

**ELK322E  
POWER TRANSMISSION SYSTEMS**



**CHAPTER 1.2: BASIC CONCEPTS**

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**PER-UNIT STEMS**

**1.10 Per-Unit Quantities**

In an electrical power system

$V \rightarrow \text{kV}$ ,  
 $P \rightarrow \text{kW, MW}$ ,  
 $Q \rightarrow \text{kVar, MVar}$ ,  
 $S \rightarrow \text{kVA, MVA}$ ,  
 $Z \rightarrow (\Omega)$ ,  
 $I \rightarrow A, kA$

$380 \text{ kV}$   
 $500 \text{ MVA}$   
 $150 \text{ kVar}$

These quantities are often expressed as a percent or per-unit of a base or reference value specified for each. The per-unit value of quantity is defined as the ratio of the quantity to its base expressed as a decimal.

Advantages:

- $(\text{pu}) = \frac{(\text{actual})}{(\text{base})}$
- using small absolute numbers around 1
- makes comparison very easy

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**PER-UNIT STEMS**

Per-Unit =  $\frac{\text{The actual Value}}{\text{Base Value (Selected)}}$

**Base Values:** All calculation is done using single phase values (Phase voltage, phase current).

**Firstly,** base voltage (kV) and base power (kVA or MVA) are chosen, the other base quantities are then calculated

Base current  $IB = \frac{\text{Base Power (SB, MVA)}}{\text{Base Voltage (Vphase,kV)}}$

Base Impedance  $ZB = \frac{\text{Base Voltage (Vphase,kV)}}{\text{Base current IB}} = \frac{VB^2}{SB} \times 1000$

Per-unit impedance =  $\frac{\text{actual impedance}}{ZB}$  (pu)

Example: For a power system  $S3 = 30 \text{ MVA} = 30 \text{ 000kVA}$ , and  $V_L = 120 \text{ kV}$

Then  $SB = 30/3 = 10 \text{ MW}$ , and  $VB = 120/\sqrt{3} = 69.2 \text{ kV}$ ,  $IB = \frac{SB}{VB} = \frac{10 \text{ 000}}{69.2} \text{ A}$

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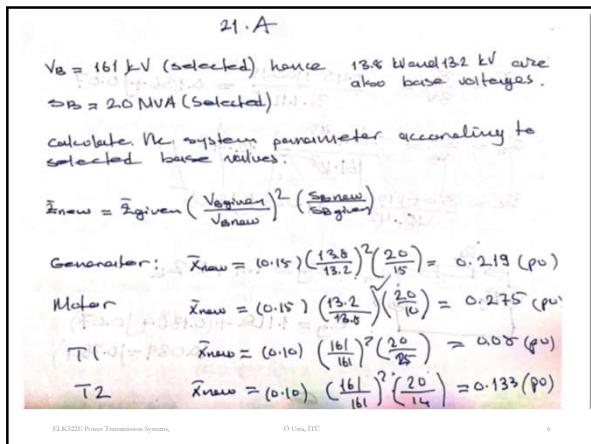
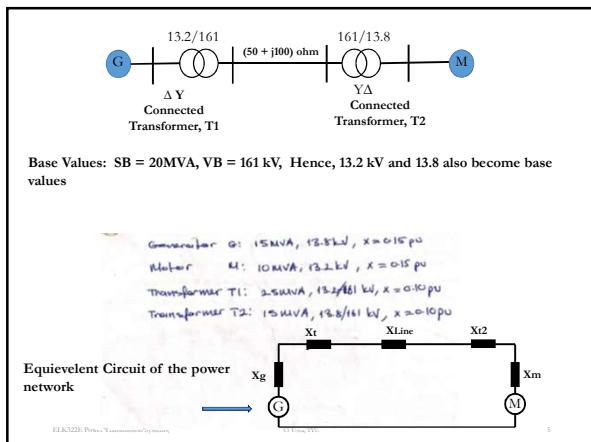
**PER-UNIT STEMS**

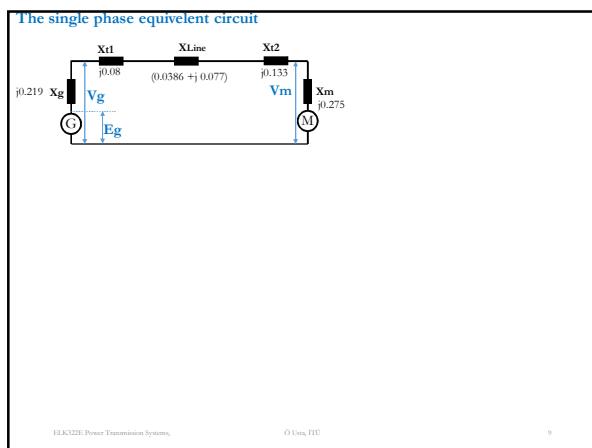
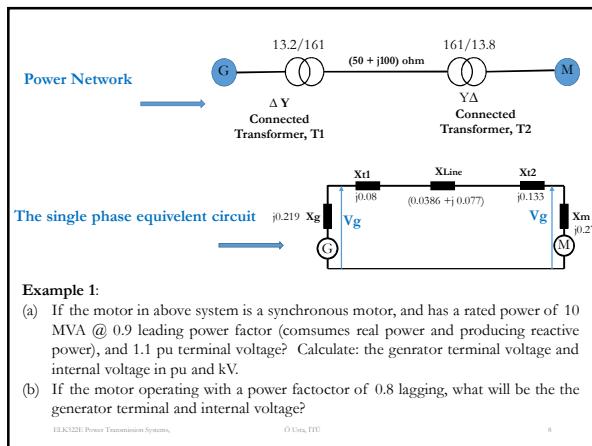
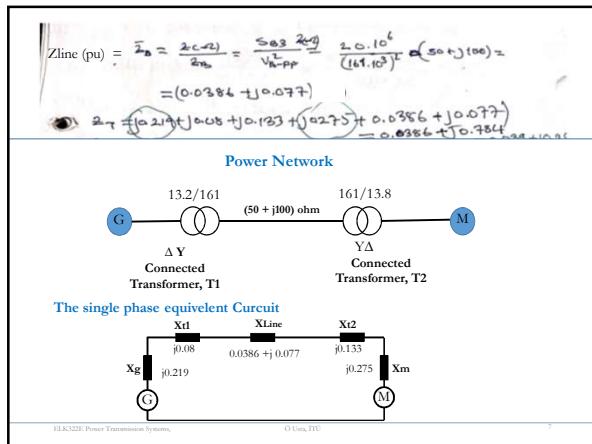
Changing the Base Value: Every element of power systems (generator, transformers, motors and lines) is provided with a manufacturer data sheet in pu values according to their base values. Since in an electrical power system, they are connected each other, their pu values need to be recalculated according to new base values.

$$\tilde{Z}_{\text{new}} = \tilde{Z}_{\text{given}} \left( \frac{V_{B\text{given}}}{V_{B\text{new}}} \right)^2 \left( \frac{S_{B\text{new}}}{S_{B\text{given}}} \right)$$

Example: If the reactance of a generator  $X_d$  is given as 0.25 pu based on generator's rating of 18 kW, 500 MVA, find the  $X_d$  which is based on 20 kV, rated 100 MVA

$$X_{\text{new}} = 0.25 \left( \frac{18}{20} \right)^2 \left( \frac{100}{500} \right) = 0.0405 \text{ pu}$$





**Example 2**

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2) **a)** Find the pu unit impedances of the system. Use 150 MVA and 13.8 kV as the base power and the base voltage in the transmission line, respectively. The ratings of the generator, motor and transformers are:

- G: 100 MVA, 13.5 kV,  $x = 0.2 \text{ pu}$
- T1: 100 MVA, 13.8/20 kV,  $x = 0.15 \text{ pu}$
- T2: 100 MVA, 150/13.8 kV,  $x = 0.1 \text{ pu}$
- M: 50 MVA, 15 kV,  $x = 0.3 \text{ pu}$

**b)** The motor is drawing 45 MVA, 0.8 PF lagging at a line-to-line terminal voltage of 13.5 kV. Determine the terminal voltage and the internal emf of the generator in pu and kV.

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$S_{\text{base}} = 150 \text{ MVA}$   
 $V_{B1} = 13.8 \text{ kV}$

At the generator's side	138	20	$V_{B1} = 20 \text{ kV}$
	138	?	

At the motor's side

(150)	13.8	?	$V_{B2} = 12.7 \text{ kV}$
(150)	13.8	?	

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**Solution 2a**

$$Z_{pu \text{ new}} = Z_{pu \text{ old}} \times \left( \frac{V_{old}}{V_{new}} \right)^2 \left( \frac{S_{old}}{S_{new}} \right)$$

$$Z_{pu} = \frac{Z_{actual}}{Z_{base}} = \frac{Z_{actual}}{\frac{V_{base}}{S_{base}}} = Z_{actual} \times \frac{S_{base}}{V_{base}^2}$$

$$\frac{G}{X_{new}} = 0.2 \times \left( \frac{13.5}{20} \right)^2 \times \left( \frac{150}{100} \right) = 0.137 \text{ pu.}$$

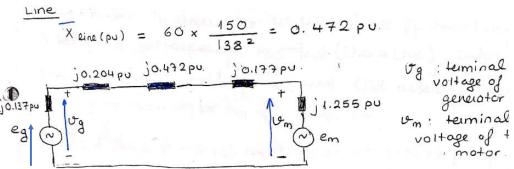
$$\frac{T1}{X_{new}} = 0.15 \times \left( \frac{20}{13.8} \right) \times \left( \frac{150}{110} \right) = 0.204 \text{ pu}$$

$$\frac{T2}{X_{new}} = 0.1 \times \left( \frac{150}{13.8} \right)^2 \times \left( \frac{150}{100} \right) = 0.177 \text{ pu.}$$

$$\frac{M}{X_{new}} = 0.3 \times \left( \frac{15}{12.7} \right)^2 \times \left( \frac{150}{50} \right) = 1.255 \text{ pu.}$$

$$\frac{\text{Line}}{X_{new}(pu)} = 60 \times \frac{150}{150} = 0.472 \text{ pu.}$$

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**Solution 2****Solution 2b**

$$S_M = 45 \angle 0.8^\circ \text{ MVA}$$

$$\dot{S}_M = \frac{45 \angle 36.87^\circ}{150} = 0.3 \angle 36.87^\circ \text{ pu}$$

$$|U_m| = \frac{13.5 \text{ kV}}{12.7 \text{ kV}} = 1.063 \text{ pu} \quad U_m = 1.063 \angle 0^\circ \text{ pu ref}$$

$$I = \frac{\dot{S}_M}{U_m^2} = \frac{0.3 \angle 36.87^\circ}{1.063 \angle 0^\circ} = 0.282 \angle -36.87^\circ \text{ pu}$$

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**Solution 2**  
Generator terminal voltage

$$V_g = 1.063 \angle 0^\circ + j(0.204 + 0.177 + 0.472) \cdot 0.282 \angle -36.87^\circ$$

$$= 1.063 + 0.853 \angle 90^\circ \times 0.282 \angle -36.87^\circ = 1.063 + 0.240 \angle 53.13^\circ$$

$$= 1.063 + 0.144 + j0.192 = 1.207 + j0.192 = 1.222 \angle 9.04^\circ \text{ pu}$$

$$V_g = 1.222 \times 20 = 24.44 \text{ kV}$$

Generator internal (produced) voltage

$$V_g = 1.063 \angle 0^\circ + j(0.204 + 0.177 + 0.472 + 0.137) \cdot 0.282 \angle -36.87^\circ$$

$$= 1.063 + 0.99 \angle 90^\circ \times 0.282 \angle -36.87^\circ = 1.063 + 0.279 \angle 53.13^\circ$$

$$= 1.063 + 0.167 + j0.223 = 1.23 + j0.223 = 1.25 \angle 10.23^\circ \text{ pu}$$

The generator line-to-line internal emf is  
 $|E_g| = 1.25 \times 20 = 25 \text{ kV}$

$$|E_g| = 24.4 \text{ kV}$$

**Solution 2b** The motor is drawing 45 MVA @ 0.8 pf leading at a terminal voltage of 13.5 kV (line-to-line), determine the terminal voltage of and the internal voltage of the generator in pu and kV.

$S = 45 \text{ MVA} @ 0.8 \text{ leading power factor means machine consumes active power and produces reactive power. Then:}$

$$S_M = 45 \text{ MVA} @ 0.8 \text{ pf leading} = 45 \angle 36.87^\circ \text{ MVA}$$

$$E_m = \frac{45}{150} \angle 36.87^\circ = 0.3 \angle 36.87^\circ$$

$\sqrt{V_M} = 1.063 \angle 0^\circ \text{ pu reference.}$

$$\text{On } E_m = \sqrt{V_M I_M} \rightarrow I_M = \frac{E_m}{\sqrt{V_M}} = \frac{0.3 \angle 36.87^\circ}{1.063 \angle 0^\circ} = 0.28 \angle 36.87^\circ \text{ pu}$$

$$E_g = (0.9137 + j0.21 + j0.47 + j0.177) \times 0.28 \angle 36.87^\circ + 0.137$$

$$= j0.99 \times 0.28 \angle 36.87^\circ + 0.06 = 0.278 \angle 126.87^\circ + 0.137$$

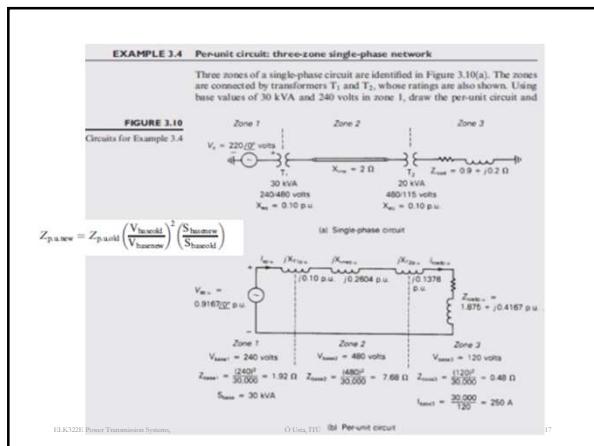
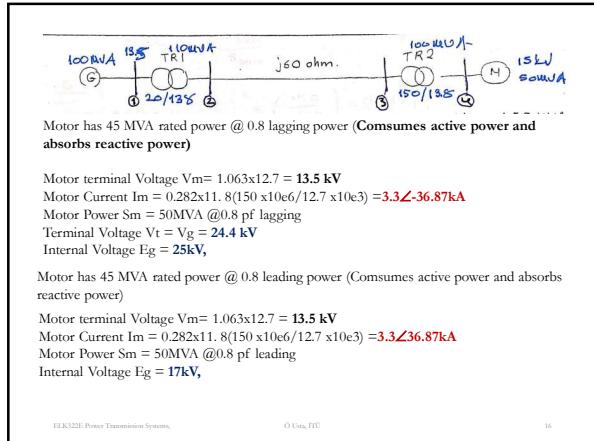
$$E_g = -j9.167 + j0.221 + j0.63 = 0.856 + j0.221 = 0.856 \angle 22.5^\circ$$

$$E_g = 0.85 \text{ pu} = 0.85 \times 20 = 17 \text{ kV}$$

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determine the per-unit impedances and the per-unit source voltage. Then calculate the load current both in per-unit and in amperes. Transformer winding resistances and shunt admittance branches are neglected.

**SOLUTION** First the base values in each zone are determined.  $S_{base} = 30 \text{ kVA}$  is the same for the entire network. Also,  $V_{base} = 240 \text{ volts}$ , as specified for zone 1. When moving across a transformer, the voltage base is changed in proportion to the transformer voltage ratings. Thus,

$$V_{base2} = \left( \frac{480}{240} \right) (240) = 480 \text{ volts}$$

and

$$V_{base3} = \left( \frac{115}{460} \right) (480) = 120 \text{ volts}$$

The base impedances in zones 2 and 3 are

$$Z_{base2} = \frac{V_{base2}^2}{S_{base}} = \frac{480^2}{30,000} = 7.68 \Omega$$

and

$$Z_{base3} = \frac{V_{base3}^2}{S_{base}} = \frac{120^2}{30,000} = 0.48 \Omega$$

and the base current in zone 3 is

$$I_{base3} = \frac{S_{base}}{\sqrt{V_{base3}}} = \frac{30,000}{\sqrt{120}} = 250 \text{ A}$$

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Next, the per-unit circuit impedances are calculated using the system base values. Since  $S_{base} = 30 \text{ kVA}$  is the same as the kVA rating of transformer  $T_1$ , and  $V_{base} = 240 \text{ volts}$  is the same as the voltage rating of the zone 1 side of transformer  $T_1$ , the per-unit leakage reactance of  $T_1$  is the same as its nameplate value,  $X_{T1p.u.} = 0.1 \text{ per unit}$ . However, the per-unit leakage reactance of transformer  $T_2$  must be converted from its nameplate rating to the system base. Using (3.3.11) and  $V_{base2} = 480 \text{ volts}$ ,

$$X_{T2p.u.} = (0.10) \left( \frac{460}{480} \right)^2 \left( \frac{30,000}{20,000} \right) = 0.1378 \text{ per unit}$$

Alternatively, using  $V_{base3} = 120 \text{ volts}$ ,

$$X_{T2p.u.} = (0.10) \left( \frac{115}{120} \right)^2 \left( \frac{30,000}{20,000} \right) = 0.1378 \text{ per unit}$$

which gives the same result. The line, which is located in zone 2, has a per-unit reactance

$$X_{linep.u.} = \frac{X_{line}}{Z_{base2}} = \frac{2}{7.68} = 0.2604 \text{ per unit}$$

and the load, which is located in zone 3, has a per-unit impedance

$$Z_{loadp.u.} = \frac{Z_{load}}{Z_{base3}} = \frac{0.9 + j0.2}{0.48} = 1.875 + j0.4167 \text{ per unit}$$

The per-unit circuit is shown in Figure 3.10(b), where the base values for each zone, per-unit impedances, and the per-unit source voltage are shown. The per-unit load current is then easily calculated from Figure 3.10(b) as follows:

$$\begin{aligned} I_{loadp.u.} &= I_{sp.u.} = \frac{V_{sp.u.}}{j(X_{T1p.u.} + X_{linep.u.} + X_{T2p.u.}) + Z_{loadp.u.}} \\ &= \frac{0.9167/0^\circ}{j(0.10 + 0.2604 + 0.1378) + (1.875 + j0.4167)} \\ &= \frac{0.9167/0^\circ}{1.875 + j0.9149} = \frac{0.9167/0^\circ}{2.086/26.01^\circ} \\ &= 0.4395/-26.01^\circ \text{ per unit} \end{aligned}$$

The actual load current is

$$I_{load} = (I_{loadp.u.}) I_{base3} = (0.4395/-26.01^\circ)(250) = 109.9/-26.01^\circ \text{ A}$$

Note that the per-unit equivalent circuit of Figure 3.10(b) is relatively easy to analyze, since ideal transformer windings have been eliminated by proper selection of base values. ■

**THANKS**