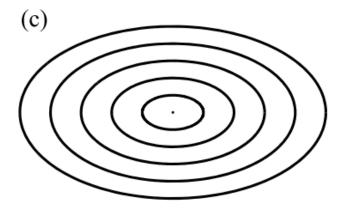
Different source scenarios



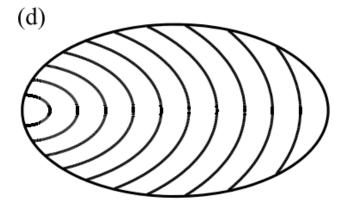
Symmetrical circular rupture



Asymmetrical circular rupture



Symmetrical elliptical rupture



Asymmetrical elliptical rupture

- Symmetry
- Geometry
- Rupture speed
- Rupture mode

Numerical scheme (Kaneko & Shearer, 2014, 2015)

Infinite homogeneous, isotropic elastic medium

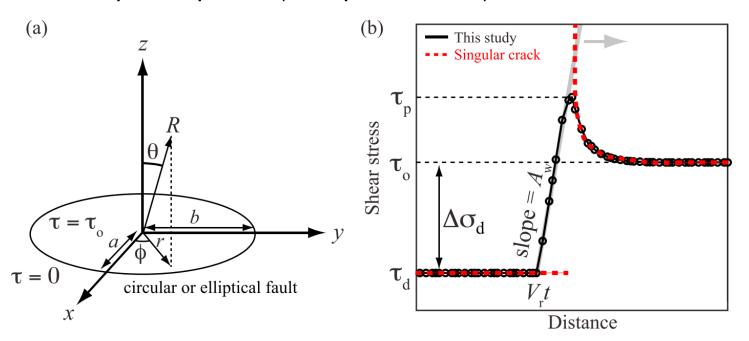
Cohesive zone model

$$\tau_{st} = \max\{\tau_d, \tau_d + A_w(|\vec{r} - V_r t|)\}$$
 (Andrews, 1985; Dunham and Bhat, 2008)

$$V_r = V_x V_y \left(\frac{x^2 + y^2}{V_y^2 x^2 + V_x^2 y^2} \right)^{1/2}$$
 (V_x : major axis, V_y : minor axis)

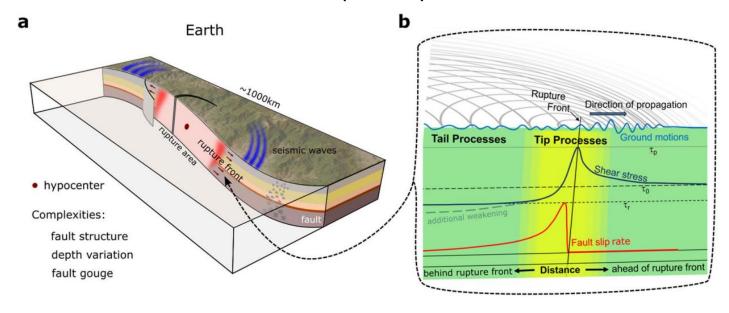
 τ_p : determined by A_w & τ_d

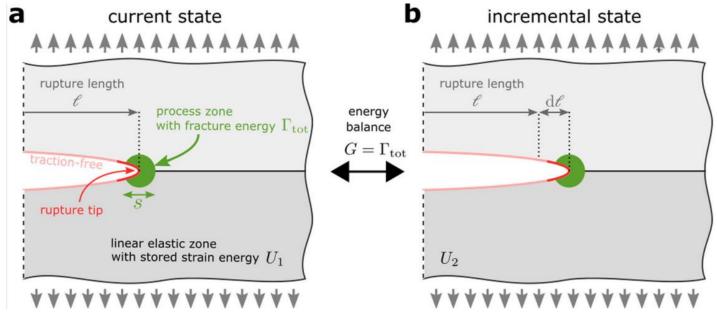
Fixed rupture speeds (not spontaneous)



Cohesive zone model (CZM)

Kammer et al., (2024)





Linear Elastic Fracture Mechanics (LEFM)

 G_0 : Static energy release rate

 Γ_{tot} : Total fracture energy

$$G_0 = -rac{d\Pi}{dl}$$
 where $d\Pi = (U_2 - U_1) - F$

To avoid infinite stresses at the crack tip, the dissipation is often smeared out in "process zone" of size $s \ll l$, commonly implemented via cohesive zone models.

LEFM predicts the crack growth speed through an energy balance

 $\rightarrow G = \Gamma_{tot}$ where $G \leq G_0$ (G: dynamic energy release rate)

$$G = \left(1 - \frac{C_f}{C_R}\right)G_0$$
 where $C_f = dl/dt$

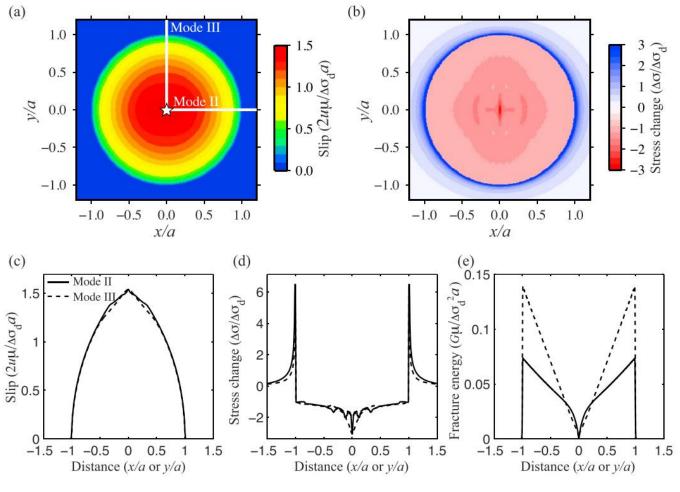
 C_R : Rayleigh wave speed

Case I Symmetrical circular rupture

Nondimensional variables (normalized)

Length
$$r'=r/\sqrt{ab}$$

Time $t'=t\beta/\sqrt{ab}$
Stress $\sigma'_{ij}=\sigma_{ij}/\Delta\sigma_d$
Displacement $u'_i=u_i\mu/\left(\Delta\sigma_d\sqrt{ab}\right)$
Weakening rate $A'_w=A_w\sqrt{ab}/\Delta\sigma_d$
Seismic moment $M'_0=M_0/\left[\Delta\sigma_d^2(ab)^{3/2}\right]$
Fracture energy density $G'=G\mu/\left(\Delta\sigma_d^2\sqrt{ab}\right)$
Radiated energy $E'_r=E\mu/\left[\Delta\sigma_d^2(ab)^{3/2}\right]$



$$A'_{w} = 84, V_{r}/\beta = 0.9$$

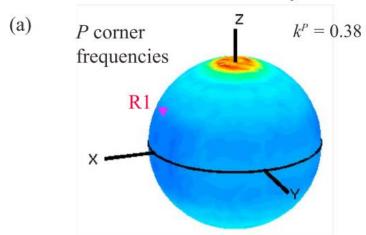
Case I Symmetrical circular rupture

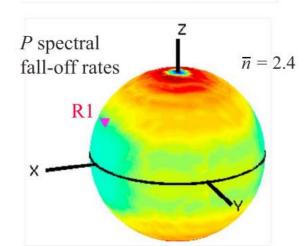
$$\overline{f_c}^P = k^P \frac{\beta}{a} = 0.38 \frac{\beta}{a}$$

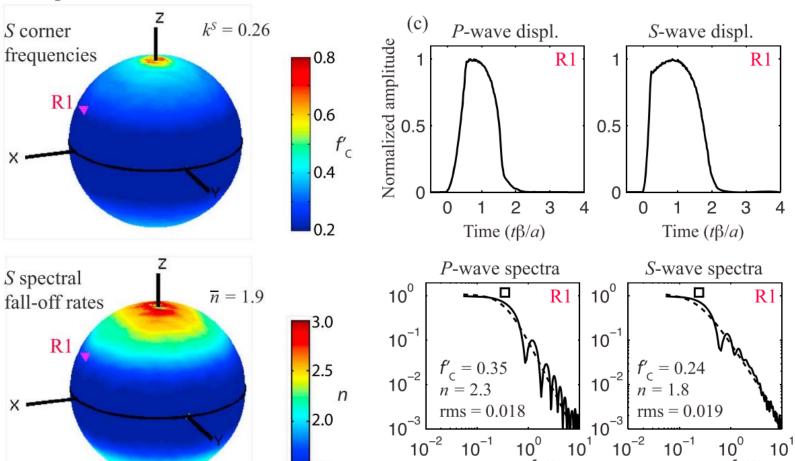
$$\overline{f_c}^S = k^S \frac{\beta}{a} = 0.26 \frac{\beta}{a}$$

(b)

Symmetrical circular rupture



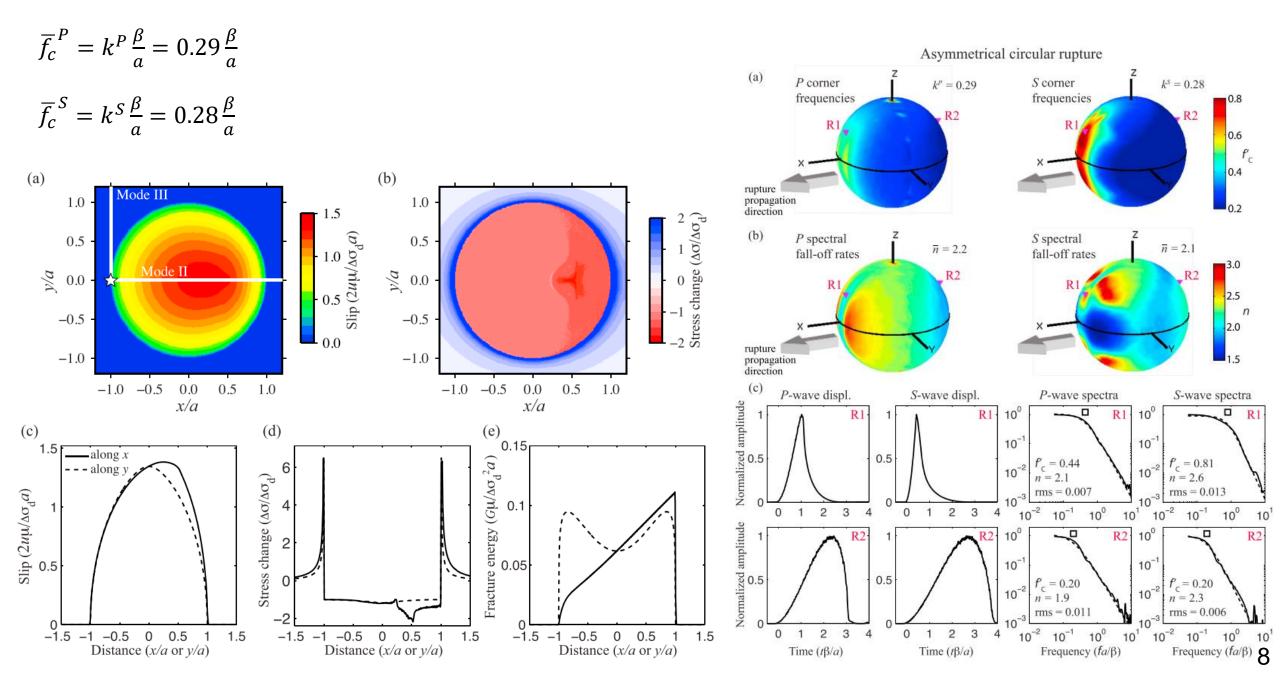




Frequency (fa/β)

Frequency (fa/β)

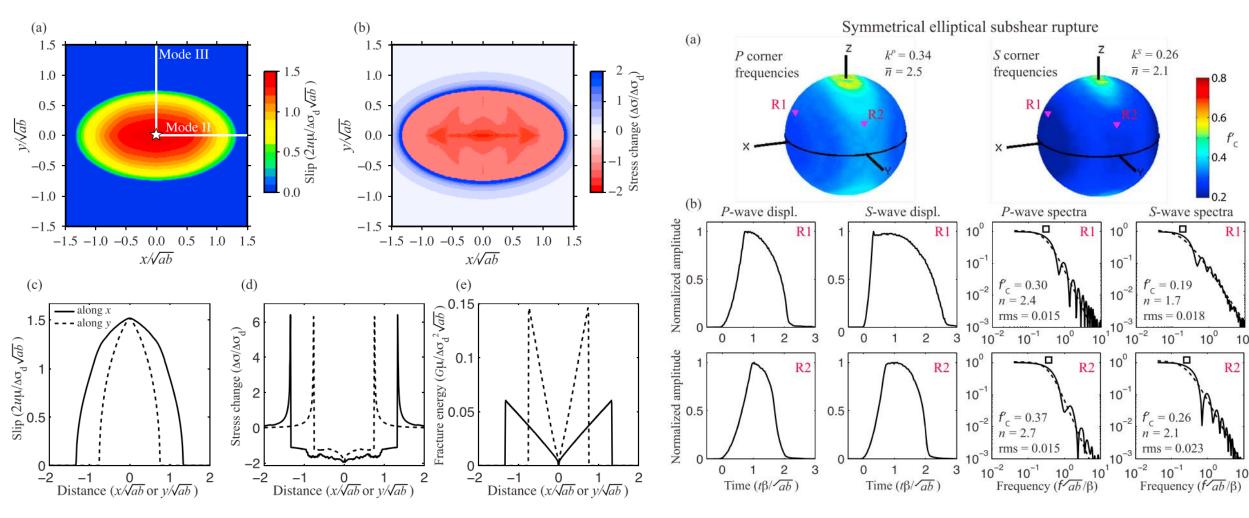
Case II Asymmetrical circular rupture



Case III Symmetrical elliptical rupture

$$\overline{f_c}^P = k^P \frac{\beta}{\sqrt{ab}} = 0.34 \frac{\beta}{\sqrt{ab}}$$

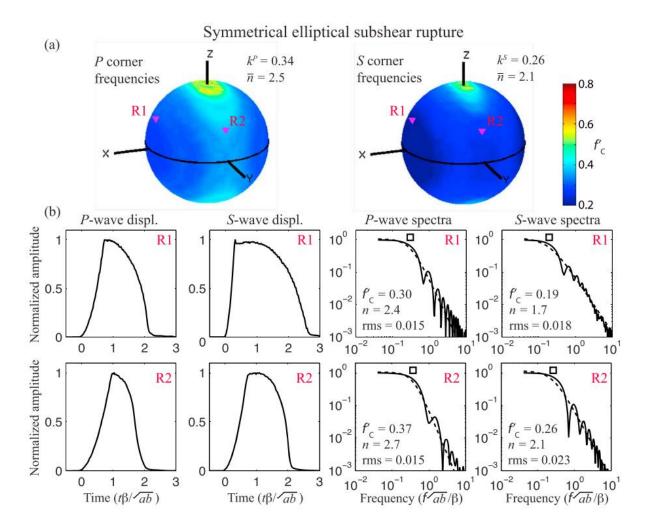
$$\overline{f_c}^S = k^S \frac{\beta}{\sqrt{ab}} = 0.26 \frac{\beta}{\sqrt{ab}}$$
 (subshear)

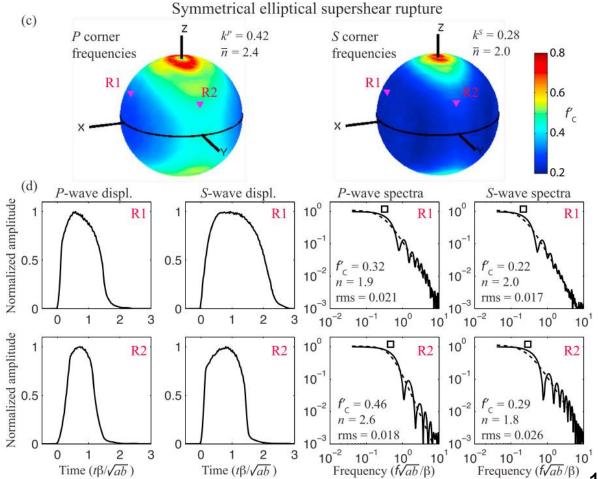


Case III Symmetrical elliptical rupture

$$\overline{f_c}^P = k^P \frac{\beta}{\sqrt{ab}} = 0.34 \frac{\beta}{\sqrt{ab}}$$
 (subshear)
$$\overline{f_c}^S = k^S \frac{\beta}{\sqrt{ab}} = 0.26 \frac{\beta}{\sqrt{ab}}$$

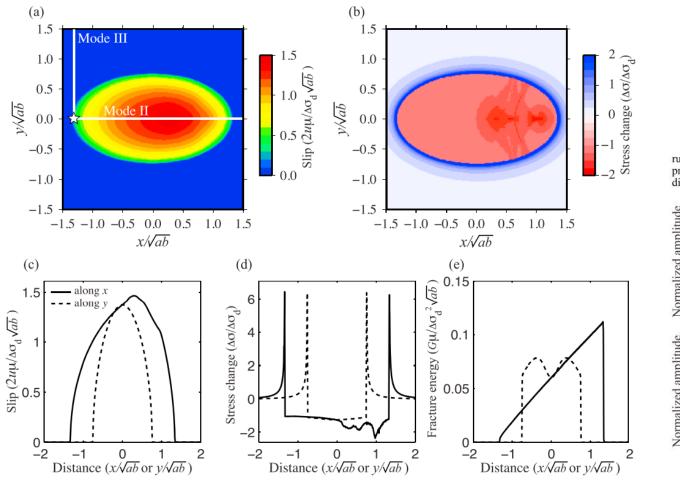
$$\overline{f_c}^P = k^P \frac{\beta}{\sqrt{ab}} = 0.42 \frac{\beta}{\sqrt{ab}}$$
 (supershear)
$$\overline{f_c}^S = k^S \frac{\beta}{\sqrt{ab}} = 0.28 \frac{\beta}{\sqrt{ab}}$$

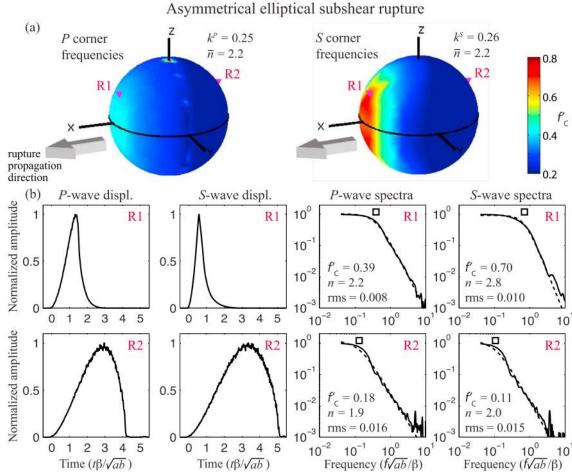




Case IV Asymmetrical elliptical rupture

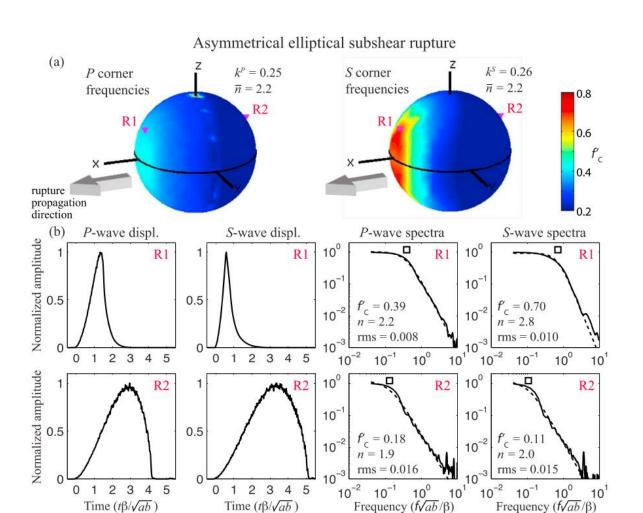
$$\overline{f_c}^P = k^P \frac{\beta}{\sqrt{ab}} = 0.25 \frac{\beta}{\sqrt{ab}}$$
 (subshear) $\overline{f_c}^S = k^S \frac{\beta}{\sqrt{ab}} = 0.26 \frac{\beta}{\sqrt{ab}}$

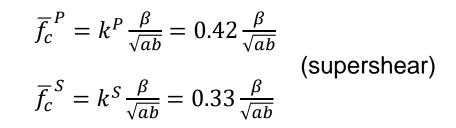


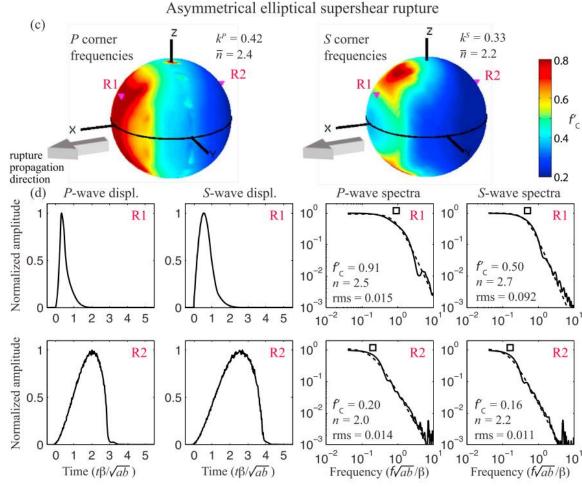


Case IV Asymmetrical elliptical rupture

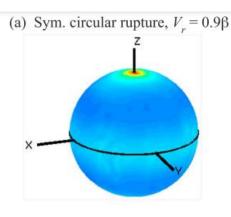
$$\overline{f_c}^P = k^P \frac{\beta}{\sqrt{ab}} = 0.25 \frac{\beta}{\sqrt{ab}}$$
 (subshear) $\overline{f_c}^S = k^S \frac{\beta}{\sqrt{ab}} = 0.26 \frac{\beta}{\sqrt{ab}}$

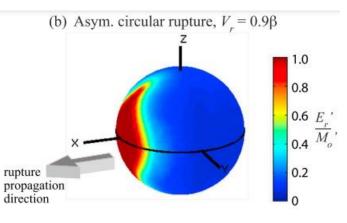


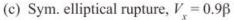


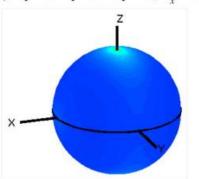


Radiated energy

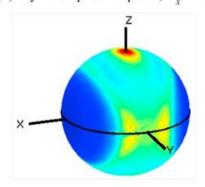




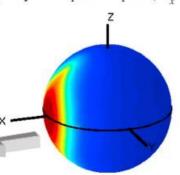




(d) Sym. elliptical rupture, $V_x = 1.6\beta$

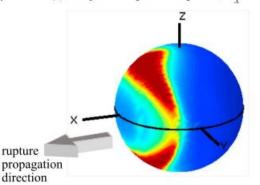


(e) Asym. elliptical rupture, $V_r = 0.9\beta$



direction

(f) Asym. elliptical rupture, $V_{x} = 1.6\beta$



$$E_r = \int_{\Sigma} \frac{\tau^o(\xi) + \tau^f(\xi)}{2} D(\xi) d\Sigma - \int_0^{\infty} \int_{\Sigma} \tau(\xi, t) V(\xi, t) d\Sigma dt$$

Far-field estimation

$$E_r = E_r^P + E_r^S = 2\rho \int_{\Gamma} \int_0^{\infty} [\alpha(\dot{u}^P)^2 + \beta(\dot{u}^S)^2] df d\Gamma$$

(frequency domain)

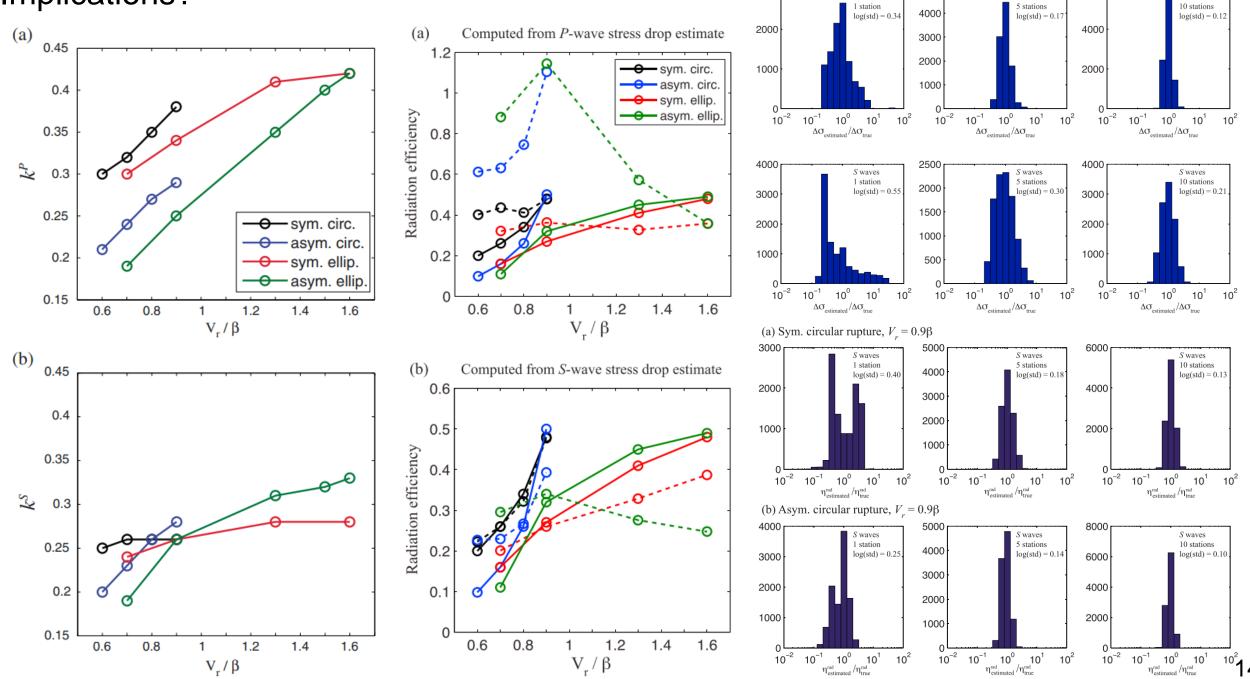
$$E_r = E_r^P + E_r^S = \rho \int_{\Gamma} \int_0^{\infty} [\alpha(\dot{u}^P)^2 + \beta(\dot{u}^S)^2] dt d\Gamma$$

(time domain)

Point source: $E_r^S / E_r^P = 23 \ (v = 0.25)$

$$E^r/M_0 \approx E_r^S/M_0 \ (E_r^S \gg E_r^P)$$

Implications?



3000

P waves

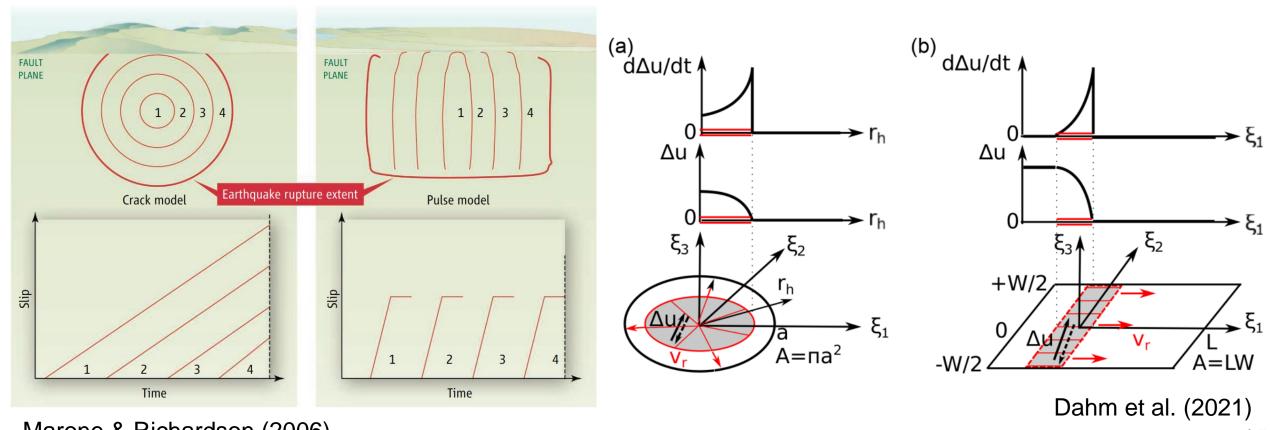
6000

o waves

P waves

Crack-like vs Pulse-like rupture

- Crack-like rupture: local slip duration ≈ rupture duration (e.g., Madariaga, 1976)
- Pulse-like rupture: local slip duration ≪ rupture duration (e.g., Haskell, 1964; Heaton, 1990)
- Exact mechanism behind pulse-like rupture is still under debate.

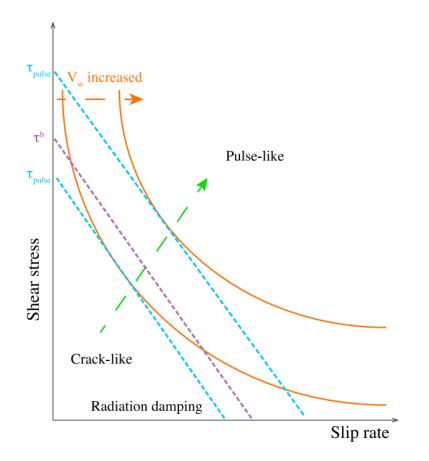


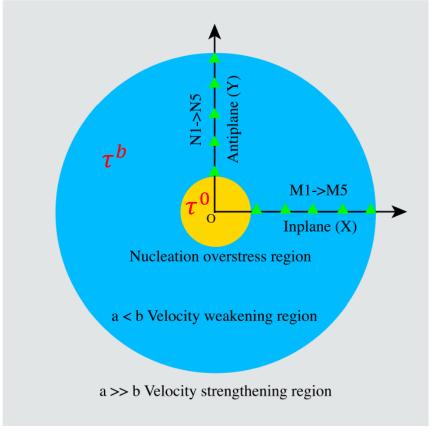
Marone & Richardson (2006)

Numerical scheme (Wang & Day, 2017)

- Slip velocity-dependent friction (rate- and state-dependent friction)
- $f(V,\psi) = a \sinh^{-1}\left[\frac{V}{2V_0}\exp\left(\frac{\psi}{a}\right)\right]$ where $\dot{\psi} = -\frac{V}{L}[\psi \psi_{SS}(V)]$, $\psi_{SS}(V) = a \ln\left\{\frac{2V_0}{V}\sinh\left[\frac{f_{SS}(V)}{a}\right]\right\}$,

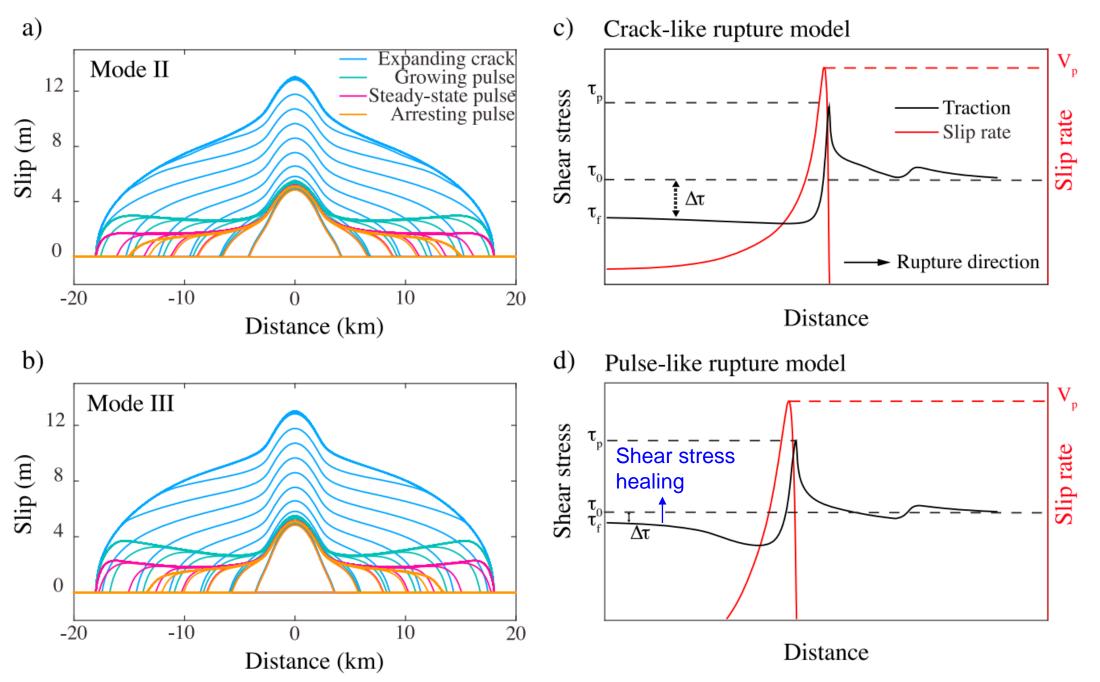
$$f_{SS}(V) = f_W + \frac{f_{lv} - f_W}{[1 + (V/V_W)^8]^{1/8}}$$
, and $f_{lv}(V) = f_0 - (b - a) \ln(V/V_0)$





- Crack → Pulse
 - 1) Decrease τ_b
 - 2) Increase V_w
- Spontaneous rupture
 - \rightarrow Not fixed V_r

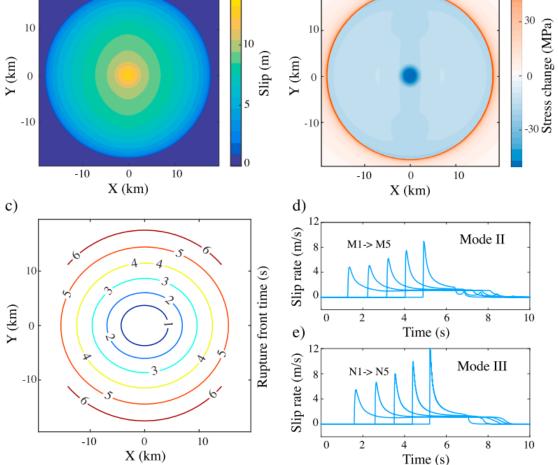
Simulation results

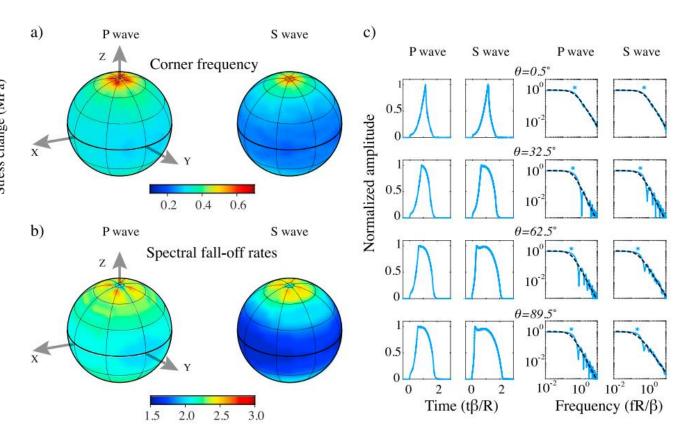


Case I Expanding crack

$$\overline{f_c}^P = k^P \frac{\beta}{a} = 0.35 \frac{\beta}{a} \qquad V_r^2 = 0.88\beta$$

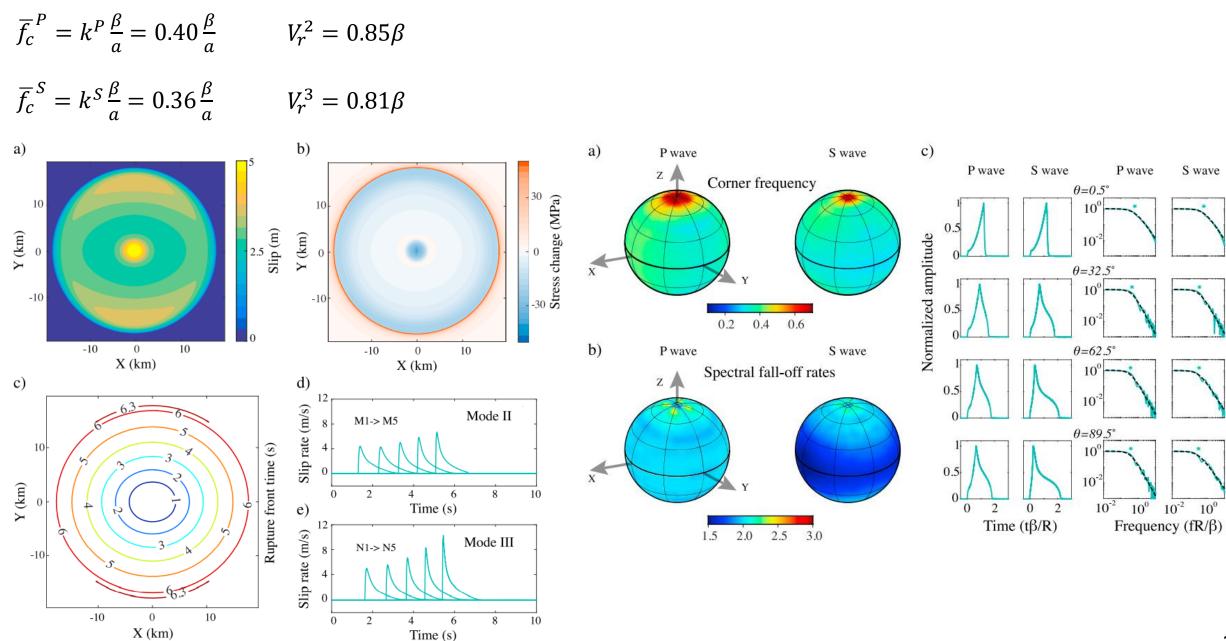
$$\overline{f_c}^S = k^S \frac{\beta}{a} = 0.27 \frac{\beta}{a} \qquad V_r^3 = 0.84\beta$$
a)
b)



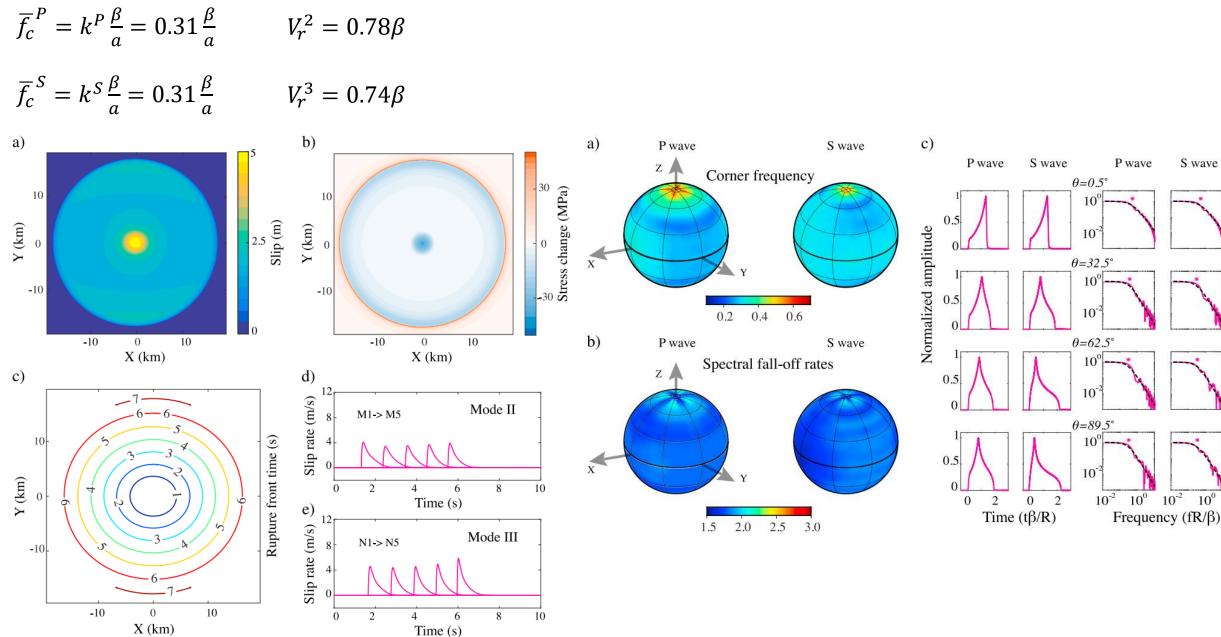


Four-lobes of high falloff rate not present in fixed rupture velocity model (Kaneko & Shearer, 2014)

Case II Growing pulse



Case II Steady state pulse

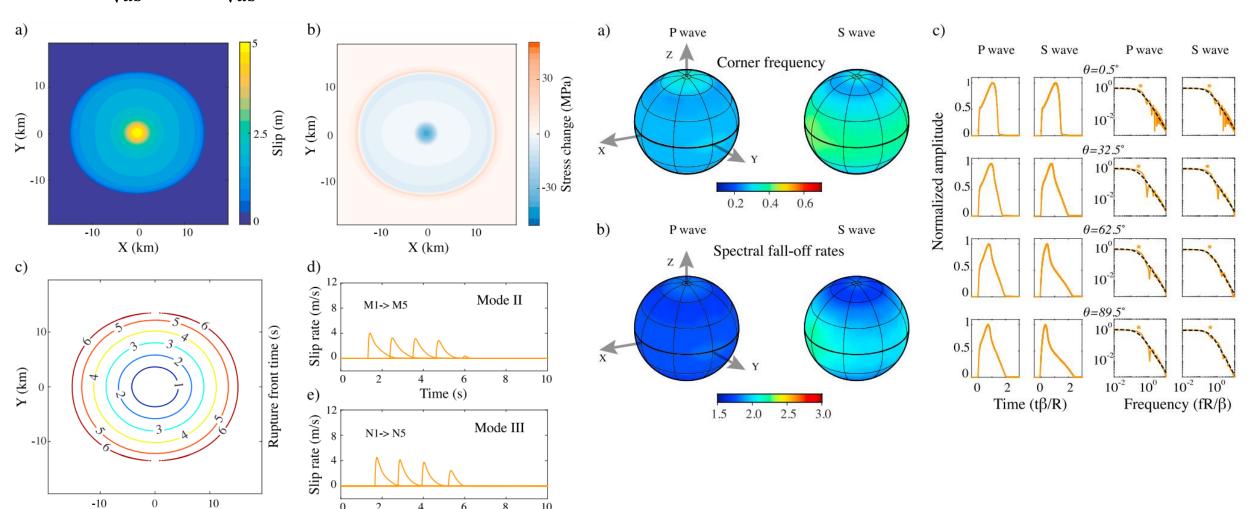


Case IV Arresting pulse

X (km)

$$\overline{f_c}^P = k^P \frac{\beta}{\sqrt{ab}} = 0.28 \frac{\beta}{\sqrt{ab}} \quad V_r^2 = 0.72 \beta$$

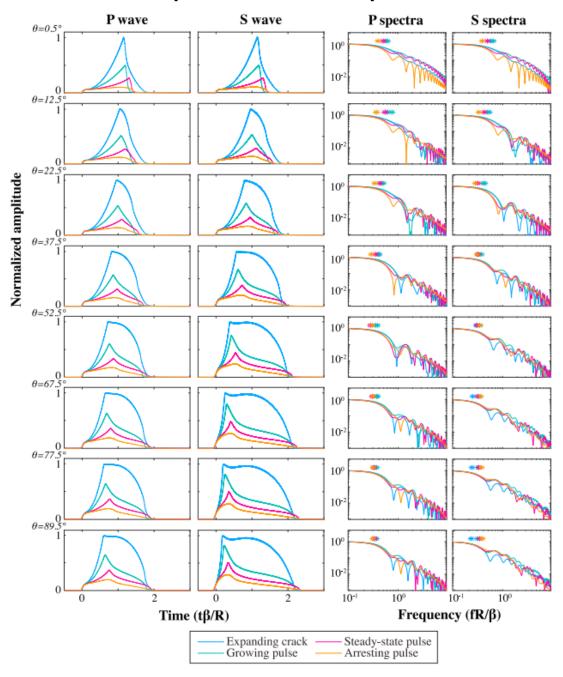
$$\overline{f_c}^S = k^S \frac{\beta}{\sqrt{ab}} = 0.34 \frac{\beta}{\sqrt{ab}} \quad V_r^3 = 0.66 \beta$$



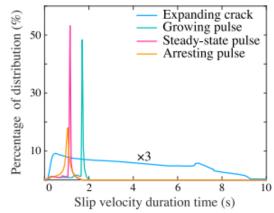
10

Time (s)

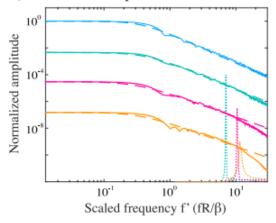
Far-field displacements/spectra



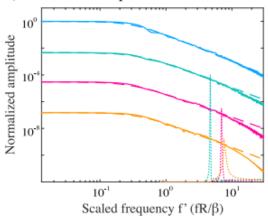
a) Slip duration distribution



b) Stacked P-wave spectra



c) Stacked S-wave spectra



Secondary corner frequency for pulse-like models

$$f_c^{2nd} = \frac{K}{\bar{T}} (\bar{T}: \text{mean risetime})$$

Radiated energy / Stress drop

