



This week's agenda

- **Concept of Stability**
- **Stability Analysis of the Closed Loop System by Routh Criterion**
- **State Space Representation and Stability**



P-3 Concept of Stability

What is stability?

- Stability is a property of the system regardless of the signals at the inputs and outputs
- Stability is an underlying requirement in every control system

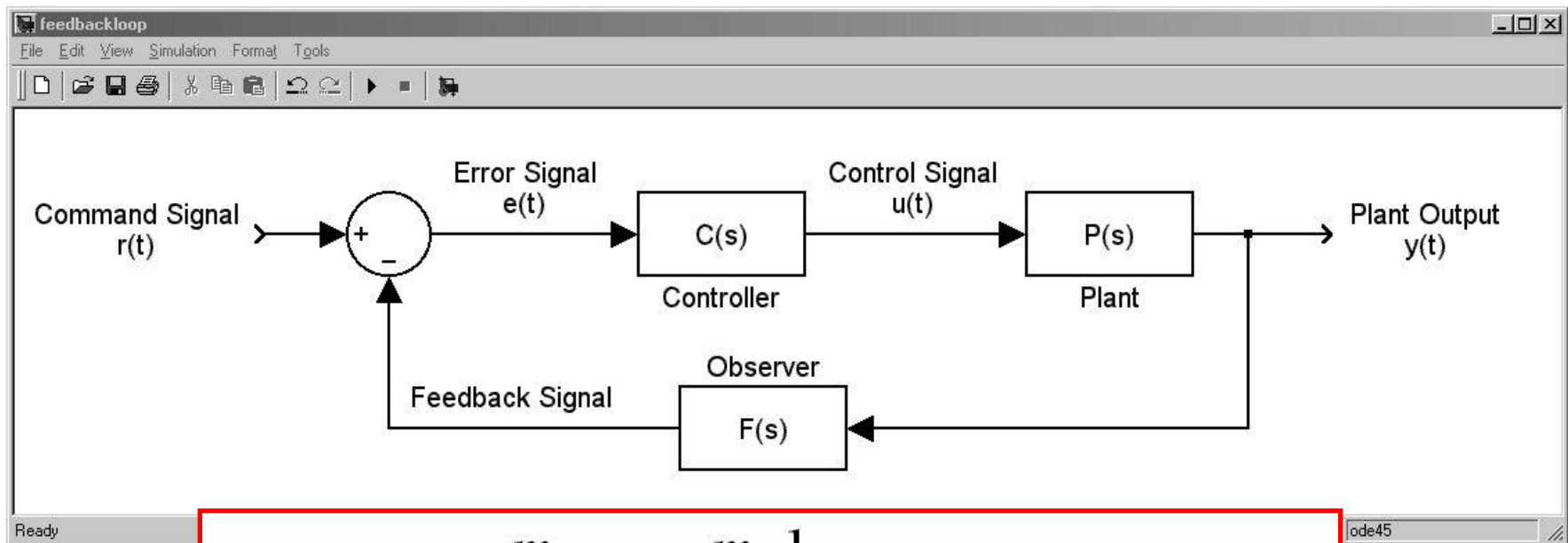
Why do we need to analyze stability?

- An unstable system is potentially dangerous!
- When the power is turned on, the output will increase (decrease/oscillate) indefinitely...
- Eventually this will damage the physical setup

P-3 Stability Analysis of the Closed Loop System by Routh Criterion

Consider the feedback loop

$$\frac{Y(s)}{R(s)} = \frac{P(s)C(s)}{1 + P(s)C(s)F(s)} = T(s)$$



$$T(s) = \frac{b'_0 s^m + b'_1 s^{m-1} + \dots + b'_{m-1} s + b'_m}{a_0 s^n + a_1 s^{n-1} + \dots + a_{n-1} s + a_n}$$

s^n	a_0	a_2	a_4	a_6	\cdot	\cdot	\cdot
s^{n-1}	a_1	a_3	a_5	a_7	\cdot	\cdot	\cdot
s^{n-2}	b_1	b_2	b_3	b_4	\cdot	\cdot	\cdot
s^{n-3}	c_1	c_2	c_3	c_4	\cdot	\cdot	\cdot
s^{n-4}	d_1	d_2	d_3	d_4	\cdot	\cdot	\cdot
\cdot	\cdot	\cdot					
\cdot	\cdot	\cdot					
\cdot	\cdot	\cdot					
s^2	e_1	e_2					
s^1	f_1						
s^0	g_1						

T(s) will let you first place these terms

$$\frac{Y(s)}{R(s)} = \frac{P(s)C(s)}{1 + P(s)C(s)F(s)} = T(s)$$

$$T(s) = \frac{b'_0 s^m + b'_1 s^{m-1} + \dots + b'_{m-1} s + b'_m}{a_0 s^n + a_1 s^{n-1} + \dots + a_{n-1} s + a_n}$$



ROW #3

Evaluate till the
remaining bs are all
zero

$$b_1 = \frac{a_1 a_2 - a_0 a_3}{a_1}$$

$$b_2 = \frac{a_1 a_4 - a_0 a_5}{a_1}$$

$$b_3 = \frac{a_1 a_6 - a_0 a_7}{a_1}$$

$$\vdots$$

s^n	a_0	a_2	a_4	a_6	\cdot	\cdot	\cdot
s^{n-1}	a_1	a_3	a_5	a_7	\cdot	\cdot	\cdot
s^{n-2}	b_1	b_2	b_3	b_4	\cdot	\cdot	\cdot
s^{n-3}	c_1	c_2	c_3	c_4	\cdot	\cdot	\cdot
s^{n-4}	d_1	d_2	d_3	d_4	\cdot	\cdot	\cdot
\cdot	\cdot	\cdot					
\cdot	\cdot	\cdot					
\cdot	\cdot	\cdot					
s^2	e_1	e_2					
s^1	f_1						
s^0	g_1						



ROW #4

Evaluate till the remaining cs are all zero

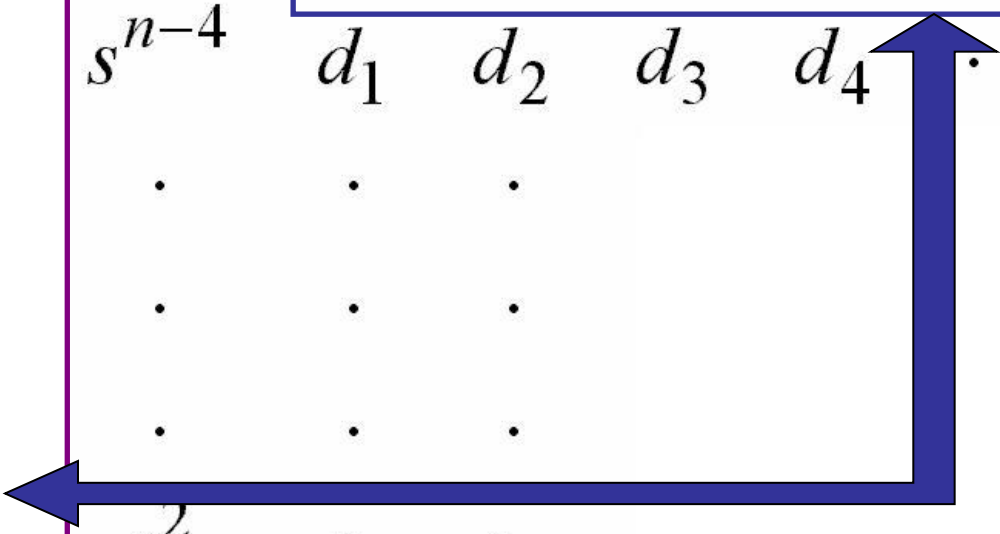
$$c_1 = \frac{b_1 a_3 - a_1 b_2}{b_1}$$

$$c_2 = \frac{b_1 a_5 - a_1 b_3}{b_1}$$

$$c_3 = \frac{b_1 a_7 - a_1 b_4}{b_1}$$

$$\vdots$$

s^n	a_0	a_2	a_4	a_6	\cdot	\cdot	\cdot
s^{n-1}	a_1	a_3	a_5	a_7	\cdot	\cdot	\cdot
s^{n-2}	b_1	b_2	b_3	b_4	\cdot	\cdot	\cdot
s^{n-3}	c_1	c_2	c_3	c_4	\cdot	\cdot	\cdot
s^{n-4}	d_1	d_2	d_3	d_4	\cdot	\cdot	\cdot
\cdot	\cdot	\cdot					
\cdot	\cdot	\cdot					
\cdot	\cdot	\cdot					
s^2	e_1	e_2					
s^1	f_1						
s^0	g_1						





ROW #5

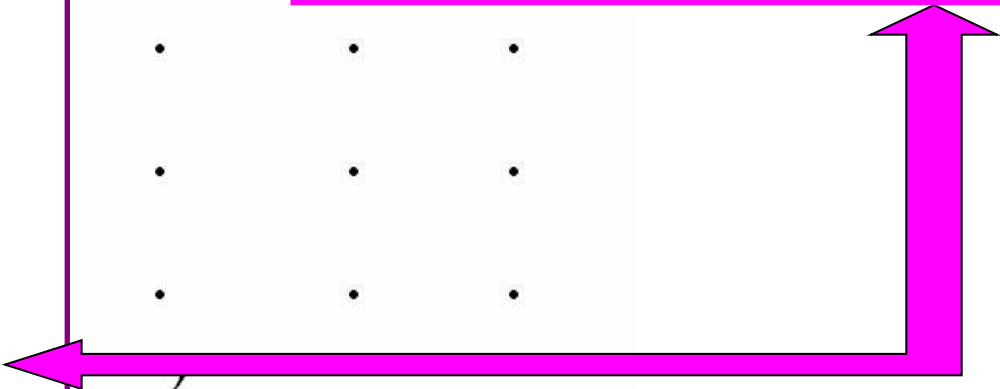
Evaluate till the
remaining bs are all
zero

$$d_1 = \frac{c_1 b_2 - b_1 c_2}{c_1}$$

$$d_2 = \frac{c_1 b_3 - b_1 c_3}{c_1}$$

$$d_3 = \frac{c_1 b_4 - b_1 c_4}{c_1}$$
$$\vdots$$

s^n	a_0	a_2	a_4	a_6	\cdot	\cdot	\cdot
s^{n-1}	a_1	a_3	a_5	a_7	\cdot	\cdot	\cdot
s^{n-2}	b_1	b_2	b_3	b_4	\cdot	\cdot	\cdot
s^{n-3}	c_1	c_2	c_3	c_4	\cdot	\cdot	\cdot
s^{n-4}	d_1	d_2	d_3	d_4	\cdot	\cdot	\cdot
\cdot	\cdot	\cdot					
\cdot	\cdot	\cdot					
\cdot	\cdot	\cdot					
s^2	e_1	e_2					
s^1	f_1						
s^0	g_1						



Routh table

s^n	a_n	a_{n-2}	a_{n-4}	a_{n-6}	\dots
s^{n-1}	a_{n-1}	a_{n-3}	a_{n-5}	a_{n-7}	\dots
s^{n-2}	$c_n = -\frac{1}{a_{n-1}} \begin{vmatrix} a_n & a_{n-2} \\ a_{n-1} & a_{n-3} \end{vmatrix} \quad c_{n-1} = -\frac{1}{a_{n-1}} \begin{vmatrix} a_n & a_{n-4} \\ a_{n-1} & a_{n-5} \end{vmatrix} \quad c_{n-2} = -\frac{1}{a_{n-1}} \begin{vmatrix} a_n & a_{n-6} \\ a_{n-1} & a_{n-7} \end{vmatrix} \quad c_{n-3} = -\frac{1}{a_{n-1}} \begin{vmatrix} a_n & a_{n-8} \\ a_{n-1} & a_{n-9} \end{vmatrix} \quad \dots$				
s^{n-3}	$d_n = -\frac{1}{c_n} \begin{vmatrix} a_{n-1} & a_{n-3} \\ c_n & c_{n-1} \end{vmatrix} \quad d_{n-1} = -\frac{1}{c_n} \begin{vmatrix} a_{n-1} & a_{n-5} \\ c_n & c_{n-2} \end{vmatrix} \quad d_{n-2} = -\frac{1}{c_n} \begin{vmatrix} a_{n-1} & a_{n-7} \\ c_n & c_{n-3} \end{vmatrix}$				
s^{n-4}	$e_n = -\frac{1}{d_n} \begin{vmatrix} c_n & c_{n-1} \\ d_n & d_{n-1} \end{vmatrix} \quad e_{n-1} = -\frac{1}{d_n} \begin{vmatrix} c_n & c_{n-2} \\ d_n & d_{n-2} \end{vmatrix} \quad e_{n-2} = -\frac{1}{d_n} \begin{vmatrix} c_n & c_{n-3} \\ d_n & d_{n-3} \end{vmatrix} \quad \dots$				
\vdots	\vdots	\vdots	\vdots	\vdots	
s^2	f_n	f_{n-1}			
s^1	g_n				
s^0	h_n				



Remarks

- **Repeat the same pattern till you reach the end i.e. g_1**
- **The complete array of coefficients is triangular**
- **Dividing or multiplying any row by a positive number can simplify the calculation without altering the stability conclusion**



Routh's stability criterion states that

For

$$T(s) = \frac{b'_0 s^m + b'_1 s^{m-1} + \dots + b'_{m-1} s + b'_m}{a_0 s^n + a_1 s^{n-1} + \dots + a_{n-1} s + a_n}$$



The number of poles on the right hand s-plane is equal to the number of sign changes in the first column of the table



Note that, we only need the signs of the numbers in the first column



In other words...

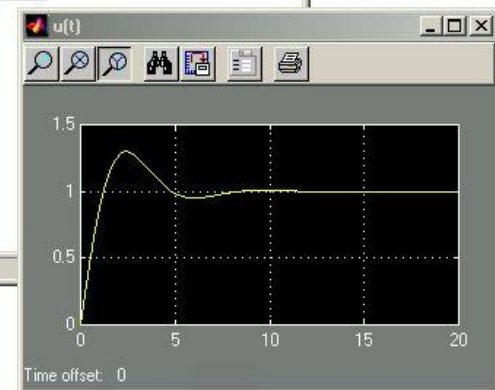
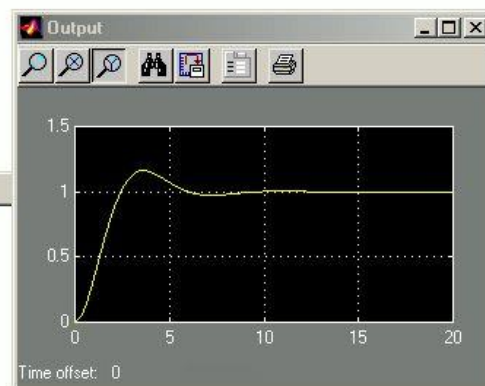
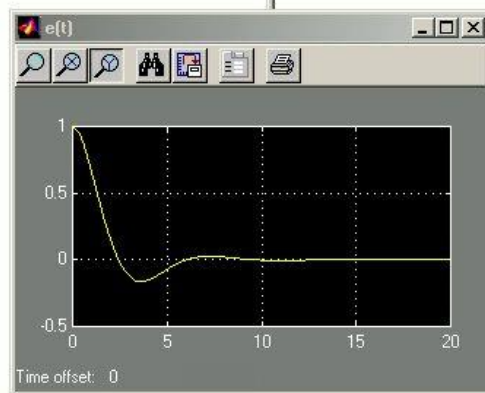
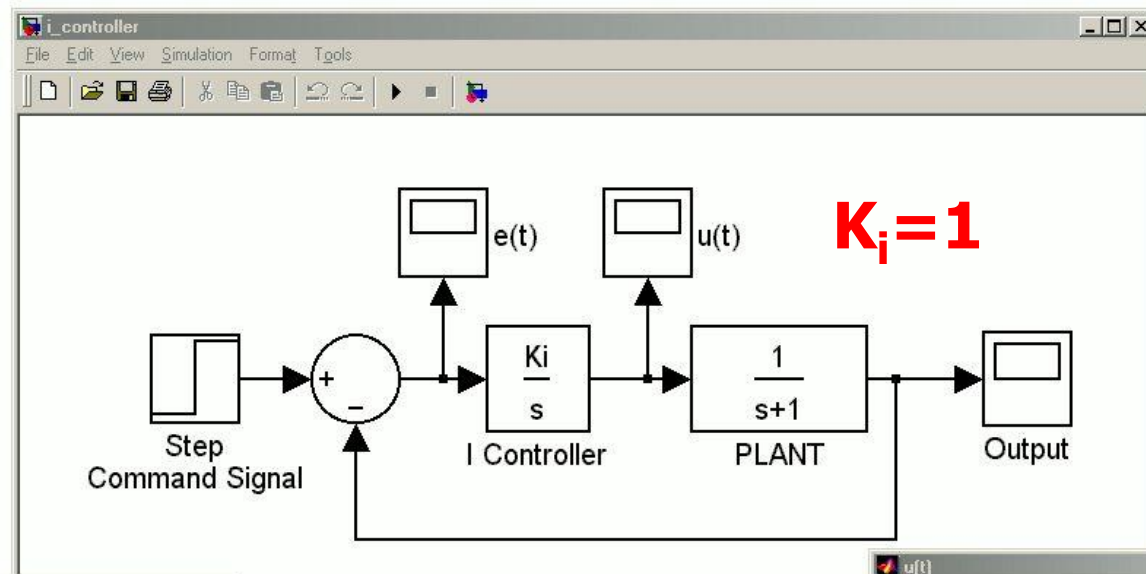
s^n	a_0	a_2	a_4	a_6	\cdot	\cdot	\cdot
s^{n-1}	a_1	a_3	a_5	a_7	\cdot	\cdot	\cdot
s^{n-2}	b_1	b_2	b_3	b_4	\cdot	\cdot	\cdot
s^{n-3}	c_1	c_2	c_3	c_4	\cdot	\cdot	\cdot
s^{n-4}	d_1	d_2	d_3	d_4	\cdot	\cdot	\cdot
\cdot	\cdot	\cdot					
\cdot	\cdot						
\cdot	\cdot						
s^2	e_1	e_2					
s^1	f_1						
s^0	g_1						



**These terms must
have the same signs
for stability**

First Example

Recall that we analyzed the following diagram in I-Controller





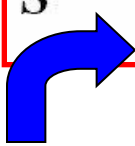
First Example

Did we have to choose $K_i=1$?

NO!

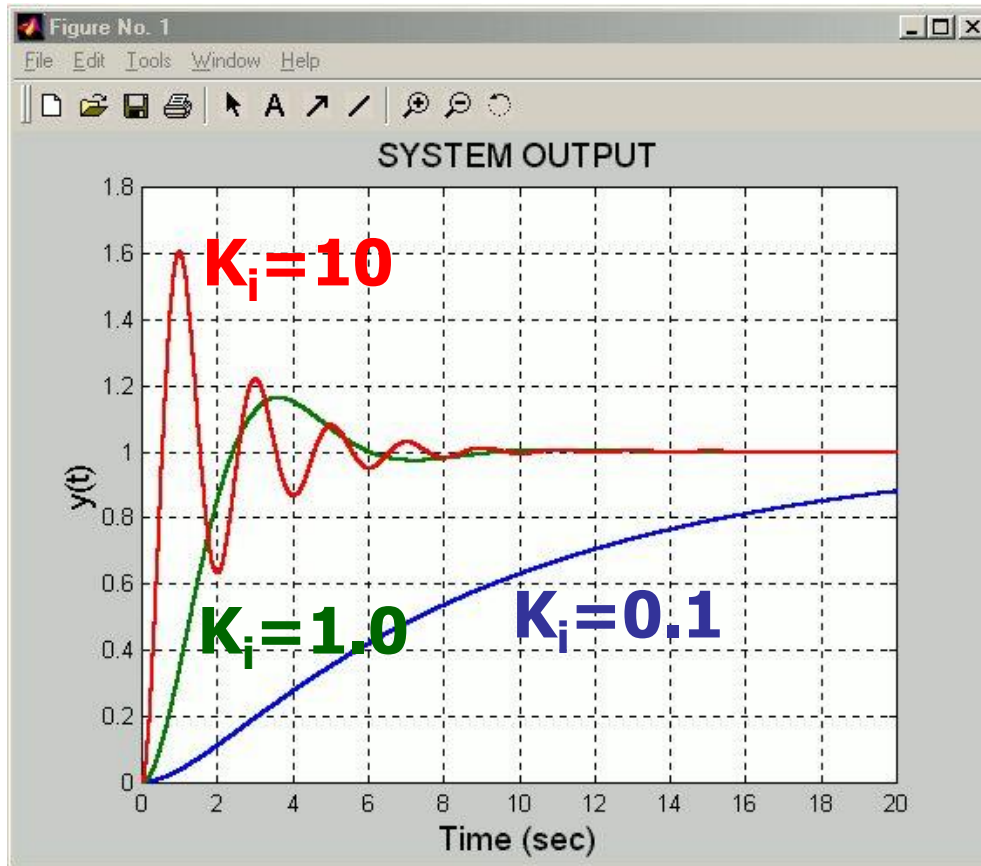
$$T(s) = \frac{K_i}{s^2 + s + K_i}$$

s^2	1	K_i
s^1	1	
s^0	K_i	



For no sign change in the first column, $K_i > 0$ is required. Any positive integral gain would work fine

First Example - System Output



Notice that what they do ultimately are the same, but how they do differ.

Small $K_i \Rightarrow$ Overdamped (Approaches very slowly)

Large $K_i \Rightarrow$ Underdamped (More quickly but with oscillations)

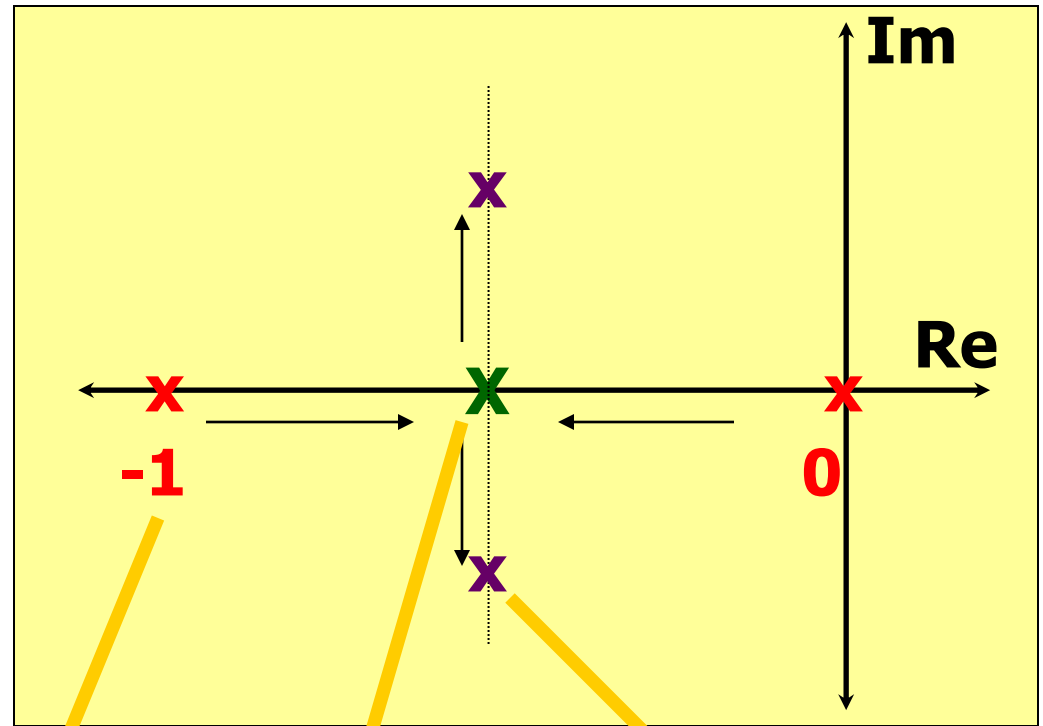
First Example

Where do the oscillations come from?

$$T(s) = \frac{K_i}{s^2 + s + K_i}$$

$$\Delta = 1 - 4K_i$$

$$s_{1,2} = -\frac{1}{2} \pm \sqrt{\frac{1}{4} - K_i}$$



$K_i = 0$

$K_i = 1/4$

$K_i > 1/4$

First Example

Where do the oscillations come from?

$$0 < K_i < 1/4$$

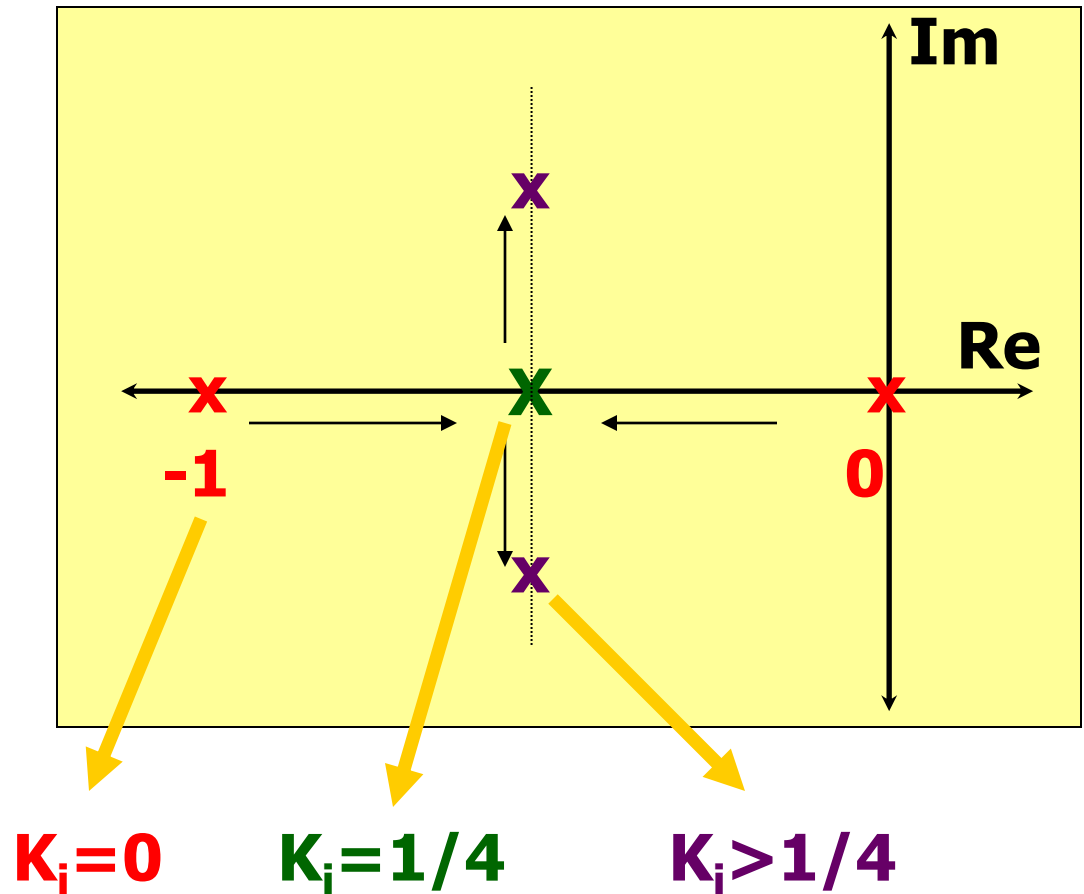
Distinct real poles

$$K_i = 1/4$$

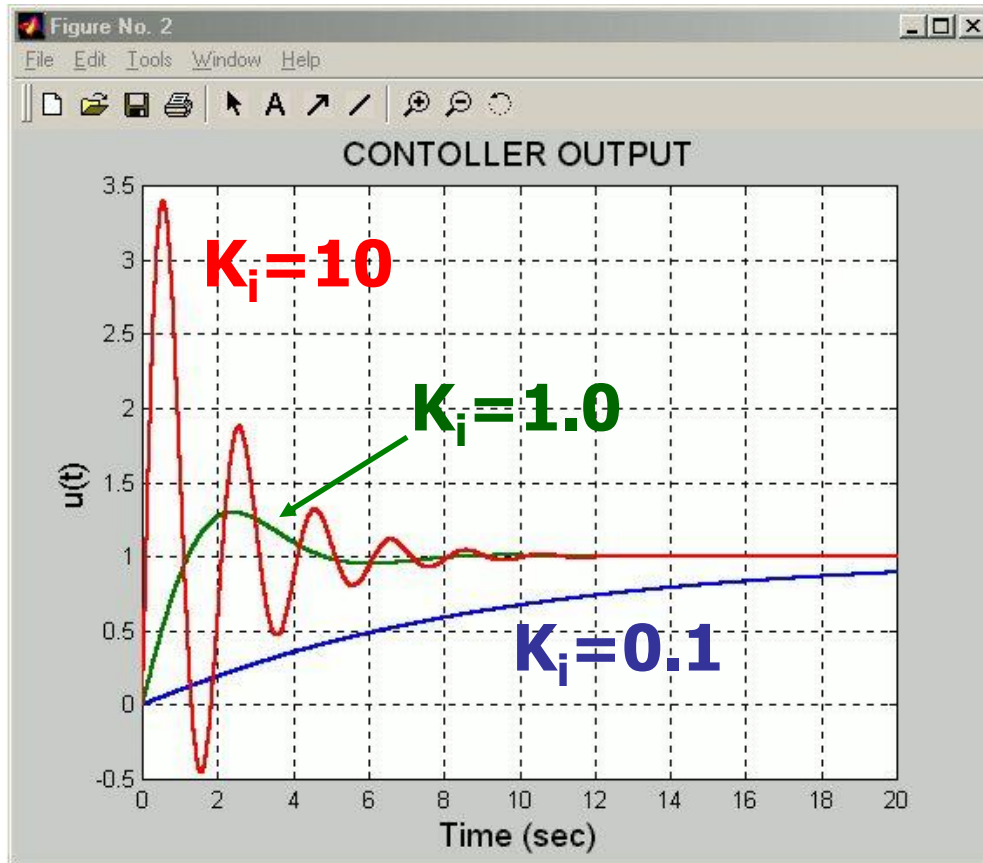
Double poles at $s = -1/2$

$$K_i > 1/4$$

Complex conjugate poles with real parts $-1/2$



First Example - Controller Output



$0 < u(t) < 1$ for $K_i = 0.1$
 $0 < u(t) < 1.3$ for $K_i = 1$
 $-0.45 < u(t) < 3.4$ for $K_i = 10$

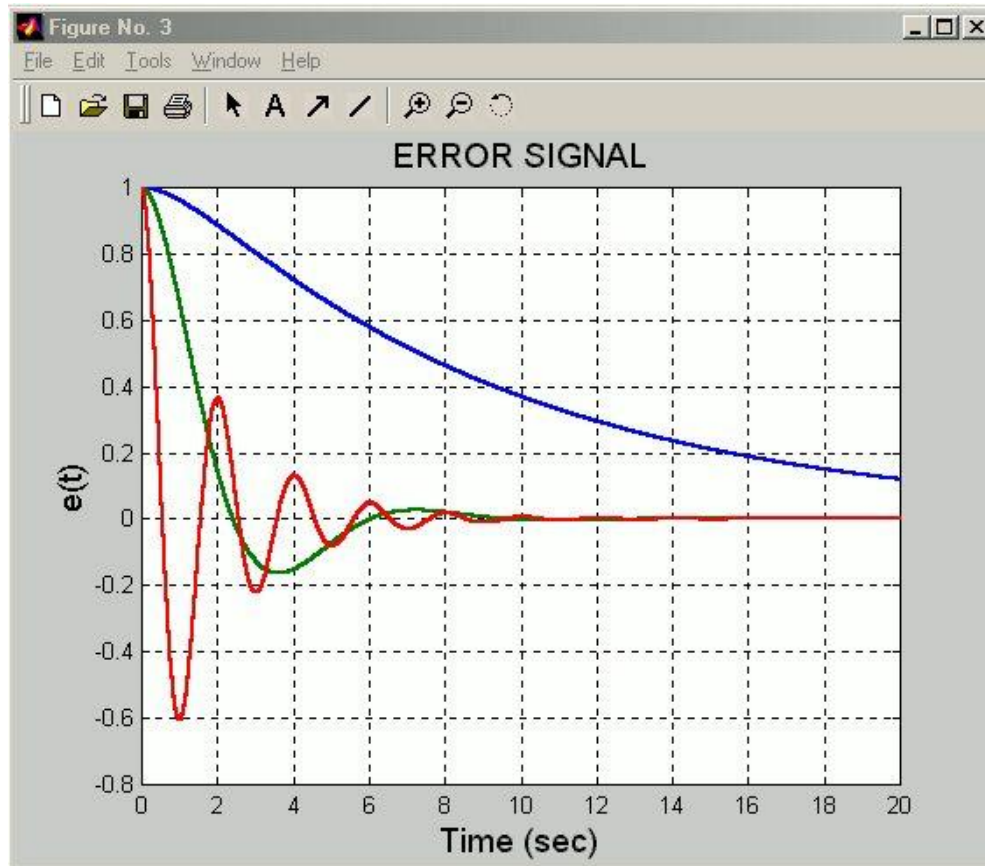
As the controller gain is increased, the range of control signal expands.

- Can your physical controller provide it?
- Is that control signal applicable?

Small $K_i \Rightarrow$ Overdamped (Approaches very slowly)

Large $K_i \Rightarrow$ Underdamped (More quickly but with oscillations)

First Example - Error Signals



How fast you want the error signal come down to zero?

This signal is the input to the controller. Is that physically applicable to your controller?



First Example - Remarks

- **We learned how to check stability of the closed loop (CL) TF**
- **A set of controller gains (K_i for this example) can result in stable CL. We analyzed what happens with different values**
- **We learned what questions to ask in the design phase**



Example-2

$$H(s) = 7 \frac{s+6}{3s^2+5s+1}$$

$$\left| \begin{array}{c|cc} s^2 & 3 & 1 \\ s^1 & 5 & \\ s^0 & * & \end{array} \right| \Rightarrow \left| \begin{array}{c|cc} s^2 & 3 & 1 \\ s^1 & 5 & 0 \\ s^0 & -\frac{1}{5}(3 \times 0 - 1 \times 5) & \end{array} \right| \Rightarrow \left| \begin{array}{c|cc} s^2 & 3 & 1 \\ s^1 & 5 & 0 \\ s^0 & 1 & \end{array} \right|$$



Example-3

$$H(s) = 2 \frac{s^2}{s^3 - 6s^2 + 11s - 6}$$

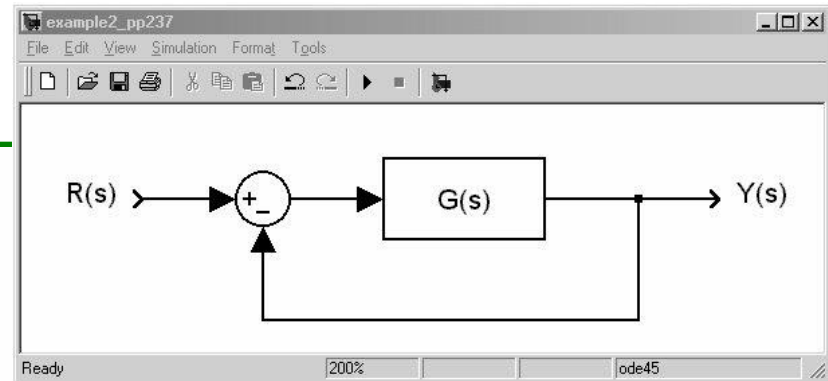
$$\begin{array}{c|cc} s^3 & 1 & 11 \\ s^2 & -6 & -6 \\ s^1 & 10 & 0 \\ s^0 & -6 & \end{array}$$

$$D(s) = (s - 1)(s - 2)(s - 3)$$

Example-4

$$G(s) = \frac{K}{s(s^2 + s + 1)(s + 2)}$$

$$T(s) = \frac{G}{1 + G} = \frac{K}{s(s^2 + s + 1)(s + 2) + K}$$



Determine the range of K for stability

The characteristic equation is

$$s^4 + 3s^3 + 3s^2 + 2s + K = 0$$

Example-4 (Textbook Ogata 3rd Ed. p.237)

$$s^4 + 3s^3 + 3s^2 + 2s + K = 0$$

s^4	1	3	K
s^3	3	2	0
s^2	$7/3$	K	
s^1	$2 - (9/7)K$		
s^0	K		

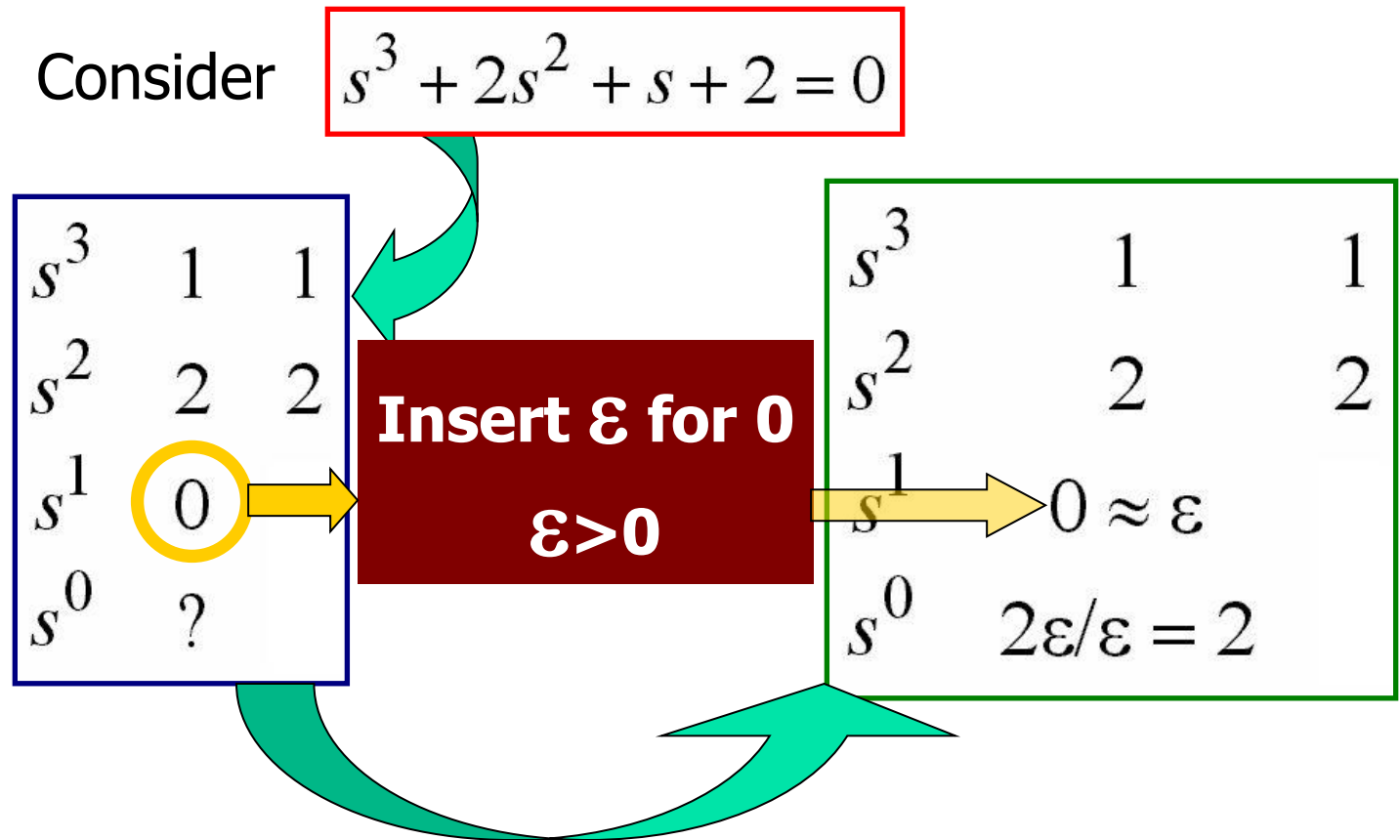
$$2 - (9/7)K > 0$$
$$K > 0$$

$$0 < K < \frac{14}{9}$$



Handling the special cases - Example 1

A zero in the first column





Handling the special cases - Example 1

A zero in the first column

■ No sign change means
no roots on the **right**
half s-plane

■ In this example, two
roots were at $s = \pm j$

$$s^3 + 2s^2 + s + 2 = 0$$

s^3	1	1
s^2	2	2
s^1	$0 \approx \varepsilon$	
s^0	$2\varepsilon/\varepsilon = 2$	



Handling the special cases - Example 2

A zero in the first column

$$s^3 - 3s + 2 = 0$$

One sign change

One sign change

s^3	1	-3
s^2	$0 \approx \varepsilon$	2
s^1	$-3 - 2/\varepsilon$	
s^0	2	

 **Two sign changes mean two roots on the right half s-plane**

$$s^3 - 3s + 2 = (s - 1)^2 (s + 2) = 0$$



Handling the special cases - Remarks

•

•

s^k positive

s^{k-1} $0 \approx \varepsilon$

s^{k-2} positive

•

•

No sign change, i.e. no roots on the right half s-plane

But, there are a pair of imaginary roots



Handling the special cases - Remarks

.		.	
.		.	
s^k	positive	s^k	negative
s^{k-1}	$0 \approx \varepsilon$	s^{k-1}	$0 \approx \varepsilon$
s^{k-2}	negative	s^{k-2}	positive
.		.	
.		.	

One sign change, i.e. there is one root on the right half s-plane from this change

Example-3 and Example 4: Use of Epsilon

$$D(s) = (s^2 + 4)(s + 1) = s^3 + s^2 + 4s + 4$$

$$\begin{array}{c|cc} s^3 & 1 & 4 \\ s^2 & 1 & 4 \\ s^1 & 0 & \\ s^0 & * & \end{array} \Rightarrow \begin{array}{c|cc} s^3 & 1 & 4 \\ s^2 & 1 & 4 \\ s^1 & \epsilon & \\ s^0 & -\frac{1}{\epsilon}(1 \times 0 - 4 \times \epsilon) & \end{array} \Rightarrow \begin{array}{c|cc} s^3 & 1 & 4 \\ s^2 & 1 & 4 \\ s^1 & \epsilon & \\ s^0 & 4 & \end{array}$$

























$$D(s) = (s^2 + 4)(s - 1) = s^3 - s^2 + 4s - 4$$

$$\begin{array}{c|cc} s^3 & 1 & 4 \\ s^2 & -1 & -4 \\ s^1 & 0 & \\ s^0 & * & \end{array} \Rightarrow \begin{array}{c|cc} s^3 & 1 & 4 \\ s^2 & -1 & -4 \\ s^1 & -\epsilon & \\ s^0 & -\frac{-1 \times 0 - (-4) \times (-\epsilon)}{-\epsilon} & \end{array} \Rightarrow \begin{array}{c|cc} s^3 & 1 & 4 \\ s^2 & -1 & -4 \\ s^1 & -\epsilon & \\ s^0 & -4 & \end{array}$$



Handling the special cases

A row is entirely zero

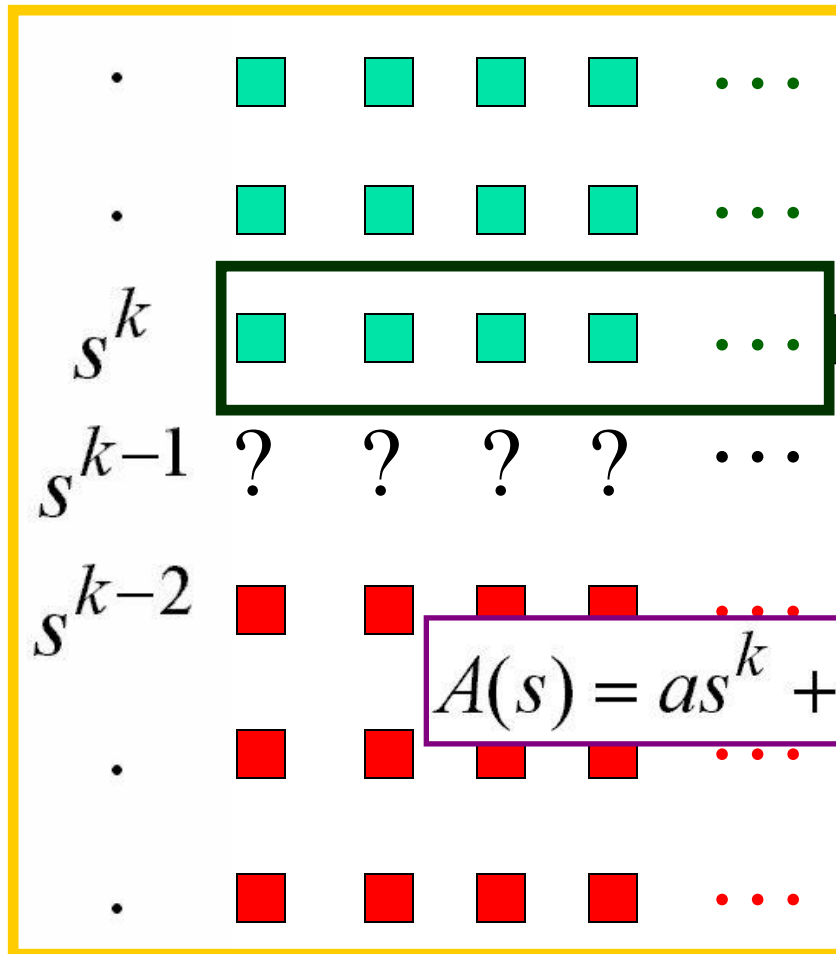
•					• • •
•					• • •
s^k					• • •
s^{k-1}	0	0	0	0	• • •
s^{k-2}					• • •
•					• • •
•					• • •

**This row is
entirely zero!**

**You cannot proceed to
calculate these terms!**

Handling the special cases

A row is entirely zero

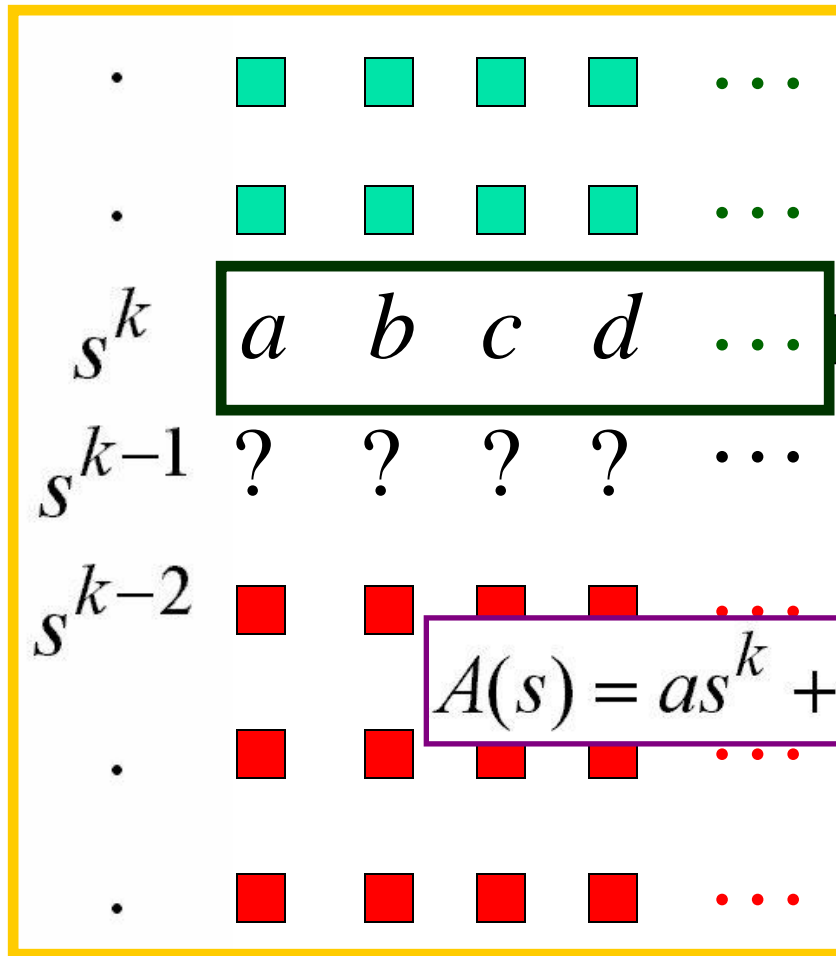


Determine the auxiliary polynomial $A(s)$ from this row

$$A(s) = as^k + bs^{k-2} + cs^{k-4} + ds^{k-6} + \dots$$

Handling the special cases

A row is entirely zero

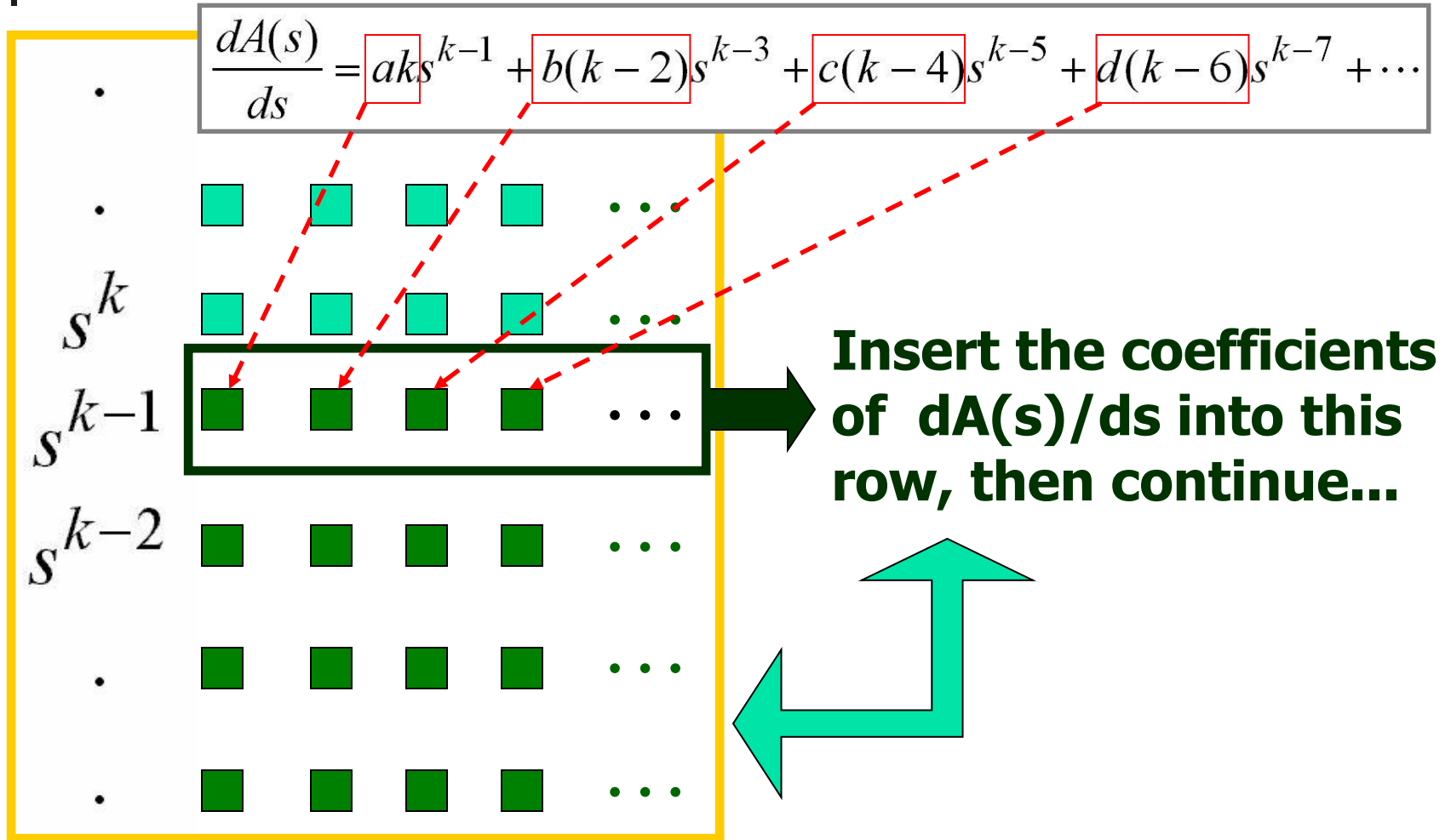


Determine the auxiliary polynomial $A(s)$ from this row

$$A(s) = as^k + bs^{k-2} + cs^{k-4} + ds^{k-6} + \dots$$

Handling the special cases

A row is entirely zero



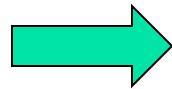


Handling the special cases - An Example

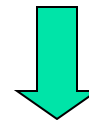
A row is entirely zero

$$s^5 + 2s^4 + 24s^3 + 48s^2 - 25s - 50 = 0$$

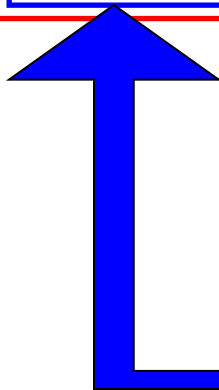
s^5	1	24	-25
s^4	2	48	-50
s^3	0	0	



$$A(s) = 2s^4 + 48s^2 - 50$$



$$\frac{dA(s)}{ds} = 8s^3 + 96s$$





Handling the special cases - An Example

A row is entirely zero

$$s^5 + 2s^4 + 24s^3 + 48s^2 - 25s - 50 = 0$$

s^5	1	24	-25
s^4	2	48	-50
s^3	8	96	
s^2	24	-50	
s^1	112.6666	0	
s^0	-50		

$$\frac{dA(s)}{ds} = 8s^3 + 96s$$

One sign change: One of the roots is in the right half s-plane



An Example

$$D(s) = s^5 + 2s^4 + 2s^3 + 4s^2 + 3s + 6$$

$\begin{array}{c ccc} s^5 & 1 & 2 & 3 \\ s^4 & 2 & 4 & 6 \\ s^3 & 0 & 0 & 0 \\ s^2 & * & * & \\ s^1 & * & & \\ s^0 & * & & \end{array}$	$A(s) = 2s^4 + 4s^2 + 6$ $\frac{dA(s)}{ds} = 8s^3 + 8s$	$\begin{array}{c ccc} s^5 & & 1 & 2 & 3 \\ s^4 & & 2 & 4 & 6 \\ s^3 & & 8 & 8 & \\ s^2 & & 2 & 6 & \\ s^1 & -16 & & & \\ s^0 & 6 & & & \end{array}$
---	--	---



Another Example

$$\begin{array}{c|cc} s^3 & 1 & 6 \\ s^2 & 3 & 1 \\ s^1 & -\frac{1}{3}(1 \times 1 - 6 \times 3) & 0 \\ s^0 & * & \end{array} \Rightarrow \begin{array}{c|cc} s^3 & 1 & 6 \\ s^2 & 3 & 1 \\ s^1 & \frac{17}{3} & 0 \\ s^0 & -\frac{1}{\frac{17}{3}}(3 \times 0 - 1 \times \frac{17}{3}) & \end{array} \Rightarrow \begin{array}{c|cc} s^3 & 1 & 6 \\ s^2 & 3 & 1 \\ s^1 & \frac{17}{3} & 0 \\ s^0 & 1 & \end{array}$$



Yet Another Example

$$\begin{array}{c|ccc} s^4 & 1 & 1 & 1 \\ s^3 & -5 & -6 & 0 \\ s^2 & -\frac{1}{5} & 1 & \\ s^1 & -31 & 0 & \\ s^0 & 1 & & \end{array}$$



Handling the special cases – Example 3

A row is entirely zero

$$\begin{array}{c|ccc} s^5 & 1 & 1 & 1 \\ s^4 & 1 & -1 & -2 \\ s^3 & 2 & 3 & \\ s^2 & -\frac{5}{2} & -2 & \\ s^1 & \frac{7}{5} & & \\ s^0 & -2 & & \end{array}$$



A Final Example

$$\begin{array}{c|cccc}
 s^6 & 1 & 4 & 1 & 1 \\
 s^5 & 2 & -1 & 6 & \\
 s^4 & \frac{9}{2} & -2 & 1 & \\
 s^3 & -\frac{1}{9} & \frac{50}{9} & & \\
 s^2 & 223 & 1 & & \\
 s^1 & \frac{11\ 151}{2007} & & & \\
 s^0 & 1 & & &
 \end{array}$$



Build the Routh Table and Find Proper K

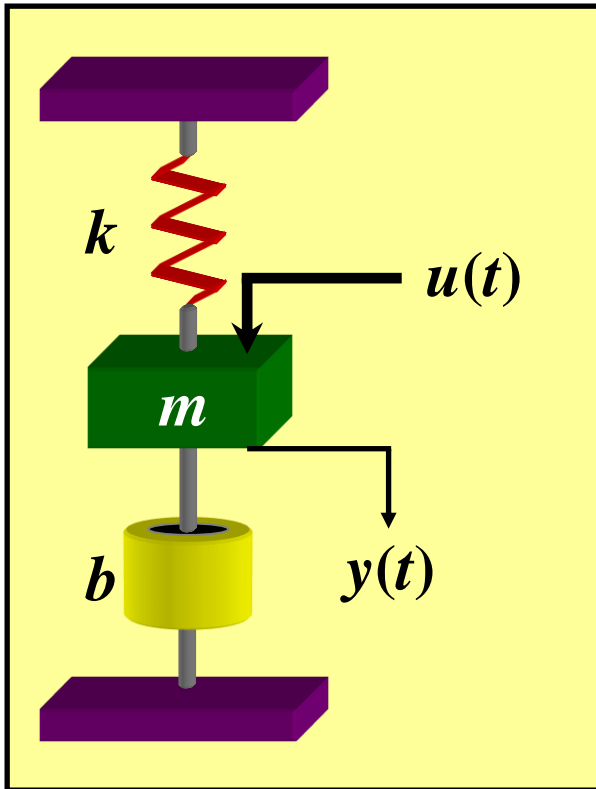
$$\begin{aligned} \text{(a)} \quad H_1(s) &= \frac{s + 1}{s^2 + Ks + 1} \\ \text{(b)} \quad H_2(s) &= \frac{s^2 + 1}{s^3 + 7s^2 + Ks + K} \\ \text{(c)} \quad H_3(s) &= \frac{K(s - 1)}{s^2 + (K - 3)s + K + 2} \end{aligned}$$



Final Remarks on Routh Criterion

- **The goal of using Routh stability criterion is to explain whether the characteristic equation has roots on the right half s -plane.**
- **A parameter (e.g. a gain) may change the locations of the CL poles, and Routh criterion lets us know for which range the CL system is stable.**

P-3 State Space Representation and Stability



Consider the mass-spring-damper system. Laws of physics lead us to

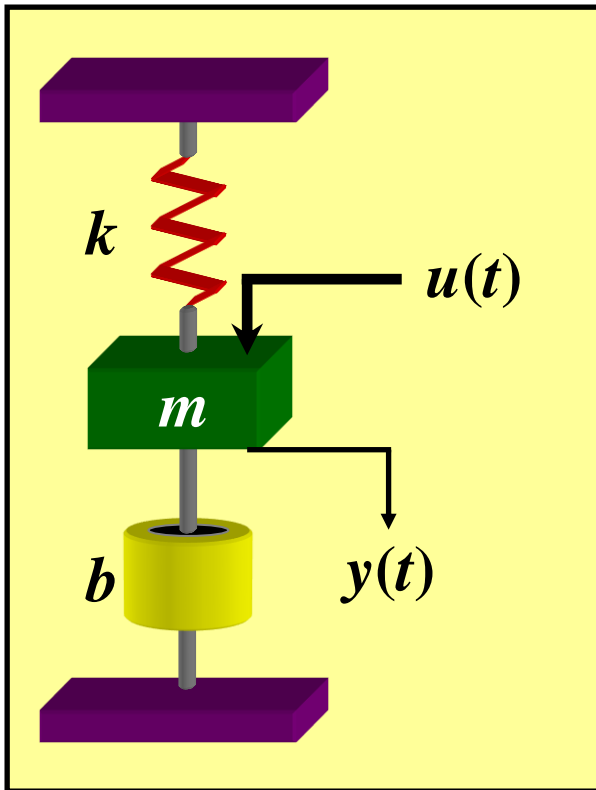
$$m\ddot{y} + b\dot{y} + ky = u$$

Let us define the state as

$$x_1(t) = y(t)$$

$$x_2(t) = \dot{y}(t)$$

State Space Representation



Dynamics

$$m\ddot{y} + b\dot{y} + ky = u$$

State

$$x_1(t) = y(t)$$

$$x_2(t) = \dot{y}(t)$$

State equation

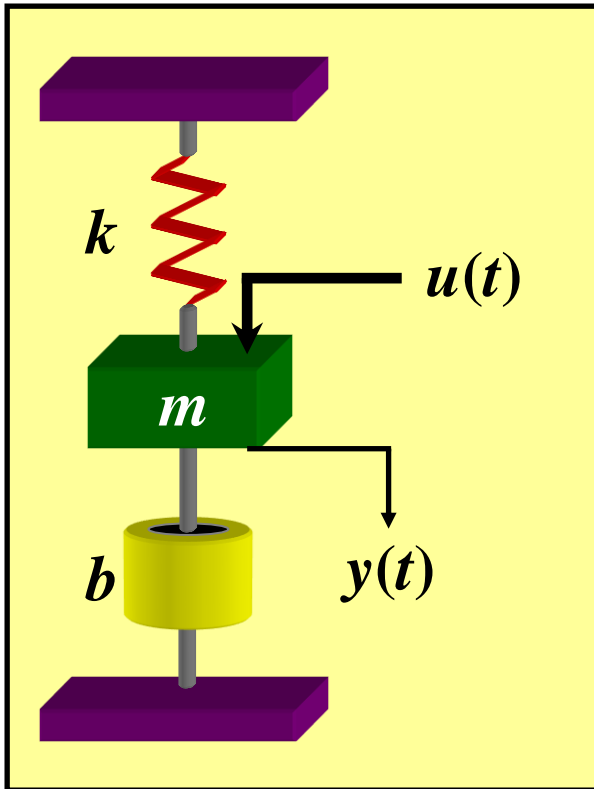
$$\dot{x}_1 = x_2$$

$$\dot{x}_2 = -\frac{k}{m}x_1 - \frac{b}{m}x_2 + \frac{1}{m}u$$

Output equation

$$y = x_1$$

State Space Representation

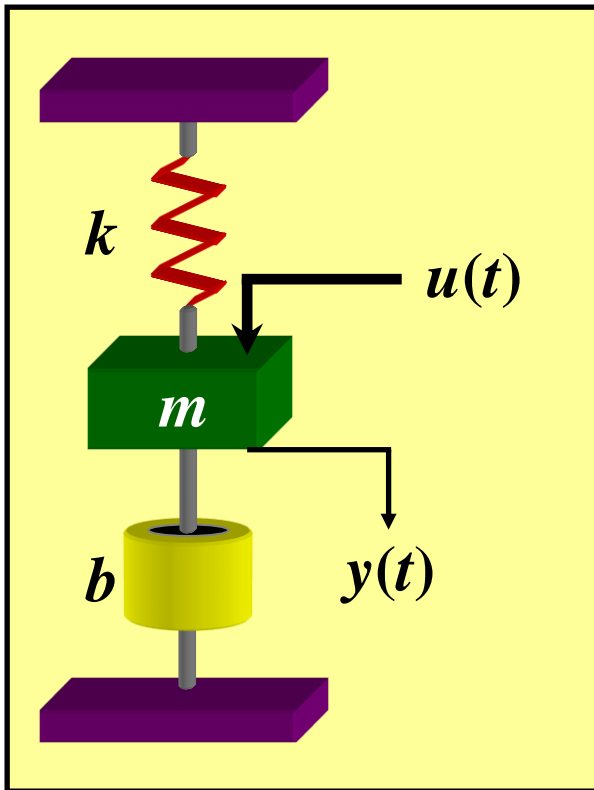


$$\begin{bmatrix} \dot{x}_1 \\ \dot{x}_2 \end{bmatrix} = \begin{bmatrix} 0 & 1 \\ -k/m & -b/m \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \end{bmatrix} + \begin{bmatrix} 0 \\ 1/m \end{bmatrix} u$$

$$y = \begin{bmatrix} 1 & 0 \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \end{bmatrix}$$

$$\begin{aligned} \dot{x} &= Ax + Bu \\ y &= Cx + Du \end{aligned}$$

Correlation between State Space Representations and Transfer Functions



$$\dot{x} = Ax + Bu$$
$$y = Cx + Du$$

$$sX(s) - x(0) = AX(s) + BU(s)$$
$$Y(s) = CX(s) + DU(s)$$

$$(sI - A)X(s) = \cancel{x(0)} + BU(s)$$
$$Y(s) = CX(s) + DU(s)$$

$$X(s) = (sI - A)^{-1}BU(s)$$
$$Y(s) = CX(s) + DU(s)$$



Correlation between State Space Representations and Transfer Functions

$$\begin{aligned} X(s) &= (sI - A)^{-1} B U(s) \\ Y(s) &= C X(s) + D U(s) \end{aligned}$$

$$\frac{Y(s)}{U(s)} = C(sI - A)^{-1} B + D$$

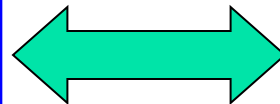
$$\frac{Y(s)}{U(s)} = \begin{bmatrix} 1 & 0 \end{bmatrix} \left\{ \begin{bmatrix} s & 0 \\ 0 & s \end{bmatrix} - \begin{bmatrix} 0 & 1 \\ -k/m & -b/m \end{bmatrix} \right\}^{-1} \begin{bmatrix} 0 \\ 1/m \end{bmatrix} + 0$$

Transfer function

$$\frac{Y(s)}{U(s)} = \frac{1}{ms^2 + bs + k}$$

Time Domain Dynamics

$$m\ddot{y} + b\dot{y} + ky = u$$





Relation between State Space Representations and Transfer Functions

What does this tell us?

Transfer Function

$$\frac{Y(s)}{U(s)} = \frac{1}{ms^2 + bs + k}$$

Time Domain Dynamics

$$m\ddot{y} + b\dot{y} + ky = u$$

$$\begin{aligned}\dot{x} &= Ax + Bu \\ y &= Cx + Du\end{aligned}$$

State Space Representation



Relation between State Space Representations and Transfer Functions



The dynamics of a linear system can be expressed in any of the forms

- **Differential equations**
- **Transfer functions**
- **State space representation**

One has to note that given the TF for a system, state space representation is not unique. Different realizations can be performed.



State Space Representation

State: The essence of past that influences the future. State is the smallest set of variables to describe the dynamics of a system

$$\begin{bmatrix} \dot{x}_1 \\ \dot{x}_2 \end{bmatrix} = \begin{bmatrix} 0 & 1 \\ -k/m & -b/m \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \end{bmatrix} + \begin{bmatrix} 0 \\ 1/m \end{bmatrix} u$$

State Variables
The dimension of the state vector is fixed for a given system



State Space Representation

The dynamics of the system can uniquely be determined with the knowledge of $x_1(t_0)$, $x_2(t_0)$ and $u(t)$ for $t \geq t_0$

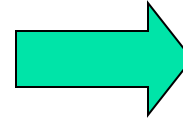
$$\begin{bmatrix} \dot{x}_1 \\ \dot{x}_2 \end{bmatrix} = \begin{bmatrix} 0 & 1 \\ -k/m & -b/m \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \end{bmatrix} + \begin{bmatrix} 0 \\ 1/m \end{bmatrix} u$$

The state space is a space whose axes are the states. For the above example, axes are x_1 axis and x_2 axis.



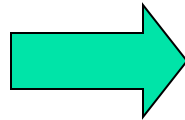
State Space Representation

In general we have a set of differential equations



$$\begin{aligned}\dot{\underline{x}} &= \underline{f}(\underline{x}, \underline{u}, t) \\ \underline{y} &= \underline{g}(\underline{x}, \underline{u}, t)\end{aligned}$$

We linearize them and get



$$\begin{aligned}\dot{\underline{x}}(t) &= A(t)\underline{x}(t) + B(t)\underline{u}(t) \\ \underline{y}(t) &= C(t)\underline{x}(t) + D(t)\underline{u}(t)\end{aligned}$$

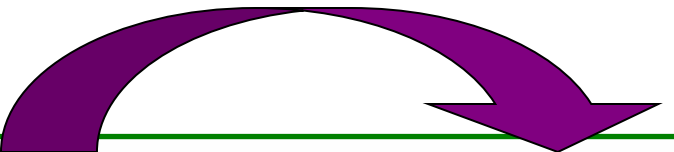
The elements of the matrices may be time-varying





State Space Representation

We simply dropped the underlines. Clearly the state will be a vector if its dimension is larger than one.


$$\begin{array}{l} \dot{\underline{x}} = A\underline{x} + B\underline{u} \\ \underline{y} = C\underline{x} + D\underline{u} \end{array} \quad \text{or} \quad \begin{array}{l} \dot{x} = Ax + Bu \\ y = Cx + Du \end{array}$$



Or may be time invariant



State Space Representation and Stability

**Assume you are
given the system**



$$\begin{aligned}\dot{x} &= Ax + Bu \\ y &= Cx + Du\end{aligned}$$



The stability of this system can be determined by checking the eigenvalues of the matrix A



Those eigenvalues are the poles of the transfer function

$$\frac{Y(s)}{U(s)} = C(sI - A)^{-1}B + D$$



State Space Representation and Stability

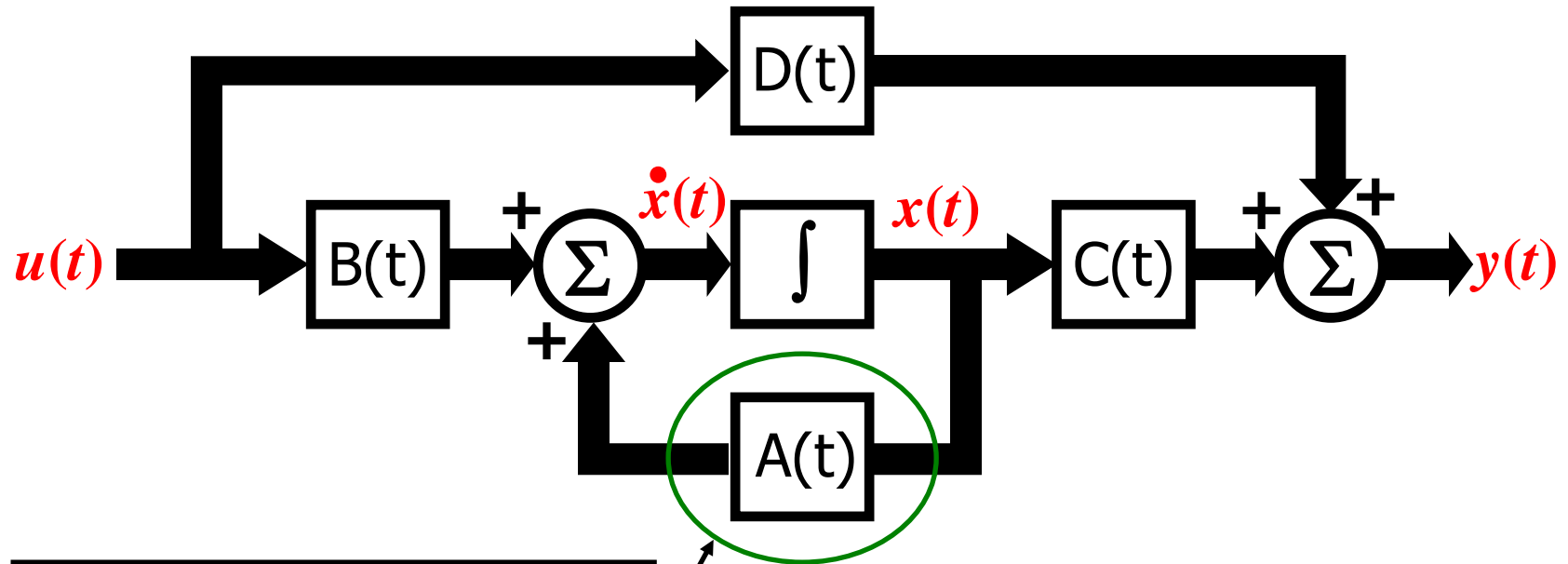
$$\text{eig}\{A\} = \{\lambda_1, \lambda_2, \lambda_3, \dots, \lambda_n\}$$

$$|\lambda I - A| = 0$$

- If $\text{Re}\{\lambda_i\} < 0$ for $i=1,2,\dots,n$
Then the system is stable
- If $\text{Re}\{\lambda_i\} > 0$ for some i
Then the system is unstable
- If $\text{Re}\{\lambda_i\} = 0$ for some i
Then the system has poles on the imaginary axis

State Space Representation and Stability

In summary...



**Check the real parts
of the eigenvalues
of $A(t)$**



An Example on Stability

$$\dot{x}_1 = x_2 - x_3$$

$$\dot{x}_2 = -x_1 + x_2 + x_3$$

$$\dot{x}_3 = ax_1 + x_2 - x_3 + u$$

$$y = x_1$$

$$T(s) = \frac{Y(s)}{U(s)} = \frac{X_1(s)}{U(s)}$$



Determine the range of a for stability



An Example on Stability

$$\dot{x}_1 = x_2 - x_3$$

$$\dot{x}_2 = -x_1 + x_2 + x_3$$

$$\dot{x}_3 = ax_1 + x_2 - x_3 + u$$

$$y = x_1$$

$$T(s) = \frac{Y(s)}{U(s)} = \frac{X_1(s)}{U(s)}$$

$$sX_1(s) = X_2(s) - X_3(s)$$

$$sX_2(s) = -X_1(s) + X_2(s) + X_3(s)$$

$$sX_3(s) = aX_1(s) + X_2(s) - X_3(s) + U(s)$$



An Example on Stability

$$sX_1(s) = X_2(s) - X_3(s)$$

$$sX_2(s) = -X_1(s) + X_2(s) + X_3(s)$$

$$sX_3(s) = aX_1(s) + X_2(s) - X_3(s) + U(s)$$

$$X_3(s) = X_2(s) - sX_1(s)$$

$$X_2(s) = -\frac{s+1}{s-2}X_1(s)$$



An Example on Stability

$$X_3(s) = X_2(s) - sX_1(s)$$

$$X_2(s) = -\frac{s+1}{s-2}X_1(s)$$

$$X_3(s) = -\frac{s^2 - s + 1}{s - 2}X_1(s)$$

An Example on Stability

$$sX_1(s) = X_2(s) - X_3(s)$$

$$sX_2(s) = -X_1(s) + X_2(s) + X_3(s)$$

$$sX_3(s) = aX_1(s) + X_2(s) - X_3(s) + U(s)$$

$$X_2(s) = -\frac{s+1}{s-2} X_1(s)$$

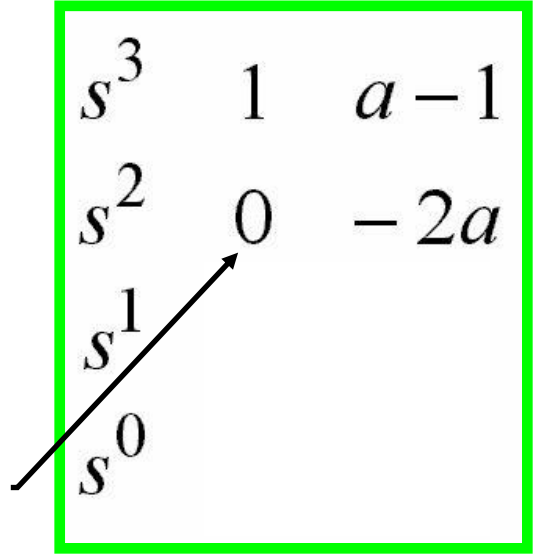
$$X_3(s) = -\frac{s^2 - s + 1}{s-2} X_1(s)$$



An Example on Stability

$$T(s) = \frac{2 - s}{s^3 + (a - 1)s - 2a}$$

Remember what to do now!



s^3	1	$a - 1$
s^2	0	$-2a$
s^1		
s^0		



An Example on Stability

$$T(s) = \frac{2 - s}{s^3 + (a - 1)s - 2a}$$

s^3	1	$a - 1$
s^2	ε	$-2a$
s^1	$[\varepsilon(a - 1) + 2a] / \varepsilon$	0
s^0	$-2a$	

An Example on Stability

$$T(s) = \frac{2-s}{s^3 + (a-1)s - 2a}$$

**This term
becomes
negative**

$$a < 0$$

s^3	1	$a-1$
s^2	ε	$-2a$
s^1	$a(1+2/\varepsilon)-1$	0
s^0	$-2a$	

An Example on Stability

$$T(s) = \frac{2-s}{s^3 + (a-1)s - 2a}$$

s^3	1	$a-1$
s^2	ε	$-2a$
s^1	$a(1+2/\varepsilon)-1$	0
s^0	$-2a$	

$$\begin{aligned} a &> 1/[1+2/\varepsilon] \\ \varepsilon &> 0 \text{ and } \varepsilon \approx 0 \\ a &> 0 \end{aligned}$$

**This term
becomes
negative**



An Example on Stability

$$T(s) = \frac{2 - s}{s^3 + (a - 1)s - 2a}$$

$$A = \begin{bmatrix} 0 & 1 & -1 \\ -1 & 1 & 1 \\ a & 1 & -1 \end{bmatrix}$$

The system is unstable regardless of the value of a . In other words, A has at least one eigenvalue in the right half s -plane



Can this system have poles on the imaginary axis?

$$T(s) = \frac{2 - s}{s^3 + (a - 1)s - 2a}$$

Assume the answer is yes... Then for $s=j\alpha$ the denominator must be zero, i.e.

$$\begin{aligned}(j\alpha)^3 + (a - 1)(j\alpha) - 2a &= 0 \\ j(-\alpha^3 + (a - 1)\alpha) - 2a &= 0\end{aligned}$$

No value of a can lead to zero real and imaginary parts simultaneously



Can this system have complex conjugate poles on the imaginary axis?

$$T(s) = \frac{2 - s}{s^3 + (a - 1)s - 2a}$$

The answer is no. Only one pole passes through the origin when $a=0$.

Watch now...

