


**ELK322E
POWER TRANSMISSION SYSTEMS**



CHAPTER 1.2: BASIC CONCEPTS

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PER-UNIT STEMS

1.10 Per-Unit Quantities

In an electrical power system

$V \rightarrow \text{kV}$
 $P \rightarrow \text{kW, MW}$
 $Q \rightarrow \text{kVA, MVA}$
 $S \rightarrow \text{kVA, MVA}$
 $Z \rightarrow \Omega$
 $I \rightarrow \text{A, kA}$

380 kV
 500 MVA
 150 kVARs

These quantities are often expressed as a percent or per-unit of a base or reference value specified for each. The per-unit value of quantities is defined as the ratio of the quantity to its base expressed as a decimal.

Advantages:

- (px)(pu) = (pu)
- using small convenient numbers around 1
- makes comparison very easy

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PER-UNIT STEMS

Per-Unit = $\frac{\text{The actual Value}}{\text{Base Value (Selected)}}$

Base Values: All calculation is done using single phase values (Phase voltage, phase current).

Firstly, base voltage (kV) and base power (kVA or MVA) are chosen, the other base quantities are then calculated

Base current $I_B = \frac{\text{Base Power (SB, MVA)}}{\text{Base Voltage (Vphase, kV)}}$

Base Impedance $Z_B = \frac{\text{Base Voltage (Vphase, kV)}}{\text{Base current } I_B} = \frac{V_B^2}{S_B} \times 1000$

Per-unit impedance = $\frac{\text{actual impedance}}{Z_B} \text{ (pu)}$

Example: For a power system $S_3 = 30 \text{ MVA} = 30\,000 \text{ kVA}$, and $V_L = 120 \text{ kV}$

Then $S_B = 30/3 = 10 \text{ MW}$, and $V_B = 120/\sqrt{3} = 69.2 \text{ kV}$, $I_B = \frac{S_B}{V_B} = \frac{10\,000}{69.2} \text{ A}$

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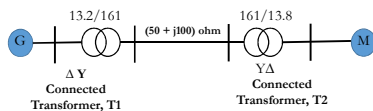
PER-UNIT STEMS

Changing the Base Value: Every element of power systems (generator, transformers, motors and lines) is provided with a manufacturer data sheet in pu values according to their base values. Since in an electrical power system, they are connected each other, their pu values need to be recalculated according to new base values.

$$\bar{Z}_{\text{new}} = \bar{Z}_{\text{given}} \left(\frac{V_{\text{given}}}{V_{\text{new}}} \right)^2 \left(\frac{S_{\text{B new}}}{S_{\text{B given}}} \right)$$

Example: If the reactance of a generator X_d is given as 0.25 pu based on generator's rating of 15 MVA, 13.2 kV, find the X_d which is based on 20 kV, and 100 MVA

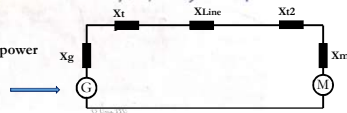
$$X_{d\text{new}} = 0.25 \left(\frac{13.2}{20} \right)^2 \left(\frac{100}{15} \right) = 0.0405 \text{ pu}$$



Base Values: $S_B = 20 \text{ MVA}$, $V_B = 161 \text{ kV}$. Hence, 13.2 kV and 13.8 also become base values

Generator G: 15 MVA, 13.2 kV, $x = 0.15 \text{ pu}$
 Motor M: 10 MVA, 13.2 kV, $x = 0.15 \text{ pu}$
 Transformer T1: 2.5 MVA, 13.2/161 kV, $x = 0.10 \text{ pu}$
 Transformer T2: 15 MVA, 161/13.8 kV, $x = 0.10 \text{ pu}$

Equivalent Circuit of the power network



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21. A

$V_B = 161 \text{ kV}$ (selected) hence 13.2 kV and 13.8 kV are also base voltages.
 $S_B = 20 \text{ MVA}$ (selected)

calculate the system parameter according to selected base values:

$$\bar{Z}_{\text{new}} = \bar{Z}_{\text{given}} \left(\frac{V_{\text{given}}}{V_{\text{new}}} \right)^2 \left(\frac{S_{\text{B new}}}{S_{\text{B given}}} \right)$$

$$\text{Generator: } \bar{Z}_{\text{new}} = (0.15) \left(\frac{13.2}{161} \right)^2 \left(\frac{20}{15} \right) = 0.219 \text{ (pu)}$$

$$\text{Motor } \bar{Z}_{\text{new}} = (0.15) \left(\frac{13.2}{161} \right)^2 \left(\frac{20}{10} \right) = 0.275 \text{ (pu)}$$

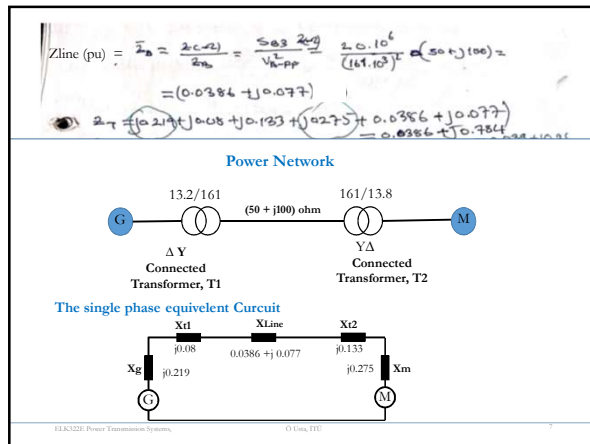
$$\text{T1: } \bar{Z}_{\text{new}} = (0.10) \left(\frac{161}{161} \right)^2 \left(\frac{20}{2.5} \right) = 0.08 \text{ (pu)}$$

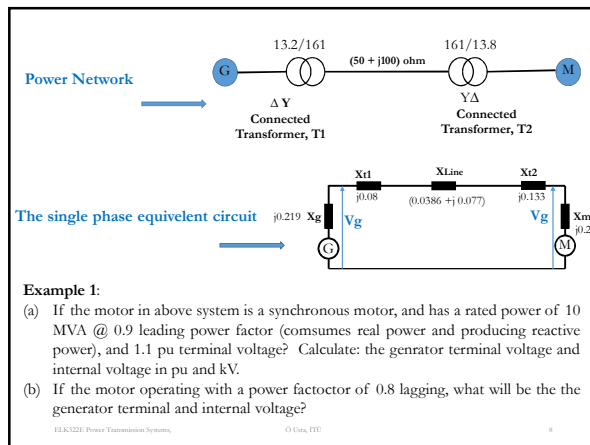
$$\text{T2: } \bar{Z}_{\text{new}} = (0.10) \left(\frac{161}{161} \right)^2 \left(\frac{20}{15} \right) = 0.133 \text{ (pu)}$$

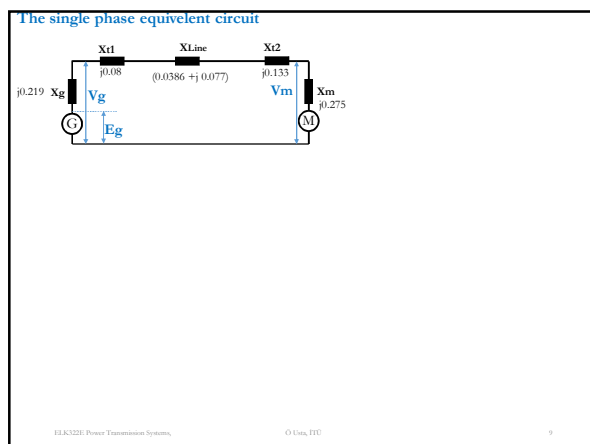
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Example 2

2)

a) Find the pu unit impedances of the system. Use 150 MVA and 138 kV as the base power and the base voltage in the transmission line, respectively. The ratings of the generator, motor and transformers are:

G : 100 MVA, 13.5 kV, $x = 0.2$ pu.
 TR1 : 110 MVA, 138/20 kV, $x = 0.15$ pu.
 TR2 : 100 MVA, 150/138 kV, $x = 0.1$ pu.
 M : 50 MVA, 15 kV, $x = 0.3$ pu.

b) The motor is drawing 45 MVA, 0.8 PF lagging at a line-to-line terminal voltage of 13.5 kV. Determine the terminal voltage and the internal emf of the generator in pu and kV.

$S_{base} = 150 \text{ MVA}$
 $V_{B1} = 138 \text{ kV}$

At the generator's side

138	20	$V_{B2} = 20 \text{ kV}$
138	?	

At the motor's side

150	13.8	$V_{B3} = 12.7 \text{ kV}$
138	?	

Solution 2a

$Z_{pu} = Z_{old} \times \left(\frac{V_{old}}{V_{new}} \right)^2 \times \left(\frac{S_{new}}{S_{old}} \right)$

$Z_{pu} = \frac{Z_{actual}}{Z_{base}} = \frac{Z_{actual}}{\frac{V_{base}^2}{S_{base}}} = Z_{actual} \times \frac{S_{base}}{V_{base}^2}$

$\frac{G}{x_{new}} = 0.2 \times \left(\frac{13.5}{20} \right)^2 \times \left(\frac{150}{100} \right) = 0.137 \text{ pu}$

$\frac{TR1}{x_{new}} = 0.15 \times \left(\frac{20}{138} \right)^2 \times \left(\frac{150}{110} \right) = 0.204 \text{ pu}$

$\frac{TR2}{x_{new}} = 0.1 \times \left(\frac{150}{138} \right)^2 \times \left(\frac{150}{100} \right) = 0.177 \text{ pu}$

$\frac{M}{x_{new}} = 0.3 \times \left(\frac{15}{12.7} \right)^2 \times \left(\frac{150}{50} \right) = 1.255 \text{ pu}$

$\frac{Line}{x_{base(pu)}} = 60 \times \frac{150}{138^2} = 0.472 \text{ pu}$

Solution 2

Line $X_{line}(pu) = 60 \times \frac{150}{138^2} = 0.472 pu$

$j0.137 pu$ $j0.204 pu$ $j0.472 pu$ $j0.177 pu$ $j1.255 pu$

E_g V_g E_m V_m

V_g : terminal voltage of generator
 V_m : terminal voltage of motor

Solution 2b

$S_m = 45 \angle \cos^{-1} 0.8 = 45 \angle 36.87^\circ MVA$

$S_m = \frac{45 \angle 36.87^\circ}{150} = 0.3 \angle 36.87^\circ pu$

$|V_m| = \frac{13.5 kV}{12.7 kV} = 1.063 pu$ $V_m = 1.063 \angle 0^\circ pu$

$I = \frac{S_m^*}{V_m^*} = \frac{0.3 \angle -36.87^\circ}{1.063 \angle 0^\circ} = 0.282 \angle -36.87^\circ pu$

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Solution 2
Generator terminal voltage

$V_g = 1.063 \angle 0^\circ + j(0.204 + 0.177 + 0.472) \cdot 0.282 \angle -36.87^\circ$

$= 1.063 + 0.853 \angle 90^\circ \times 0.282 \angle -36.87^\circ = 1.063 + 0.240 \angle 53.13^\circ$

$= 1.063 + 0.144 + j0.192 = 1.207 + j0.192 = 1.222 \angle 9.04^\circ pu$

$V_g = 1.222 \times 20 = 24.44 kV$

Generator internal (produced) voltage

$E_g = 1.063 \angle 0^\circ + j(0.204 + 0.177 + 0.472 + 0.137) \cdot 0.282 \angle -36.87^\circ$

$= 1.063 + 0.99 \angle 90^\circ \times 0.282 \angle -36.87^\circ = 1.063 + 0.279 \angle 53.13^\circ$

$= 1.063 + 0.167 + j0.223 = 1.23 + j0.223 = 1.25 \angle 10.23^\circ pu$

The generator line-to-line internal emf is $|E_g| = 1.25 \times 20 = 25 kV$ $V_g = 24.4 kV$

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Solution 2b

The motor is drawing 45 MVA @ 0.8 pf leading at a terminal voltage of 13.5 kV (line to line). Determine the terminal voltage of the generator in pu and kV.

$S = 45 MVA @ 0.8$ leading power factor means machine consumes active power and produces reactive power. Then:

$S_m = 45 MVA @ 0.8$ pf leading $= 45 \angle -36.87^\circ MVA$

$S_m = \frac{45 \angle -36.87^\circ}{150} = 0.3 \angle -36.87^\circ$

$V_m = 1.063 \angle 0^\circ pu$ reference.

Or $S_m = V_m I_m^* \rightarrow I_m^* = \frac{S_m}{V_m} = \frac{0.3 \angle -36.87^\circ}{1.063 \angle 0^\circ} = 0.282 \angle -36.87^\circ$

$E_g = (j0.137 + j0.21 + j0.472 + j0.177) \times 0.282 \angle -36.87^\circ + 1.063$

$= j0.99 \times 0.282 \angle -36.87^\circ + 1.063 = 0.279 \angle 53.13^\circ + 1.063$

$E_g = 1.063 + 0.167 + j0.223 = 1.23 + j0.223 = 1.25 \angle 10.23^\circ pu$

$E_g = 0.85 pu = 0.85 \times 20 = 17 kV$

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Motor has 45 MVA rated power @ 0.8 lagging power (Consumes active power and absorbs reactive power)

Motor terminal Voltage $V_m = 1.063 \times 12.7 = 13.5 \text{ kV}$
 Motor Current $I_m = 0.282 \times 11.8 (150 \times 10^6 / (12.7 \times 10^3)) = 3.32 - j36.87 \text{ kA}$
 Motor Power $S_m = 50 \text{ MVA @ } 0.8 \text{ pf lagging}$
 Terminal Voltage $V_t = V_g = 24.4 \text{ kV}$
 Internal Voltage $E_g = 25 \text{ kV}$

Motor has 45 MVA rated power @ 0.8 leading power (Consumes active power and absorbs reactive power)

Motor terminal Voltage $V_m = 1.063 \times 12.7 = 13.5 \text{ kV}$
 Motor Current $I_m = 0.282 \times 11.8 (150 \times 10^6 / (12.7 \times 10^3)) = 3.32 - j36.87 \text{ kA}$
 Motor Power $S_m = 50 \text{ MVA @ } 0.8 \text{ pf leading}$
 Internal Voltage $E_g = 17 \text{ kV}$

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EXAMPLE 3.4 Per-unit circuit: three-zone single-phase network

Three zones of a single-phase circuit are identified in Figure 3.10(a). The zones are connected by transformers T_1 and T_2 , whose ratings are also shown. Using base values of 30 kVA and 240 volts in zone 1, draw the per-unit circuit and

FIGURE 3.10
Circuits for Example 3.4

$Z_{p.u.\text{new}} = Z_{p.u.\text{old}} \left(\frac{V_{\text{base,old}}}{V_{\text{base,new}}} \right)^2 \left(\frac{S_{\text{base,old}}}{S_{\text{base,new}}} \right)$

(a) Single-phase circuit

(b) Per-unit circuit

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determine the per-unit impedances and the per-unit source voltage. Then calculate the load current both in per-unit and in amperes. Transformer winding resistances and shunt admittance branches are neglected.

SOLUTION First the base values in each zone are determined. $S_{\text{base}} = 30 \text{ kVA}$ is the same for the entire network. Also, $V_{\text{base1}} = 240 \text{ volts}$, as specified for zone 1. When moving across a transformer, the voltage base is changed in proportion to the transformer voltage ratings. Thus,

$$V_{\text{base2}} = \left(\frac{480}{240} \right) (240) = 480 \text{ volts}$$

and

$$V_{\text{base3}} = \left(\frac{115}{460} \right) (480) = 120 \text{ volts}$$

The base impedances in zones 2 and 3 are

$$Z_{\text{base2}} = \frac{V_{\text{base2}}^2}{S_{\text{base}}} = \frac{480^2}{30,000} = 7.68 \text{ } \Omega$$

and

$$Z_{\text{base3}} = \frac{V_{\text{base3}}^2}{S_{\text{base}}} = \frac{120^2}{30,000} = 0.48 \text{ } \Omega$$

and the base current in zone 3 is

$$I_{\text{base3}} = \frac{S_{\text{base}}}{V_{\text{base3}}} = \frac{30,000}{120} = 250 \text{ A}$$

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Next, the per-unit circuit impedances are calculated using the system base values. Since $S_{base} = 30 \text{ kVA}$ is the same as the kVA rating of transformer T_1 , and $V_{base1} = 240 \text{ volts}$ is the same as the voltage rating of the zone 1 side of transformer T_1 , the per-unit leakage reactance of T_1 is the same as its nameplate value, $X_{T1p.u.} = 0.1$ per unit. However, the per-unit leakage reactance of transformer T_2 must be converted from its nameplate rating to the system base. Using (3.3.11) and $V_{base2} = 480 \text{ volts}$,

$$X_{T2p.u.} = (0.10) \left(\frac{460}{480} \right)^2 \left(\frac{30,000}{20,000} \right) = 0.1378 \text{ per unit}$$

Alternatively, using $V_{base3} = 120 \text{ volts}$,

$$X_{T2p.u.} = (0.10) \left(\frac{115}{120} \right)^2 \left(\frac{30,000}{20,000} \right) = 0.1378 \text{ per unit}$$

which gives the same result. The line, which is located in zone 2, has a per-unit reactance

$$X_{linep.u.} = \frac{X_{line}}{Z_{base2}} = \frac{2}{7.68} = 0.2604 \text{ per unit}$$

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and the load, which is located in zone 3, has a per-unit impedance

$$Z_{loadp.u.} = \frac{Z_{load}}{Z_{base3}} = \frac{0.9 + j0.2}{0.48} = 1.875 + j0.4167 \text{ per unit}$$

The per-unit circuit is shown in Figure 3.10(b), where the base values for each zone, per-unit impedances, and the per-unit source voltage are shown. The per-unit load current is then easily calculated from Figure 3.10(b) as follows:

$$\begin{aligned} I_{loadp.u.} = I_{sp.u.} &= \frac{V_{sp.u.}}{j(X_{T1p.u.} + X_{linep.u.} + X_{T2p.u.}) + Z_{loadp.u.}} \\ &= \frac{0.9167/0^\circ}{j(0.10 + 0.2604 + 0.1378) + (1.875 + j0.4167)} \\ &= \frac{0.9167/0^\circ}{1.875 + j0.9149} = \frac{0.9167/0^\circ}{2.086/26.01^\circ} \\ &= 0.4395/-26.01^\circ \text{ per unit} \end{aligned}$$

The actual load current is

$$I_{load} = (I_{loadp.u.})_{base3} = (0.4395/-26.01^\circ)(250) = 109.9/-26.01^\circ \text{ A}$$

Note that the per-unit equivalent circuit of Figure 3.10(b) is relatively easy to analyze, since ideal transformer windings have been eliminated by proper selection of base values. ■

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THANKS

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