

# Neutron Brilliance of the Liquid Deuterium Cold Source as Measured from the ICON Beamline at the Swiss Spallation Neutron Source (SINQ)

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## Abstract

A brilliance measurement was conducted on July 21, 2014 at the ICON beamline at SINQ as a benchmark before any potential changes are made to the liquid deuterium cold neutron source in a future extended shutdown period. The peak brilliance of the deuterium cold source at SINQ has been measured to be  $3.33 \pm 0.15 \times 10^{11} \text{ n cm}^{-2} \text{ s}^{-1} \text{ mA}^{-1} \text{ \AA}^{-1} \text{ sterad}^{-1}$  at 1.8 Å, and the total brilliance (energy-integrated) has been measured to be  $9.12 \pm 0.76 \times 10^{11} \text{ n cm}^{-2} \text{ s}^{-1} \text{ mA}^{-1} \text{ sterad}^{-1}$  for wavelengths above 0.7 Å via a time-of-flight measurement at the ICON beamline. Using a detailed MCNP model, the peak brilliance has been calculated to be  $3.1 \pm 0.14 \times 10^{11} \text{ n cm}^{-2} \text{ s}^{-1} \text{ mA}^{-1} \text{ \AA}^{-1} \text{ sterad}^{-1}$  at 1.65 Å, and the total brilliance (energy-integrated) has been calculated to be  $8.97 \pm 1.7 \times 10^{11} \text{ n cm}^{-2} \text{ s}^{-1} \text{ mA}^{-1} \text{ sterad}^{-1}$  for wavelengths above 0.7 Å. The peak brilliance value and wavelength position disagree only slightly between the measurement and model (7% difference in value, 8% difference in wavelength position), and the total brilliance agrees within the uncertainty bounds. The close agreement validates the models and benchmarks the state of the cold source.

**Keywords:** spallation, neutron, source, brilliance, cold, deuterium, measurement, helium-3, detector

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## 1. Introduction

The Swiss Spallation Neutron Source (SINQ) is a spallation neutron source driven by a continuous 590 MeV proton beam at the Paul Scherrer Institut in Villigen, Switzerland [1]. Inside SINQ, incoming protons impinge on a lead target cooled with heavy water, producing high energy neutrons. These neutrons are moderated by the tank of room temperature D<sub>2</sub>O surrounding the target. Within the D<sub>2</sub>O moderator tank, there is a 20 liter volume of approximately 25 K liquid D<sub>2</sub> whose innermost face is approximately 35 cm

away from the center of the target. This volume, the “cold source”, serves to further reduce the energies of the “thermal” neutrons coming from the D<sub>2</sub>O tank into a regime that is more useful to scientific instruments at SINQ.

There is an extended shutdown of SINQ ambitiously planned for 2018/19 which will provide an opportunity for changes to be made to the cold neutron source and the neutron guides [2]. The brilliance measurement presented in this paper was conducted to provide a reference to compare to after the upgrade has been completed. Several time-of-flight (TOF) neutron spectrum measurements were conducted on July 21, 2014 at the ICON beamline at SINQ to determine the brilliance of the cold source. ICON is the cold neutron imaging facility at SINQ. The beamline offers an aperture wheel to change beam intensity and

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collimation ratio, as well as large, evacuated flight tubes to minimize losses from scattering in the air [3]. ICON was chosen for the measurement since it does not incorporate any neutron optics, has good collimation, and looks directly on the surface of the cold source. Measuring at ICON removes additional uncertainty associated with the current state of the neutron guides, eliminates having to model additional physics involved with neutron-reflective surfaces, and limits the detector view in a well-defined way.

## 2. Experimental Setup

The layout of the experiment is shown in Figure 1 as a horizontal cut of the MCNP model geometry. The target and moderators are shown furthest to the right. The vertical line is the shielding monolith boundary, which is mostly steel blocks. The ICON bunker is to the left of the monolith, the walls of which are made of heavy concrete and are shown as rectangular blocks. The velocity selector that is usually mounted on the monolith wall in the ICON bunker was removed for this measurement. A large number of shielding elements were used in this measurement since there is a large fast neutron background present at the ICON beamline.

Figure 2 shows a photograph of the  $^3\text{He}$  detector used in the TOF measurements with the iron pinhole collimator positioned in front of it. This picture was taken before the large shielding blocks and sapphire crystals were positioned around the detector.

The principle components in the neutron path, in order of increasing distance from the detector during the measurement, are shown in the following list.

### In-bunker components

1. Spherical neutron detector, 2.3/1.2 atm  $^3\text{He}/\text{Kr}$  gas mixture, 3.20 cm  $\varnothing$  gas volume, 0.5 mm thick stainless steel walls, surrounded by 1 mm cadmium sheets on all sides except towards the pinhole collimator
2. Cadmium aperture, 1 mm  $\pm 0.01$   $\varnothing$  hole, 1 mm thick, 1 mm from the detector surface

3. Iron pinhole collimator, 2 mm  $\varnothing$  hole, 100 mm long, immediately after the cadmium aperture, surrounded by heavy concrete, lead, and polyethylene shielding
4. Polycrystalline sapphires, 20x20 mm faces, 80 mm total thickness, within the heavy concrete, lead, and polyethylene shielding
5. Three evacuated flight tubes with 1.0 mm thick aluminum windows, 7410 mm total length, decreasing  $\varnothing$  of 41 cm, 30 cm, and 20 cm as distance to the source decreases.
6. Neutron chopper, Al-clad Cd, 420 mm  $\varnothing$  wheel, 1.5 mm thick, 15 Hz rotation speed, 7430 $\pm$ 50 mm from the  $^3\text{He}$  detector, 2 $\pm$ 0.05 mm wide slit corresponding to a 0.16% duty cycle
7. Steel collimator, 50x50 mm aperture, 30 cm thick, 7548 mm from detector

### In-pile components

8. Movable gadolinium circular aperture wheel, set to the largest opening of 80 mm  $\varnothing$
9. High energy shutters
10. “Zapfen” unit, 40x120 mm
11. D<sub>2</sub>O moderator tank
12. Low pressure nozzle which penetrates the D<sub>2</sub>O moderator tank, opening size is approximately 148x138 mm (HxW) at the cold source surface
13. Liquid deuterium cold source
14. Lead “cannelloni” spallation target

Since brilliance was the goal of the measurement, the solid angle seen by the detector was needed to normalize the neutron spectra. The cadmium aperture limits the sensitive region of the helium detector to a 1 mm diameter circle, and the other items in the beam path created a system that limited the angular view of the detector. Table 1 shows the maximum solid angle

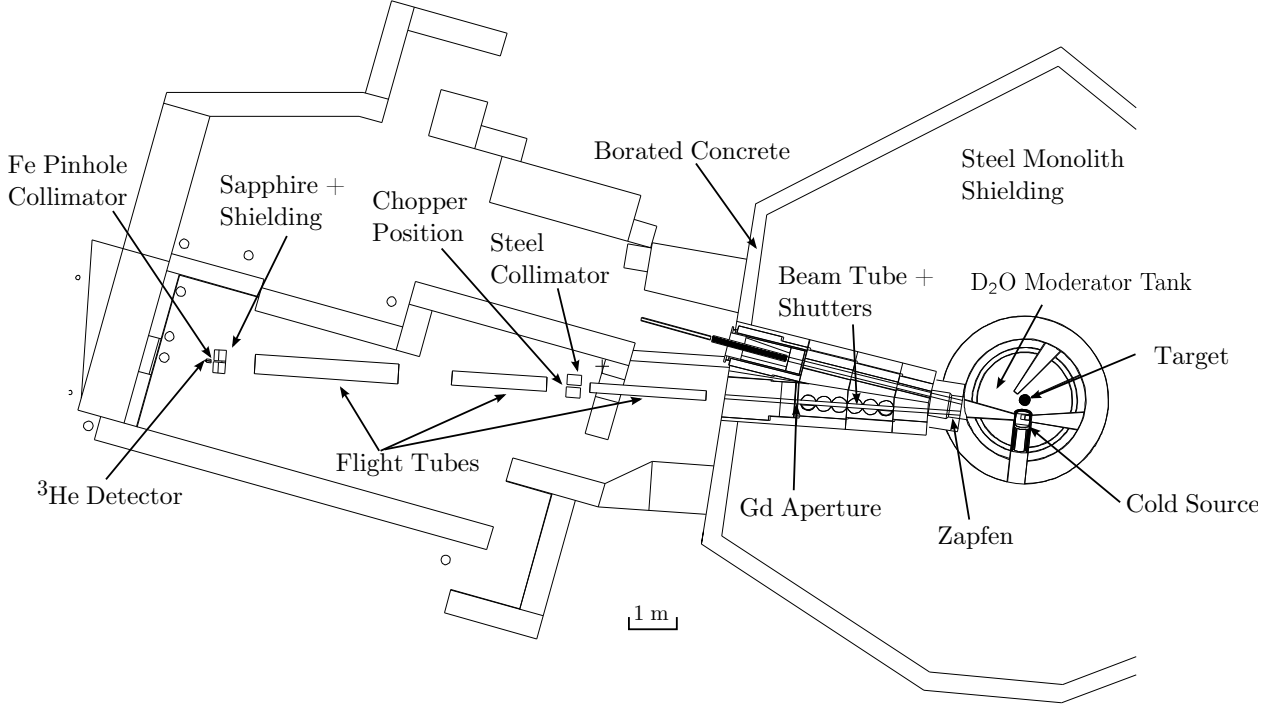


Figure 1: A horizontal cut through the MCNP simulation geometry showing the major items in the neutron path.

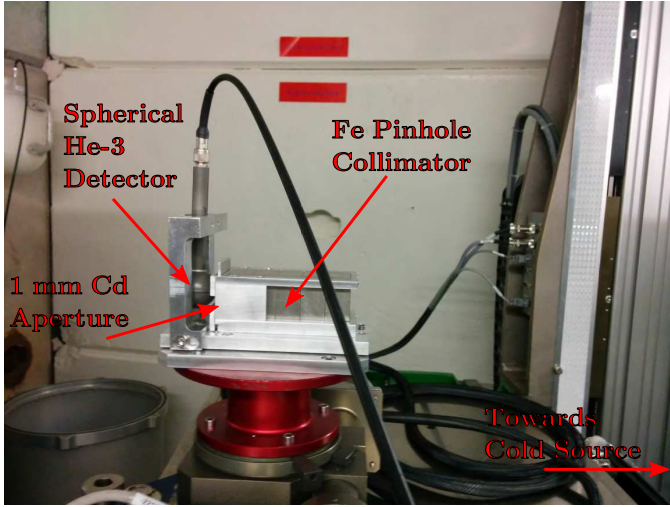


Figure 2:  $^3\text{He}$  detector with iron collimator.

limiting item. In the vertical plane, the limiting item is the beam tube between the Zapfen and the monolith wall. In the plane at 45 degrees of azimuthal angle, the aperture wheel is the limiting case. These items are shown in the pinhole image calculated with MCNP and discussed in Section 4.

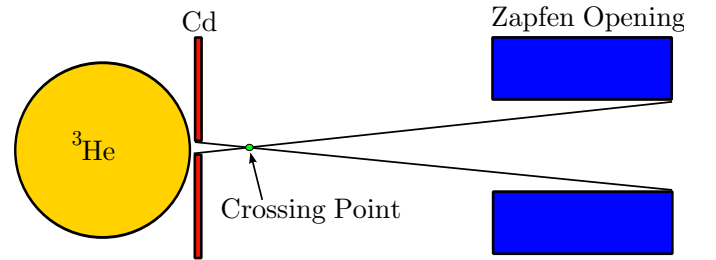


Figure 3: The limiting collimation system in the measurement in the horizontal plane (not to scale), and the crossing point where the point detector was placed in the MCNP simulations.

of the various items in the neutron beam (i.e the penumbra created by these objects). The values are the minima of the item's self-collimation (due to its thickness) and the collimation of the system formed by the item and the hole in the cadmium sheet. Figure 3 shows a cartoon of the collimation system formed by the items and the cadmium hole. It can be seen that in the horizontal plane, the Zapfen opening (where the beamline opens into large nozzle in the moderator tank) is the

Two measurements were done in total: centered in the beam with sapphire crystals inside the nearest shielding and centered with a beryllium crystal cooled below 120 K (under which transmission does not change much) in the beamline to show the 4.0 Å bin of the analyzer. The center

Table 1: Table of solid angles with the limiting member marked with boldface and a star (\*).

	Horizontal	Vertical	Diagonal
Fe Collimator	6.93E-4	6.93E-4	6.93E-4
Cadmium Hole	1.84E-0	1.84E-0	1.84E-0
Sapphire	1.98E-3	1.98E-3	3.84E-3
Steel	3.32E-5	3.32E-5	6.56E-5
Aperture	3.40E-5	3.40E-5	* <b>3.40E-5</b>
Tube	2.26E-5	* <b>2.26E-5</b>	4.49E-5
Zapfen	* <b>2.07E-5</b>	4.62E-5	6.66E-5
Nozzle	5.13E-5	5.13E-5	1.02E-4

of the beam was found by scanning a neutron-sensitive CCD camera (which has layers of iron and cadmium before the CCD) through the beam and assuming the flux maximum was the beam center. Once positioned at the center, the vertical tilt of the  $^3\text{He}$  detector/pinhole system was scanned to find the maximum once again. Since a measurement was not done with the shutter closed to collect background, the average value of lower-energy tail of the measured spectrum between 10.0 and 11.4 Å was assumed to be the background level. The chopper slit width, rotation speed, and distance from the detector gave a wavelength binning width ( $\Delta\lambda$ ) of about 0.056 Å for the measurement.

Since the viewing angle was wide for this measurement, it should be insensitive to variations introduced by alignment. The detector saw almost the entire surface of the cold source during the measurement, rather than looking at a highly collimated point on the surface. Therefore, moving it to the left or right in space should have produced similar intensities as long as a new structure did not occlude the view. Because of this wide view, there is little uncertainty on which region of the cold source the detector saw. In other words, spectral variations between measured and calculated values should not be because the detector was simulated with a different view of the cold source compared to what was measured.

### 3. Detector Efficiency

In order to calculate the spectrum from the TOF data, the response curve, or efficiency, of the helium detector has to be known. This curve

gives a relation between how many counts can be expected in the detector compared to the number of neutrons incident on the detector. For this study, the efficiency curve was calculated using MCNP6.1. A detailed model of the helium detector was used, and a neutron beam 1 mm in diameter was modelled to be incident on the detector center. The energy distribution used was equiprobable in wavelength space, with 512 wavelength bins between 0.5 and 11.5 Å. The efficiency curve was calculated by dividing a reaction tally for (n,p) reactions inside the  $^3\text{He}$  volume (with identical binning as source) by a surface tally to count the number of incoming neutrons in each bin. The result of the simulation is shown in 4. The relative error from statistics of every bin of the curve is below 0.5%. The pressure uncertainty was specified to be  $\pm 5\%$  by the manufacturer. This efficiency curve was used to calculate the experimental neutron spectrum, shown in Section 5, from the measured counts from the detector.

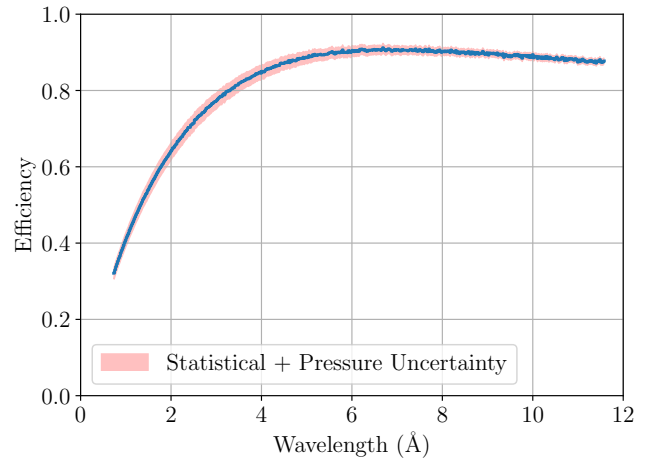


Figure 4: The calculated efficiency curve.

### 4. Monte Carlo Simulations

Simulations were done with MCNP6.1 and with ENDF/B-VII.1 data. Thermal scattering data for the room temperature sapphire crystals were used [4], as were 77 K thermal scattering data for beryllium, various data for ortho-/para-deuterium, 273 K data for heavy water, 273 K data for light water [5], and 293 K data for aluminum, and 25 K data



for zirconium [6]. The aluminum and zirconium data are important for accurately simulating the transmission through the various hulls surrounding the deuterium in the cold source. The overall model geometry has already been shown in Figure 1, and was created to be as true-to-life as possible with very high levels of detail in the cold source and cannelloni target. The detailed plot of the cold source geometry is shown on the right side of Figure 5. The cannelloni target in use during the measurement was “target 10”, which is shown in left side of Figure 5. This target had a hemispherical beam entrance window and “SINO Target Irradiation Program” (STIP) material radiation samples within the target. Both of these features reduce the neutron flux compared to the highest performing target and were modelled in the MCNP simulation.

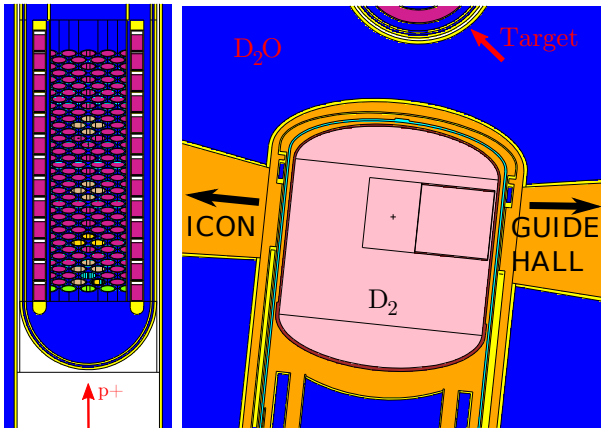


Figure 5: LEFT: Vertical cross section of the cannelloni target geometry. RIGHT: Horizontal cross section of the cold source geometry of the MCNP model. The STIP samples are visible in the target model as brown, yellow and blue rods. The magenta colored rods in the target are filled with lead.

#### 4.1. Solid Angle Calculation

Since the detector is very far away from the neutron source, special methods had to be used in order to gather sufficient statistics in a reasonable amount of time. A point detector is a “next event” estimator that calculates tally contributions at every neutron collision event [7]. The contribution to the tally is weighted by the probability of the neutron scattering into the direction

of the detector point and travelling to the detector without colliding again (i.e. weight is reduced by the attenuation of the material in-between the scatter event and the detector position).

Using a point detector would be a reasonable solution if only the calculated flux was desired, but the brilliance also depends on the viewable solid angle of the detector system. The physical system responds to a view limited by the beam-line components and cadmium aperture, and a regular point detector would integrate all visible contributions and wouldn’t report any angular information needed for calculating the brilliance. In order to calculate the solid angle visible to the  $^3\text{He}$  detector, a “pinhole radiography tally” was used in MCNP. This tally calculates contributions the same way as a point detector, but it projects the contributions through the pinhole point onto a pre-defined image plane. If such a pinhole detector is placed behind all the items which limit the detector view, the solid angle visible to the  $^3\text{He}$  detector can be calculated by summing the individual solid angle values each pixel of the pinhole image corresponds to.

Figure 6 shows a pinhole radiography tally image generated at the upstream surface of the cadmium sheet with the pinhole placed at the horizontal collimation crossing point. The Zapfen limits the view on the horizontal plane, so the hole in the cadmium (grey) lines up with projection of the Zapfen (magenta). The other limiting objects are also projected onto the image plane in Figure 6 to show the areas where they limit the detector view. The projections from the limiting objects are shown as dashed colored lines.

The Zapfen is indeed the limiting member in the horizontal plane of the collimation system since it can be seen that the image does not extend past the magenta Zapfen projection line. A horizontal and vertical gradient is also apparent in the projected image. Since the dimensions are mirrored and the image is plotted from the view point of the pinhole towards the Cd sheet, the target would be to the right in the image and thermal flux maximum would be in the downward direction.

From this image, it was deduced that the total solid angle visible to the detector was limited to

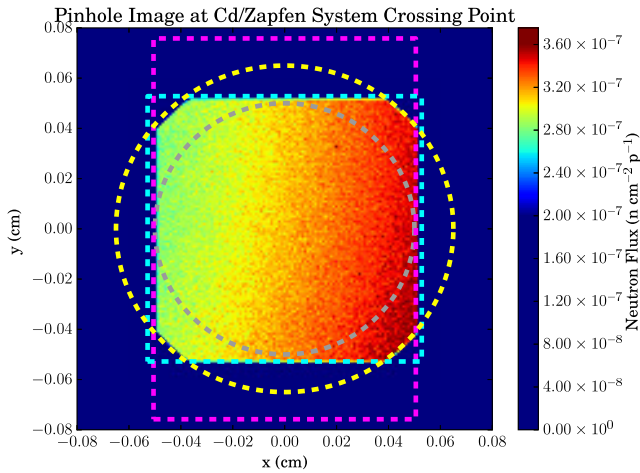


Figure 6: The flux image created by a pinhole radiography tally in MCNP at the horizontal collimation crossing point. The image plane is at upstream surface of the cadmium sheet. The outlines show the projections of the limiting geometry through the pinhole: Grey=cadmium hole, blue=beam port, magenta=Zapfen, yellow=Gd aperture. Note, the flux values shown are those resulting from a pinhole-limited view (not the real, full view).

$2.14 \times 10^{-5}$  steradians. The hole is fully illuminated (there are no spots on the Cd sheet where a radiography tally produced a zero result), so the area used to normalize the spectra is simply the area of the hole ( $7.85398 \times 10^{-3} \text{ cm}^2$ ). This value was used to normalize both the calculated and measured spectra, and therefore was not a source of uncertainty between the two. The uncertainty in the distance between the chopper and the detector is approximately 5 cm, which corresponds to an uncertainty in the solid angle of about 0.6%.

#### 4.2. Sensitivity to Scattering Data

To calculate an accurate neutron spectrum emitted from the liquid deuterium in the cold source at low energies, thermal scattering data must be used to account for the influence of molecular bonds, crystal structure, nuclear alignment, etc. There were several data libraries available when doing these MCNP calculations. Namely, the default libraries from the ENDF/B-VII.1 data [5], several libraries from the Institut für Kernenergetik und Energiesysteme (IKE) at Universität Stuttgart [6], and those published by Centro Atómico Bariloche (CAB) [8]. The spectra calculated at

the  $^3\text{He}$  detector position using the various liquid  $\text{D}_2$  data are shown in Figure 7. It can be seen that the 24 K IKE data produce a significantly different spectrum compared to the ENDF 19 K data. The 19 K CAB data also produce a significantly different spectrum compared to that produced with the 19 K ENDF data. Since the effects are relatively large, the 24 K IKE data was chosen for the final simulation since it is nearest to the true temperature of the cold source. The whole range of these data were incorporated into the uncertainty of the final simulated brilliance spectrum, since these data have a relatively large influence and are relatively imprecise (the CAB and ENDF data for the same 19K temperature are the bounding cases from 1-2 Å!).

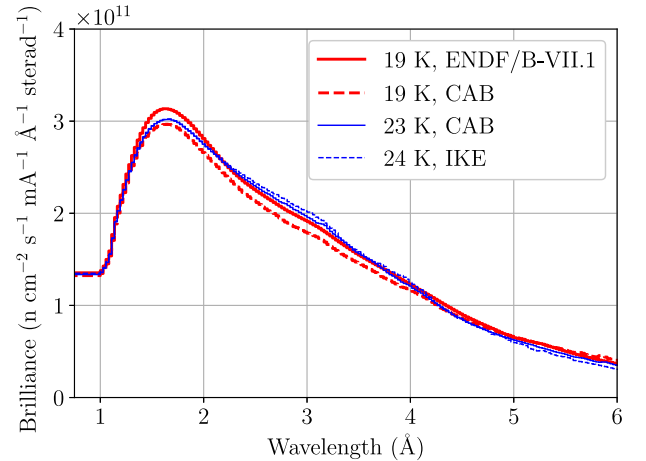


Figure 7: Simulated neutron spectra emitted from liquid deuterium cold source using various  $S(\alpha, \beta)$  scattering data for  $\text{D}_2$ .

Bariloche also released improved thermal scattering data for light and heavy water as well [9, 10, 11]. The effect of replacing the ENDF/B-VII.1 data with the CAB data for both light and heavy water in the SINQ tank are shown in Figure 8 when the standard  $\text{D}_2$  scattering data and with liquid deuterium at 25 K saturation density and long-time, 1.2 mA equilibrium o- $\text{D}_2$  fraction. The figure shows that the updated heavy water data has very little effect on the emitted neutron spectrum from the cold source. Therefore, the standard ENDF/B-VII.1 data was used in the final calculations, and this variation was not consid-

ered to be an uncertainty in the final calculated result.

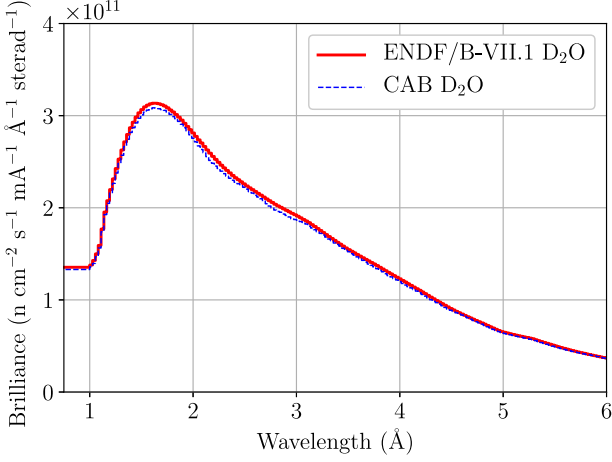


Figure 8: Simulated neutron spectra emitted from liquid deuterium cold source using the standard ENDF/B-VII.1 and the new Bariloche  $S(\alpha, \beta)$  scattering data for the  $D_2O$  moderator.

#### 4.3. Sensitivity to Ortho-/Para- $D_2$ Fraction and $D_2$ Density

Other than the data themselves, the spectrum emitted from the cold source is also sensitive to the density and the ortho- and para- $D_2$  fractions of the liquid deuterium. These parameters effect the scattering length as well as the scattering kinematics of the moderator. From the operational experience at the Institut Laue-Langevin (ILL), their 20  $\ell$  liquid deuterium cold source runs at about 80% nominal density at 25 K at full reactor power [12]. The nominal saturation density of liquid deuterium at 25 K is 0.162 g/cm<sup>3</sup> [13]. Figure 9 shows the variation of the neutron spectrum due to density reduction from boiling in the deuterium. A reduction of 80% was chosen to be the maximum limiting case since the power deposition in the ILL cold source should be greater than that deposited in the SINQ deuterium volume. It is doubtful that the cold source had 20% void during the measurement due to the low proton current. For this reason, a density range of 93-100% was chosen to bound the uncertainty in the  $D_2$  density.

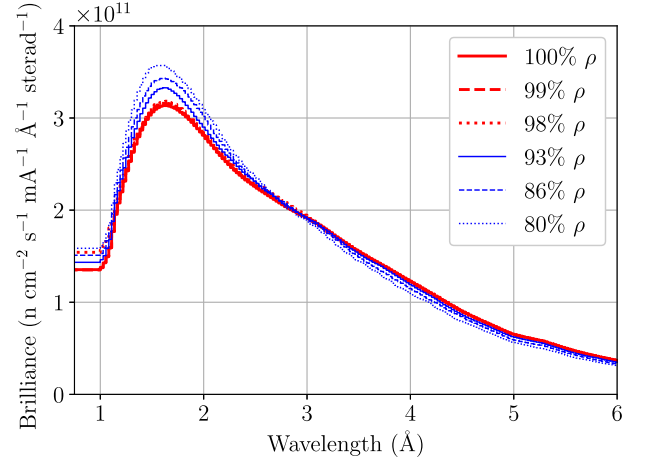


Figure 9: Simulated neutron spectra emitted from liquid deuterium cold source at various  $D_2$  densities. ENDF-B/VII.1 19 K scattering data and a o- $D_2$  fraction of 0.762 was used.

Figure 9 shows that the peak of calculated spectrum increases with density reduction. Since the deuterium is more transparent to neutrons at lower densities, the emission region of the moderator becomes larger and less cold, increasing the thermal peak of the spectrum and reducing the cold region (wavelengths greater than the crossing point at 2.75 Å). From the MCNP simulations done, reducing the deuterium to 80% nominal density (0.130 g/cm<sup>3</sup>) increases thermal peak by about 12%.

With no other influences, the thermodynamic equilibrium fraction of ortho- $D_2$  at 25 K is 0.955, but radiation-induced recombination of the deuterium molecules results in an equilibrium ratio of 0.762 for 1.2 mA of proton current on the SINQ target [14]. This ratio gradually returns to thermodynamic equilibrium when the beam is shut off. The proton current on SINQ prior to the brilliance measurement is shown in bottom plot in Figure 10. There was a relatively steady period of 1.5 mA for 13 weeks, with a service period of zero current of 1 week about 6 weeks before the measurement was taken. The ortho- $D_2$  fraction was calculated based on this proton current history using the methods described in [14], which accounts for the irradiation induced recombination, thermal conversion, catalytic conversion, and con-

version from free atom collisions. The results of the calculation are shown in upper plot in Figure 10, with an initial ortho/para fraction of 2/3 (the room temperature, “bottle” equilibrium) after the shutdown period which ended May 1, 2014. Figure 10 suggests the o-D<sub>2</sub> fraction during the measurement on July 21 should have been around 0.761.

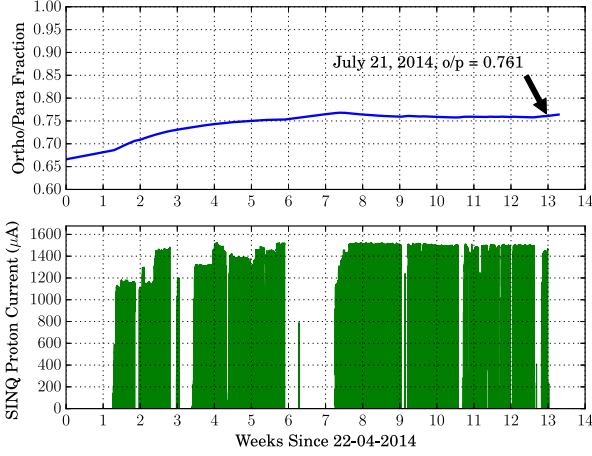


Figure 10: The proton current history for SINQ in the weeks leading up to the measurement time.

There is some uncertainty in this value, however, and Figure 11 shows the variation in the emitted neutron spectrum caused by changing the o/p ratio in a range of 0.66 to 0.955 when the deuterium is at the 25 K saturation density of 0.162 g/cm<sup>3</sup> [13]. It is apparent that higher ortho fractions produce spectra with reduced neutron density at the thermal peak and enhanced density in cold regions >3.75 Å. An ortho fraction within the 60-99.5% range was considered to contribute to the uncertainty in the simulated results since the parameters entered into the fraction calculation were approximations (especially the catalytic conversion parameter).

## 5. Measured Brilliance and Best Matching Case

As mentioned previously, the state of the deuterium was uncertain due to the uncertainty in the irradiation history of the source (o/p fraction) and the total power deposited in the deu-

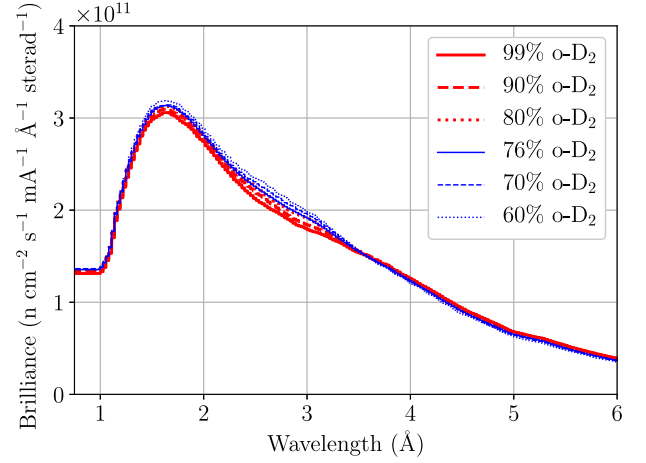


Figure 11: Simulated neutron spectra emitted from liquid deuterium cold source at various ortho/para-D<sub>2</sub> ratios. ENDFB/VII.1 19 K scattering data and a D<sub>2</sub> density of 0.162 was used.

terium (density), but using the best information available, the most accurate results should come from a simulation using the 24 K thermal scattering data from IKE and using an ortho-D<sub>2</sub> ratio of 0.761. The beam current during the measurement was approximately 150 μA, so the power deposition inside the D<sub>2</sub> volume should have been approximately 75 Watts [15]. Therefore, based on previous studies on the void fraction in liquid D<sub>2</sub> under irradiation [16], the density should be near 98% of the saturation density. Figure 12 shows the simulated spectrum at 98% saturation density. The simulated spectrum has a peak brilliance of  $3.1 \pm 0.14 \times 10^{11} \text{ n cm}^{-2} \text{ s}^{-1} \text{ mA}^{-1} \text{ Å}^{-1} \text{ sterad}^{-1}$  (8%) at 1.65 Å, and the total brilliance (energy-integrated) of  $8.97 \pm 1.7 \times 10^{11} \text{ n cm}^{-2} \text{ s}^{-1} \text{ mA}^{-1} \text{ sterad}^{-1}$ . The 1-σ uncertainty bounds are a combination of statistical error and the sum of the spectral variation due to aforementioned shifts in the density, shifts in the ortho fraction, and using different scattering data.

Figure 12 also shows the measured spectrum, which has a peak brilliance of  $3.33 \pm 0.15 \times 10^{11} \text{ n cm}^{-2} \text{ s}^{-1} \text{ mA}^{-1} \text{ Å}^{-1} \text{ sterad}^{-1}$  (8%) at 1.80 Å, and the total brilliance (energy-integrated) of  $9.12 \pm 0.76 \times 10^{11} \text{ n cm}^{-2} \text{ s}^{-1} \text{ mA}^{-1} \text{ sterad}^{-1}$ . The error bounds on the measured data were calculated using the uncertainty of live time (based on the



dead time correction), the uncertainty of distance between the chopper to the detector, the time binning of DAQ (time resolution), the fluctuations of proton beam, the uncertainty of the chopper duty cycle (from the uncertainty of the slit width), the uncertainty of solid angle, the uncertainty of beam size (from the uncertainty of Cd aperture machining), the uncertainty of the simulated efficiency with MCNP, and statistical error from averaging over 5 raw data channels. In order to keep the count rate acceptably low during the measurement, a very small current ( $150 \mu\text{A}$ ) was used on the target. In this regime, the beam is not very stable and fast beam trips happened frequently. The beam monitoring system used has a sampling rate of one sample per 5 seconds, and this slow sampling could be a large source of uncertainty for the total amount of charge incident on the target during the measurement.

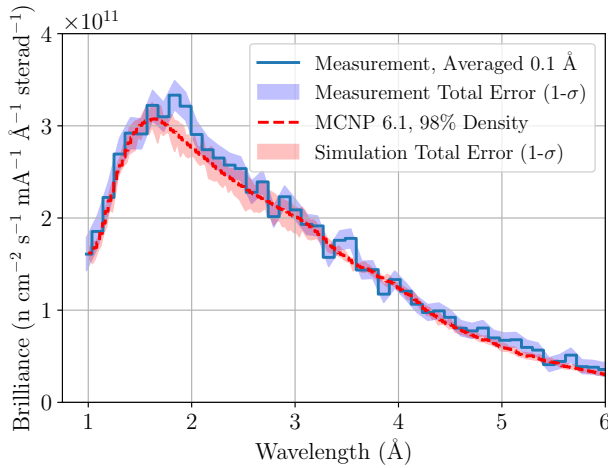


Figure 12: Measured and simulated cold neutron source brilliance at the ICON beamline. IKE 24 K scattering data and a  $\text{o-D}_2$  fraction of 0.762 was used.

Figure 12 also shows that the peaks of simulated spectra are shifted about  $0.2 \text{ Å}$  shorter with respect to the peak of the measured spectrum. This phenomenon has been documented previously, and it is suspected that it arises from some inaccuracies in the liquid deuterium thermal scattering data [17]. The wavelength calibration has an uncertainty of  $\pm 0.125 \text{ Å}$ , which comes from the width of the  $4.0 \text{ Å}$  edge in the neutron spectrum transmitted through a beryl-

lium filter. Instead of there being a sharp step in the measured flux which would determine the channel containing  $4.0 \text{ Å}$ , there was a transition region about  $0.25 \text{ Å}$  wide.

## 6. Conclusions

There are uncertainties associated with the state of the deuterium during the measurement, but reasonable attempts have been made to reduce or bound them where possible. An approximate radiation-adjusted ortho- $\text{D}_2$  fraction was calculated using the proton beam history from the weeks leading up to the measurement time, the void fraction due to radiation heating was approximated, and appropriate scattering kernels for the deuterium temperature were used. A measurement to determine the efficiency of the  $^3\text{He}$  detector was also done, the results of which match very well with MCNP simulation results.

The  $0.2 \text{ Å}$  wavelength shift seen at the spectrum peak is within the positioning uncertainty of the measurement, and further conclusions about it cannot be made at this point. The total view of the detector system was calculated to be  $2.14 \pm 0.13 \times 10^{-5}$  steradians via a MCNP calculation using a pinhole radiography tally. The peak brilliance of the deuterium cold source at SINQ has been measured to be  $3.7 \pm 0.3 \times 10^{11} \text{ n cm}^{-2} \text{ s}^{-1} \text{ mA}^{-1} \text{ Å}^{-1} \text{ sterad}^{-1}$  at  $1.8 \text{ Å}$  via a time-of-flight measurement at the ICON beamline in July 2014. The total brilliance (energy-integrated) has been measured to be  $9.88 \pm 1.6 \times 10^{11} \text{ n cm}^{-2} \text{ s}^{-1} \text{ mA}^{-1} \text{ sterad}^{-1}$  for wavelengths above  $0.7 \text{ Å}$ . The MCNP calculations have yielded a peak brilliance values of  $3.33 \pm 0.15 \times 10^{11} \text{ n cm}^{-2} \text{ s}^{-1} \text{ mA}^{-1} \text{ Å}^{-1} \text{ sterad}^{-1}$  at  $1.65 \text{ Å}$ , and the total brilliance (energy-integrated) value of  $9.12 \pm 0.76 \times 10^{11} \text{ n cm}^{-2} \text{ s}^{-1} \text{ mA}^{-1} \text{ sterad}^{-1}$ . The simulated spectrum from the most probable state of the deuterium is within the uncertainty bounds of the measured spectrum at ICON for almost the entire measured wavelength range, except for the peak value. This close agreement validates the MCNP model being used and sets a benchmark for future upgrade to be compared against.

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