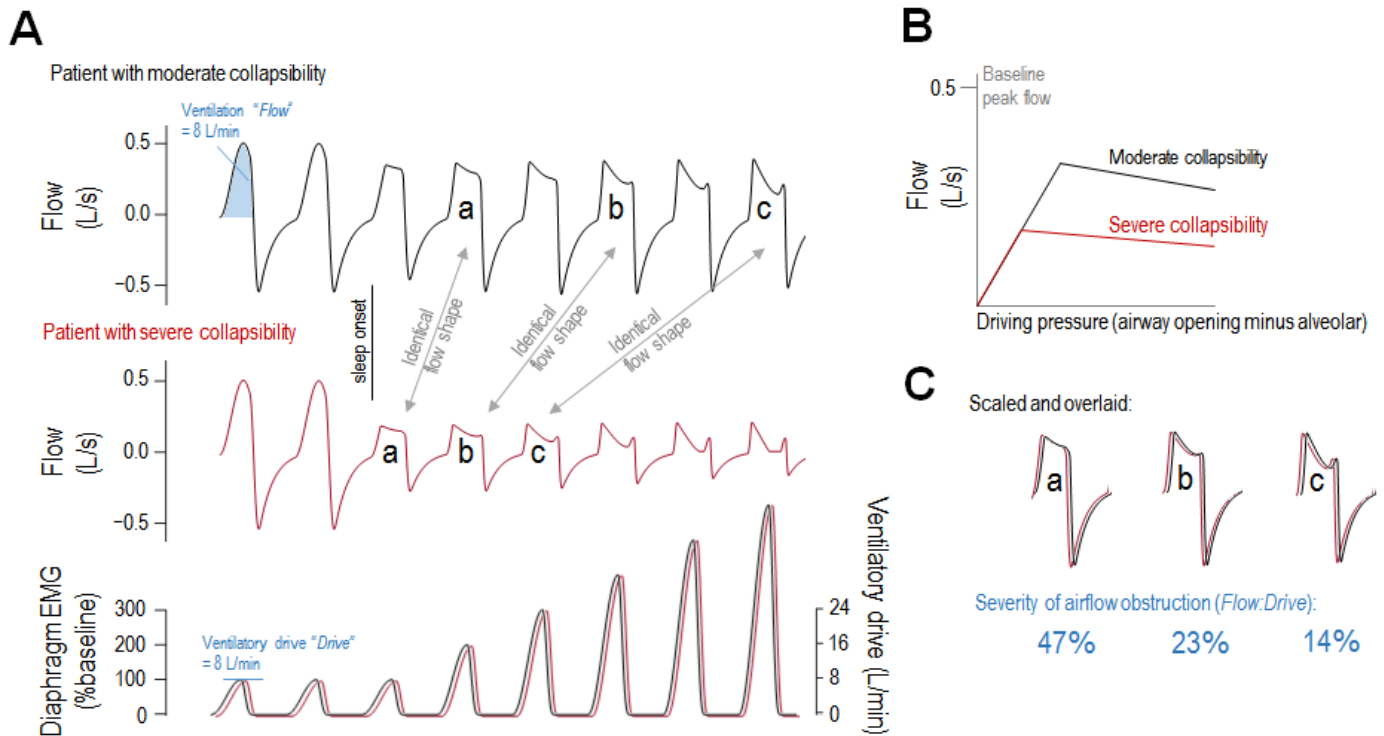


# **Quantifying the Magnitude of Pharyngeal Obstruction During Sleep Using Airflow Shape**

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## **Online Data Supplement**

## Simulation illustrating the relationship between airflow obstruction and flow shape



**Figure S1: The flow-time profile ("flow shape") is theoretically a manifestation of the degree of mismatch between the actual ventilatory flow and the intended airflow or ventilatory drive, i.e. *flow:drive*.** (A) Two computer simulations are presented. In both "patients", the same progressive rise in ventilatory drive was provided (diaphragm EMG). The "patient" with moderate collapsibility (black, top) has an airway that permits twice the airflow of the "patient" with severe collapsibility (red, middle), see airway flow-pressure profile in Panel B. Note that a more collapsible airway (black vs red) and increased ventilatory drive both promote more apparent flow limitation (flattening and scooping of inspiratory flow, elongation of inspiratory time). Note that the exact same flow shape occurs whenever moderate collapse is exposed to twice that of the severe collapse (flow shapes "a", "b", "c"). In each case of identical shape, there has been no change in the ratio of ventilation to ventilatory drive (*flow:drive* = 47% in "a", 23% in "b", 14% in "c"), hence no change in manifest flow shape, see Panel C for scaled and overlaid signals.

Model details pertaining to Figure S1 are as follows: The equation of motion of the respiratory system was a standard lumped resistance and compliance model, modified to include a nonlinear resistance consistent with flow-limitation (see Panel B); respiratory system compliance = 80 ml/cmH<sub>2</sub>O, resistance (linear portion at low flow) was based on a time constant of 0.6 s, peak inspiratory muscle pressure (shown as "diaphragm EMG") was 8 cmH<sub>2</sub>O at baseline. A short time-constant for pharyngeal collapse (30 ms) was incorporated to mimic physiological signals. Greater collapsibility was simulated by reducing the maximum inspiratory flow while maintaining the shape of the pressure-flow profile constant.

### **Calibration of diaphragm EMG to measure ventilatory drive**

To calibrate intraesophageal diaphragm EMG swings (EMGdi, units of  $\mu\text{V}$ ) to reflect *intended ventilation* or *ventilatory drive* (units of L/min) i.e. the ventilation expected based on neural output when the respiratory mechanics are normal for each individual, we identified suitable reference breaths throughout the night as follows: Breaths during wake or arousal (at least two breaths away from scored sleep) were selected. Breaths were excluded if they were within the margins of a scored respiratory event or had a reduced ventilation (more than 30% below local average). We expected that *ventilation* and *ventilatory drive* were equal at these times. The use of wakefulness levels to calibrate drive and define normal respiratory mechanics means that any baseline non-sleep-related mechanical deficits can be avoided in the measurement, i.e. only a sleep-related mismatch between flow and drive will be captured by our gold standard.

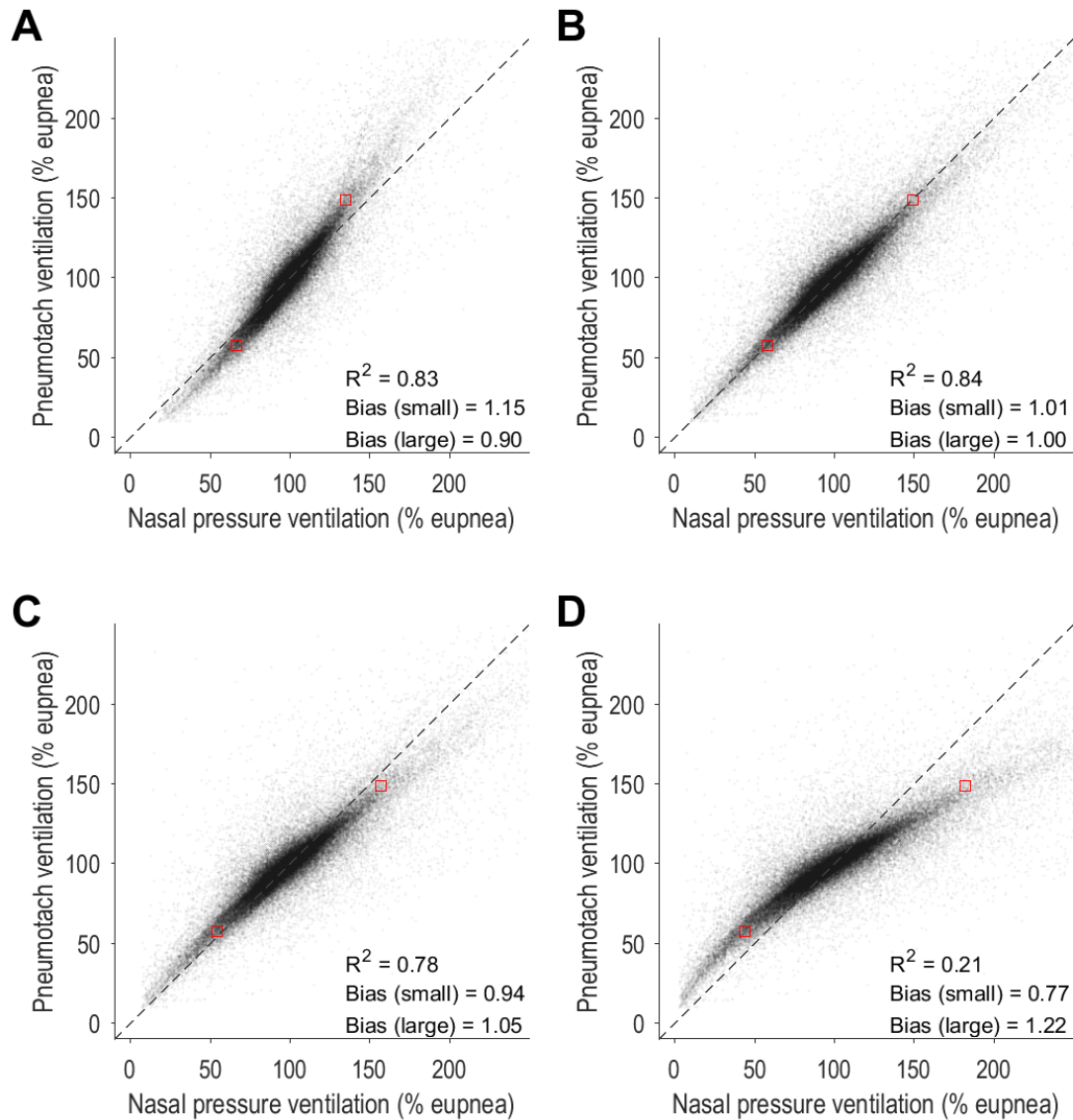
For each breath, we calculated the ratio of the ventilation ( $V_E$ ) to EMGdi (root-mean-squared diaphragm EMG signal, 160 ms smoothing; EMG swings (in  $\mu\text{V}$ ) were taken as the peak minus pre-inspiratory values, and normalised to yield values in L/min using automatically-identified reference breaths defined above), given by  $G = V_E : \text{EMGdi}$  (units of L/min/ $\mu\text{V}$ ). Rather than define a single average value of G for calibration of diaphragm EMG, we considered that in some circumstances the diaphragm EMG signal amplitude may change over time. Thus, a moving-time average of G was calculated to handle possible overnight calibration drift; a weighting approach allowed the moving-time-averaged calibration factor to be determined predominantly by local calibration data where available. EMGdi for each breath was multiplied by G to yield *ventilatory drive* (units of L/min).

### **Nasal pressure linearisation**

The nasal pressure signal was linearised using a power-law transform. Traditionally, nasal pressure has been linearised to correspond more closely with relative changes in (gold-standard) pneumotachograph flow using an “exponent” of  $\frac{1}{2}$ , i.e. the square-root transform [1-3]. However, it is evident from the original data, that the square-root transformation is an excessive approximation [1, 2]. In our recent studies, we instead advocated using a transform that was more subtle (i.e. power of  $\frac{2}{3}$ ) to obtain a closer match to data from the pneumotachograph ventilation signal [4, 5].

In the current study we measured gold-standard oronasal pneumotachograph flow and nasal pressure in 17 patients simultaneously, via a modified cannula referenced to mask pressure to reflect the clinically-available intranasal pressure signal; DC-coupled. Individual breaths were identified and segmented by an automated computer algorithm. Here we formally assessed several nasal pressure transforms:  $\frac{1}{2}$  (square-root),  $\frac{2}{3}$ ,  $\frac{3}{4}$ , and 1 (untransformed) and compared magnitude of ventilation (tidal volume  $\times$  respiratory rate) on each breath (normalised to the local average) to gold standard values. Data from all patients were pooled. Results are

shown in Figure S2. We found that linearisation was best with  $\frac{2}{3}$  exponent, illustrated by greater symmetry around the line of identity; this exponent no longer led to the systematic overestimation of large breaths and underestimation of small breaths like the untransformed signal (Figure S2D), but also did not yield systematic *underestimation* of large breaths and *overestimation* of small breaths as with the square-root transform (Figure S2A).



**Figure S2.** Nasal pressure transforms for clinical estimation of ventilation. Gold standard breath-by-breath ventilation in 17 patients (normalised to eupnoea i.e. local average in 3 min period) is compared to values estimated using nasal pressure. Values of 1 denote eupneic (average) ventilation. Transforms using the following exponents are shown **(A)**  $\frac{1}{2}$  (square-root), **(B)**  $\frac{2}{3}$ , **(C)**  $\frac{3}{4}$ , and **(D)** 1 (untransformed). Note the improved symmetry about the line of identity (as shown by dashed line) with the  $\frac{2}{3}$  transform in **(B)**. The small red squares are shown to illustrate systematic discrepancies between measures (or lack thereof); median values are shown for large ( $>1.3 \times$  eupnoea) and small ( $<0.7 \times$  eupnoea) breaths. Note the systematic overestimation of small breaths (bias  $>1$ , where bias = nasal pressure ventilation / pneumotach ventilation), and underestimation of large breaths (bias  $<1$ ) in panel A, with the traditional square root transform.  $R^2$  = coefficient of determination.

## Initial feature list

We identified 85 features from the literature and our own development that met the following criteria:

- Features represented shape aspects of pharyngeal airflow obstruction or flow limitation including: flattening, asymmetry, scooping, altered ratios of inspiratory/expiratory durations and volumes, irregularities, fluttering.
- Features were *breath independent*, i.e. stand-alone values could be obtained from a single breath without context, and do not rely on differences with respect to neighbouring breaths or selected reference breaths in the same individual. Thus we did not include features such as the change in inspiratory time relative to normal reference breaths [6].
- Features were *amplitude independent*, i.e. a breath that was simply larger but had the same shape would yield the same exact features, thereby enabling application in cases of un-calibrated flow signals.
- Features were *timing independent*, i.e. a breath that was simply slower and longer would yield the same features, thereby having equal potential application in cases where breathing is faster e.g. children. Accordingly, features from the “Asymmetry” and “Flutter” categories used uniform time spacing, to ensure timing independence. The time series for each inspiratory breath was resampled to 200 data points, while the time series for each expiratory breath was resampled to 250 data points prior to determination of feature values.
- Features consistently yield real values, i.e. yield “indeterminant” values <0.1% of the time.
- Features can be easily and rapidly computed without comparison to a template, lookup table, database, neural network or otherwise.

At the outset of the current investigation, we recognised that detection of appropriate inspiratory and expiratory start and end times could play a major role in determining values from each feature. Two approaches were employed: 1) our “original” in-house algorithm for detecting start and end times of breaths based primarily on volume maxima and minima, and 2) a modified timing algorithm that separately identifies the start and end times of inspiration and expiration based on the periods where 95% of the volume inspired/expired is observed, referred to as “transition” timing [7]. Based on preliminary univariate analysis indicating non-linear relationships, transformed features (square and square-root) were included as additional candidate features for selection.

**Table S1. List of 85 flow-shape features used throughout the study**

No.	Feature Label	Description	Ref.	Bivariate (R <sup>2</sup> ) vs. flow:drive		Pnasal vs. Pneumotach. R <sup>2</sup> (bias)
				Pneumotach.	Pnasal	
Flattening (N=28)						
1	MIF_PIF	mean Insp Flow/Peak Insp Flow	¶[8, 9]	0.46 [O, 2]	0.31	0.73 (0.96)
2	Ali_InspFlat	AUC of abs(Insp Flow(Insp Time(0.1 to 0.9)) - MIF)	¶[9, 10]	(-) 0.29 [T, 2]	0.25	0.65 (1.01)
3	Ali_ExpFlat	AUC of abs(Exp Flow(Exp Time(0.2 to 0.8)) - MEF)	¶[9, 10]	0.28 [T, 1/2]	0.23	0.6 (0.99)
4	Ali_InspExpFlat	Insp flat index / Exp flat index	[9]	(-) 0.3 [T, 1/2]	0.23	0.32 (1.01)
5	AA_InspFlat9020	sum(Insp Flow>0.9)/sum(Insp Flow>0.2);	[11]	0.4 [O, 1/2]	0.30	0.68 (0.96)
6	AA_InspFlat8020	sum(Insp Flow>0.8)/sum(Insp Flow>0.2);	[11]	0.42 [O, 1]	0.30	0.72 (0.97)
7	AA_InspFlat7020	sum(Insp Flow>0.7)/sum(Insp Flow>0.2);	[11]	0.42 [O, 2]	0.30	0.73 (0.96)
8	AA_InspFlat6020	sum(Insp Flow>0.6)/sum(Insp Flow>0.2);	[11]	0.42 [O, 2]	0.31	0.71 (0.98)
9	AA_InspFlat5020	sum(Insp Flow>0.5)/sum(Insp Flow>0.2);	[11]	0.41 [O, 2]	0.30	0.65 (0.98)
10	AA_InspFlat90Ti	sum(Insp Flow>0.9)/sum(Insp Flow>0);	[11]	0.42 [O, 1/2]	0.30	0.68 (0.96)
11	AA_InspFlat80Ti	sum(Insp Flow>0.8)/sum(Insp Flow>0);	[11]	0.43 [O, 1]	0.30	0.73 (0.97)
12	AA_InspFlat70Ti	sum(Insp Flow>0.7)/sum(Insp Flow>0);	[11]	0.43 [O, 1]	0.30	0.73 (0.98)
13	AA_InspFlat60Ti	sum(Insp Flow>0.6)/sum(Insp Flow>0);	[11]	0.44 [O, 2]	0.31	0.73 (0.97)
14	AA_InspFlat50Ti	sum(Insp Flow>0.5)/sum(Insp Flow>0);	[11]	0.43 [O, 2]	0.30	0.69 (0.98)
15	AA_ExpFlat9020	sum(Exp Flow>0.9)/sum(Exp Flow>0.2);	[11]	0.34 [O, 1]	0.24	0.49 (0.95)
16	AA_ExpFlat8020	sum(Exp Flow>0.8)/sum(Exp Flow>0.2);	[11]	0.35 [O, 1]	0.25	0.49 (0.99)
17	AA_ExpFlat7020	sum(Exp Flow>0.7)/sum(Exp Flow>0.2);	[11]	0.34 [O, 1]	0.26	0.5 (1)
18	AA_ExpFlat6020	sum(Exp Flow>0.6)/sum(Exp Flow>0.2);	[11]	0.33 [O, 1]	0.26	0.52 (1.01)
19	AA_ExpFlat5020	sum(Exp Flow>0.5)/sum(Exp Flow>0.2);	[11]	0.33 [T, 2]	0.24	0.36 (1)
20	AA_ExpFlat90Te	sum(Exp Flow>0.9)/sum(Exp Flow>0);	[11]	0.35 [O, 1/2]	0.24	0.55 (0.98)
21	AA_ExpFlat80Te	sum(Exp Flow>0.8)/sum(Exp Flow>0);	[11]	0.35 [O, 1/2]	0.25	0.59 (1)
22	AA_ExpFlat70Te	sum(Exp Flow>0.7)/sum(Exp Flow>0);	[11]	0.35 [T, 2]	0.24	0.56 (0.98)
23	AA_ExpFlat60Te	sum(Exp Flow>0.6)/sum(Exp Flow>0);	[11]	0.35 [T, 2]	0.24	0.55 (0.99)
24	AA_ExpFlat50Te	sum(Exp Flow>0.5)/sum(Exp Flow>0);	[11]	0.35 [T, 2]	0.24	0.54 (1)
25	MIF50	mean(Insp Flow(time(0.25 to 0.75)))	¶[10, 12]	0.48 [O, 2]	0.33	0.83 (0.98)
26	MEF50	mean(Exp Flow(time(0.25 to 0.75)))	¶[10, 12]	(-) 0.32 [T, 1/2]	0.23	0.49 (1.02)
27	Teschler	AUC btw y=1 and mean normalised flow (time(0.25:0.75))	[10]	(-) 0.34 [T, 1]	0.26	0.66 (1.02)
28	MostPromPeakW	Duration of Most Prominent Insp Peak / Ti. See Matlab “findpeaks” for details.	New	0.48 [O, 1]	0.35	0.7 (0.96)
Scooping (deviation away from normal round contour) (N=8)						
29	AA_NED	(PIF - Flow at mid-Inspiration) / PIF	[13]	(-) 0.42 [O, 1/2]	0.29	0.74 (1.04)
30	AreaUnderPeaksI	AUC between flow and connected peaks	New	(-) 0.49 [O, 1/2]	0.35	0.76 (1.12)
31	QuadI	Absolute AUC between a quadratic best fit to 3 points in inspiration (x,y: start insp, 0; Ti/2, 1; end insp, Ti) and actual inspiratory waveform, divided by Ti.	[14]	(-) 0.46 [O, 1/2]	0.31	0.82 (1.02)
32	QuadI50	Same as SinI but AUC from 25 <sup>th</sup> to 75 <sup>th</sup> centiles of inspiratory time, divided by Ti	[12]	(-) 0.46 [O, 1/2]	0.31	0.82 (1.02)
33	QuadE	Same as SinI but during expiration	New	(-) 0.33 [O, 1/2]	0.30	0.77 (1)
34	InvParabI	Absolute AUC between an inverted parabola (with matched peak flow [value=1] forced to be zero at the start and end of inspiration) and inspiratory waveform, divided by Ti: Fit equation is $y=c \times ((1-(x.^2)/(N/2)^2))$ : c is maximum	New	(-) 0.45 [O, 1/2]	0.33	0.78 (1)

		inspiratory flow (equal to 1), N is the length of the inspiratory flow, x is the adjusted time base, shifted to be equal about zero.				
35	Ellipsel	Same as InvParabl but using an ellipse fit to Inspiration: $y=c \times (((1-(x.^2)/(N/2)^2)).^(1/2))$	New	(-) 0.49 [O, 1/2]	0.35	0.78 (1.03)
36	Hypcosl	Same as InvParabl but using hyperbolic cosine fit to Inspiration, $y=c \times ((1-\cosh((x/(N/2)) \times \log(1+b+\sqrt{2+b} \times \sqrt{b}))+b)/b)$ ; b is set as a constant = 10.	New	(-) 0.49 [O, 1/2]	0.36	0.8 (1.02)
<b>Asymmetry (N=9)</b>						
37	AsymIndex +	Expiratory flow limitation algorithm based on asymmetry	[15]	(-) 0.32 [O, 2]	0.23	0.61 (1.04)
38	SkewDistInsp * §	skewness(distribution data of Insp flow)	¶[16]	0.27 [T, 1/2]	0.24	0.82 (1.01)
39	KurtDistInsp * §	kurtosis(distribution data of Insp flow)	¶[14]	(-) 0.3 [T, 1]	0.24	0.44 (1)
40	SkewDistExp * §	skewness(distribution data of Exp flow)	¶[16]	(-) 0.3 [T, 1]	0.24	0.54 (0.91)
41	KurtDistExp * §	kurtosis(distribution data of Exp flow)	¶[14]	(-) 0.28 [T, 1/2]	0.23	0.25 (0.96)
42	AsymmetryInsp *	(areaL/AreaInsp Flow)-(areaR/AreaInsp Flow)	[11]	0.27 [O, 2]	0.24	0.6 (1)
43	KurtDataInsp *	kurtosis(Insp Flow);	[11]	0.27 [O, 1/2]	0.23	0.66 (0.96)
44	AsymmetryExp *	(areaL/AreaExp Flow)-(areaR/AreaExp Flow)	[11]	(-) 0.29 [T, 2]	0.24	0.51 (0.73)
45	KurtDataExp *	kurtosis(Exp Flow)	[11]	(-) 0.31 [T, 1/2]	0.23	0.42 (1.01)
<b>Timing and volume ratio measures (N=28)</b>						
46	Ti_Ttot	Ti / (Ti+Te)	[8, 17]	(-) 0.32 [O, 2]	0.28	0.7 (1.04)
47	Ti_Te	Ti / Te	[18]	(-) 0.32 [T, 1]	0.28	0.62 (1.04)
48	TTran_i_Ti ‡	Transition time (Insp to Exp) / Ti	[7]	0.27 [T, 1/2]	0.28	0.66 (1.03)
49	TTran_i_Ttot ‡	Transition time (Insp to Exp) / Ttot	[7]	0.27 [T, 1/2]	0.26	0.69 (1.04)
50	TTran_e_Te ‡	Transition time (Exp to Insp) / Te	[7]	(-) 0.29 [T, 1/2]	0.25	0.45 (0.95)
51	TTran_e_Ttot ‡	Transition time (Exp to Insp) / Ttot	[7]	(-) 0.27 [T, 1]	0.23	0.56 (0.89)
52	VTi_VTe	VTi / VTe	[9]	(-) 0.3 [T, 1]	0.23	0.15 (0.99)
53	VTi_VT	VTi / VT where VT = (VTi×Ti+VTe×Te) / (Ti + Te)	[9]	(-) 0.3 [T, 1]	0.23	0.15 (0.99)
54	VTe_VT	VTe / VT where VT = (VTi×Ti+VTe×Te) / (Ti + Te)	[9]	0.28 [T, 1/2]	0.23	0.33 (1)
55	VPEF/VTe	Volume at PEF / VTe	[19, 20]	0.27 [T, 2]	0.23	0.14 (1.1)
56	VPIFVTi	Insp Volume at PIF / VTi	¶[21]	(-) 0.27 [O, 2]	0.23	0.67 (1.01)
57	InspVol_03Ti	Insp Volume at 1/3 × Ti	¶[21]	(-) 0.27 [T, 2]	0.23	0.71 (0.98)
58	PIF_MIF	Peak Insp flow / Mean Insp flow	[16]	(-) 0.41 [O, 1/2]	0.30	0.72 (1.01)
59	FTi	Inspiratory fall time, 90% to 10% (of PIF) / Ti	¶[22]	(-) 0.28 [O, 2]	0.23	0.69 (1.11)
60	RTi	Inspiratory rise time, 10% to 90% (of PIF) / Ti	¶[22]	(-) 0.3 [O, 2]	0.26	0.67 (1.2)
61	DTi	Inspiratory dwell time, flow >= 90% (of PIF) / Ti	¶[22]	0.37 [O, 1/2]	0.27	0.55 (0.97)
62	FTe	Expiratory fall time, 90% to 10% (of PEF) / Te	[22]	(-) 0.31 [O, 2]	0.26	0.47 (1.02)
63	RTe	Expiratory rise time, 10% to 90% (of PEF) / Te	[22]	0.3 [T, 1/2]	0.25	0.57 (1)
64	DTe	Expiratory dwell time, flow >= 90% (of PEF) Te	[22]	0.33 [O, 1/2]	0.24	0.57 (1)
65	PIF_PEF	Peak Insp flow / Peak Exp flow	[16, 23]	(-) 0.28 [O, 1/2]	0.27	0.62 (0.97)
66	MIF_MEF	mean Insp flow to mean Exp flow	¶[16]	(-) 0.32 [O, 1/2]	0.28	0.64 (0.96)
67	MIF50_MEF50	mean (Insp Flow(time(0.25 to 0.75))) / same in Exp	¶(17)	(-) 0.28 [O, 1/2]	0.24	0.64 (0.96)
68	SeriesIeflow	ratio of Insp flow to Exp flow at mid volumes	[24]	(-) 0.27 [T, 1]	0.23	0.13 (1.03)
69	SeriesIetime	ratio of Insp time to Exp time at mid volumes	¶[24]	(-) 0.36 [T, 1]	0.32	0.55 (0.97)
70	KaplanEvol	ratio of Insp volume to Exp volume at mid times	¶[24]	0.27 [T, 2]	0.23	0.14 (1.1)
71	TpeakI_Ti	Time to PIF / Ti	¶[25]	(-) 0.27 [O, 2]	0.24	0.72 (1)
72	TpeakE_Te	Time to PEF / Te	[19, 25, 26]	0.32 [T, 1/2]	0.26	0.59 (1.01)

73	TpeakI_TpeakE	Time to PIF / time to PEF	¶(17)	(-) 0.33 [O, 1/2]	0.28	0.61 (1.01)
<b>Fluttering (N=12)</b>						
74	Power5to12I *	power in Insp flutter [5 to (Fs/2) Hz] / PIF squared	[9]	(-) 0.47 [O, 1/2]	0.42	0.6 (1.02)
75	Power5to12E *	power in Exp flutter [5 to (Fs/2) Hz] / PEF squared	[9]	(-) 0.31 [O, 1/2]	0.26	0.54 (1.04)
76	InspExpFlutPowOrig *	power in Insp flutter / power in Exp flutter [5 to (Fs/2)]	¶[9]	(-) 0.3 [O, 2]	0.24	0.46 (0.83)
77	InspExpFlutPowOrig_Sum *	power in Insp / (Pow Insp + Pow Exp)	¶[9]	(-) 0.3 [O, 2]	0.24	0.46 (0.83)
78	InspFlutPow4to7 *	power in Insp flutter [4-7 Hz] / PIF squared	¶[9]	(-) 0.34 [O, 1/2]	0.29	0.57 (0.95)
79	ExpFlutPow4to7 *	power in Exp flutter [4-7 Hz] / PEF squared	¶[9]	(-) 0.31 [T, 1/2]	0.24	0.49 (1.01)
80	InspExpFlutPow4to7 *	power in Insp flutter / power in Exp flutter [4-7 Hz]	¶[9]	0.28 [O, 1/2]	0.25	0.58 (0.97)
81	InspExpFlutPow4to7_Sum *	power in Insp flutter / (pow in Insp + pow in Exp [4-7 Hz])	¶[9]	0.28 [O, 1/2]	0.25	0.58 (0.97)
82	InspFlutPow8to12 *	power in Insp flutter [8-12 Hz] / PIF squared	¶[9]	(-) 0.43 [O, 1/2]	0.40	0.57 (0.92)
83	ExpFlutPow8to12 *	power in Exp flutter [8-12 Hz] / PEF squared	¶[9]	(-) 0.31 [T, 1/2]	0.24	0.53 (0.85)
84	InspExpFlutPow8to12 *	power in Insp flutter / power in Exp flutter [8-12 Hz]	¶[9]	(-) 0.29 [O, 1]	0.23	0.2 (0.9)
85	InspExpFlutPow8to12_Sum *	power in Insp flutter / (pow in Insp + pow in Exp [8-12 Hz])	¶[9]	(-) 0.28 [O, 2]	0.23	0.36 (0.91)

Bivariate results are not cross-validated, showing timing variant as O (original) or transition (T) and transform (1/2, 1 or 2) for highest coefficient of determination for pneumotachograph (Pneumotach.) derived feature value vs *flow:drive*. Transform and timing variant held for nasal pressure (Pnasal) derived feature value vs *flow:drive*. The sign of the corresponding correlation coefficient is presented as prefix (-) if negative. Bias is nasal pressure feature value / pneumotach feature value. AUC = Area Under Curve. Ti = Inspiratory Time. Te = Expiratory Time. Insp = Inspiration. Exp = Expiration. PIF = Peak Inspiratory Flow. PEF = Peak Expiratory Flow. MIF = Mean Inspiratory Flow. MEF = Mean Expiratory Flow. btw = between. Ref = Reference. Fs = Sample Rate. Hz = Hertz. ¶ Adapted based on cited reference. \*Uses uniform length for timing. § Flow waveform shape preserved as a distribution. † Only original timing variant used during processing. ‡ Only transition timing variant used during processing.

## Feature reduction

*Removal of non-robust features.* We conducted a sensitivity analysis to ensure that the model presented is robust, and not subject to significant performance degradation due to subtle changes in input parameters. As demonstrated in Table S2, we observed no reduction in model performance when increasing the  $R^2$  threshold for inclusion, up to 0.5. Further increases to the inclusion threshold resulted in a steady progressive reduction in performance using pneumotachograph, and a step static decline in performance using nasal pressure.

*Pre-screening with separate data.* In a preliminary implementation of this work (prior to the discovery of non-robust features) we used a feature pre-screening process with a separate dataset (see “Feature pre-screening with external data” below). However, we chose not to implement pre-screening for the final method based on the following: 1) The discovery of non-robust features (pneumotach versus nasal pressure) meant that pre-screening (before robustness was known) would remove robust features from the selection pool that would then be excluded later. 2) Pre-screening had negligible influence on the model performance but added complexity.



**Table S2. Sensitivity analysis**

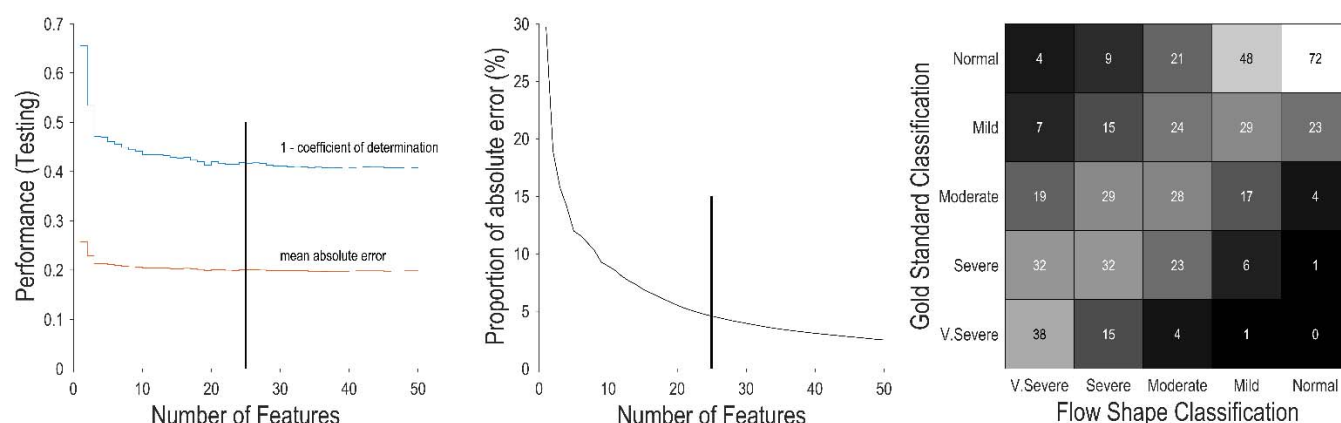
<b>R<sup>2</sup> threshold for feature-term inclusion</b>	<b>Number of feature-terms in model</b>	<b>Performance using pneumotachograph (R<sup>2</sup>)</b>	<b>Performance using nasal pressure (R<sup>2</sup>)</b>
0	495	0.59	0.48
$\frac{1}{3}$	406	0.58	0.48
$\frac{1}{2}$	295	0.58	0.48
$\frac{2}{3}$	127	0.56	0.39
$\frac{3}{4}$	44	0.54	0.39

Threshold for threshold for inclusion is the association (as coefficient of determination, R<sup>2</sup>) between pneumotachograph derived feature-term and corresponding nasal pressure derived feature-term. The Number of feature-terms in model is the minimum number from each loop of the leave-one-out cross-validation. The results reported are breath level association for cross-validated multivariable model predicted *flow:drive* and gold-standard *flow:drive*. Results presented are cross-validated values.

### **Multivariable linear regression to predict airflow obstruction**

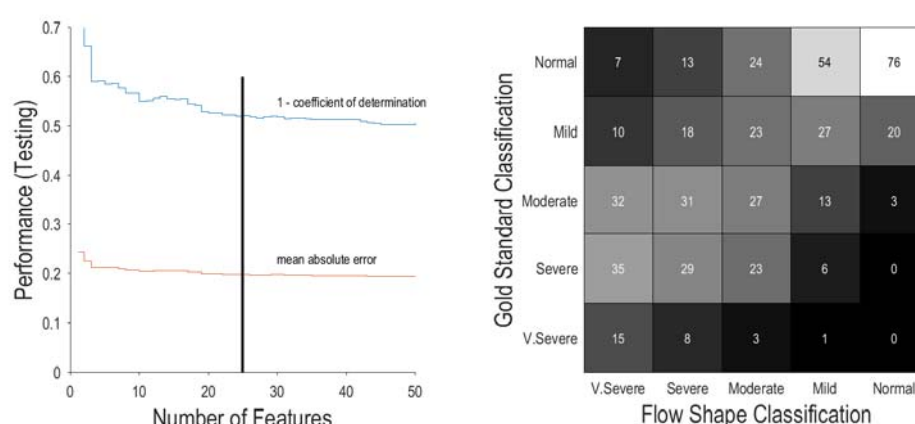
As described in the main manuscript, multivariable linear regression with backwards elimination was used to model the relationships between shape features and airflow obstruction (continuous variable, ratio of *flow:drive*). Feature-terms with coefficient of determination  $R^2 \leq 0.5$  between pneumotachograph derived feature and nasal pressure derived feature, were excluded from analysis. Figure S3 shows cross-validated testing performance increasing rapidly, while mean absolute error falls rapidly for the first three features. We observed a steady and progressive increase in performance with increasing feature number and model complexity, with performance plateauing by 30 features. We choose a value of 25 features as a sensible compromise between accuracy and complexity.

*Model weighting.* The regression was inversely weighted based on the number of breaths in each airflow obstruction class (normal: *flow:drive* > 90%; mild: 70-90%, moderate: 50-70%; severe: 30-50%, very severe: < 30%).



**Figure S3.** *Left.* Performance versus number of feature terms with pneumotachograph airflow. Performance (cross-validated) increased with each additional feature included. *Middle.* By 25 features (vertical bar), performance was at ~4.6% of the total error (at 100 feature-terms). *Right.* Predictive performance confusion matrix for each severity classification, with thresholds being >90% Normal, 70-90% Mild, 50-70% Moderate, 30-50% Severe, <30% Very Severe (V.Severe). Each column sums to 100%, and indicates the fraction of predicted breaths in each class that were correctly classified. On average, the classification prediction was exact in 39.7% of breaths, and within one severity class in 81.7% of breaths. Classification performance for individuals is provided in Table S4.

For consistency with our primary analysis with pneumotachograph flow, we used 25 features and the corresponding beta coefficients in our nasal pressure flow surrogate analysis. Similar to our primary results, we observed an initial rapid increase in performance, followed by varied increases in performance up to 25 features (Figure S4). In contrast to our primary analysis, we observed that performance continued to rise beyond 25 features, albeit very slowly. This may indicate that a model developed using nasal pressure signal requires a different number of features to train. We note that the results of this analysis could be improved simply by selecting the optimal number of features.



**Figure S4.** *Left:* Performance versus number of feature terms with transformed nasal pressure. Performance increased with each feature added, and continued to increase slowly beyond 25 features. *Right:* Predictive performance confusion matrix for each severity classification, with thresholds being >90% Normal, 70-90% Mild, 50-70% Moderate, 30-50% Severe, <30% Very Severe (V.Severe). Each column sums to 100%, and indicates the fraction of predicted breaths in each class that were correctly classified. On average, the classification prediction was exact in 34.8% of breaths, and within one severity class in 76.3% of breaths.

**Table S3. Multivariable linear regression model (25 features) to estimate airflow obstruction severity**

Feature No.	Feature	Timing method	Transform	Multivariate	Bivariate (R <sup>2</sup> )		Bias (Pnasal / Pnemo.)
				$\beta \pm SE$	Pnemo. feature vs flow:drive	Pnemo. feature vs Pnasal feature	
	Intercept			-1.22 $\pm$ 0.04			
75	Power5to12E	O	1/2	-1.88 $\pm$ 0.05	(-) 0.31	0.54	1.04
74	Power5to12I	O	1/2	-4.48 $\pm$ 0.09	(-) 0.47	0.6	1.02
33	QuadE	O	1/2	-0.70 $\pm$ 0.02	(-) 0.33	0.77	1
32	QuadI50	O	1/2	0.91 $\pm$ 0.02	(-) 0.46	0.82	1.02
30	AreaUnderPeaksI	O	1/2	-0.39 $\pm$ 0.01	(-) 0.49	0.76	1.12
30	AreaUnderPeaksI	O	2	1.53 $\pm$ 0.04	(-) 0.37	0.69	1.57
38	SkewDistInsp	O	1/2	0.12 $\pm$ 0.003	0.27	0.81	1.13
57	InspVol_03Ti	O	1	-0.75 $\pm$ 0.02	(-) 0.26	0.64	1
1	MIF_PIF	O	1	0.87 $\pm$ 0.01	0.45	0.74	0.98
33	QuadE	O	1	0.25 $\pm$ 0.01	(-) 0.32	0.71	1
3	Ali_ExpFlat	T	1/2	0.98 $\pm$ 0.03	0.28	0.6	0.99
46	Ti_Ttot	O	1	-3.44 $\pm$ 0.08	(-) 0.31	0.72	1.02
46	Ti_Ttot	O	1/2	4.15 $\pm$ 0.10	(-) 0.3	0.72	1.01
45	KurtDataInsp	O	1/2	0.26 $\pm$ 0.01	0.27	0.66	0.96
45	KurtDataInsp	O	1	-0.043 $\pm$ 0.002	0.27	0.65	0.93
31	QuadI	T	1	-0.42 $\pm$ 0.01	(-) 0.43	0.81	1.01
3	Ali_ExpFlat	T	1	-0.71 $\pm$ 0.02	0.27	0.63	0.98
21	AA_ExpFlat80Te	O	2	0.18 $\pm$ 0.01	0.34	0.56	0.99
74	Power5to12I	T	1	27.6 $\pm$ 0.69	(-) 0.37	0.51	1.04
74	Power5to12I	T	1/2	-3.28 $\pm$ 0.11	(-) 0.42	0.65	1.02
44	AsymmetryExp	T	1	-0.12 $\pm$ 0.005	(-) 0.28	0.65	0.85
72	TpeakE_Te	O	1	-0.43 $\pm$ 0.01	0.29	0.7	1.03
55	VPEF_VTe	O	1/2	0.45 $\pm$ 0.02	0.31	0.54	1
73	TpeakI_TpeakE	T	1/2	0.031 $\pm$ 0.001	(-) 0.33	0.54	1.03
78	InspFlutPow4to7	O	1/2	0.82 $\pm$ 0.05	(-) 0.34	0.57	0.95

Features are in order of importance based on backwards feature elimination (i.e. Power5to12E was the final feature remaining after sequential elimination). Feature No. corresponds with Table S1. Timing method O and T denote “original” timing and “transition” timing methods for breath detection. Transform describes the exponent: 1/2 = square-root transformed, 1 = un-transformed, 2 = squared (note: only magnitudes were transformed i.e. negative values remained negative).  $\beta$ , the beta coefficient estimates. SE, standard error of the coefficient estimates. All terms were statistically significant contributors (note very small values of SE) with  $P < 1 \times 10^{-50}$ . Bivariate performance is not cross-validated.

**Table S4. Cross-validated classification performance in individuals**

Patient ID#	Pneumotachograph flow features		Nasal pressure features	
	Exact Class %	Within One Class %	Exact Class %	Within One Class %
1	57.7	94.8	-	-
2	40.2	82.1	45.4	90
3	47.1	85.3	-	-
4	37.3	83.3	34.6	82.1
5	37.5	73.9	-	-
6	37.3	72	30	68.1
7	30.1	72.3	29.2	69.3
8	38.4	76.4	-	-
9	23.1	52.5	-	-
10	52.4	92.1	-	-
11	46.2	88.5	-	-
12	35.8	75.9	-	-
13	40.8	81.9	40.1	83.7
14	30.7	64.8	-	-
15	55	94	-	-
16	54.7	95.5	-	-
17	34	79.7	35.5	78.5
18	28.5	60.1	-	-
19	43.9	81.8	-	-
20	45.9	85.1	-	-
21	42.6	84.8	-	-
22	36.3	79.2	-	-
23	35.8	75.7	-	-
24	48.8	86.9	-	-
25	42.5	82.4	-	-
26	43.7	89.2	40.2	81
27	49.2	90.8	41.9	84.8
28	36.4	81	25	54.6
29	23.7	68.6	27.9	68.5
30	34.9	76.8	36.2	78.2
31	30.1	79.3	-	-
32	39.9	76.6	-	-
33	33.6	73.5	-	-
34	46.5	86.9	39.3	77
35	37	75.8	-	-
36	37.5	82.2	-	-
37	43.6	83.9	42.3	83.2
38	39.1	80.2	29.1	66.6
39	42.6	82.4	35.8	74.6
40	42.9	84.6	44.8	84.4
41	30.8	58.1	28.3	56.1

Individual patient performance for categorisation into normal, mild, moderate, severe and very severe flow-limited classes using the pneumotachograph flow shape features. The “Exact Class %” column indicates the proportion of breaths that classified exactly, while the “Within One Class %” column shows the proportion of breaths that were correct, if accepting the adjacent class as correct. All values represent the percentage correctly classified using flow shape alone, assessed against gold-standard.

### Simplified 5-feature model

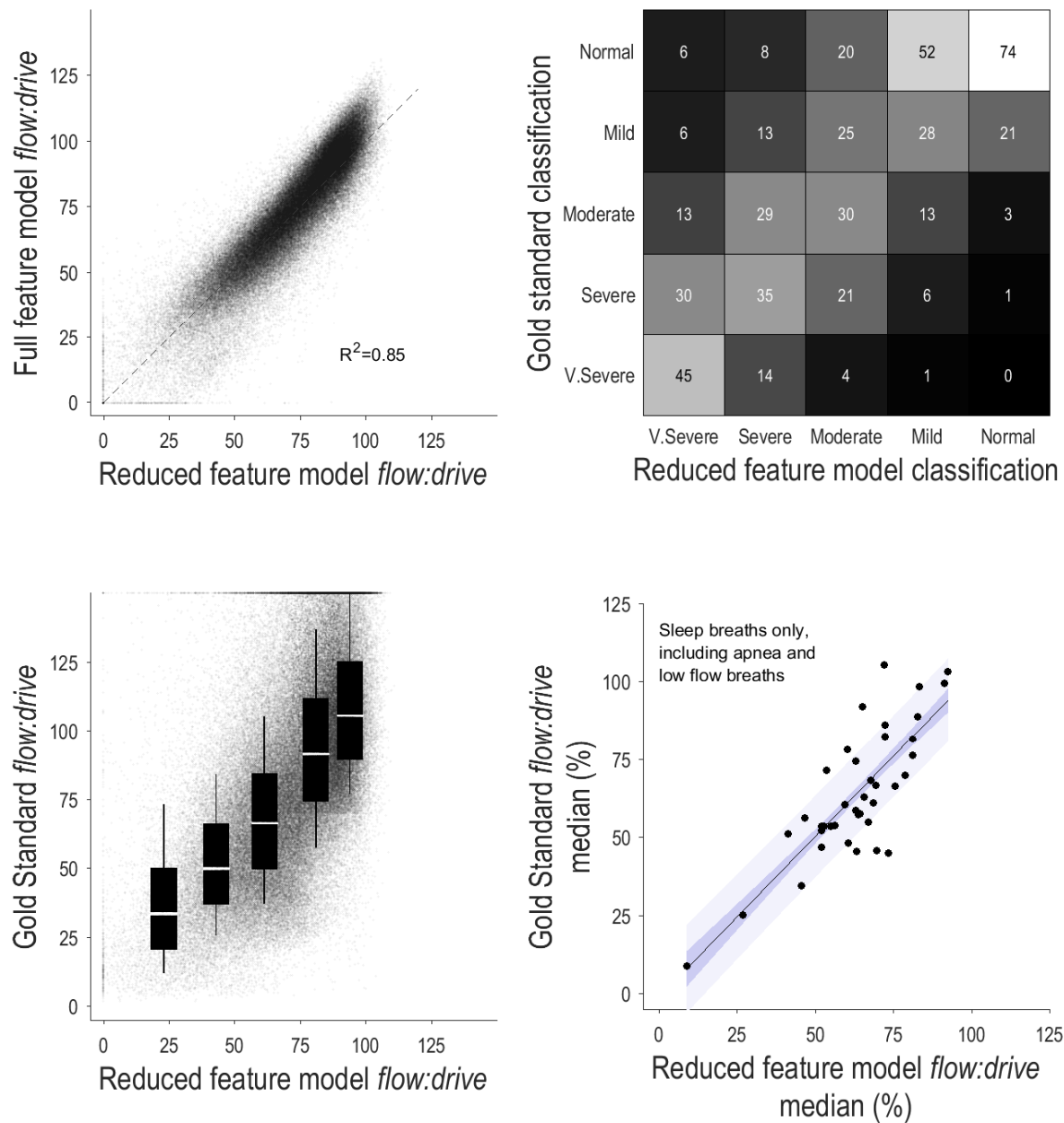
Table S5 presents a simplified model for estimating *flow:drive* utilising only five feature-terms. While we observe a slight reduction in breath-level overall performance, it continues to perform remarkably well at the patient-level, in pneumotachograph derived feature-terms (see Figure S5). This reduced feature model performs adequately well in nasal pressure derived feature terms (see Figure S6).

The five features-terms in our simplified model quantified signal variability (spectral power) in inspiration and expiration respectively, the deviation from a normal rounded contour in inspiration and expiration respectively, and the magnitude of “scooping” between multiple inspiratory peaks (when present). The major role of expiratory shape abnormalities in our estimation of pharyngeal airflow obstruction (often referred to as “inspiratory flow limitation”)—was unexpected, but is consistent with the increased expiratory resistance observed in some patients [15, 27, 28].

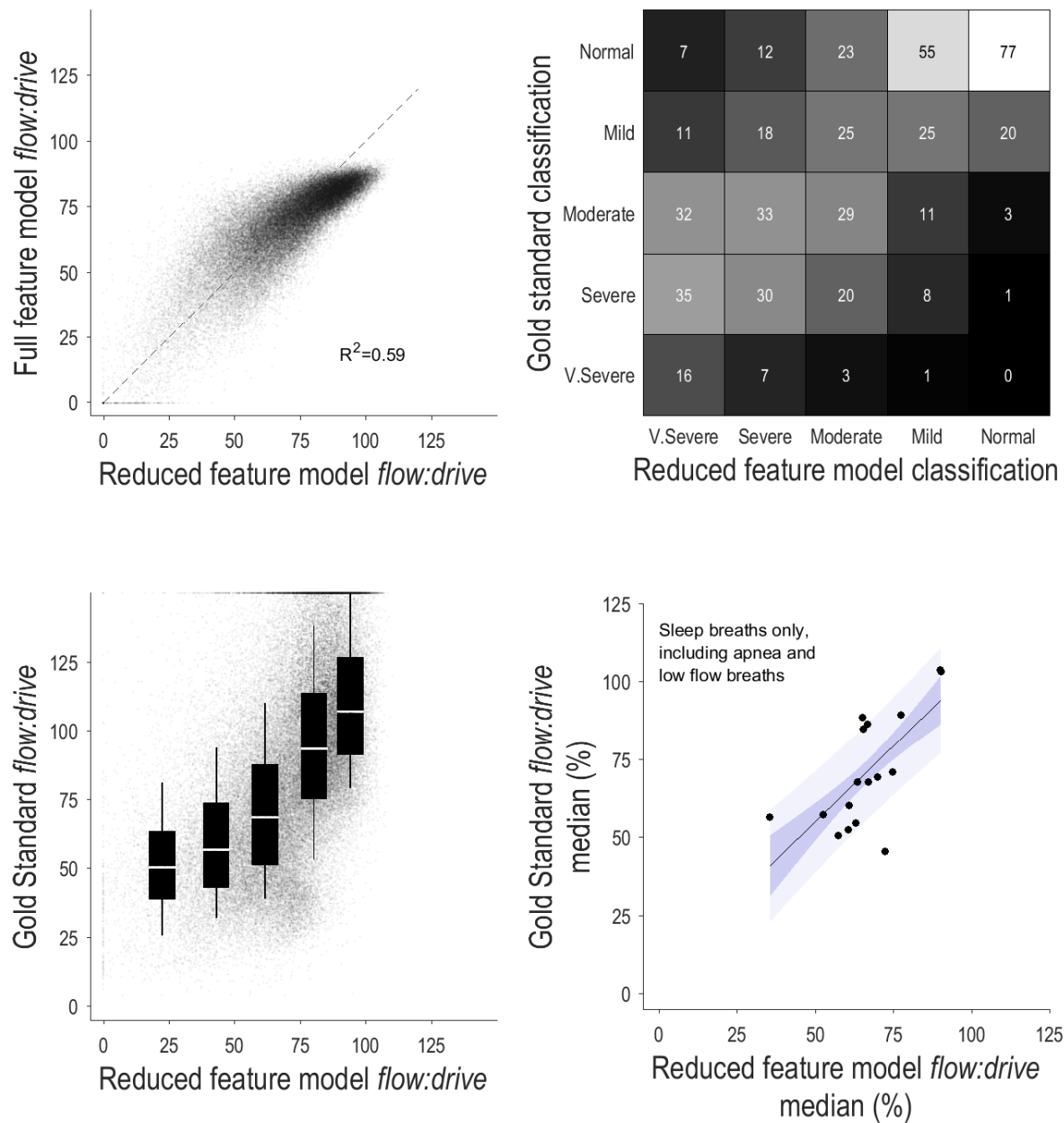
**Table S5. Multivariable linear regression model (5 features) to estimate airflow obstruction severity**

Feature No.	Feature	Timing method	Transform	Multivariate
				$\beta \pm \text{SE}$
	Intercept			$1.3 \pm 0.003$
75	Power5to12E	O	$\frac{1}{2}$	$-2.32 \pm 0.04$
74	Power5to12I	O	$\frac{1}{2}$	$-4.17 \pm 0.05$
33	QuadE	O	$\frac{1}{2}$	$-0.24 \pm 0.003$
32	QuadI50	O	$\frac{1}{2}$	$-0.68 \pm 0.01$
30	AreaUnderPeaksI	O	$\frac{1}{2}$	$-0.3 \pm 0.01$

Feature No. corresponds with Table S1. Timing method O and T denote “original” timing and “transition” timing methods for breath detection. Transform describes the exponent:  $\frac{1}{2}$  = square-root transformed, 1 = un-transformed, 2 = squared (note: only magnitudes were transformed i.e. negative values remained negative).  $\beta$ , the beta coefficient estimates. SE, standard error of the coefficient estimates.



**Figure S5.** Reduced feature model performance, using *pneumotachograph flow features*. **(Top Left)** The association between the reduced feature model predicted *flow:drive* values and the full 25 feature model predicted *flow:drive* values is very high ( $R^2=0.85$ ). **(Top Right)** Predictive performance confusion matrix for each severity classification, with thresholds being >90% Normal, 70-90% Mild, 50-70% Moderate, 30-50% Severe, <30% Very Severe (V.Severe). Each column sums to 100%, and indicates the fraction of predicted breaths in each class that were correctly classified. On average, the classification prediction was exact in 42.6% of breaths, and within one severity class in 83.8% of breaths. **(Bottom Left)** Scatter plot showing a strong association between reduced feature model predicted *flow:drive* and gold-standard *flow:drive* values. The box plot overlay shows summary statistics (box and central line show IQR and median respectively, whiskers show 10<sup>th</sup> and 90<sup>th</sup> percentiles) for breaths within each severity classification. **(Bottom Right)** Scatter plot showing the novel patient level metric, median *flow:drive* (during sleep, including apnoea breaths). A very strong association exists between reduced feature model predicted and gold-standard patient median *flow:drive* during sleep. ( $R^2$ , coefficient of determination)

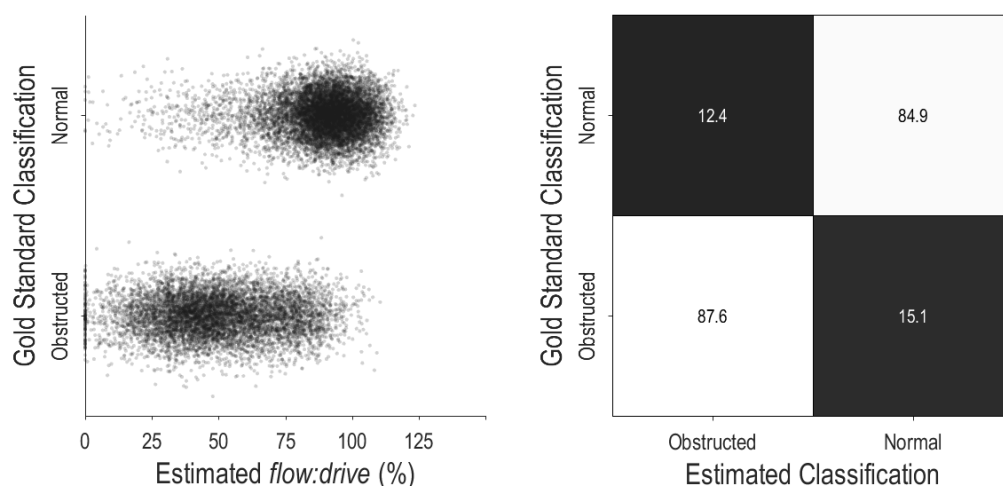


**Figure S6.** Reduced feature model performance, using *nasal pressure features*. **(Top Left)** The association between the reduced feature model predicted *flow:drive* values and the full 25 feature model predicted *flow:drive* values is moderate ( $R^2=0.59$ ). **(Top Right)** Predictive performance confusion matrix for each severity classification, with thresholds being >90% Normal, 70-90% Mild, 50-70% Moderate, 30-50% Severe, <30% Very Severe (V.Severe). Each column sums to 100%, and indicates the fraction of predicted breaths in each class that were correctly classified. On average, the classification prediction was exact in 35.2% of breaths, and within one severity class in 76.4% of breaths. **(Bottom Left)** Scatter plot showing a strong association between reduced feature model predicted *flow:drive* and gold-standard *flow:drive* values. The box plot overlay shows summary statistics (box and central line show IQR and median respectively, whiskers show 10<sup>th</sup> and 90<sup>th</sup> percentiles) for breaths within each severity classification. **(Bottom Right)** Scatter plot showing the novel patient level metric, median *flow:drive* (during sleep, including apnoea breaths). A very strong association exists between reduced feature model predicted and gold-standard patient median *flow:drive* during sleep. ( $R^2$ , coefficient of determination).

## External validation

We examined 29 baseline sleep studies as part of a separate investigation (NCT02489591) in which pneumotachograph airflow was measured via a sealed nasal mask. Participants details: 19M:10F, age =  $49 \pm 11$  years, BMI =  $32 \pm 7$  kg/m<sup>2</sup>, neck circumference =  $40 \pm 5$  cm, AHI =  $45 \pm 28$  events/hr (range = 2 to 105 events/hr). Each study was scored carefully for clinically-relevant respiratory events (30% reduction in flow in association with either 3% desaturation or arousal) and EEG arousal start and end times were carefully scored (>3 seconds with no upper limit). Breaths were automatically labelled as likely “normal” or likely “obstructed” as follows: Breaths within the margins of a scored arousal that had a level of ventilation above the local 3 min average were considered likely “normal”. Breaths within the margins of scored obstructive hypopnoea with a level of ventilation at least 30% below the local average were considered likely “obstructed”. In total, we identified 9183 “normal” (arousal) breaths and 7544 “obstructed” (hypopnoea) breaths.

We estimated *flow:drive* values by applying the final 25 feature final model presented above, and examined the discriminative capacity of our method to separate “normal” versus “obstructed” breaths. A threshold of *flow:drive* < 70% (moderate-to-severe airflow obstruction) was used for a binary classification. We observed a positive predictive value of 88% and negative predictive value of 85% (Figure S7). Alternatively, use of the 5-feature model yielded similar results, with a positive predictive value of 88% and negative predictive value of 84% (not shown).



**Figure S7.** Classification performance using the 25 feature final model, with flow shape feature-terms derived from pneumotachograph flow in an alternate dataset. *Left:* Scatter plot showing the probability of a breath being “normal” (i.e. in arousal with larger than average flow) or “obstructed” (i.e. obstructive hypopnoea with <70% of normal flow). *Right:* Performance matrix. Each column sums to 100%, and as such can be used to quickly assess the fraction of breaths correctly classified. The values within each division of the confusion matrix show the proportion of total breaths. Positive predictive value is 88%. Negative predictive value = 85%.



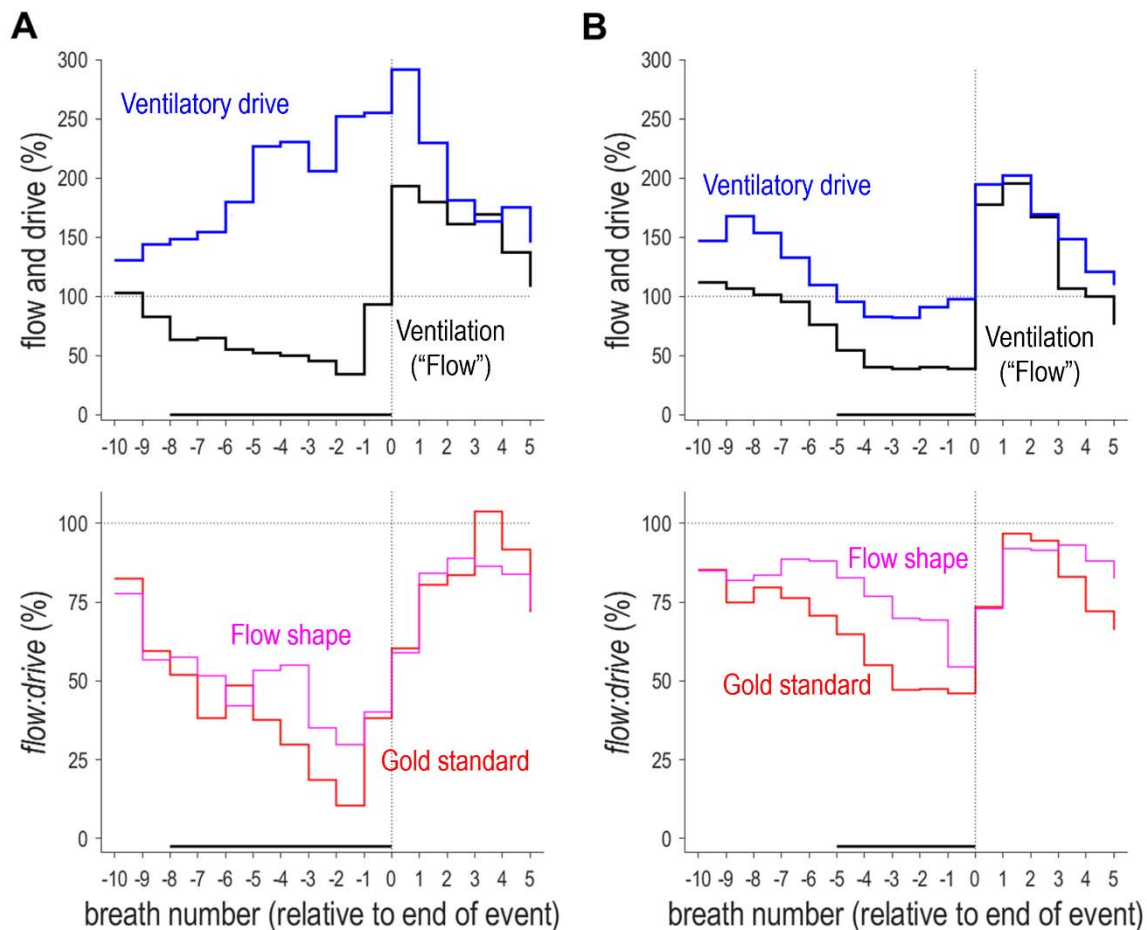
### **Feature pre-screening with external data**

As mentioned above, we also tested whether pre-screening features using this separate dataset might have improved the final model predictive value (potentially by early elimination of features that were of limited independent value in the determination of airflow obstruction). First, 165 feature terms were calculated (81/85 with “original” timing, and 84/85 with “transition” timing); multivariable *logistic* regression with backwards elimination was used to identify the 50 best feature terms (including timing variants) that discriminated between “normal” (arousal) breaths and “obstructed” (hypopnoea) breaths as defined above. This logistic regression model had positive predictive value of 89% and negative predictive value of 89% (cross-validated performance).

We then repeated the main flow shape analysis (Table S3, Figures 3 and 5) starting with pre-screened feature list (50 instead of 165), calculating the 3 transforms (square-root, untransformed, squared; 150 instead of 495), and then removing features with  $R^2$  (pneumotach versus nasal pressure)  $<0.5$  (leaving 92 instead of 295). Model performance at a breath level was similar with versus without pre-screening: For pneumotach analysis,  $R^2 = 0.58$  under both conditions. For nasal pressure analysis,  $R^2 = 0.43$  and  $0.48$  respectively. Thus there was no evidence to support the utility of the feature pre-screening approach described.

## Assessing Central versus Obstructive Pathophysiology: Future Directions

Strictly speaking, *flow:drive* indicates the magnitude of pharyngeal obstruction. Out of context with the changes in flow during respiratory events, *flow:drive* alone provides insufficient information to strictly determine a) the magnitude of central drive during events ( $Y = \text{flow} \div \text{flow:drive}$ ), and b) whether drive is rising or falling during hypopneas. Example analysis showing two patients with significantly different flow and drive patterns, which can be inferred from the estimated *flow:drive* (flow shapes), are shown in Figure S8.



**Figure S8.** Ensemble-averaged hypopnea data in two patients illustrating evolving flow, drive, and obstruction across breaths. **(A)** The first patient (AHI=39 events/hr) exhibits increasing drive in response to falling flow throughout the hypopnea (horizontal bar, 8 breaths; top traces). Here, a progressively rising drive can be inferred from the observation that *flow:drive* falls by more than flow (bottom traces). **(B)** The second patient (AHI=80) exhibits a reduction in drive concurrent with the loss of flow; drive briefly falls marginally below the eupneic level. Here, a progressively falling drive can be inferred from the observation that *flow:drive* falls by less than flow. Drive and flow also change in parallel (positively associated); one may interpret that the fall in drive is facilitating the event itself. Ensemble averages were calculated for all available scored hypopneas in both patients; median data are shown for each breath. Ventilatory drive data are based on calibrated diaphragm EMG.

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