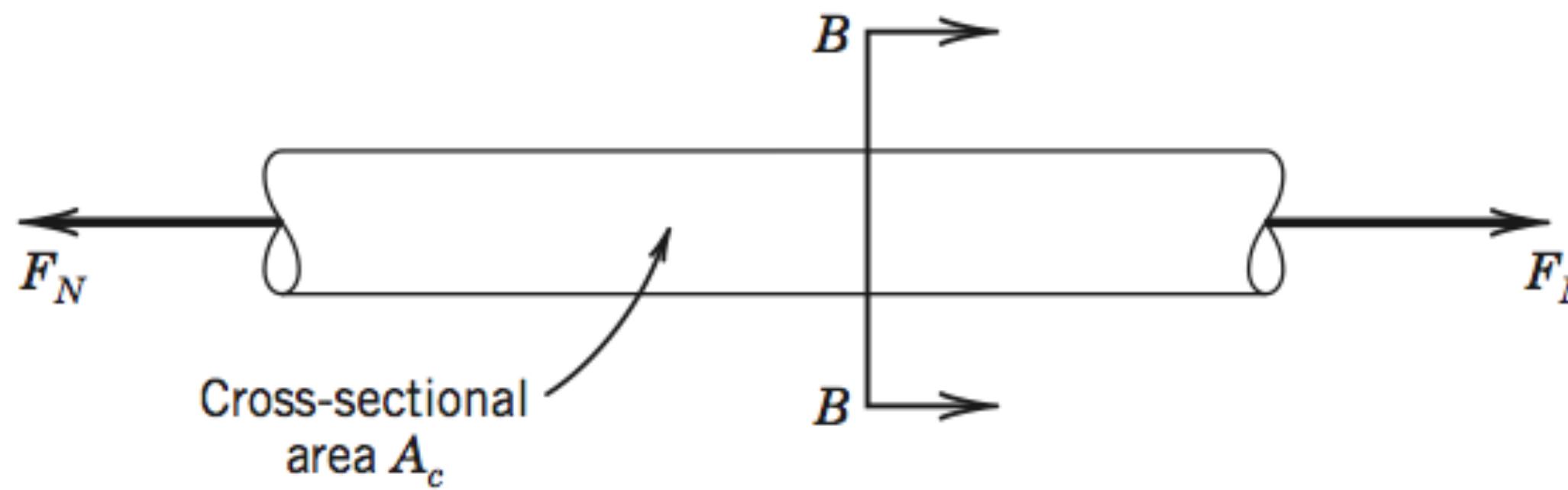


Measuring Stress, Strain, and Force

Rick Sellens

Applications

- Stress is hard to measure, but you can infer it from strain (MECH 221 Solids, MECH 270 Materials)
- Strain will tell you how mechanical systems are deforming under stress
- Force is key to simple measurements like weighing systems, and more complex dynamic loads (MECH 228 Dynamics)
- **Want something we could attach to a beam and know how much it has deformed under load**



$$\text{Poisson's Ratio } v_P = -\frac{\text{Lateral strain}}{\text{Axial strain}} = -\frac{\epsilon_L}{\epsilon_a}$$



$$\epsilon_a = \delta L / L$$

Strain is the fractional elongation, usually in micrometres/metre or microstrain

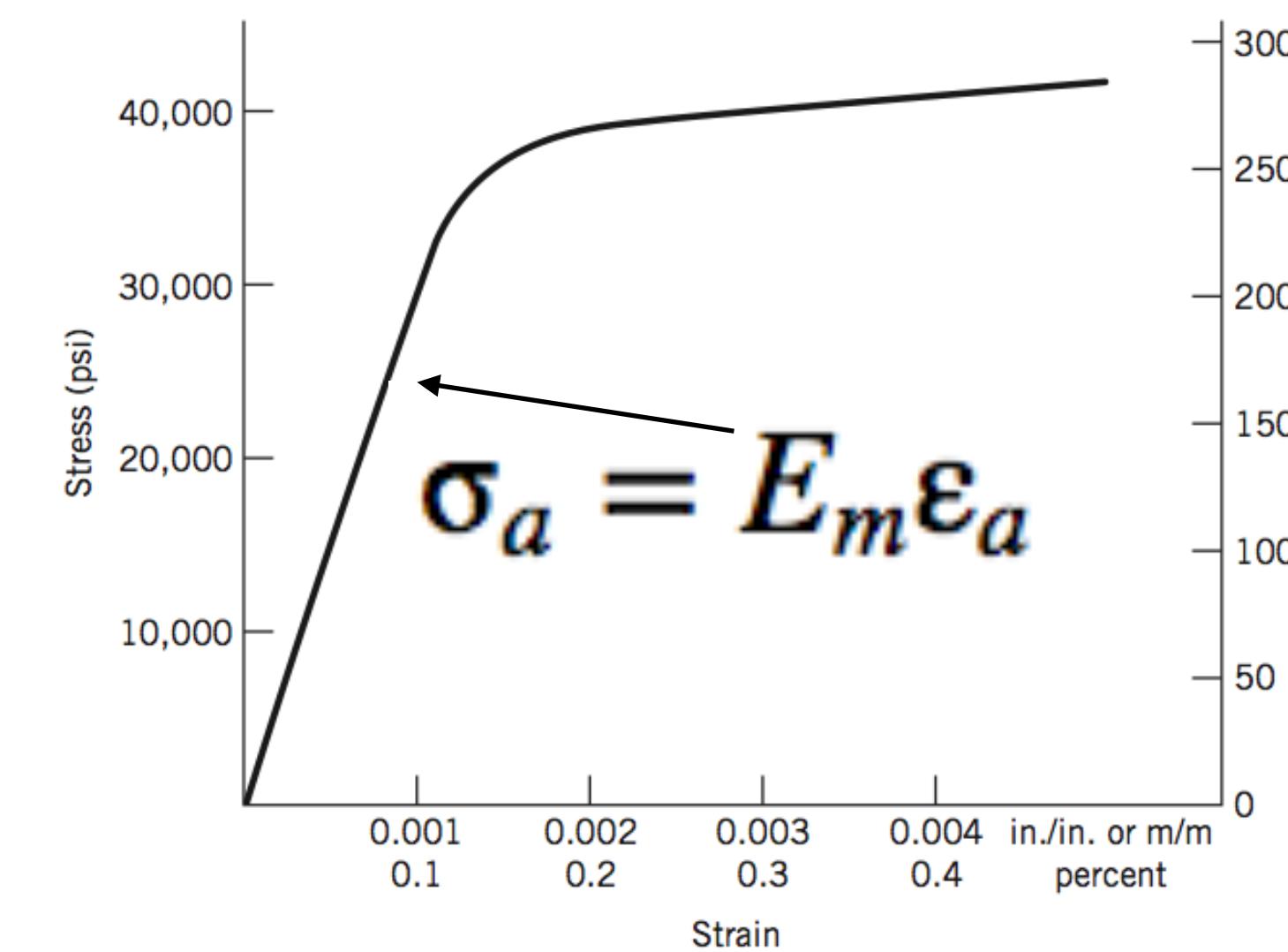
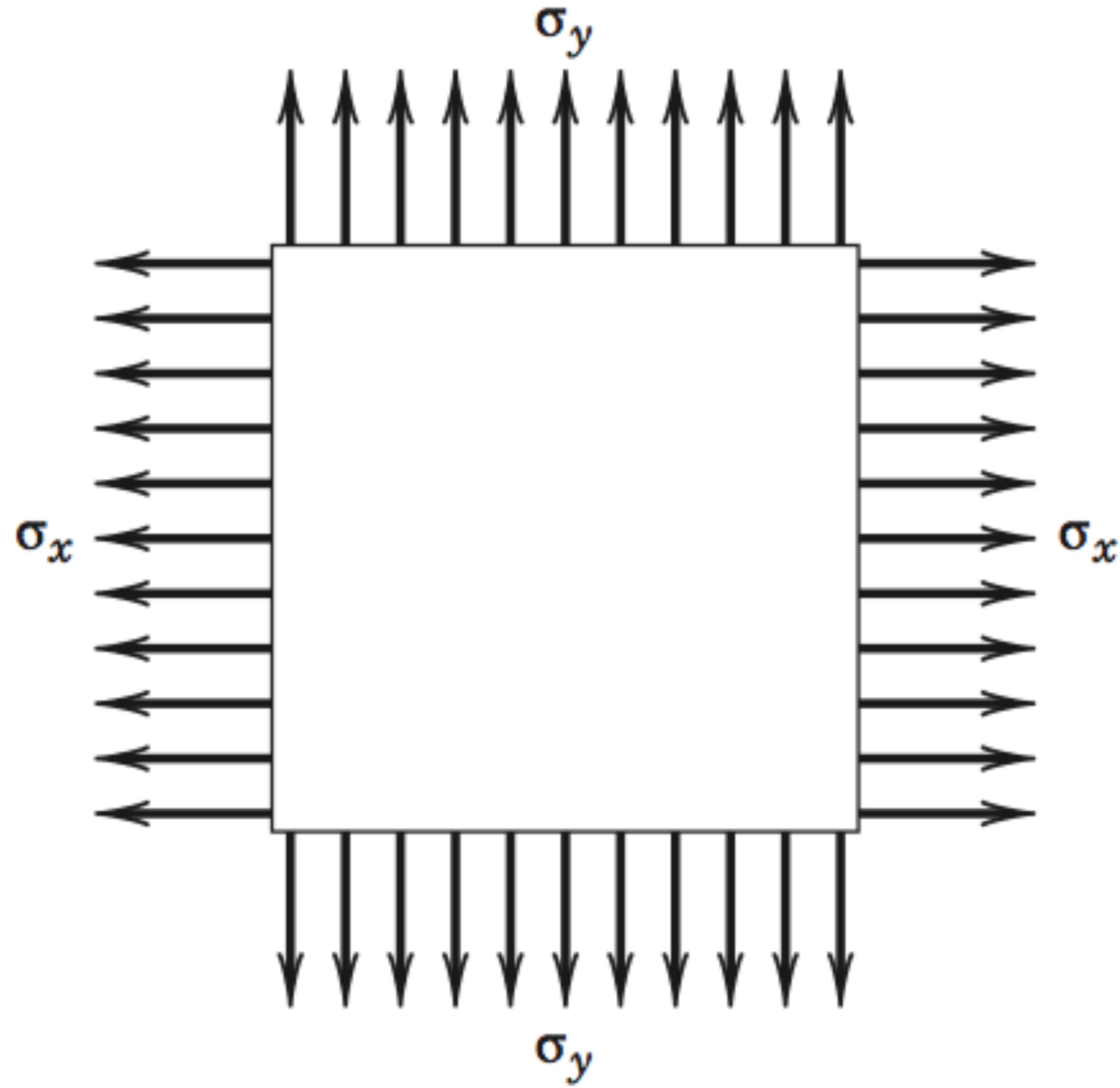


Figure 11.1 Free-body diagram illustrating internal forces for a rod in uniaxial tension.

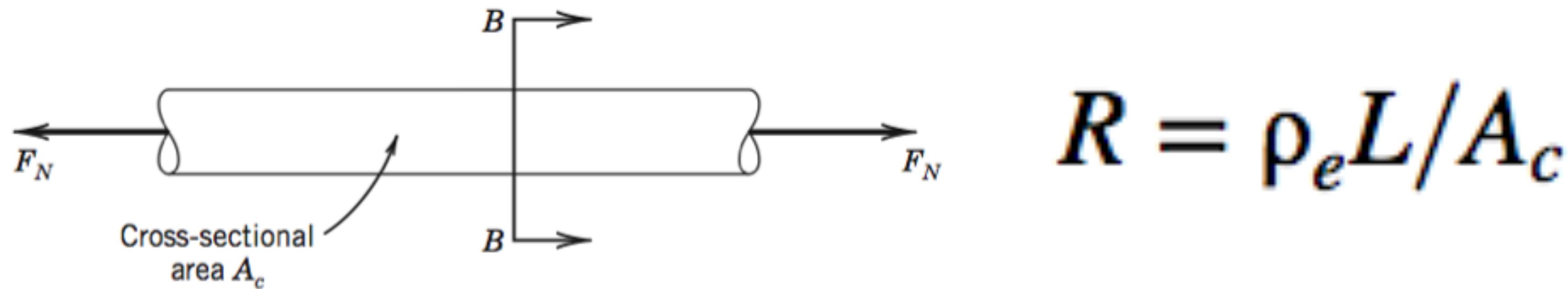
Figure 11.2 A typical stress-strain curve for mild steel.



Ideally we could
make our gauge
sensitive to only one
direction

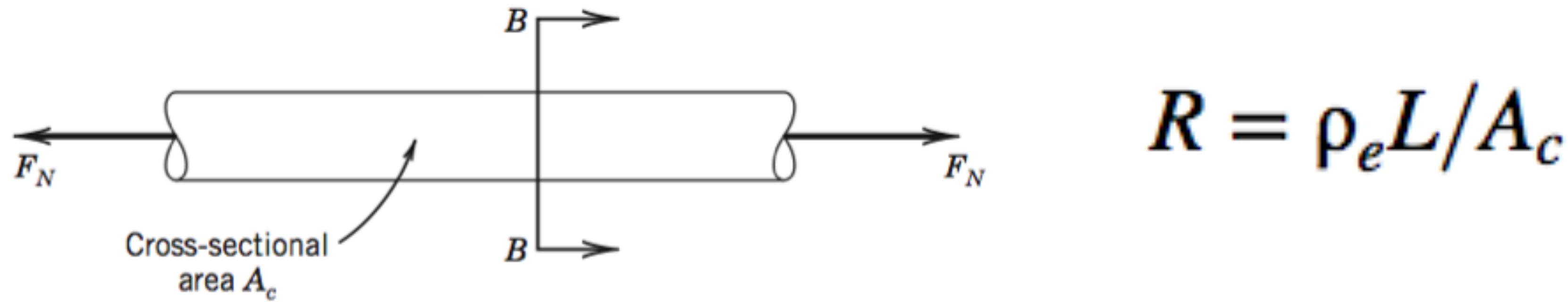
Figure 11.3 Biaxial state of stress.

Electrical Resistance of a Bar of Metal



- Resistivity is the inverse of conductivity, ohms/metre, low for copper, higher for steel
- The longer the bar, the higher the resistance
- The bigger the transverse area, the lower the resistance
- More complicated for high currents, so don't go there...

Apply a Load to the Bar



- Strain increases the length,
- decreases the diameter (Poisson's ratio),
- distorts the crystal structure, changing the resistivity (piezo resistive effects)
- all of which will increase the resistance of the bar

Change in Resistance

$$R = \rho_e L / A_c$$

$$dR = \frac{\partial R}{\partial L} dL + \frac{\partial R}{\partial A_c} dA_c + \frac{\partial R}{\partial \rho_e} d\rho_e$$

$$dR = \frac{\rho_e}{A_c} dL - \frac{\rho_e L}{A_c^2} dA_c + \frac{L}{A_c} d\rho_e$$

$$dR = \frac{A_c (\rho_e dL + L d\rho_e) - \rho_e L dA_c}{A_c^2} \quad (11.8)$$

which may be expressed in terms of Poisson's ratio as

$$\frac{dR}{R} = \frac{dL}{L} (1 + 2v_p) + \frac{d\rho_e}{\rho_e} \quad (11.9)$$

and resistivity is linear

Hence, the changes in resistance are caused by two basic effects: the change in geometry as the length and cross-sectional area change and the change in the value of the resistivity, ρ_e . The dependence of resistivity on mechanical strain is called piezoresistance and may be expressed in terms of a piezoresistance coefficient, π_1 , defined by

$$\pi_1 = \frac{1}{E_m} \frac{d\rho_e/\rho_e}{dL/L} \quad (11.10)$$

With this definition, the change in resistance may be expressed

$$dR/R = dL/L(1 + 2v_p + \pi_1 E_m) \quad (11.11)$$

at least if we choose our materials carefully

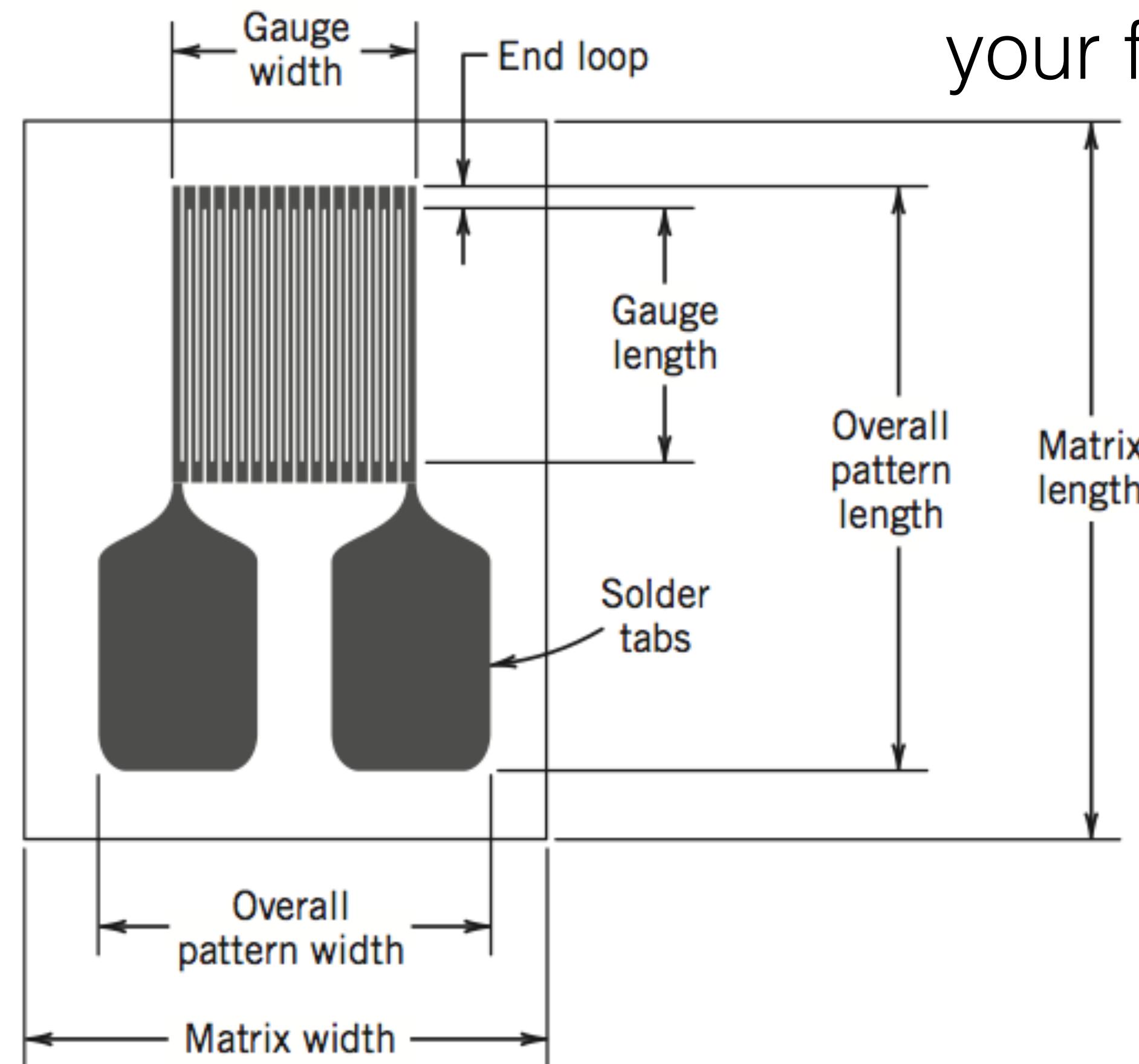
Bottom Line

$$\Delta R \propto \Delta L$$

$$\frac{\Delta R}{R} \propto \frac{\Delta L}{L} = \epsilon_a$$

Measure small changes in R and we
measure small changes in L

Foil Strain Gauge



smaller than
your finger nail

Thin, sensitive
elements oriented
vertically

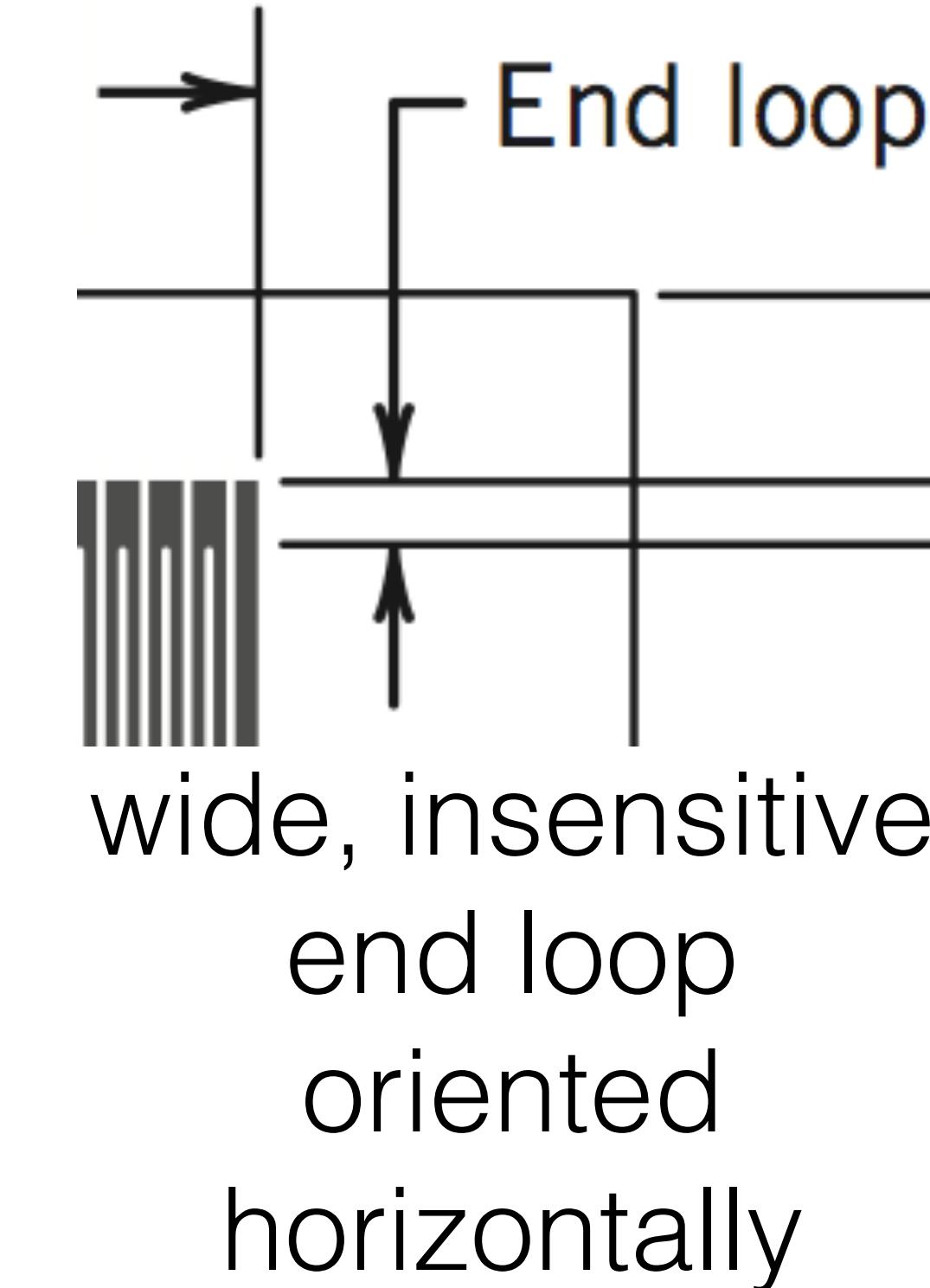
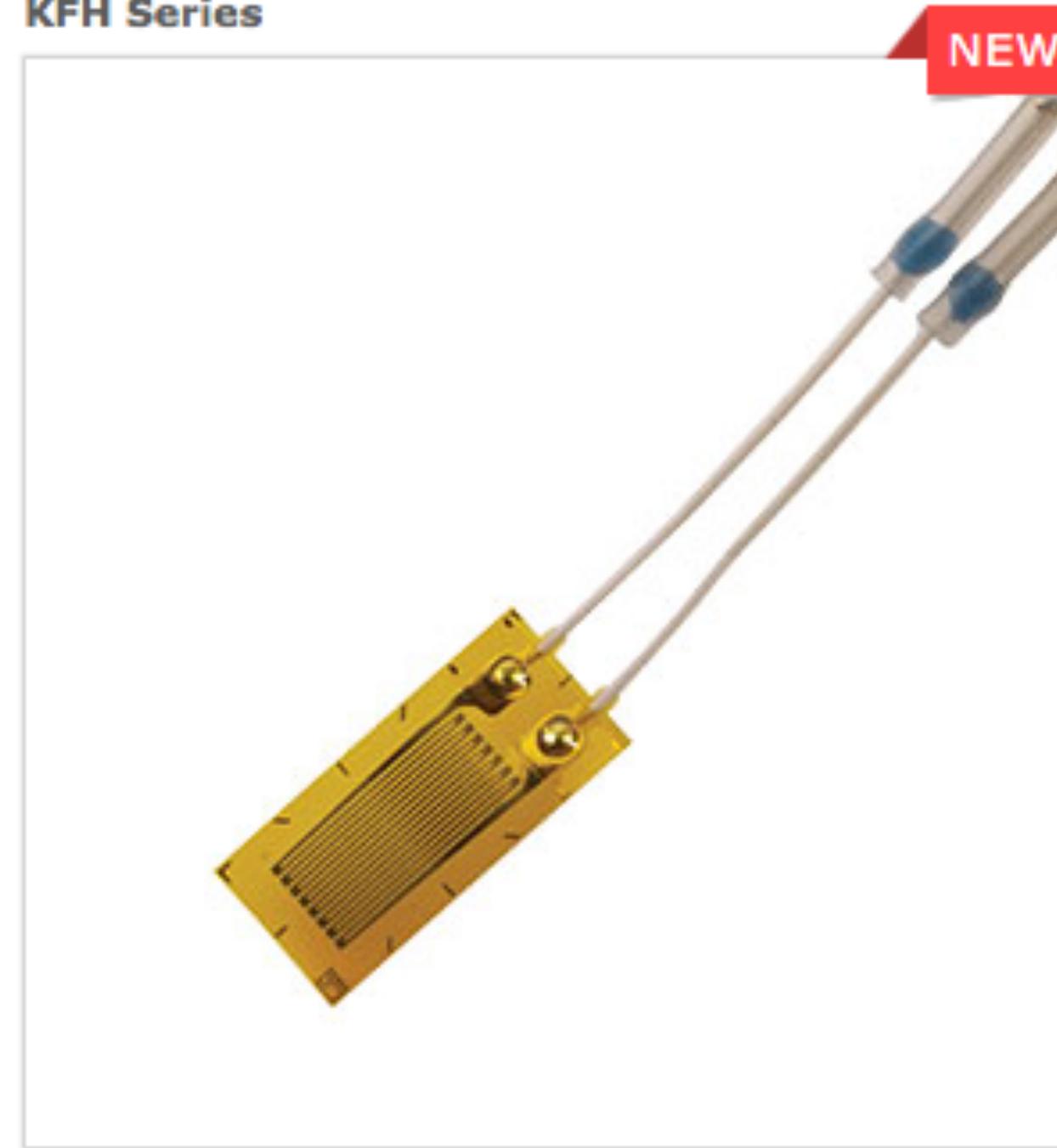


Figure 11.5 Construction of a typical metallic foil strain gauge. (Courtesy of Micro-Measurements, Raleigh, NC, USA.)

Foil Strain Gauges

thin conducting foil on flexible plastic carrier

KFH Series



NEW

CAD 206.00

KFH-3-350-C1-11L3M3R

PLACE ORDER

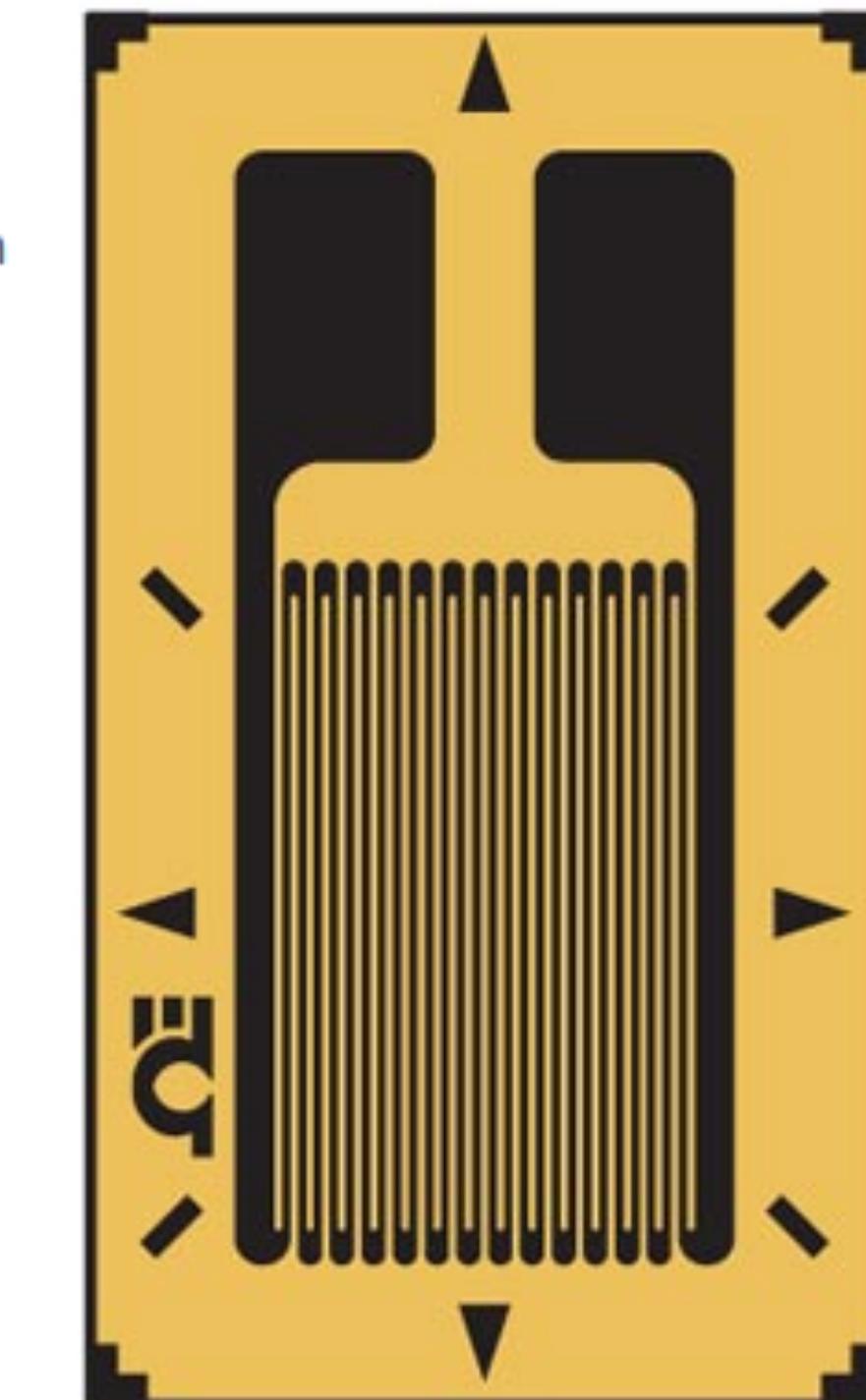
- Pre-Wired Gages Make Installations Easy!
- No Soldering at the Measuring Point
- Linear Gages, 0.3 mm to 20 mm Grids
- XY Gages (Tee Rosettes) 0.6 to 6 mm Grids
- 0°/45°/90° Planar Rosettes 0.6 to 6 mm Grids
- Each Gage has 50 mm of PTFE Cable before Transitioning to AWG 28 Leads to Prevent Leads from Adhering During Installation
- Rugged Polyimide Carrier
- Fully Encapsulated Gages for Protection from the Environment

PRE WIRED STRAIN GAGES

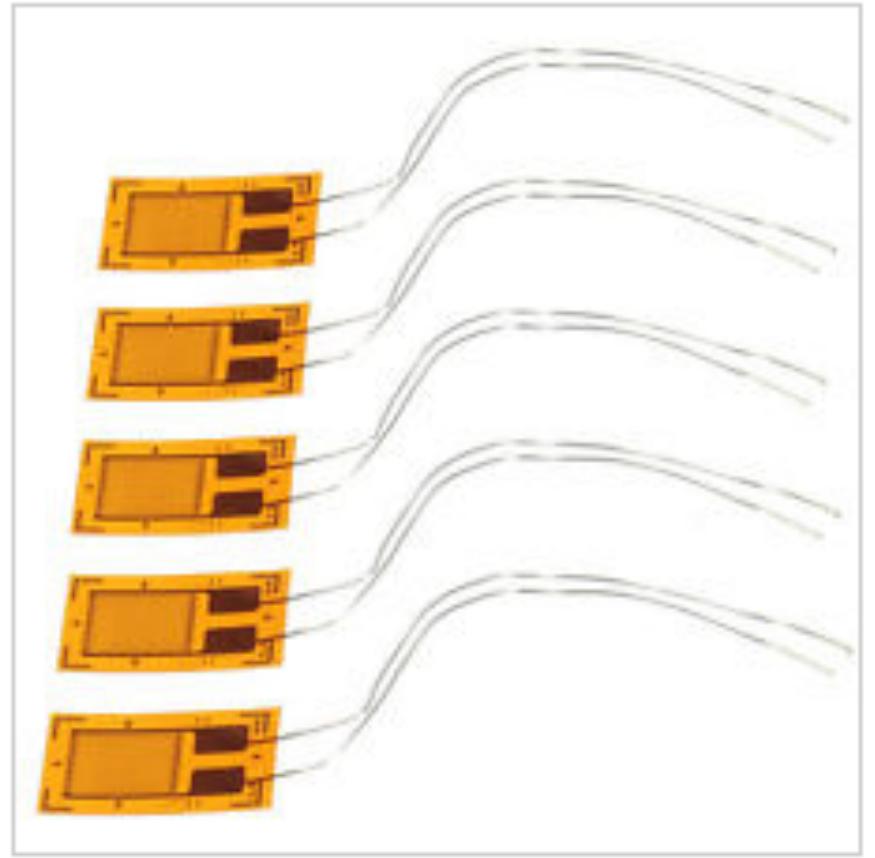


Strain Gages, Accessories and Instrumentation -
[View related products](#)

packages of 10



http://www.omega.ca/pptst_eng/KFH.html



5Pcs BF350-3AA Type Constantan Metal Foil Resistance Steel Strain Gauge 350Ω

\$4.44

Buy It Now

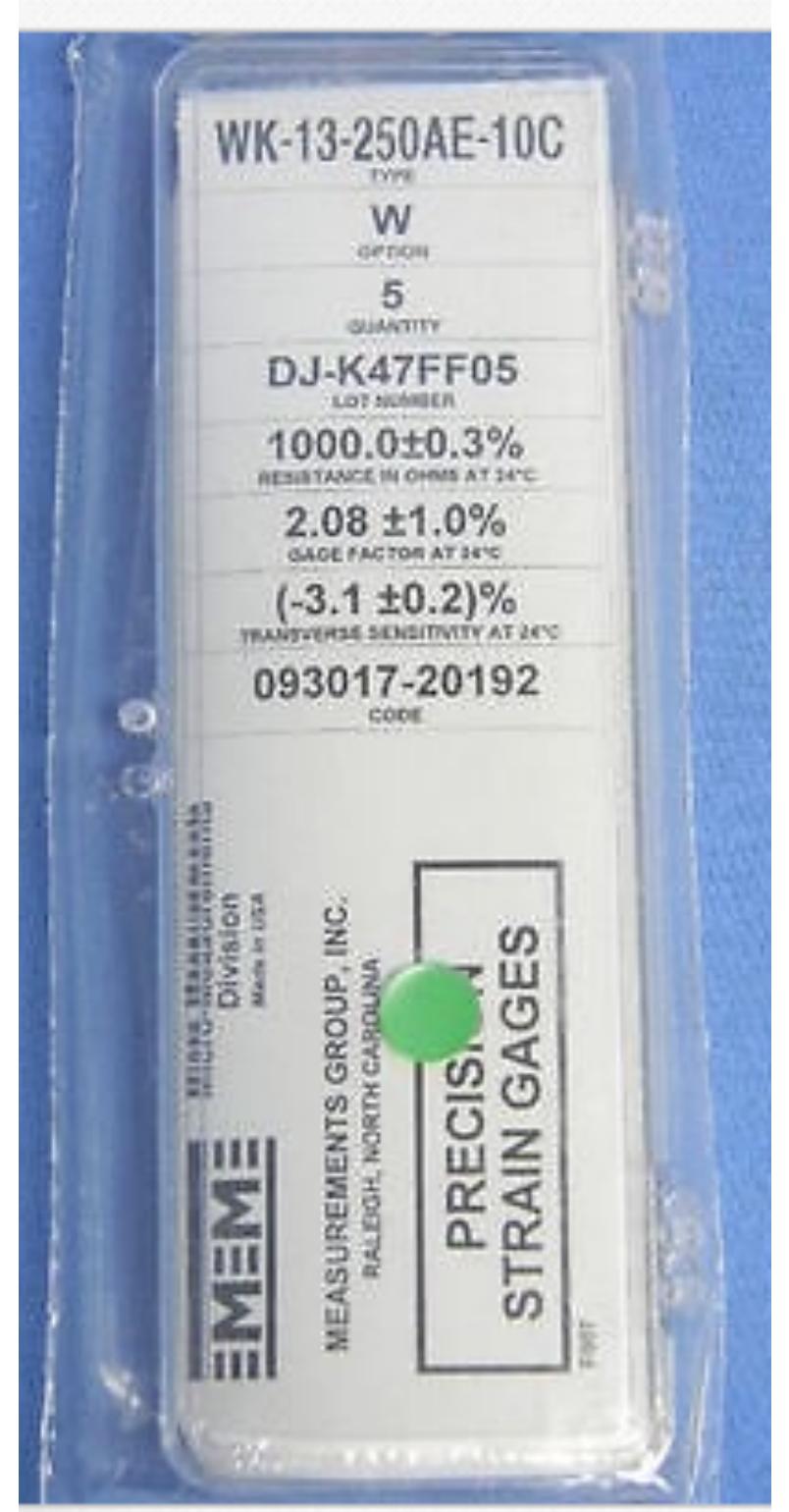
16 watching | 🔥 223 sold

5 x BF350 high-precision resistance strain gauges. BF350-3AA type constantan metal foil resistance strain gauge. Strain limit: 2.0%. Made of copper foil. Resistance: 350 / -0.1 Ω. High accuracy, good...

Gauge Factor Provided by Manufacturer

Gauge Factor

The change in resistance of a strain gauge is normally expressed in terms of an empirically determined parameter called the gauge factor (GF). For a particular strain gauge, the gauge factor is supplied by the manufacturer. The gauge factor is defined as



$$GF \equiv \frac{\delta R/R}{\delta L/L} = \frac{\delta R/R}{\epsilon_a} \quad (11.12)$$

GF is typically ~ 2 so the resistance change is about twice as big as the change in length

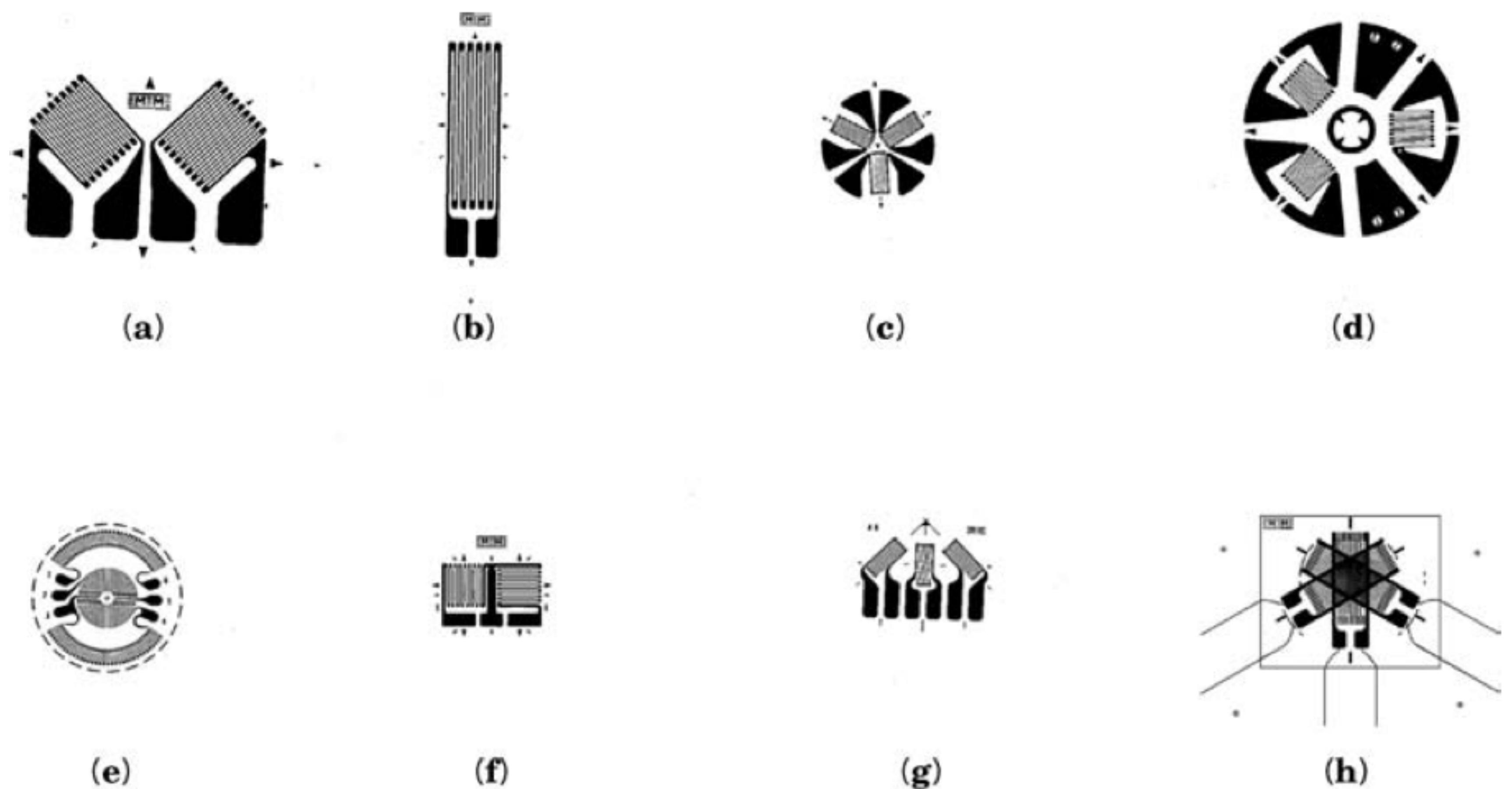
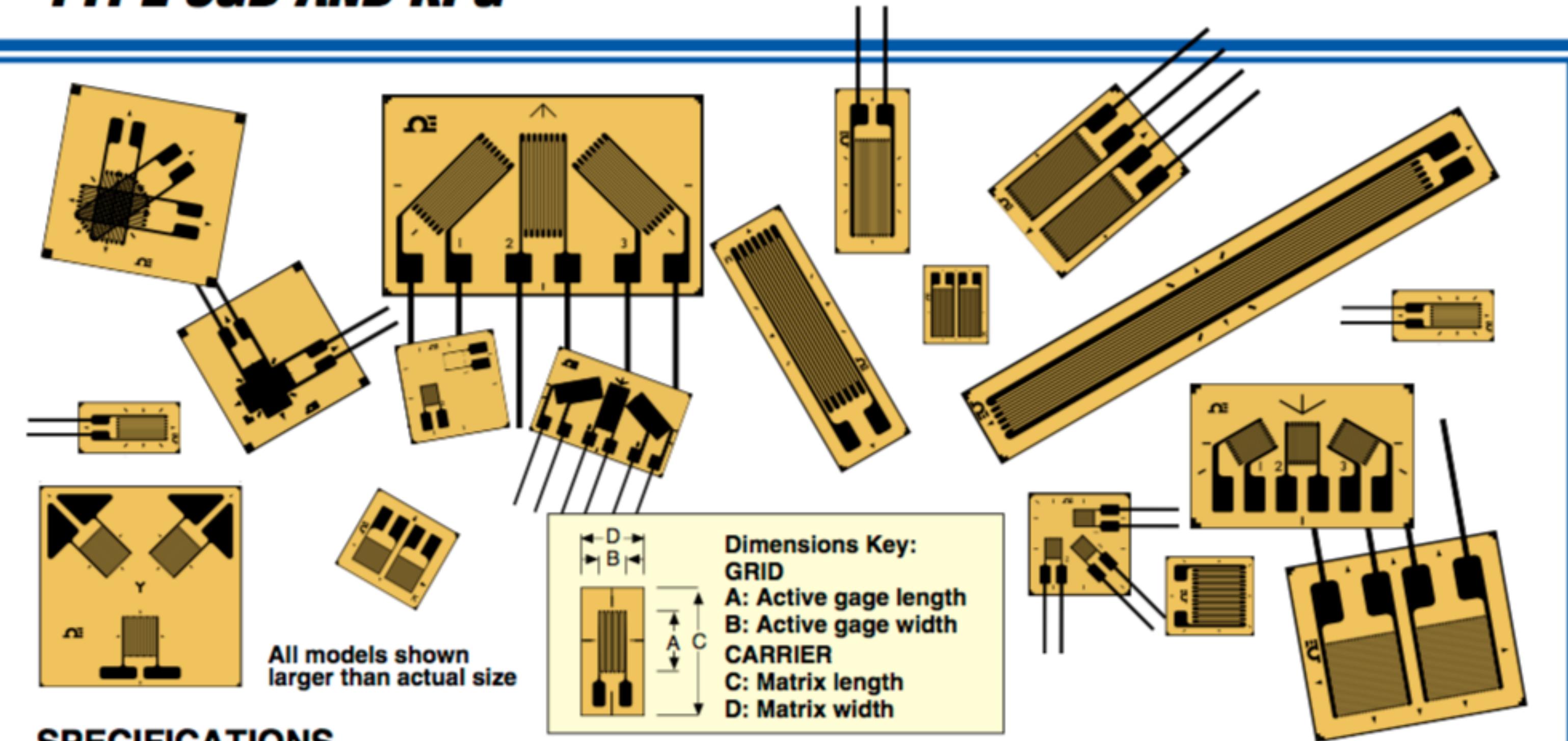


Figure 11.6 Strain gauge configurations. (a) Torque Rosette; (b) Linear Pattern; (c) Delta Rosette; (d) Residual Stress Pattern; (e) Diaphragm Pattern; (f) Tee Pattern; (g) Rectangular Rosette; (h) Stacked Rosette. (Courtesy of Micro-Measurements, Raleigh, NC, USA.)

OMEGA® STRAIN GAGE SPECIFICATIONS CHART

TYPE SGD AND KFG



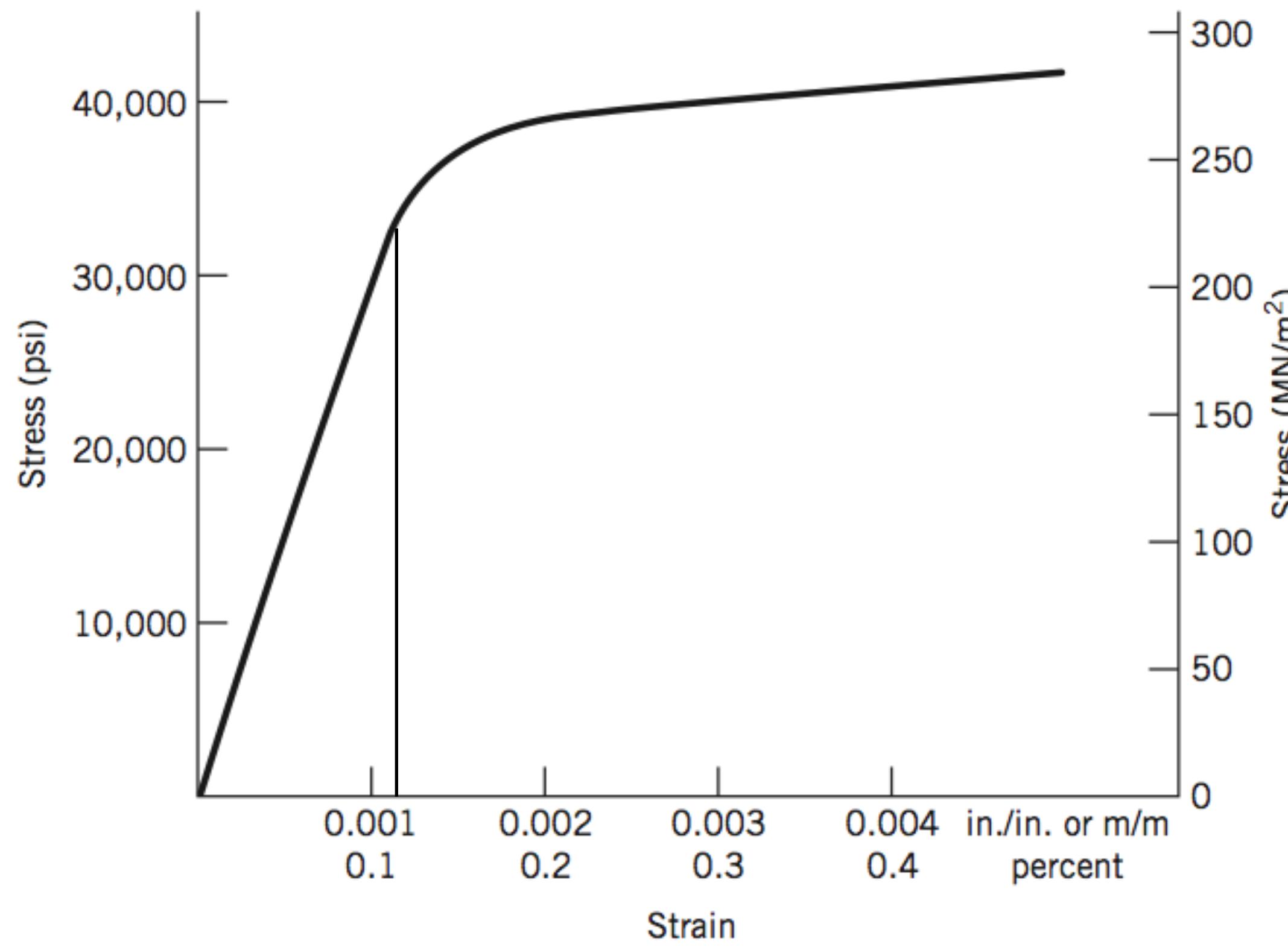
SPECIFICATIONS

	SGD SERIES	KFG SERIES—PRE-WIRED
Foil Measuring Grid	Constantan foil 5 microns thick	Constantan foil 6 microns thick
Carrier	Polyimide	Kapton®
Substrate Thickness	20 microns	15 microns
Cover Thickness	25 microns	9 microns
Connection Dimensions: mm (inch)	Solder pads or ribbon leads, tinned copper flat wire 30 L x 0.1 D x 0.3 mm W (1.2 x 0.004 x 0.012")	Pre-wired, 2 or 3 leads 27 AWG strand polyvinyl insulation 1 x 2 mm (0.04 x 0.08")
Nominal Resistance	Stated in "To Order" box	120 ± 0.4 or 350Ω
Resistance Tolerance Per Package	$\pm 0.15\%$ to $\pm 0.5\%$ depending on gage spec	0.3%
Gage Factor (Actual Value Printed on Each Package)	$2.0 \pm 5\%$	$2.10 \pm 10\%$
Gage Factor Tolerance Per Package	1.00%	1.00%

THERMAL PROPERTIES		
Reference Temperature	23°C (73°F)	23°C (73°F)
SERVICE TEMPERATURE		
Static Measurements	-75 to 200°C (-100 to 392°F)	-20 to 100°C (-4 to 212°F)
Dynamic Measurements	-75 to 200°C (-100 to 392°F)	-20 to 100°C (-4 to 212°F)
TEMPERATURE CHARACTERISTICS		
Steel (and Certain Stainless Steels)	11 ppm/°C (6.1 ppm/°F)	10.8 ppm/°C (6 ppm/°F)
Aluminum	23 ppm/°C (12.8 ppm/°F)	—
Uncompensated	±20 ppm/°C (11.1 ppm/°F)	—
Temperature Compensated Range	-5 to 120°C (5 to 248°F)	10 to 80°C (50 to 176°F)
Tolerance of Temp Compensation	2 ppm/°C (1.0 ppm/°F)	1 ppm/°C (0.5 ppm/°F)
MECHANICAL PROPERTIES		
Maximum Strain	3% or 30,000 microstrain	5% or 50,000 microstrain
Hysteresis	Negligible	Negligible
Fatigue (at ±1500 microstrain)	>10,000,000 cycles	>10,000,000 cycles
Smallest Bending Radius	3 mm ($\frac{1}{8}$ "")	3 mm ($\frac{1}{8}$ "")
Transverse Sensitivity	—	Stated on each package

How big is the resistance change?

The maximum possible load of interest in non-destructive testing is yield



- Yield in mild steel is happening around 0.001 mm/mm, or about 1 mm/m
- With a gauge factor of about 2, that would result in a change of about 0.002 ohms/ohm
- A 100 ohm gauge would rise to 100.2 ohms, or drop to 99.8 ohms

Figure 11.2 A typical stress-strain curve for mild steel.

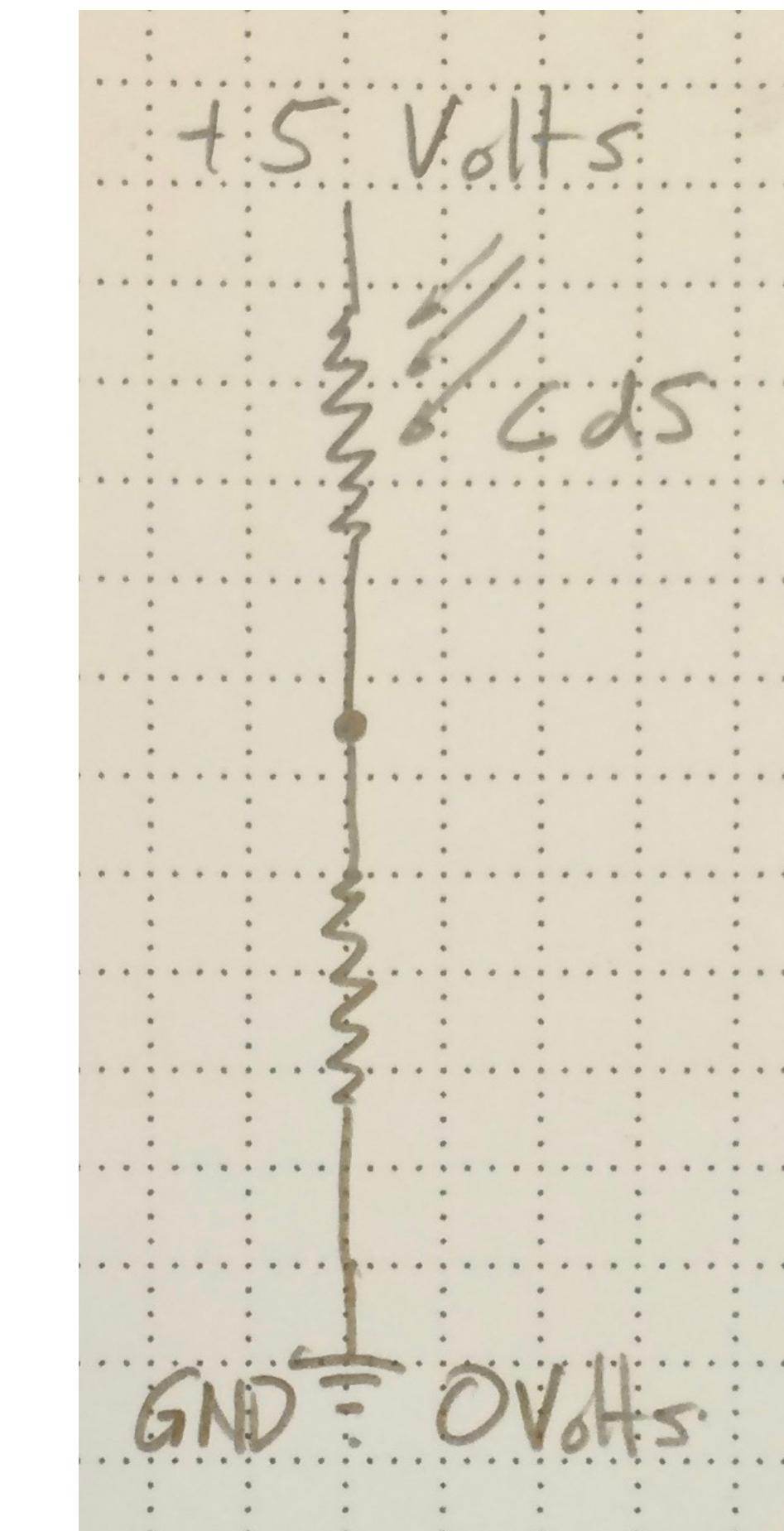
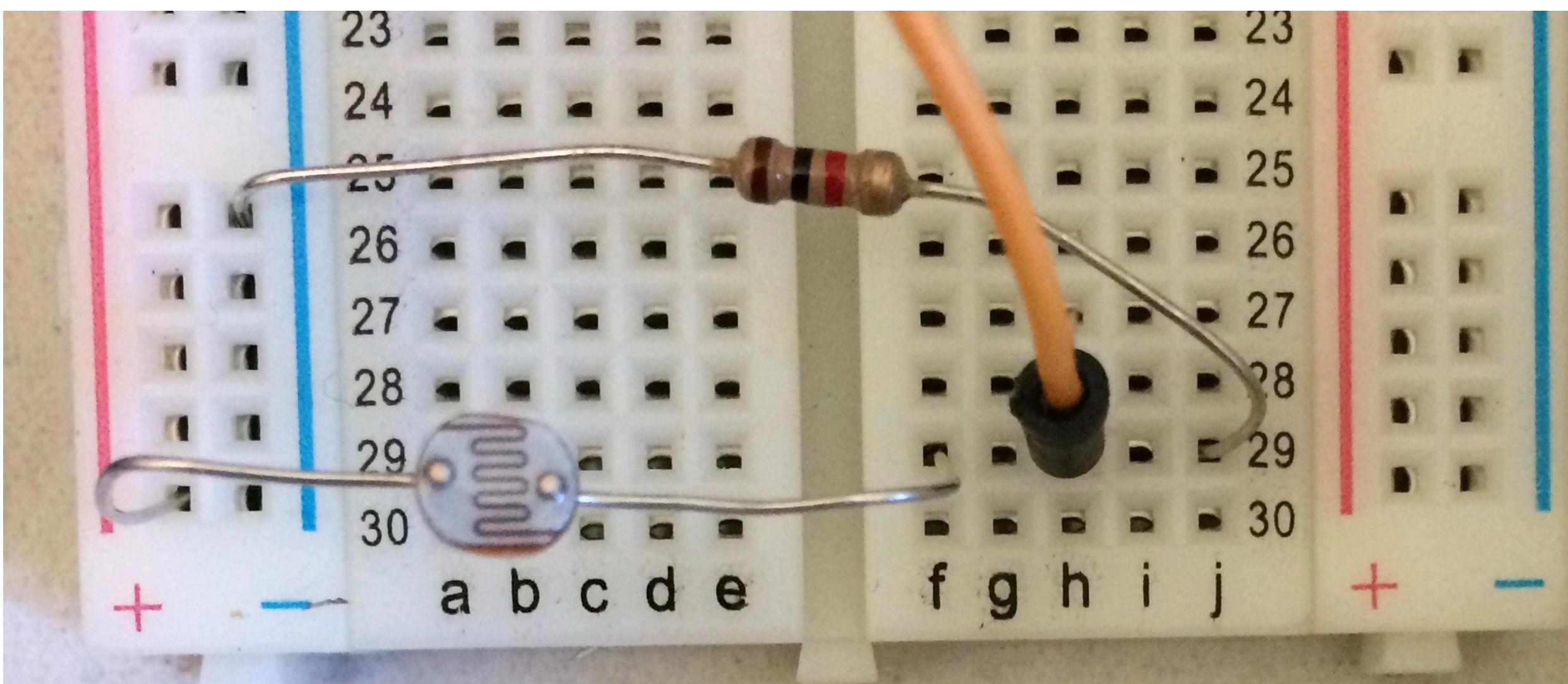
Voltage Divider for CdS Photocell or Thermistor

Resistance varies strongly with light

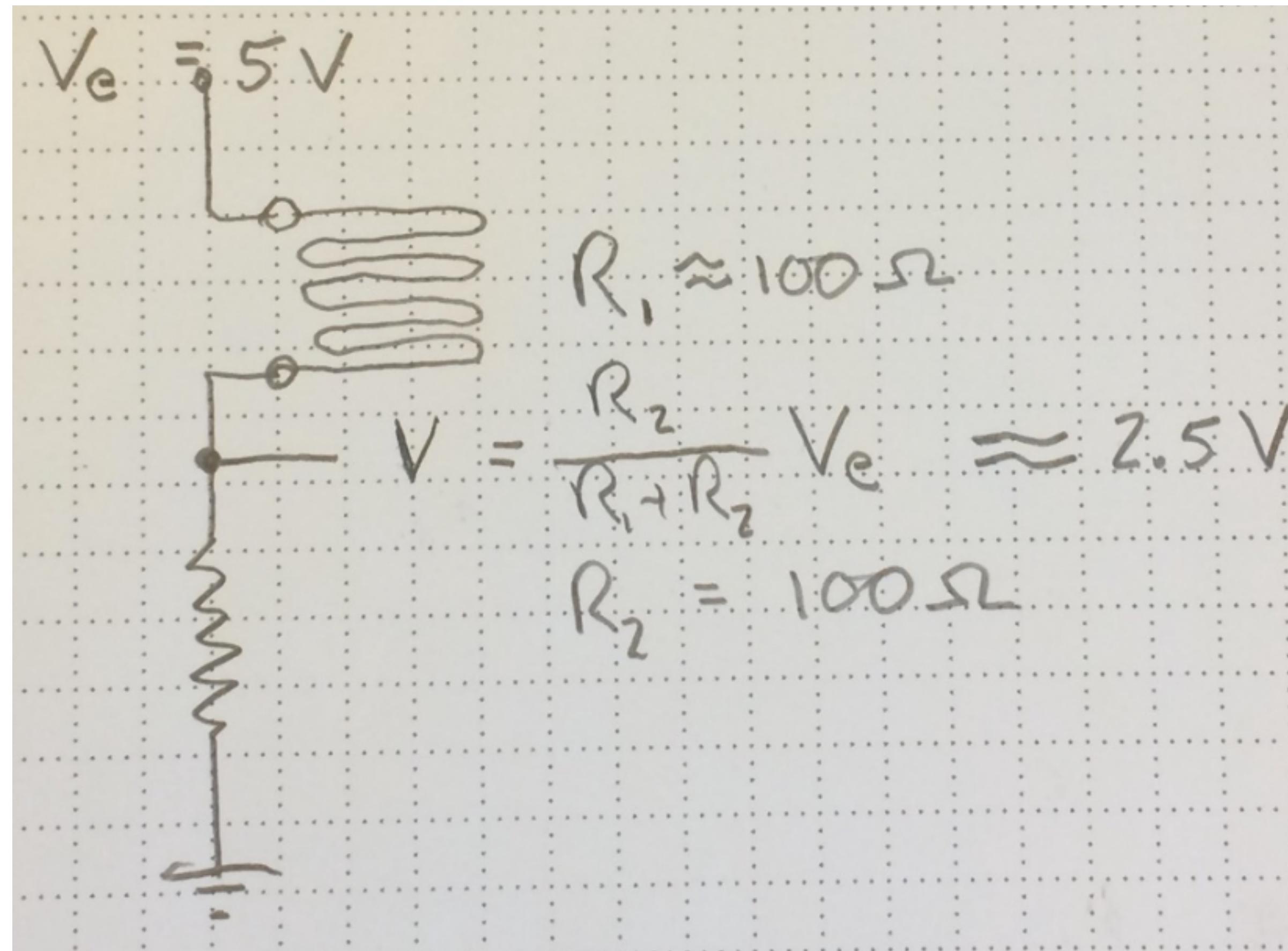
Connect as a voltage divider

Get a large variation in voltage

This would also work for a thermistor



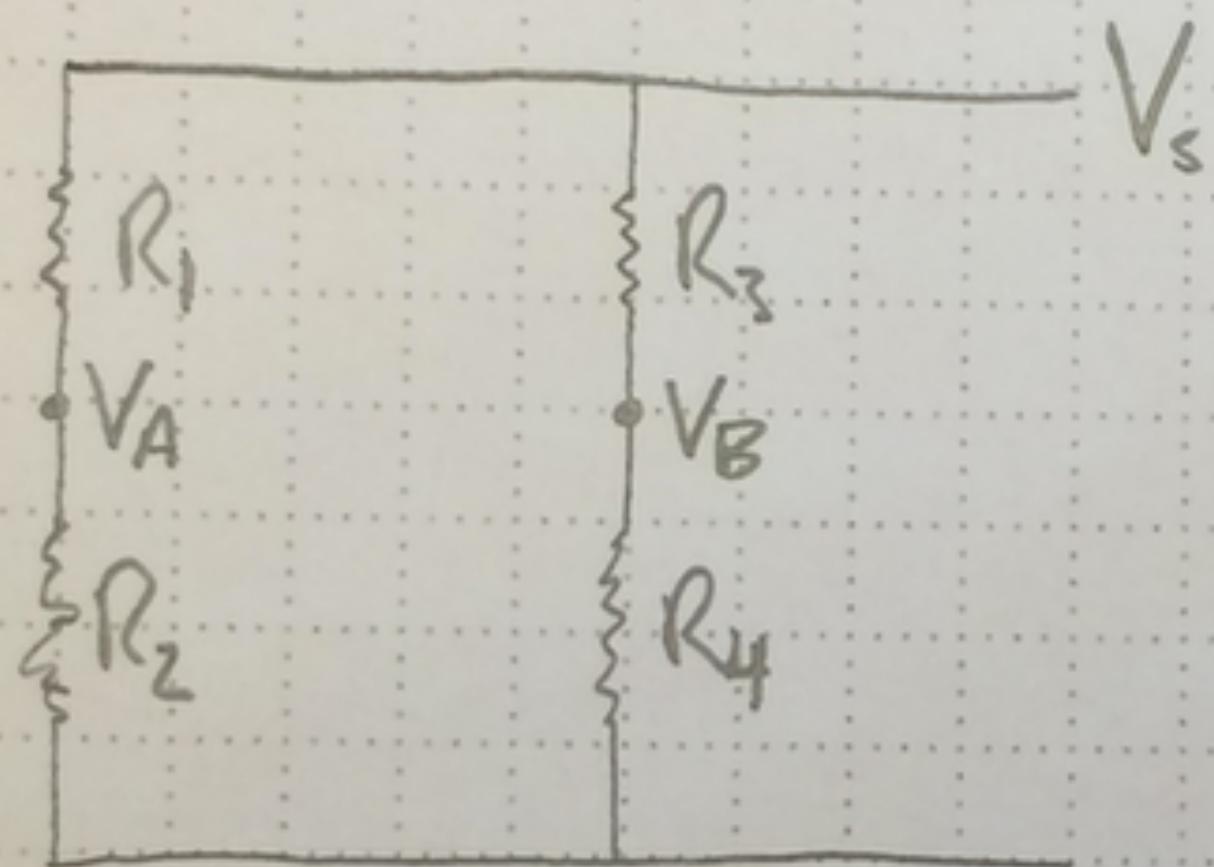
Voltage Divider too coarse for Strain Gauge



- 2.5 volts if $R_1 = R_2$
- 2.50125 volts if R_1 drops to 99.9 ohms
- 2.49875 volts if R_1 rises to 100.1 ohms
- Hard to resolve on a 5 volt scale

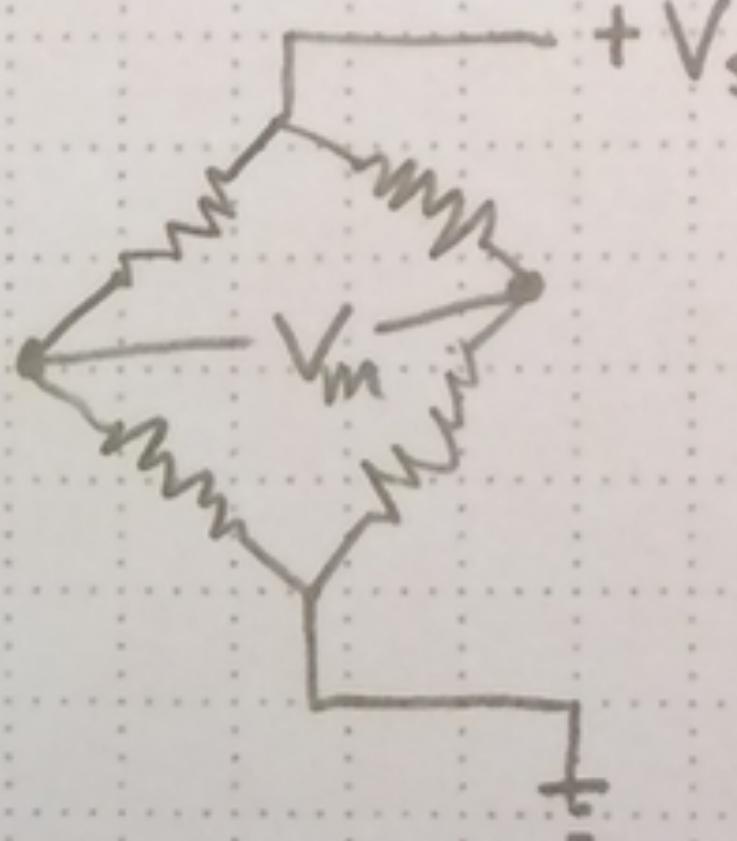
from the workbench of:
date

Wheatstone Bridge



$$V_A = \frac{R_2}{R_1 + R_2} V_s$$

$$V_B = \frac{R_4}{R_3 + R_4} V_s$$



ground
0 Volts

if $R_1 \approx R_2 \approx R_3 \approx R_4$

$$V_A \approx V_B \approx V_s / 2$$

V_A goes up if $R_2 \uparrow$ or $R_1 \downarrow$

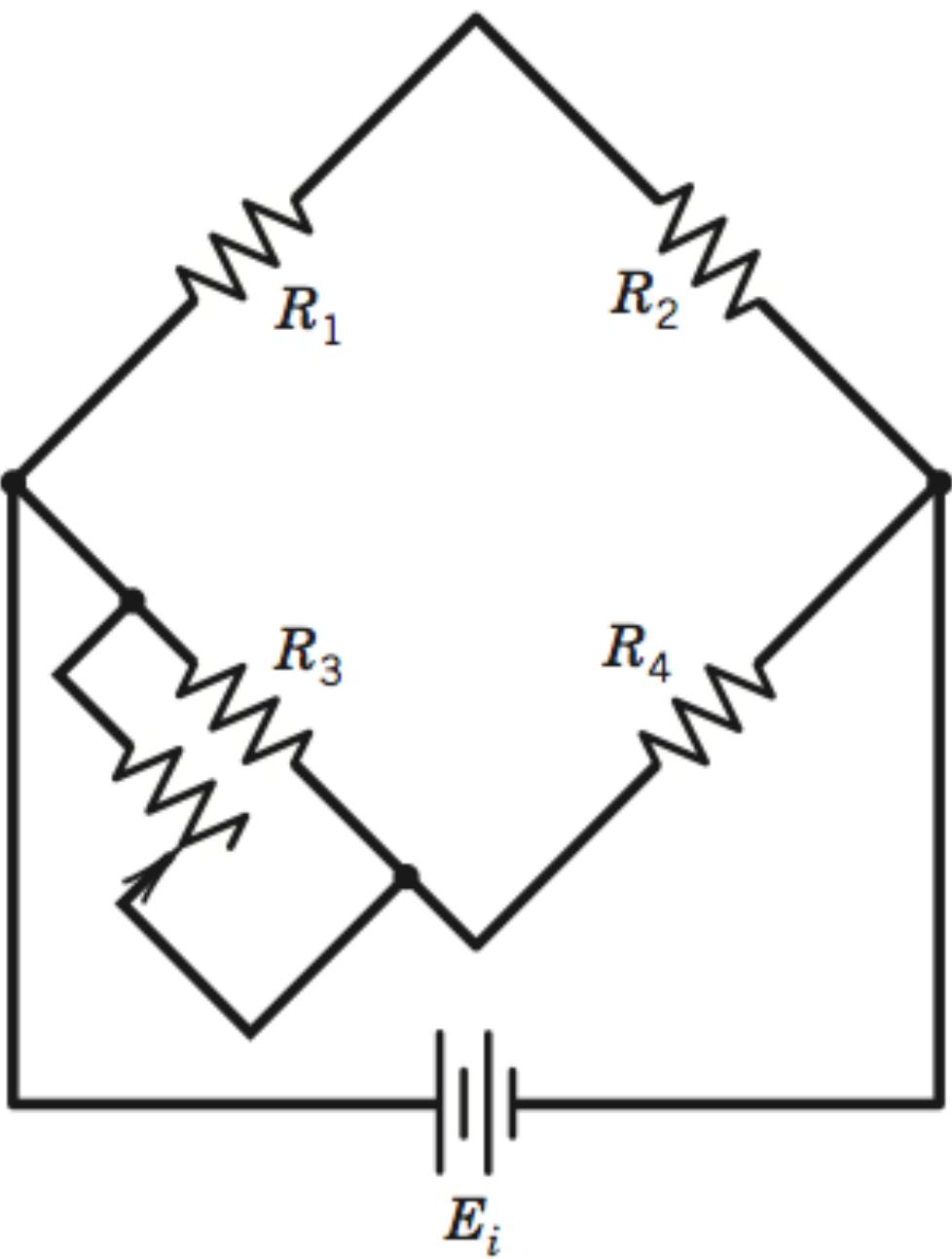
V_B goes down if $R_3 \uparrow$ or $R_4 \downarrow$

$V_A - V_B$ goes up with $R_2 \uparrow$ & $R_3 \uparrow$ down with $R_1 \downarrow$ & $R_4 \downarrow$

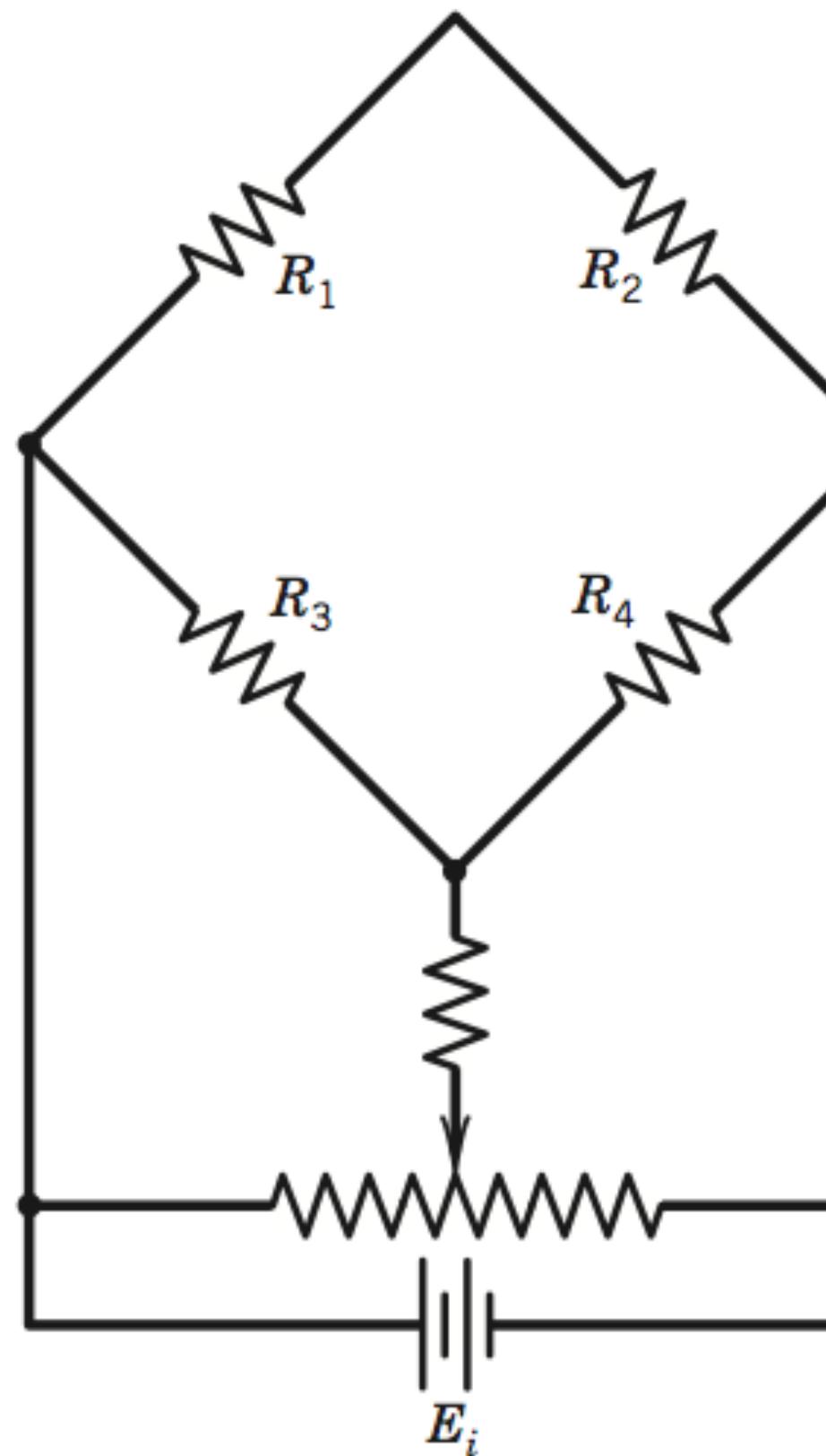
Try it in a notebook to see how linear

A Wheatstone bridge shows up small changes in resistance as a small change in difference voltage that we can measure accurately on a low voltage scale

Circuit arrangement for shunt balance

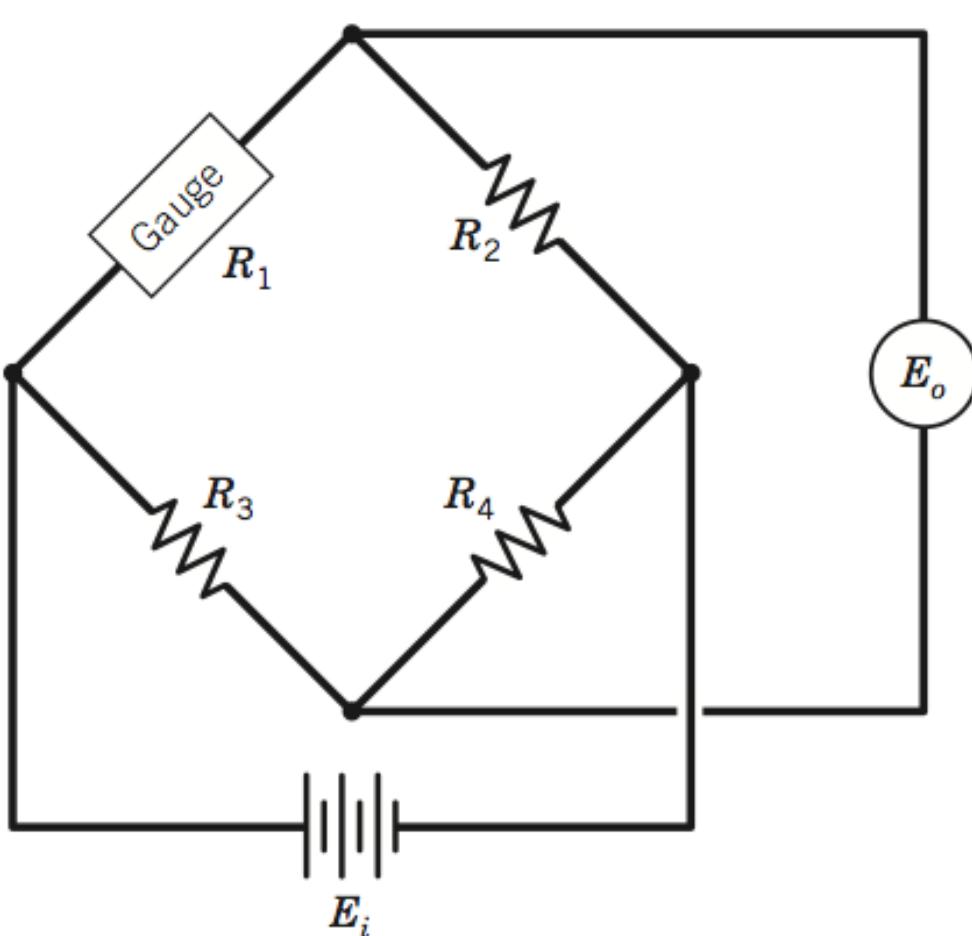


Differential shunt balance arrangement



**Balancing:
Do we
need it?**

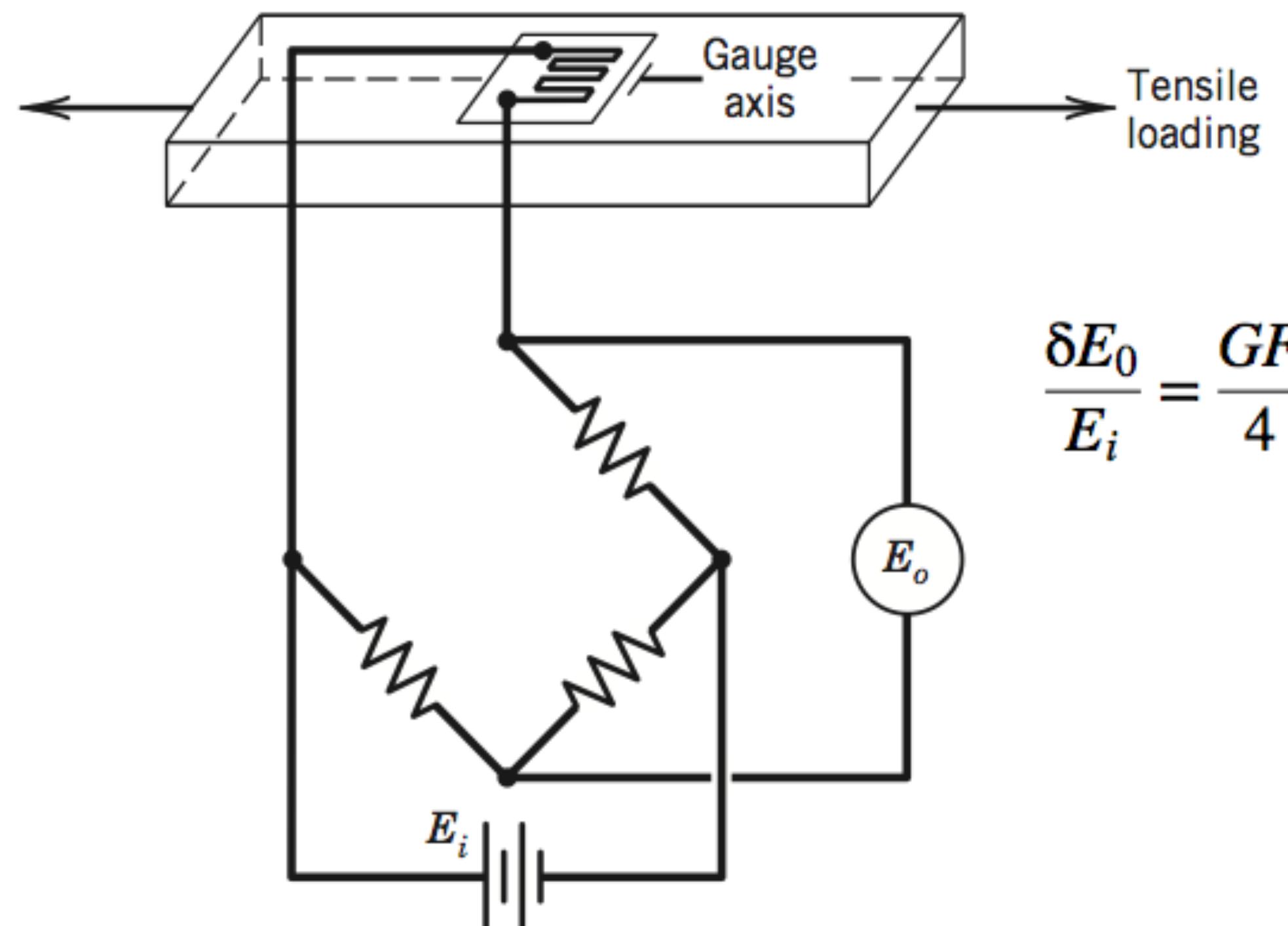
Figure 11.10 Balancing schemes for bridge circuits.



Add some extra resistors and you can adjust to make $V_A = V_B$ so that the bridge output will be zero at rest

Figure 11.9 Basic strain gauge Wheatstone bridge circuit.

$$\frac{\delta E_0}{E_i} = \frac{\delta R_1/R_1}{4 + 2(\delta R_1/R_1)} \approx \frac{\delta R_1/R_1}{4} \quad (11.15)$$



With no balancing
you will have to
track change in E_0

$$\frac{\delta E_0}{E_i} = \frac{GF}{4} \epsilon_a \quad (11.33)$$

Figure 11.11 Strain gauge circuit subject to uniaxial tension.

E_0 will also change if there's bending, or thermal expansion

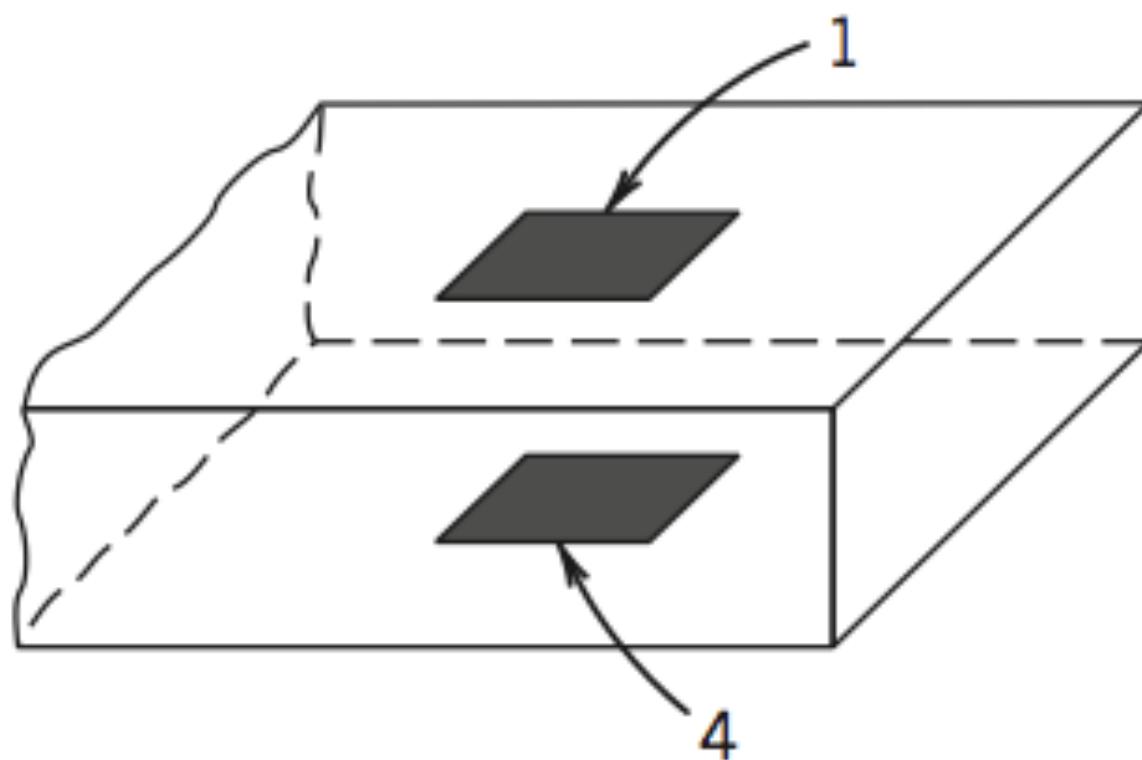
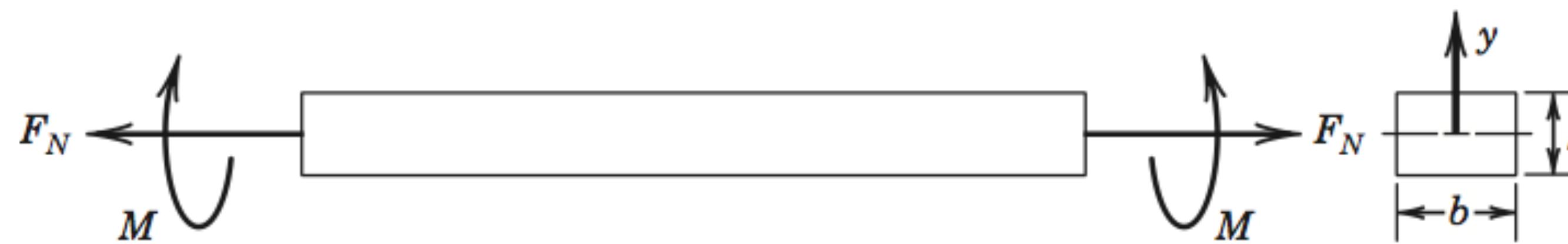
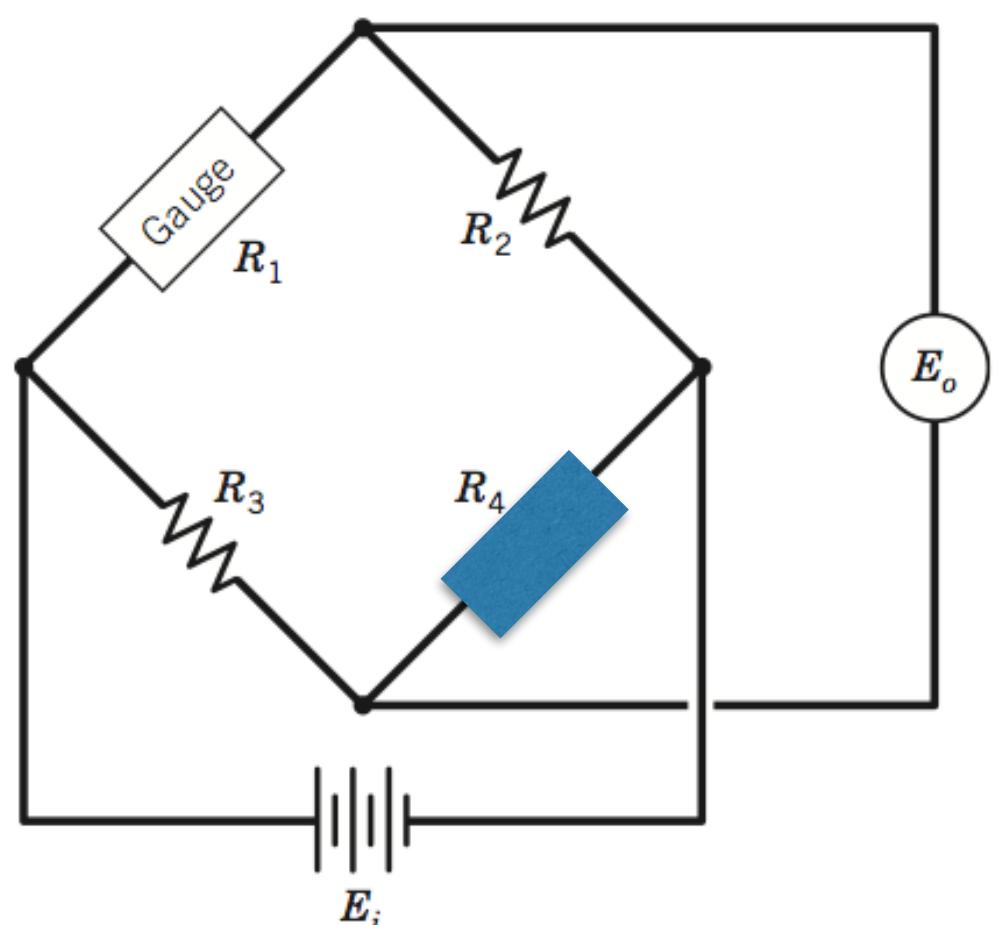


Figure 11.13 Strain gauge installation for bending compensation.

$$\frac{\delta E_0}{E_i} = \frac{GF}{4} (\epsilon_1 + \epsilon_4) \quad (11.31)$$



Both gauges stretched by Force
Moment stretches one, compresses
the other, effects cancel out

Figure 11.9 Basic strain gauge Wheatstone bridge circuit.