Complete Simulation Results for On the Use of Information Criteriz for Subset Selection in Least Squares Regression

Sen Tian, Clifford M. Hurvich, Jeffrey S. Simonoff

- Orthogonal X, simulation setups are discussed in the Supplemental Material Section B.1.
 - The performance of selection rules for BS. The selection rules include C_p , AICc, BIC, GCV and 10-fold CV. For each selection rule except CV, there are two columns in the table indicating the degrees of freedoms to use in calculating the information criterion. The "edf" (effective degrees of freedom) is estimated using definition (3) by assuming the knowledge of μ and σ , and hence it is an infeasible rule. The "ndf/hdf/bdf" (naive degrees of freedom / heuristic degrees of freedom / degrees of freedom based on bootstrap) are feasible selection rules in practice.

* Orth-Sparse-Ex1: tables S1-S2 * Orth-Sparse-Ex2: tables S3-S4 * Orth-Dense: tables S5-S6

- General X, simulation setups are discussed in Supplemental Material Section B.2.
 - The performance of BOSS compared to BS, FS and regularization methods (n > p). For BOSS, we consider three selection rules, that are AICc-hdf, C_p -hdf and CV. For lasso and gamma lasso, we consider AICc and CV. And for the remaining methods, we use CV. Note that for lasso, we use the number of non-zero coefficients $k(\lambda)$ in place of edf in the AICc formula (7). Zou et al. (2007) showed that $k(\lambda)$ is an unbiased estimator of edf for lasso. For gamma lasso, Taddy (2017) suggested a heuristic degrees of freedom to be plugged into (7) in order to use AICc as the selection rule.

* Sparse-Ex1: tables S7-S12
* Sparse-Ex2: tables S13-S18
* Sparse-Ex3: tables S19-S24
* Sparse-Ex4: tables S25-S30
* Dense: tables S31-S36

- The performance of BOSS compared to FS and regularization methods (n < p). For FS, we consider EBIC (Wang, 2009), HDBIC and HDHQ (Ing and Lai, 2011). We also consider the stopping rule, the trimming rule, and a combination of both introduced by Ing and Lai (2011) for FS.

* Sparse-Ex1: tables S37-S39
* Sparse-Ex2: tables S40-S42
* Sparse-Ex3: tables S43-S45
* Sparse-Ex4: tables S46-S48
* Dense: tables S49-S51

Table S1: The performance of BS using different selection rules, Orth-Sparse-Ex1, n=200

| | | | C_p | | AICc | | BIC | | GCV | CV |
|------|-------|----------|------------------------------|----------|----------------------------|--------------|----------------------------|----------|-----------------------------|----------|
| | | edf | ndf/hdf/bdf | edf | ndf/hdf/bdf | edf | ndf/hdf/bdf | edf | ndf/hdf/bdf | CV |
| | | | | | % worse that | n the best | possible BS | | | |
| | p=14 | 8 | 33/9/11 | 7 | 33/6/9 | 0 | 10/0/1 | 9 | 34/8/10 | 19 |
| ١, ا | p=30 | 4 | 84/5/7 | 2 | 83/2/5 | 0 | 28/0/0 | 4 | 86/4/7 | 24 |
| hsnr | p=60 | 2 | 157/3/5 | 1 | 159/2/3 | 0 | 64/0/0 | 2 | 167/3/4 | - |
| | p=180 | 1 | 338/30/32 | 0 | 392/1/2 | 0 | 206/0/0 | 0 | 431/2/3 | - |
| | p=14 | 8 | 33/14/12 | 7 | 33/11/10 | 0 | 10/2/1 | 9 | 34/14/12 | 19 |
| | p=30 | 4 | 84/12/11 | 2 | 83/8/7 | 0 | 28/1/2 | 4 | 86/10/10 | 24 |
| msnr | p=60 | 2 | 157/13/10 | 1 | 159/8/7 | 0 | 64/2/2 | 2 | 167/11/9 | - |
| | p=180 | 1 | 338/40/38 | 0 | 392/7/6 | 0 | 206/3/4 | 0 | 431/10/8 | - |
| | p=14 | 18 | 16/23/23 | 18 | 17/24/24 | 93 | 43/97/93 | 18 | 16/23/23 | 26 |
| ١, | p=30 | 20 | 25/36/33 | 21 | 24/37/35 | 68 | 23/68/67 | 21 | 26/37/35 | 28 |
| lsnr | p=60 | 18 | 44/28/27 | 21 | 45/31/30 | 43 | 17/43/43 | 20 | 48/30/29 | - |
| | p=180 | 15 | 108/35/34 | 18 | 132/22/22 | 25 | 50/25/25 | 17 | 149/22/21 | - |
| | | | | | Rela | tive efficie | ency | | | |
| | p=14 | 0.93 | 0.75/0.92/0.9 | 0.94 | 0.75/0.94/0.92 | 1 | 0.91/1/0.99 | 0.92 | 0.75/0.92/0.91 | 0.84 |
| | p=30 | 0.96 | 0.54/0.95/0.93 | 0.98 | 0.55/0.98/0.96 | 1 | 0.78/1/1 | 0.96 | 0.54/0.96/0.94 | 0.81 |
| hsnr | p=60 | 0.98 | 0.39/0.97/0.95 | 0.99 | 0.39/0.98/0.97 | 1 | 0.61/1/1 | 0.98 | 0.38/0.97/0.96 | - |
| | p=180 | 0.99 | 0.23/0.77/0.76 | 1 | 0.2/0.99/0.98 | 1 | 0.33/1/1 | 1 | 0.19/0.98/0.97 | - |
| | p=14 | 0.93 | 0.75/0.88/0.89 | 0.94 | 0.75/0.9/0.91 | 1 | 0.91/0.99/0.99 | 0.92 | 0.75/0.88/0.9 | 0.84 |
| | p=30 | 0.96 | 0.54/0.89/0.9 | 0.98 | 0.55/0.92/0.93 | 1 | 0.78/0.99/0.98 | 0.96 | 0.54/0.91/0.91 | 0.81 |
| msnr | p=60 | 0.98 | 0.39/0.89/0.91 | 0.99 | 0.39/0.92/0.93 | 1 | 0.61/0.98/0.98 | 0.98 | 0.38/0.9/0.92 | - |
| | p=180 | 0.99 | 0.23/0.71/0.72 | 1 | 0.2/0.93/0.94 | 1 | 0.33/0.97/0.96 | 1 | 0.19/0.91/0.92 | - |
| | p=14 | 0.99 | 1/0.95/0.95 | 0.98 | 1/0.94/0.94 | 0.6 | 0.82/0.59/0.6 | 0.99 | 1/0.95/0.94 | 0.92 |
| ١, | p=30 | 1 | 0.97/0.89/0.9 | 1 | 0.97/0.88/0.89 | 0.72 | 0.98/0.72/0.72 | 0.99 | 0.96/0.88/0.89 | 0.94 |
| lsnr | p=60 | 0.99 | 0.81/0.92/0.92 | 0.97 | 0.81/0.89/0.9 | 0.82 | 1/0.82/0.82 | 0.98 | 0.79/0.9/0.91 | - |
| | p=180 | 1 | 0.55/0.86/0.86 | 0.97 | 0.5/0.95/0.95 | 0.93 | 0.77/0.93/0.93 | 0.98 | 0.46/0.95/0.95 | - |
| | | | | | Sparsistency (n | umber of e | extra variables) | | | |
| | p=14 | 6(0.2) | 6(1.3)/6(0.4)/6(0.4) | 6(0.2) | 6(1.2)/6(0.2)/6(0.3) | 6(0) | 6(0.2)/6(0)/6(0) | 6(0.3) | 6(1.3)/6(0.4)/6(0.4) | 6(0.7) |
| ١, | p=30 | 6(0.1) | 6(3.9)/6(0.2)/6(0.2) | 6(0) | 6(3.8)/6(0.1)/6(0.1) | 6(0) | 6(0.6)/6(0)/6(0) | 6(0.1) | 6(4.1)/6(0.1)/6(0.1) | 6(0.7) |
| hsnr | p=60 | 6(0) | 6(8.9)/6(0)/6(0.1) | 6(0) | 6(9.2)/6(0)/6(0) | 6(0) | 6(1.6)/6(0)/6(0) | 6(0) | 6(10.5)/6(0)/6(0.1) | - |
| | p=180 | 6(0) | 6(32.2)/6(6.4)/6(6.3) | 6(0) | 6(48.9)/6(0)/6(0) | 6(0) | 6(9.5)/6(0)/6(0) | 6(0) | 6(74.6)/6(0)/6(0) | - |
| | p=14 | 6(0.2) | 6(1.3)/6(0.7)/6(0.4) | 6(0.2) | 6(1.2)/6(0.5)/6(0.3) | 6(0) | 6(0.2)/6(0)/6(0) | 6(0.3) | 6(1.3)/6(0.6)/6(0.4) | 6(0.7) |
| | p=30 | 6(0.1) | 6(3.9)/6(0.4)/6(0.3) | 6(0) | 6(3.8)/6(0.2)/6(0.1) | 6(0) | 6(0.6)/6(0)/6(0) | 6(0.1) | 6(4.1)/6(0.3)/6(0.2) | 6(0.7) |
| msnr | p=60 | 6(0) | 6(8.9)/6(0.3)/6(0.2) | 6(0) | 6(9.2)/6(0.1)/6(0.1) | 6(0) | 6(1.6)/6(0)/6(0) | 6(0) | 6(10.5)/6(0.2)/6(0.1) | - |
| | p=180 | 6(0) | 6(32.2)/6(6.6)/6(6.6) | 6(0) | 6(48.9)/6(0.1)/6(0.1) | 6(0) | 6(9.5)/6(0)/6(0) | 6(0) | 6(74.6)/6(0.1)/6(0.1) | - |
| | p=14 | 5.5(2.3) | 5.2(1.3)/5.6(4.6)/5.4(3.6) | 5.4(2.1) | 5.2(1.2)/5.4(4.2)/5.3(3.2) | 0.9(0.1) | 3.6(0.2)/0.7(0.1)/0.9(0.1) | 5.5(2.4) | 5.3(1.3)/5.6(4.6)/5.4(3.5) | 4.9(1.6) |
| 1 | p=30 | 4.5(1.9) | 5.3(3.9)/4.2(4.9)/4.2(4) | 4.2(1.2) | 5.2(3.8)/3.3(2.2)/3.4(1.8) | 0.1(0) | 3.7(0.6)/0.1(0)/0.2(0) | 4.5(2) | 5.3(4.1)/3.9(4.1)/3.9(3.3) | 4(1.9) |
| lsnr | p=60 | 3.4(1.1) | 5.2(8.9)/2.7(1.8)/2.8(1.6) | 2.7(0.6) | 5.3(9.2)/1.5(0.2)/1.7(0.3) | 0(0) | 3.8(1.4)/0.1(0)/0.1(0) | 3.1(0.9) | 5.4(10.4)/2(0.6)/2.1(0.7) | - |
| | p=180 | 1.9(0.5) | 5.3(32.2)/1.8(10.9)/1.9(9.8) | 1.1(0.1) | 5.6(49)/0.5(0)/0.6(0) | 0(0) | 4.2(8.4)/0(0)/0(0) | 1.4(0.2) | 5.8(74.6)/0.7(0.1)/0.8(0.1) | - |

 $\textbf{Table S2:} \ \, \textbf{The performance of BS using different selection rules, Orth-Sparse-Ex1, n=2000}$

| | | edf | C_p ndf/hdf/bdf | edf | AICc ndf/hdf/bdf | edf | BIC ndf/hdf/bdf | edf | GCV ndf/hdf/bdf | CV |
|----------|-------------------------------|--|--|--|--|------------------------------|---|----------------------------------|--|----------------------------|
| | | | nar, nar, bar | Cur | % worse than the | | | car | nar/nar/sar | <u> </u> |
| hsnr | p=14 p=30 p=60 p=180 | 8 3 2 0 | 33/7/9 $85/3/6$ $155/2/4$ $334/1/3$ | 8 3 2 1 | 33/7/9 $85/3/6$ $156/2/4$ $337/1/3$ | 0 0 0 0 | 3/0/0 9/0/0 21/0/0 60/0/0 | 8 3 2 1 | 33/7/9 $86/3/6$ $156/2/4$ $340/1/3$ | 18 23 - |
| msnr | p=14 p=30 p=60 p=180 | 8 3 2 0 | 33/7/9 85/3/6 155/2/4 334/1/3 | 8 3 2 1 | 33/7/9 85/3/6 156/2/4 337/1/3 | 0 0 0 0 | 3/0/0 9/0/0 21/0/0 60/0/0 | 8 3 2 1 | 33/7/9 $86/3/6$ $156/2/4$ $340/1/3$ | 18 23 - |
| lsnr | p=14 p=30 p=60 p=180 | 8 3 2 0 | 33/9/9 $85/6/7$ $155/5/5$ $334/5/4$ | 8 3 2 1 | 33/9/9 $85/5/6$ $156/5/5$ $337/4/4$ | 0 0 0 0 | 3/0/0 9/0/0 21/0/0 60/1/1 | 8 3 2 1 | 33/9/9 $86/6/7$ $156/5/5$ $340/5/4$ | 18 23 - - |
| <u> </u> | Relative efficiency | | | | | | | 1 004 | | |
| hsnr | p=14 p=30 p=60 p=180 | 0.93 0.97 0.98 1 | 0.75/0.94/0.92 0.54/0.97/0.94 0.39/0.98/0.96 0.23/0.99/0.97 | 0.93 0.97 0.98 0.99 | 0.75/0.94/0.92 0.54/0.97/0.94 0.39/0.98/0.96 0.23/0.99/0.97 | 1 1 1 1 | 0.97/1/1 $0.92/1/1$ $0.83/1/1$ $0.62/1/1$ | 0.92 0.97 0.98 0.99 | 0.75/0.94/0.92 0.54/0.97/0.94 0.39/0.98/0.96 0.23/0.99/0.97 | 0.84 0.81 - |
| msnr | p=14 p=30 p=60 p=180 | 0.93 0.97 0.98 1 | 0.75/0.94/0.92 0.54/0.97/0.94 0.39/0.98/0.96 0.23/0.99/0.97 | 0.93 0.97 0.98 0.99 | 0.75/0.94/0.92 0.54/0.97/0.94 0.39/0.98/0.96 0.23/0.99/0.97 | 1 1 1 1 | 0.97/1/1 0.92/1/1 0.83/1/1 0.62/1/1 | 0.92 0.97 0.98 0.99 | 0.75/0.94/0.92 0.54/0.97/0.94 0.39/0.98/0.96 0.23/0.99/0.97 | 0.84 0.81 - |
| lsnr | p=14 p=30 p=60 p=180 | 0.93 0.97 0.98 1 | 0.75/0.92/0.92 0.54/0.95/0.94 0.39/0.95/0.95 0.23/0.96/0.96 | 0.93 0.97 0.98 0.99 | 0.75/0.92/0.92 0.54/0.95/0.94 0.39/0.95/0.95 0.23/0.96/0.96 | 1 1 1 1 | $\begin{array}{c} 0.97/1/1 \\ 0.92/1/1 \\ 0.83/1/1 \\ 0.62/0.99/0.99 \end{array}$ | 0.92 0.97 0.98 0.99 | 0.75/0.92/0.92 0.54/0.95/0.94 0.39/0.95/0.95 0.23/0.96/0.96 | 0.84 0.81 - |
| | | | | | Sparsistency (num | ber of e | extra variables) | | | |
| hsnr | p=14 p=30 p=60 p=180 | 6(0.3) 6(0.1) 6(0) 6(0) | $\begin{array}{c} 6(1.2)/6(0.3)/6(0.3) \\ 6(3.8)/6(0.1)/6(0.2) \\ 6(8.6)/6(0)/6(0) \\ 6(27.5)/6(0)/6(0) \end{array}$ | 6(0.3) 6(0.1) 6(0) 6(0) | $\begin{array}{c} 6(1.2)/6(0.3)/6(0.3) \\ 6(3.8)/6(0.1)/6(0.2) \\ 6(8.6)/6(0)/6(0) \\ 6(28.2)/6(0)/6(0) \end{array}$ | 6(0) 6(0) 6(0) 6(0) | $\begin{array}{c} 6(0)/6(0)/6(0) \\ 6(0.1)/6(0)/6(0) \\ 6(0.3)/6(0)/6(0) \\ 6(1.1)/6(0)/6(0) \end{array}$ | 6(0.3) 6(0.1) 6(0) 6(0) | $\begin{array}{c} 6(1.2)/6(0.3)/6(0.3) \\ 6(3.9)/6(0.1)/6(0.2) \\ 6(8.7)/6(0)/6(0) \\ 6(28.9)/6(0)/6(0) \end{array}$ | 6(0.6) 6(0.6) - |
| msnr | p=14 p=30 p=60 p=180 | 6(0.3) 6(0.1) 6(0) 6(0) | 6(1.2)/6(0.3)/6(0.3) 6(3.8)/6(0.1)/6(0.2) 6(8.6)/6(0)/6(0) 6(27.5)/6(0)/6(0) | 6(0.3) 6(0.1) 6(0) 6(0) | $\begin{array}{c} 6(1.2)/6(0.3)/6(0.3) \\ 6(3.8)/6(0.1)/6(0.2) \\ 6(8.6)/6(0)/6(0) \\ 6(28.2)/6(0)/6(0) \end{array}$ | 6(0) 6(0) 6(0) 6(0) | $\begin{array}{c} 6(0)/6(0)/6(0) \\ 6(0.1)/6(0)/6(0) \\ 6(0.3)/6(0)/6(0) \\ 6(1.1)/6(0)/6(0) \end{array}$ | 6(0.3) 6(0.1) 6(0) 6(0) | $\begin{array}{c} 6(1.2)/6(0.3)/6(0.3) \\ 6(3.9)/6(0.1)/6(0.2) \\ 6(8.7)/6(0)/6(0) \\ 6(28.9)/6(0)/6(0) \end{array}$ | 6(0.6) 6(0.6) - |
| lsnr | p=14 p=30 p=60 p=180 | $ \begin{vmatrix} 6(0.3) \\ 6(0.1) \\ 6(0) \\ 6(0) \end{vmatrix} $ | 6(1.2)/6(0.4)/6(0.3) 6(3.8)/6(0.2)/6(0.2) 6(8.6)/6(0.1)/6(0.1) 6(27.5)/6(0.1)/6(0) | $ \begin{vmatrix} 6(0.3) \\ 6(0.1) \\ 6(0) \\ 6(0) \end{vmatrix} $ | $\begin{array}{c} 6(1.2)/6(0.4)/6(0.3) \\ 6(3.8)/6(0.2)/6(0.2) \\ 6(8.6)/6(0.1)/6(0.1) \\ 6(28.2)/6(0.1)/6(0) \end{array}$ | 6(0) 6(0) 6(0) 6(0) | $\begin{array}{c} 6(0)/6(0)/6(0) \\ 6(0.1)/6(0)/6(0) \\ 6(0.3)/6(0)/6(0) \\ 6(1.1)/6(0)/6(0) \end{array}$ | 6(0.3) 6(0.1) 6(0) 6(0) | $\begin{array}{c} 6(1.2)/6(0.4)/6(0.3) \\ 6(3.9)/6(0.2)/6(0.2) \\ 6(8.7)/6(0.1)/6(0.1) \\ 6(28.9)/6(0.1)/6(0) \end{array}$ | 6(0.6) 6(0.6) - - |

Table S3: The performance of BS using different selection rules, Orth-Sparse-Ex2, n=200

| | | edf | C_p ndf/hdf/bdf | edf | AICc ndf/hdf/bdf | edf | BIC ndf/hdf/bdf | edf | GCV ndf/hdf/bdf | CV |
|------|-------------------------------|--|---|--|--|--|--|--|---|-------------------------|
| i | | | ,, | | % worse than t | | - / - / | | ,, | 1 |
| hsnr | p=14 p=30 p=60 p=180 | 23 21 17 12 | 21/32/29 48/27/26 89/20/19 200/32/33 | 23 21 17 11 | 21/32/28 $47/25/23$ $91/18/18$ $236/11/11$ | 39 27 19 11 | $\begin{array}{c} 20/40/38 \\ 20/27/26 \\ 33/19/18 \\ 112/11/11 \end{array}$ | 24 21 17 11 | 21/32/29 $49/27/25$ $96/18/18$ $262/11/12$ | 23 24 - |
| msnr | p=14 p=30 p=60 p=180 | 13 6 3 3 | 33/23/20 78/21/19 146/20/17 314/50/50 | 11 4 3 2 | 33/21/17 78/15/14 148/14/13 365/15/15 | 3 1 1 2 | $\begin{array}{c} 14/12/11 \\ 28/19/18 \\ 59/34/28 \\ 184/65/57 \end{array}$ | 14 6 3 3 | 34/23/19 80/18/17 155/17/15 400/16/16 | 21 24 - |
| lsnr | p=14 p=30 p=60 p=180 | 25 21 19 15 | $\begin{array}{c} 26/34/32 \\ 54/37/34 \\ 95/34/32 \\ 198/57/54 \end{array}$ | 25 20 17 15 | 26/34/33 54/34/31 97/33/31 235/39/35 | 52 48 49 56 | 24/91/77 23/90/79 35/84/76 105/72/68 | 26 22 18 15 | 27/34/33 56/35/33 102/33/32 260/37/34 | 27 29 - - |
| | | | | | | e efficier | v | | | |
| hsnr | p=14 p=30 p=60 p=180 | 0.97 0.99 0.99 0.99 | 0.99/0.91/0.93 0.81/0.94/0.95 0.62/0.97/0.98 0.37/0.84/0.84 | 0.97 0.99 1 1 | 0.99/0.91/0.93 0.81/0.96/0.97 0.61/0.99/0.99 0.33/1/1 | 0.86 0.94 0.98 1 | 1/0.86/0.87 1/0.94/0.95 0.87/0.98/0.98 0.52/1/1 | 0.97 0.99 1 1 | 0.99/0.91/0.93 0.8/0.95/0.96 0.59/0.98/0.99 0.31/1/0.99 | 0.97 0.97 - - |
| msnr | p=14 p=30 p=60 p=180 | 0.91 0.95 0.98 0.99 | 0.77/0.83/0.85 0.57/0.84/0.85 0.41/0.84/0.86 0.25/0.68/0.68 | 0.92 0.97 0.99 | 0.77/0.85/0.87 0.57/0.88/0.89 0.41/0.88/0.89 0.22/0.89/0.89 | 1 1 1 1 | 0.9/0.92/0.93 0.79/0.85/0.86 0.64/0.76/0.79 0.36/0.62/0.65 | 0.9 0.95 0.98 1 | 0.77/0.83/0.86 0.56/0.86/0.86 0.4/0.86/0.88 0.2/0.88/0.88 | 0.85 0.81 |
| lsnr | p=14 p=30 p=60 p=180 | 0.99 0.99 0.99 1 | 0.98/0.92/0.93 0.78/0.88/0.9 0.6/0.88/0.89 0.39/0.73/0.75 | 0.99 1 1 1 | 0.98/0.92/0.93 0.78/0.9/0.92 0.6/0.88/0.9 0.34/0.83/0.85 | 0.81 0.82 0.79 0.74 | 1/0.65/0.7 0.98/0.63/0.67 0.87/0.64/0.67 0.56/0.67/0.69 | 0.98 0.98 0.99 1 | 0.97/0.92/0.93 0.77/0.89/0.9 0.58/0.88/0.89 0.32/0.84/0.86 | 0.97 0.93 - |
| | | | | | Sparsistency (num | ber of ex | ctra variables) | | | |
| hsnr | p=14 p=30 p=60 p=180 | 5.3(0.9) 4.8(0.4) 4.5(0.2) 4.2(0) | 5.6(1.3)/5.1(1.7)/5.2(1.2) 5.6(3.9)/4.6(0.8)/4.7(0.7) 5.6(8.9)/4.3(0.3)/4.4(0.3) 5.7(32.2)/4.3(7.8)/4.4(7.4) | 5.2(0.7) 4.7(0.2) 4.4(0.1) 4.1(0) | $\begin{array}{c} 5.6(1.2)/5(1.3)/5.1(1) \\ 5.6(3.8)/4.5(0.2)/4.6(0.2) \\ 5.7(9.2)/4.2(0.1)/4.3(0.1) \\ 5.8(48.9)/4.1(0)/4.1(0) \end{array}$ | 4.1(0) 4(0) 4(0) 4(0) 4(0) | 5.1(0.2)/4.1(0)/4.2(0) 5.1(0.6)/4(0)/4.1(0) 5.1(1.5)/4(0)/4(0) 5.3(9.1)/4(0)/4(0) | 5.3(0.9) 4.8(0.4) 4.4(0.1) 4.2(0) | $\begin{array}{c} 5.6(1.3)/5.1(1.6)/5.2(1.2) \\ 5.7(4.1)/4.5(0.6)/4.6(0.6) \\ 5.7(10.5)/4.3(0.1)/4.4(0.1) \\ 5.9(74.6)/4.1(0)/4.2(0.1) \end{array}$ | 5.3(1) 5(0.9) |
| msnr | p=14 p=30 p=60 p=180 | 4.2(0.4) 4.1(0.1) 4(0) 4(0) | 4.8(1.3)/4.5(1.2)/4.4(0.9) 4.8(3.9)/4.2(0.7)/4.2(0.6) 4.8(8.9)/4.1(0.3)/4.1(0.3) 4.8(32.2)/4.1(7.3)/4.1(7) | 4.2(0.3) 4(0.1) 4(0) 4(0) | 4.8(1.2)/4.4(1)/4.3(0.6) 4.8(3.8)/4.1(0.3)/4.1(0.2) 4.8(9.3)/4(0.2)/4(0.1) 5.1(49.2)/3.9(0.1)/3.9(0.1) | 4(0) 4(0) 4(0) 4(0) | 4.3(0.2)/4(0)/4(0) 4.3(0.6)/3.8(0)/3.9(0) 4.3(1.5)/3.7(0)/3.8(0) 4.4(8.9)/3.4(0)/3.5(0) | 4.2(0.5) 4.1(0.2) 4(0) 4(0) | $\begin{array}{c} 4.8(1.3)/4.5(1.2)/4.4(0.8) \\ 4.8(4.1)/4.2(0.5)/4.1(0.5) \\ 4.9(10.5)/4.1(0.2)/4(0.2) \\ 5.3(74.7)/3.9(0.1)/3.9(0.1) \end{array}$ | 4.4(0.7) 4.2(0.7) |
| lsnr | p=14 p=30 p=60 p=180 | 3.4(1) 2.7(0.6) 2.3(0.3) 1.9(0.3) | 3.8(1.3)/3.9(2.4)/3.7(1.8) 3.8(3.9)/2.8(2)/2.7(1.5) 3.8(8.9)/2.2(0.9)/2.2(0.8) 3.9(32.2)/1.8(9)/1.9(8.2) | 3.3(0.8) 2.6(0.4) 2.2(0.2) 1.8(0.2) | 3.8(1.2)/3.7(2.1)/3.5(1.5) 3.8(3.8)/2.5(0.9)/2.4(0.7) 3.9(9.3)/1.8(0.2)/1.9(0.3) 4.3(49.6)/1.1(0.1)/1.2(0.1) | 1.8(0) 1.5(0) 1.2(0) 0.6(0) | 2.8(0.2)/1.1(0)/1.4(0) 2.8(0.6)/0.6(0)/0.9(0) 2.8(1.5)/0.4(0)/0.6(0) 3.1(8.4)/0.2(0)/0.3(0) | 3.4(1.1) 2.7(0.7) 2.2(0.3) 1.9(0.2) | 3.8(1.3)/3.9(2.4)/3.6(1.7) 3.9(4.1)/2.7(1.4)/2.6(1.2) 4(10.5)/2(0.4)/2(0.4) 4.7(74.7)/1.2(0.1)/1.3(0.1) | 3.2(0.8) 2.8(1) - |

Table S4: The performance of BS using different selection rules, Orth-Sparse-Ex2, n=2000

| | | edf | C_p ndf/hdf/bdf | edf | AICc ndf/hdf/bdf | edf | BIC ndf/hdf/bdf | edf | GCV ndf/hdf/bdf | CV |
|------|-------------------------------|--|--|--|--|------------------------------------|---|--|--|----------------------|
| į | | i | | | % worse than | the best | possible BS | | | |
| hsnr | p=14 p=30 p=60 p=180 | 8 3 2 0 | 33/10/9 $85/6/7$ $155/4/5$ $334/4/4$ | 8 3 2 1 | 33/9/9 85/5/6 156/4/5 337/4/3 | 0 0 0 0 | 3/0/1 $9/0/0$ $21/1/1$ $60/4/3$ | 8 3 2 1 | 33/9/9 $86/6/7$ $156/4/5$ $340/4/4$ | 18 23 - |
| msnr | p=14 p=30 p=60 p=180 | 13 14 15 15 | 27/31/28 66/39/35 111/39/35 217/37/35 | 13 13 14 16 | 27/32/27 66/39/35 111/38/35 219/37/35 | 47 74 80 63 | 26/95/80 23/93/86 22/82/78 34/63/62 | 13 13 15 16 | 27/32/28 66/39/35 112/39/35 221/37/35 | 22 31 - |
| lsnr | p=14 p=30 p=60 p=180 | 15 7 3 1 | $\begin{array}{c} 29/19/17 \\ 71/13/12 \\ 131/10/9 \\ 288/9/8 \end{array}$ | 15 7 3 1 | $\begin{array}{c} 29/19/17 \\ 71/13/12 \\ 131/10/9 \\ 291/8/7 \end{array}$ | 1 1 0 | 8/8/7 11/10/7 19/16/11 51/35/30 | 15 7 3 1 | $\begin{array}{c} 29/19/17 \\ 71/13/12 \\ 132/10/9 \\ 293/9/8 \end{array}$ | 20 24 - - |
| | | | | | | ve efficie | b . | | | |
| hsnr | p=14 p=30 p=60 p=180 | 0.93 0.97 0.98 1 | 0.75/0.91/0.91 0.54/0.95/0.94 0.39/0.96/0.95 0.23/0.96/0.97 | 0.93 0.97 0.98 0.99 | 0.75/0.92/0.92 0.54/0.95/0.94 0.39/0.96/0.96 0.23/0.97/0.97 | 1 1 1 1 | 0.97/1/0.99 0.92/1/1 0.83/0.99/0.99 0.62/0.96/0.97 | 0.92 0.97 0.98 0.99 | 0.75/0.91/0.91 0.54/0.95/0.94 0.39/0.96/0.95 0.23/0.96/0.97 | 0.84 0.81 - |
| msnr | p=14 p=30 p=60 p=180 | 1 1 1 1 | 0.89/0.86/0.88 0.68/0.82/0.84 0.54/0.83/0.85 0.36/0.84/0.85 | 1 1 1 1 | 0.89/0.86/0.89 0.68/0.82/0.84 0.54/0.83/0.85 0.36/0.84/0.85 | 0.77 0.65 0.64 0.71 | 0.9/0.58/0.63 0.92/0.59/0.61 0.94/0.63/0.64 0.86/0.71/0.71 | 1 1 1 1 | 0.89/0.86/0.88 0.68/0.82/0.84 0.54/0.83/0.85 0.36/0.84/0.85 | 0.93 0.87 |
| lsnr | p=14 p=30 p=60 p=180 | 0.9 0.95 0.98 0.99 | 0.81/0.88/0.89 0.59/0.9/0.9 0.44/0.91/0.92 0.26/0.92/0.93 | 0.91 0.95 0.98 0.99 | 0.81/0.88/0.89 0.59/0.9/0.91 0.43/0.92/0.93 0.26/0.93/0.93 | 1 1 1 1 | 0.96/0.97/0.97 0.92/0.92/0.95 0.84/0.87/0.9 0.66/0.74/0.77 | 0.91 0.95 0.98 0.99 | 0.81/0.88/0.89 0.59/0.9/0.91 0.43/0.91/0.93 0.26/0.92/0.93 | 0.87 0.82 |
| | | | | | Sparsistency (nun | nber of e | xtra variables) | | | |
| hsnr | p=14 p=30 p=60 p=180 | 6(0.3) 6(0.1) 6(0) 6(0) | 6(1.2)/6(0.4)/6(0.3) 6(3.8)/6(0.2)/6(0.2) 6(8.6)/6(0.1)/6(0.1) 6(27.5)/6(0)/6(0) | 6(0.3) 6(0.1) 6(0) 6(0) | 6(1.2)/6(0.4)/6(0.3) 6(3.8)/6(0.2)/6(0.2) 6(8.6)/6(0.1)/6(0.1) 6(28.2)/6(0)/6(0) | 6(0) 6(0) 6(0) 6(0) | $\begin{array}{c} 6(0)/6(0)/6(0) \\ 6(0.1)/6(0)/6(0) \\ 6(0.3)/6(0)/6(0) \\ 6(1.1)/6(0)/6(0) \end{array}$ | 6(0.3) 6(0.1) 6(0) 6(0) | 6(1.2)/6(0.4)/6(0.3) 6(3.9)/6(0.2)/6(0.2) 6(8.7)/6(0.1)/6(0.1) 6(28.9)/6(0)/6(0) | 6(0.6) 6(0.6) |
| msnr | p=14 p=30 p=60 p=180 | 5.9(0.6) 5.8(0.4) 5.6(0.4) 5.4(0.3) | $\begin{array}{c} 6(1.2)/5.8(1.7)/5.8(1.2) \\ 6(3.8)/5.5(1)/5.6(0.8) \\ 6(8.6)/5.2(0.3)/5.3(0.3) \\ 6(27.5)/4.8(0.1)/4.8(0.1) \end{array}$ | 5.9(0.6) 5.8(0.4) 5.6(0.4) 5.4(0.3) | $\begin{array}{c} 6(1.2)/5.8(1.7)/5.8(1.1) \\ 6(3.8)/5.5(0.9)/5.5(0.8) \\ 6(8.6)/5.2(0.3)/5.3(0.3) \\ 6(28.2)/4.8(0.1)/4.8(0.1) \end{array}$ | 5.1(0) 4.5(0) 4.1(0) 4(0) | 5.5(0)/4.4(0)/4.6(0) 5.5(0.1)/4.2(0)/4.3(0) 5.5(0.3)/4.1(0)/4.2(0) 5.5(1.1)/4(0)/4.1(0) | 5.9(0.6) 5.8(0.4) 5.6(0.4) 5.4(0.3) | $\begin{array}{c} 6(1.2)/5.8(1.7)/5.8(1.2) \\ 6(3.9)/5.5(1)/5.6(0.8) \\ 6(8.7)/5.2(0.3)/5.3(0.3) \\ 6(28.9)/4.8(0.1)/4.8(0.1) \end{array}$ | 5.9(0.8) 5.7(1) |
| lsnr | p=14 p=30 p=60 p=180 | 4.3(0.5) 4.1(0.2) 4(0) 4(0) | 4.9(1.2)/4.5(1)/4.4(0.6) 4.9(3.8)/4.2(0.4)/4.1(0.4) 4.9(8.6)/4.1(0.2)/4.1(0.1) 4.9(27.5)/4(0.1)/4(0.1) | 4.3(0.5) 4.1(0.2) 4(0) 4(0) | $\begin{array}{c} 4.9(1.2)/4.5(0.9)/4.4(0.6) \\ 4.9(3.8)/4.2(0.4)/4.1(0.3) \\ 4.9(8.6)/4.1(0.1)/4.1(0.1) \\ 4.9(28.2)/4(0.1)/4(0.1) \end{array}$ | 4(0) 4(0) 4(0) 4(0) | 4.1(0)/4(0)/4(0) 4.1(0.1)/3.9(0)/4(0) 4.1(0.3)/3.9(0)/3.9(0) 4.1(1.1)/3.7(0)/3.8(0) | 4.3(0.5) 4.1(0.2) 4(0) 4(0) | 4.9(1.2)/4.5(1)/4.4(0.6) 4.9(3.9)/4.2(0.4)/4.1(0.3) 4.9(8.7)/4.1(0.2)/4.1(0.1) 4.9(28.9)/4(0.1)/4(0.1) | 4.5(0.7) 4.3(0.8) |

Table S5: The performance of BS using different selection rules, Orth-Dense, n=200

| | | edf | C_p ndf/hdf/bdf | edf | AICc ndf/hdf/bdf | edf | BIC ndf/hdf/bdf | edf | GCV ndf/hdf/bdf | CV |
|----------|--------------|---------------------|-------------------|------|---------------------|--------|--------------------|------|--------------------|--|
| | | eur | nar/nar/bar | eur | , , | | st possible BS | eur | nar/nar/bar | <u> </u> |
| <u> </u> | p=14 | 0 | 0/0/0 | 0 | 0/0/0 | 0 | 1/0/0 | 0 | 0/0/0 | 0 |
| | p=14 p=30 | 1 | $\frac{0}{0}$ | 1 | $\frac{0}{0}$ | 1 | 28/3/5 | 1 | $\frac{0}{0}$ | 7 |
| hsnr | p=60 | 8 | 7/9/9 | 9 | 7/11/11 | 20 | 8/32/33 | 8 | 8/10/10 | ' |
| | p=180 | 7 | 45/21/20 | 9 | 52/18/19 | 18 | 26/39/42 | 7 | 64/13/13 | - |
| <u> </u> | p=14 | 0 | 9/0/1 | 0 | 10/0/1 | 0 | 36/1/2 | 0 | 9/0/1 | 6 |
| | p=30 | 3 | 10/3/4 | 3 | 11/4/5 | 21 | 27/19/25 | 3 | 10/4/4 | 11 |
| msnr | p=60 | 10 | 11/14/13 | 10 | 11/13/13 | 26 | 10/48/48 | 10 | 12/14/13 | - |
| | p=180 | 8 | 52/23/23 | 10 | 62/18/19 | 21 | 25/61/56 | 8 | 74/14/14 | - |
| | p=14 | 5 | 22/6/8 | 7 | 23/8/10 | 73 | 50/73/72 | 6 | 22/7/8 | 19 |
| , | p=30 | 15 | 10/16/16 | 20 | 10/21/20 | 27 | 16/27/27 | 17 | 10/18/18 | 16 |
| lsnr | p=60 | 13 | 25/17/16 | 13 | 25/13/13 | 13 | 11/13/13 | 13 | 26/14/14 | - |
| | p=180 | 8 | 86/22/22 | 7 | 102/7/7 | 7 | 39/7/7 | 7 | 116/7/7 | - |
| | | Relative efficiency | | | | | | | | |
| | p=14 | 1 | 1/1/1 | 1 | 1/1/1 | 1 | 0.99/1/1 | 1 | 1/1/1 | 1 |
| , | p=30 | 1 | 0.91/1/1 | 1 | 0.9/1/0.99 | 1 | 0.79/0.98/0.96 | 1 | 0.91/1/1 | 0.95 |
| hsnr | p=60 | 0.99 | 1/0.98/0.98 | 0.98 | 1/0.97/0.96 | 0.89 | 0.99/0.81/0.8 | 0.99 | 0.99/0.98/0.98 | - |
| | p=180 | 1 | 0.74/0.89/0.89 | 0.99 | 0.71/0.91/0.9 | 0.91 | 0.85/0.77/0.76 | 1 | 0.65/0.95/0.95 | - |
| | p=14 | 1 | 0.92/1/0.99 | 1 | 0.91/1/0.99 | 1 | 0.74/1/0.99 | 1 | 0.92/1/0.99 | 0.95 |
| | p=30 | 1 | 0.93/0.99/0.99 | 0.99 | 0.92/0.98/0.98 | 0.85 | 0.81/0.87/0.82 | 1 | 0.93/0.99/0.99 | 0.93 |
| msnr | p=60 | 1 | 0.99/0.96/0.97 | 1 | 0.99/0.97/0.97 | 0.87 | 1/0.74/0.74 | 1 | 0.98/0.97/0.97 | - |
| | p=180 | 1 | 0.71/0.88/0.88 | 0.98 | 0.67/0.91/0.91 | 0.89 | 0.87/0.67/0.69 | 1 | 0.62/0.95/0.95 | - |
| | p=14 | 0.98 | 0.85/0.97/0.96 | 0.97 | 0.84/0.96/0.94 | 0.6 | 0.69/0.6/0.6 | 0.98 | 0.85/0.97/0.95 | 0.86 |
| ١, | p=30 | 0.95 | 1/0.95/0.95 | 0.91 | 1/0.91/0.91 | 0.86 | 0.94/0.86/0.86 | 0.93 | 1/0.93/0.93 | 0.94 |
| lsnr | p=60 | 0.98 | 0.89/0.95/0.96 | 0.99 | 0.89/0.99/0.99 | 0.98 | 1/0.98/0.98 | 0.98 | 0.88/0.97/0.98 | - |
| | p=180 | 1 | 0.58/0.88/0.88 | 1 | 0.53/1/1 | 1 | 0.77/1/1 | 1 | 0.5/1/1 | - |
| | | | | | Sparsistency (nu | mber o | f extra variables) | | | |
| | p=14 | 14 | 14/14/14 | 14 | 14/14/14 | 14 | 14/14/14 | 14 | 14/14/14 | 14 |
| , | p=30 | 30 | 24.7/29.5/29 | 30 | 24.2/29.4/28.8 | 30 | 20.9/28.8/27.5 | 30 | 24.7/29.5/29 | 26.6 |
| hsnr | p=60 | 29.8 | 30.5/38.4/35.8 | 22.2 | 29.4/25.6/24.5 | 17.8 | 22.5/16.8/16.5 | 28.6 | 31.3/36.8/34 | - |
| | p=180 | 20.5 | 53.3/37.4/35.5 | 18.3 | 62.3/16.3/16.3 | 16.1 | 35/13.7/13.5 | 19.4 | 89.8/17.8/17.8 | - |
| | p=14 | 14 | 13.2/14/13.9 | 14 | 13.2/14/13.9 | 14 | 11.8/13.9/13.8 | 14 | 13.2/14/13.9 | 13.4 |
| man- | p=30 | 27.3 | 18.8/27.4/26.1 | 26.5 | 18.3/26.8/25.3 | 18 | 13.4/20.4/17.6 | 27.3 | 18.8/27.4/26.1 | 20.8 |
| msnr | p=60 | 19.4 | 24.1/29.6/27 | 13.9 | 23.4/15.6/15.2 | 9.3 | 14.5/7.5/7.4 | 18.3 | 25.2/26/24.1 | - |
| | p=180 | 12.6 | 47.1/29.1/28.1 | 10.4 | 59/8.8/8.8 | 8.1 | 24.4/4.8/5 | 11.3 | 86.4/10/10 | - |
| | p=14 | 13.6 | 7.7/12.7/11.7 | 13.4 | 7.6/12.3/11.3 | 0.7 | 3.6/0.7/0.8 | 13.5 | 7.8/12.6/11.6 | 8.8 |
| lsnr | p=30 | 12.8 | 10.5/14.6/13 | 7.6 | 10.3/8.5/7.6 | 0 | 4/0/0 | 11.3 | 10.8/12.3/11.2 | 7.5 |
| ISIII | p=60 | 3.4 | 15.7/6.5/6 | 1 | 15.8/0.8/1 | 0 | 4.9/0/0 | 2 | 17.3/2.4/2.4 | - |
| | p=180 | 0.8 | 39/14.5/13.7 | 0.3 | 55.2/0.2/0.3 | 0 | 11.8/0/0 | 0.4 | 81.7/0.3/0.4 | - |

Table S6: The performance of BS using different selection rules, Orth-Dense, n=2000

| $ \begin{array}{ c c c c c c c c c c c c c c c c c c c$ | | | 10 | C _p | 10 | AICc | 10 | BIC | 10 | GCV | CV |
|--|------|---------------------|------|----------------|------|------------------|--------|--------------------|------|----------------|------|
| $ \begin{array}{ c c c c c c c c c c c c c c c c c c c$ | 1 | | edf | ndf/hdf/bdf | edf | ndf/hdf/bdf | edf | ndf/hdf/bdf | edf | ndf/hdf/bdf | |
| $\begin{array}{ c c c c c c c c c c c c c c c c c c c$ | | | | | | % worse than | tne be | st possible BS | | | |
| $\begin{array}{ c c c c c c c c c c c c c c c c c c c$ | | p=14 | 0 | | 0 | , , | 0 | / / | 1 | , , | 0 |
| $\begin{array}{ c c c c c c c c c c c c c c c c c c c$ | 1 | 1 * | | | | , , | | , , | | | 1 |
| $\begin{array}{ c c c c c c c c c c c c c c c c c c c$ | nsnr | 1 * | | | | , , | | , , | | , , | - |
| $\begin{array}{ c c c c c c c c c c c c c c c c c c c$ | | p=180 | 6 | 34/8/8 | 6 | 34/8/8 | 19 | 7/36/37 | 6 | 35/8/8 | - |
| $\begin{array}{ c c c c c c c c c c c c c c c c c c c$ | | p=14 | 0 | 0/0/0 | 0 | 0/0/0 | 0 | 0/0/0 | 0 | 0/0/0 | 0 |
| $\begin{array}{ c c c c c c c c c c c c c c c c c c c$ | | p=30 | | | 1 | | | | 1 | | 5 |
| $ \begin{vmatrix} p=14 & 0 & 5/0/0 & 0 & 5/0/0 & 0 & 49/0/1 & 0 & 5/0/0 & 4 \\ p=30 & 2 & 11/3/3 & 2 & 11/3/3 & 44 & 41/36/45 & 2 & 11/3/3 & 10 \\ p=60 & 10 & 10/13/12 & 10 & 10/13/12 & 32 & 16/45/48 & 10 & 10/13/12 & - \\ p=180 & 8 & 48/10/10 & 8 & 48/10/10 & 24 & 8/45/47 & 8 & 49/10/10 & - \\ \hline $ | msnr | p=60 | 1 | | | | | | | | - |
| $ \begin{array}{ c c c c c c c c c c c c c c c c c c c$ | | p=180 | 6 | 39/9/9 | 6 | 39/8/9 | 21 | 7/38/40 | 6 | 40/8/9 | - |
| $ \begin{array}{ c c c c c c c c c c c c c c c c c c c$ | | p=14 | 0 | 5/0/0 | 0 | 5/0/0 | 0 | 49/0/1 | 0 | 5/0/0 | 4 |
| $\begin{array}{ c c c c c c c c c c c c c c c c c c c$ | , | p=30 | 2 | 11/3/3 | 2 | 11/3/3 | 44 | 41/36/45 | 2 | 11/3/3 | 10 |
| $ \begin{array}{ c c c c c c c c } \hline & & & & & & & & & & & & & & & & & & $ | Isnr | p=60 | 10 | 10/13/12 | 10 | | 32 | 16/45/48 | | | - |
| $\begin{array}{ c c c c c c c c c c c c c c c c c c c$ | | p=180 | 8 | 48/10/10 | 8 | 48/10/10 | 24 | 8/45/47 | 8 | 49/10/10 | - |
| $\begin{array}{ c c c c c c c c c c c c c c c c c c c$ | | Relative efficiency | | | | | | | | | |
| $ \begin{array}{ c c c c c c c c } \hline hsnr & p=60 & 0.99 & 1/0.99/0.99 & 0.99 & 1/0.99/0.99 & 0.83 & 0.89/0.78/0.76 & 0.99 & 1/0.99/0.99 & - \\ p=180 & 1 & 0.79/0.98/0.98 & 1 & 0.79/0.98/0.98 & 0.89 & 1/0.78/0.78 & 1 & 0.79/0.98/0.98 & - \\ \hline \\ p=14 & 1 & 1/1/1 & 1 & 1/1/1 & 1 & 1/1/1 & 1 & $ | | p=14 | 1 | 1/1/1 | 1 | 1/1/1 | 1 | 1/1/1 | 1 | 1/1/1 | 1 1 |
| $\begin{array}{ c c c c c c c c c c c c c c c c c c c$ | | p=30 | 1 | 0.99/1/1 | 1 | 0.99/1/1 | 1 | 0.85/1/0.99 | 1 | 0.99/1/1 | 0.99 |
| $ \begin{array}{ c c c c c c c c c c c c c c c c c c c$ | hsnr | p=60 | 0.99 | 1/0.99/0.99 | 0.99 | 1/0.99/0.99 | 0.83 | 0.89/0.78/0.76 | 0.99 | 1/0.99/0.99 | - |
| $\begin{array}{ c c c c c c c c c c c c c c c c c c c$ | | p=180 | 1 | 0.79/0.98/0.98 | 1 | 0.79/0.98/0.98 | 0.89 | 1/0.78/0.78 | 1 | 0.79/0.98/0.98 | - |
| $\begin{array}{ c c c c c c c c c c c c c c c c c c c$ | | p=14 | 1 | 1/1/1 | 1 | 1/1/1 | 1 | 1/1/1 | 1 | 1/1/1 | 1 1 |
| $ \begin{array}{ c c c c c c c c c c c c c c c c c c c$ | | p=30 | 1 | 0.92/1/1 | 1 | 0.92/1/1 | 1 | 0.72/0.99/0.96 | 1 | 0.92/1/1 | 0.96 |
| $ \begin{vmatrix} p=14 & 1 & 0.95/1/1 & 1 & 0.95/1/1 & 1 & 0.67/1/0.99 & 1 & 0.92/0.99/0.99 \\ p=30 & 1 & 0.92/0.99/0.99 & 1 & 0.92/0.99/0.99 & 0.71 & 0.73/0.75/0.7 & 1 & 0.92/0.99/0.99 & 0.93 \\ p=60 & 1 & 1/0.97/0.98 & 1 & 1/0.97/0.98 & 0.83 & 0.94/0.75/0.74 & 1 & 1/0.97/0.98 & - \\ p=180 & 1 & 0.73/0.98/0.98 & 1 & 0.73/0.98/0.98 & 0.87 & 1/0.74/0.73 & 1 & 0.72/0.98/0.98 & - \\ $ | msnr | p=60 | 0.99 | 1/0.98/0.98 | 0.99 | 1/0.98/0.98 | 0.83 | 0.92/0.77/0.76 | 0.99 | 1/0.98/0.98 | - |
| $ \begin{vmatrix} \text{lsnr} & \text{p=30} & 1 & 0.92/0.99/0.99 & 1 & 0.92/0.99/0.99 & 0.71 & 0.73/0.75/0.7 & 1 & 0.92/0.99/0.99 & 0.93 \\ \text{p=60} & 1 & 1/0.97/0.98 & 1 & 1/0.97/0.98 & 0.83 & 0.94/0.75/0.74 & 1 & 1/0.97/0.98 & - \\ \text{p=180} & 1 & 0.73/0.98/0.98 & 1 & 0.73/0.98/0.98 & 0.87 & 1/0.74/0.73 & 1 & 0.72/0.98/0.98 & - \\ $ | | p=180 | 1 | 0.76/0.98/0.98 | 1 | 0.76/0.98/0.98 | 0.88 | 1/0.77/0.76 | 1 | 0.76/0.98/0.98 | - |
| $ \begin{array}{ c c c c c c c c c c c c c c c c c c c$ | | p=14 | 1 | 0.95/1/1 | 1 | 0.95/1/1 | 1 | 0.67/1/0.99 | 1 | 0.95/1/1 | 0.96 |
| $\begin{array}{ c c c c c c c c c c c c c c c c c c c$ | , | p=30 | 1 | 0.92/0.99/0.99 | 1 | 0.92/0.99/0.99 | 0.71 | 0.73/0.75/0.7 | 1 | 0.92/0.99/0.99 | 0.93 |
| $ \begin{array}{ c c c c c c c c c c c c c c c c c c c$ | lsnr | p=60 | 1 | 1/0.97/0.98 | 1 | 1/0.97/0.98 | 0.83 | 0.94/0.75/0.74 | 1 | 1/0.97/0.98 | - |
| $\begin{array}{ c c c c c c c c c c c c c c c c c c c$ | | p=180 | 1 | 0.73/0.98/0.98 | 1 | 0.73/0.98/0.98 | 0.87 | 1/0.74/0.73 | 1 | 0.72/0.98/0.98 | - |
| $ \begin{array}{ c c c c c c c c c c c c c c c c c c c$ | | | | | | Sparsistency (nu | mber o | f extra variables) | | | |
| $ \begin{array}{ c c c c c c c c c c c c c c c c c c c$ | | p=14 | 14 | 14/14/14 | 14 | 14/14/14 | 14 | 14/14/14 | 14 | 14/14/14 | 14 |
| $ \begin{array}{ c c c c c c c c c c c c c c c c c c c$ | | 1 * | | | 1 | | | , , | 1 | | |
| $ \begin{array}{ c c c c c c c c c c c c c c c c c c c$ | hsnr | p=60 | 44.9 | , , | 44.2 | | 28.5 | 30.5/27.6/27.4 | 45.1 | , , | - |
| $ \begin{array}{ c c c c c c c c c c c c c c c c c c c$ | | p=180 | 32.1 | 58.9/32.4/32.3 | 31.8 | 58.9/31.6/31.6 | 27 | 31.3/25/24.9 | 32 | 59.9/32.1/32 | - |
| $ \begin{array}{ c c c c c c c c c c c c c c c c c c c$ | | p=14 | 14 | 14/14/14 | 14 | 14/14/14 | 14 | 14/14/14 | 14 | 14/14/14 | 14 |
| $ \begin{array}{ c c c c c c c c c c c c c c c c c c c$ | | 1 * | 1 | | | | | | l | | |
| $ \begin{array}{ c c c c c c c c c c c c c c c c c c c$ | msnr | p=60 | 34.8 | 33.3/42.8/40.1 | 33.9 | , , | 20.4 | , , | 34.6 | 33.3/42.8/40 | - |
| $ \begin{vmatrix} p = 30 & 28.8 & 19.9/28.2/26.9 \\ p = 60 & 21.6 & 24.8/30.6/27.9 \end{vmatrix} \begin{vmatrix} 28.8 & 19.9/28.1/26.8 \\ 20.9 & 24.7/29.2/26.9 \end{vmatrix} \begin{vmatrix} 13.5 & 12.5/16.7/14.1 \\ 10.5 & 12.5/16.7/14.1 \end{vmatrix} \begin{vmatrix} 28.8 & 19.9/28.2/26.9 \\ 21.8 & 24.9/30.4/27.7 \end{vmatrix} \begin{vmatrix} 22.3 & 24.8/30.6/27.9 \\ 22.3 & 24.8/30.6/27.9 \end{vmatrix} \begin{vmatrix} 22.3 & 24.8/30.6/27.9 \\ 22.3 & 24.8/30.6/27.9 \end{vmatrix} \begin{vmatrix} 22.3 & 24.8/30.6/27.9 \\ 22.3 & 24.8/30.6/27.9 \end{vmatrix} \begin{vmatrix} 22.3 & 24.8/30.6/27.9 \\ 22.3 & 24.8/30.6/27.9 \end{vmatrix} \begin{vmatrix} 22.3 & 24.8/30.6/27.9 \\ 22.3 & 24.8/30.6/27.9 \end{vmatrix} \begin{vmatrix} 22.3 & 24.8/30.6/27.9 \\ 22.3 & 24.8/30.6/27.9 \end{vmatrix} \begin{vmatrix} 22.3 & 24.8/30.6/27.9 \\ 22.3 & 24.8/30.6/27.9 \end{vmatrix} \begin{vmatrix} 22.3 & 24.8/30.6/27.9 \\ 22.3 & 24.8/30.6/27.9 \end{vmatrix} \begin{vmatrix} 22.3 & 24.8/30.6/27.9 \\ 22.3 & 24.8/30.6/27.9 \end{vmatrix} \begin{vmatrix} 22.3 & 24.8/30.6/27.9 \\ 22.3 & 24.8/30.6/27.9 \end{vmatrix} \begin{vmatrix} 22.3 & 24.8/30.6/27.9 \\ 22.3 & 24.8/30.6/27.9 \end{vmatrix} \begin{vmatrix} 22.3 & 24.8/30.6/27.9 \\ 22.3 & 24.8/30.6/27.9 \end{vmatrix} \begin{vmatrix} 22.3 & 24.8/30.6/27.9 \\ 22.3 & 24.8/30.6/27.9 \end{vmatrix} \begin{vmatrix} 22.3 & 24.8/30.6/27.9 \\ 22.3 & 24.8/30.6/27.9 \end{vmatrix} \begin{vmatrix} 22.3 & 24.8/30.6/27.9 \\ 22.3 & 24.8/30.6/27.9 \end{vmatrix} \begin{vmatrix} 22.3 & 24.8/30.6/27.9 \\ 22.3 & 24.8/30.6/27.9 \end{vmatrix} \begin{vmatrix} 22.3 & 24.8/30.6/27.9 \\ 22.3 & 24.8/30.6/27.9 \end{vmatrix} \begin{vmatrix} 22.3 & 24.8/30.6/27.9 \\ 22.3 & 24.8/30.6/27.9 \end{vmatrix} \begin{vmatrix} 22.3 & 24.8/30.6/27.9 \\ 22.3 & 24.8/30.6/27.9 \end{vmatrix} \begin{vmatrix} 22.3 & 24.8/30.6/27.9 \\ 22.3 & 24.8/30.6/27.9 \end{vmatrix} \begin{vmatrix} 22.3 & 24.8/30.6/27.9 \\ 22.3 & 24.8/30.6/27.9 \end{vmatrix} \begin{vmatrix} 22.3 & 24.8/30.6/27.9 \\ 22.3 & 24.8/30.6/27.9 \end{vmatrix} \begin{vmatrix} 22.3 & 24.8/30.6/27.9 \\ 22.3 & 24.8/30.6/27.9 \end{vmatrix} \begin{vmatrix} 22.3 & 24.8/30.6/27.9 \\ 22.3 & 24.8/30.6/27.9 \end{vmatrix} \begin{vmatrix} 22.3 & 24.8/30.6/27.9 \\ 22.3 & 24.8/30.6/27.9 \end{vmatrix} \begin{vmatrix} 22.3 & 22.8 & 24.8/30.6/27.9 \\ 22.3 & 24.8/30.6/27.9 \end{vmatrix} \begin{vmatrix} 22.3 & 22.8 & 24.8/30.6/27.9 \\ 22.3 & 23.8 & 24.8/30.6/27.9 \end{vmatrix} \begin{vmatrix} 22.3 & 22.8 & 24.8/30.6/27.9 \\ 22.3 & 23.8 & 24.8/30.6/27.9 \end{vmatrix} \begin{vmatrix} 22.3 & 22.8 & 24.8/30.6/27.9 \\ 22.3 & 23.8 & 24.8/30.6/27.9 \end{vmatrix} \begin{vmatrix} 22.3 & 22.8 & 24.8/30.6/27.9 \\ 22.3 & 23.8 & 24.8/30.6/27.9 \end{vmatrix} \end{vmatrix} \begin{vmatrix} 22.3 & 22.8 & 22.8 & 24.8/30.6/27.9 \\ 22.3 & 23.8 & 24.8/30.6/27.9 \end{vmatrix} \begin{vmatrix} 22.3 & 22.8 & 22.8 & 22.8 & 22.8 \\ 22.3 & 22.8 & 22.8 & 22.8 & 22.8 \end{vmatrix}$ | | p=180 | 24.2 | 52.4/24.4/24.3 | 24 | 52.6/23.6/23.6 | 19.2 | 23.6/17.3/17.2 | 24.1 | 53.5/24.1/24.1 | - |
| $ \begin{vmatrix} p = 30 & 28.8 & 19.9/28.2/26.9 \\ p = 60 & 21.6 & 24.8/30.6/27.9 \end{vmatrix} \begin{vmatrix} 28.8 & 19.9/28.1/26.8 \\ 20.9 & 24.7/29.2/26.9 \end{vmatrix} \begin{vmatrix} 13.5 & 12.5/16.7/14.1 \\ 10.5 & 12.5/16.7/14.1 \end{vmatrix} \begin{vmatrix} 28.8 & 19.9/28.2/26.9 \\ 21.8 & 24.9/30.4/27.7 \end{vmatrix} \begin{vmatrix} 22.3 & 24.8/30.6/27.9 \\ 22.3 & 24.8/30.6/27.9 \end{vmatrix} \begin{vmatrix} 22.3 & 24.8/30.6/27.9 \\ 22.3 & 24.8/30.6/27.9 \end{vmatrix} \begin{vmatrix} 22.3 & 24.8/30.6/27.9 \\ 22.3 & 24.8/30.6/27.9 \end{vmatrix} \begin{vmatrix} 22.3 & 24.8/30.6/27.9 \\ 22.3 & 24.8/30.6/27.9 \end{vmatrix} \begin{vmatrix} 22.3 & 24.8/30.6/27.9 \\ 22.3 & 24.8/30.6/27.9 \end{vmatrix} \begin{vmatrix} 22.3 & 24.8/30.6/27.9 \\ 22.3 & 24.8/30.6/27.9 \end{vmatrix} \begin{vmatrix} 22.3 & 24.8/30.6/27.9 \\ 22.3 & 24.8/30.6/27.9 \end{vmatrix} \begin{vmatrix} 22.3 & 24.8/30.6/27.9 \\ 22.3 & 24.8/30.6/27.9 \end{vmatrix} \begin{vmatrix} 22.3 & 24.8/30.6/27.9 \\ 22.3 & 24.8/30.6/27.9 \end{vmatrix} \begin{vmatrix} 22.3 & 24.8/30.6/27.9 \\ 22.3 & 24.8/30.6/27.9 \end{vmatrix} \begin{vmatrix} 22.3 & 24.8/30.6/27.9 \\ 22.3 & 24.8/30.6/27.9 \end{vmatrix} \begin{vmatrix} 22.3 & 24.8/30.6/27.9 \\ 22.3 & 24.8/30.6/27.9 \end{vmatrix} \begin{vmatrix} 22.3 & 24.8/30.6/27.9 \\ 22.3 & 24.8/30.6/27.9 \end{vmatrix} \begin{vmatrix} 22.3 & 24.8/30.6/27.9 \\ 22.3 & 24.8/30.6/27.9 \end{vmatrix} \begin{vmatrix} 22.3 & 24.8/30.6/27.9 \\ 22.3 & 24.8/30.6/27.9 \end{vmatrix} \begin{vmatrix} 22.3 & 24.8/30.6/27.9 \\ 22.3 & 24.8/30.6/27.9 \end{vmatrix} \begin{vmatrix} 22.3 & 24.8/30.6/27.9 \\ 22.3 & 24.8/30.6/27.9 \end{vmatrix} \begin{vmatrix} 22.3 & 24.8/30.6/27.9 \\ 22.3 & 24.8/30.6/27.9 \end{vmatrix} \begin{vmatrix} 22.3 & 24.8/30.6/27.9 \\ 22.3 & 24.8/30.6/27.9 \end{vmatrix} \begin{vmatrix} 22.3 & 24.8/30.6/27.9 \\ 22.3 & 24.8/30.6/27.9 \end{vmatrix} \begin{vmatrix} 22.3 & 24.8/30.6/27.9 \\ 22.3 & 24.8/30.6/27.9 \end{vmatrix} \begin{vmatrix} 22.3 & 24.8/30.6/27.9 \\ 22.3 & 24.8/30.6/27.9 \end{vmatrix} \begin{vmatrix} 22.3 & 24.8/30.6/27.9 \\ 22.3 & 24.8/30.6/27.9 \end{vmatrix} \begin{vmatrix} 22.3 & 24.8/30.6/27.9 \\ 22.3 & 24.8/30.6/27.9 \end{vmatrix} \begin{vmatrix} 22.3 & 24.8/30.6/27.9 \\ 22.3 & 24.8/30.6/27.9 \end{vmatrix} \begin{vmatrix} 22.3 & 22.8 & 24.8/30.6/27.9 \\ 22.3 & 24.8/30.6/27.9 \end{vmatrix} \begin{vmatrix} 22.3 & 22.8 & 24.8/30.6/27.9 \\ 22.3 & 23.8 & 24.8/30.6/27.9 \end{vmatrix} \begin{vmatrix} 22.3 & 22.8 & 24.8/30.6/27.9 \\ 22.3 & 23.8 & 24.8/30.6/27.9 \end{vmatrix} \begin{vmatrix} 22.3 & 22.8 & 24.8/30.6/27.9 \\ 22.3 & 23.8 & 24.8/30.6/27.9 \end{vmatrix} \begin{vmatrix} 22.3 & 22.8 & 24.8/30.6/27.9 \\ 22.3 & 23.8 & 24.8/30.6/27.9 \end{vmatrix} \end{vmatrix} \begin{vmatrix} 22.3 & 22.8 & 22.8 & 24.8/30.6/27.9 \\ 22.3 & 23.8 & 24.8/30.6/27.9 \end{vmatrix} \begin{vmatrix} 22.3 & 22.8 & 22.8 & 22.8 & 22.8 \\ 22.3 & 22.8 & 22.8 & 22.8 & 22.8 \end{vmatrix}$ | | p=14 | 14 | 13.6/14/13.9 | 14 | 13.6/14/13.9 | 14 | 11.7/14/13.9 | 14 | 13.6/14/13.9 | 13.7 |
| $ \begin{array}{ c c c c c c c c c c c c c c c c c c c$ | , | 1 * | | | | | | , , | | | |
| $ \begin{array}{c ccccccccccccccccccccccccccccccccccc$ | lsnr | p=60 | 21.6 | 24.8/30.6/27.9 | 20.9 | | 10 | 12.7/8.7/8.5 | 21.8 | 24.9/30.4/27.7 | - |
| | | p=180 | 13.9 | 43.8/14/14 | 13.6 | 44.1/13.3/13.3 | 9.1 | 13.4/7/6.8 | 13.8 | 45/13.7/13.6 | - |

Table S7: The performance of BOSS compared to other methods, Sparse-Ex1, ρ =0, n=200

| | | BOSS C_v -hdf/AICc-hdf/CV | BS CV | FS CV | LASSO AICc/CV | Gamma LASSO AICc/CV | SparseNet CV | rLASSO CV |
|-------|-------|---|----------|-------------|------------------------|------------------------|-----------------|--------------|
| | | , | | % worse t | than the best possible | BOSS | | |
| i | p=14 | 8/6/18 | 19 | 19 | 42/41 | 16/20 | 13 | 15 |
| | p=30 | 5/3/23 | 25 | 23 | 71/69 | 32/23 | 14 | 19 |
| hsnr | p=60 | 4/2/21 | - | 23 | 87/85 | 51/24 | 16 | 19 |
| | p=180 | 34/1/19 | - | 22 | 119/121 | 134/25 | 17 | 19 |
| | p=14 | 17/14/18 | 19 | 19 | 43/42 | 23/23 | 14 | 16 |
| | p=30 | 15/11/23 | 25 | 23 | 71/69 | 49/28 | 16 | 20 |
| msnr | p=60 | 13/9/22 | - | 24 | 87/85 | 82/28 | 17 | 20 |
| | p=180 | 44/7/20 | - | 22 | 119/121 | 222/30 | 17 | 20 |
| | p=14 | 22/24/25 | 26 | 25 | 8/9 | 13/15 | 18 | 15 |
| 1 | p=30 | 32/34/26 | 26 | 26 | 2/2 | 14/9 | 10 | 7 |
| lsnr | p=60 | 27/29/24 | - | 24 | -1/-2 | 27/5 | 6 | 3 |
| | p=180 | 32/22/18 | - | 19 | -4/-2 | 83/2 | 1 | 1 |
| | | | | | Relative efficiency | | | |
| | p=14 | 0.98/1/0.89 | 0.89 | 0.89 | 0.74/0.75 | 0.91/0.88 | 0.93 | 0.92 |
| , | p=30 | 0.98/1/0.84 | 0.82 | 0.83 | 0.6/0.61 | 0.78/0.83 | 0.9 | 0.87 |
| hsnr | p=60 | 0.99/1/0.84 | - | 0.83 | 0.55/0.55 | 0.68/0.83 | 0.88 | 0.86 |
| | p=180 | 0.75/1/0.85 | - | 0.83 | 0.46/0.46 | 0.43/0.81 | 0.87 | 0.85 |
| | p=14 | 0.98/1/0.96 | 0.96 | 0.96 | 0.8/0.81 | 0.93/0.93 | 1 | 0.98 |
| | p=30 | 0.96/1/0.9 | 0.89 | 0.9 | 0.65/0.66 | 0.75/0.87 | 0.96 | 0.93 |
| msnr | p=60 | 0.97/1/0.9 | - | 0.88 | 0.58/0.59 | 0.6/0.85 | 0.94 | 0.91 |
| | p=180 | 0.75/1/0.9 | - | 0.88 | 0.49/0.49 | 0.33/0.83 | 0.91 | 0.89 |
| | p=14 | 0.89/0.88/0.87 | 0.86 | 0.86 | 1/1 | 0.95/0.94 | 0.92 | 0.95 |
| lsnr | p=30 | 0.78/0.76/0.81 | 0.81 | 0.81 | 1/1 | 0.9/0.94 | 0.93 | 0.96 |
| ISIII | p=60 | 0.77/0.76/0.79 | - | 0.79 | 1/1 | 0.78/0.94 | 0.93 | 0.96 |
| | p=180 | 0.73/0.79/0.81 | - | 0.81 | 1/0.98 | 0.52/0.94 | 0.95 | 0.95 |
| | | | Ç | Sparsistenc | y (number of extra va | ariables) | | |
| | p=14 | 6(0.4)/6(0.2)/6(0.6) | 6(0.6) | 6(0.6) | 6(3.8)/6(4.6) | 6(0.9)/6(1.4) | 6(0.7) | 6(0.6) |
| 1 | p=30 | 6(0.1)/6(0)/6(0.6) | 6(0.7) | 6(0.6) | 6(7.3)/6(8.4) | 6(2.3)/6(1.7) | 6(1) | 6(0.7) |
| hsnr | p=60 | 6(0.1)/6(0)/6(0.5) | - | 6(0.5) | 6(10)/6(11.3) | 6(4.6)/6(1.8) | 6(1.4) | 6(0.7) |
| | p=180 | 6(8.9)/6(0)/6(0.4) | - | 6(0.4) | 6(15.3)/6(20.3) | 6(18.1)/6(2.1) | 6(2.3) | 6(0.7) |
| | p=14 | 6(0.8)/6(0.6)/6(0.6) | 6(0.6) | 6(0.6) | 6(3.8)/6(4.6) | 6(1.1)/6(1.4) | 6(0.6) | 6(0.6) |
| man- | p=30 | 6(0.4)/6(0.2)/6(0.6) | 6(0.7) | 6(0.6) | 6(7.4)/6(8.4) | 6(2.9)/6(1.6) | 6(0.7) | 6(0.7) |
| msnr | p=60 | 6(0.2)/6(0.1)/6(0.5) | - | 6(0.5) | 6(10)/6(11.3) | 6(6.2)/6(1.6) | 6(1) | 6(0.8) |
| | p=180 | 6(9.1)/6(0.1)/6(0.4) | - | 6(0.4) | 6(15.3)/6(20.3) | 6(27.7)/6(1.7) | 6(1.4) | 6(0.8) |
| | p=14 | 5.4(4.5)/5.2(4.1)/4.6(1.7) | 4.5(1.6) | 4.6(1.7) | 5.5(3.3)/5.5(3.9) | 5(1.5)/5.1(2.9) | 5(2.7) | 5(2.1) |
| lsnr | p=30 | 4(4.7)/3.1(2.1)/3.7(2) | 3.7(2) | 3.7(2) | 5.3(6.4)/5.3(7.1) | 4.9(3.8)/4.8(4.9) | 4.8(5.3) | 4.6(3.6) |
| 18111 | p=60 | 2.8(1.9)/2(0.3)/2.9(1.4) | - | 3(1.4) | 5.1(8.5)/5.2(9.2) | 4.8(8.1)/4.5(6.3) | 4.5(7) | 4.3(4.4) |
| | p=180 | 2.1(13.8)/1(0.1)/1.8(0.8) | - | 1.8(0.8) | 4.4(11.8)/4.5(15.4) | 4.7(36.6)/3.8(10.1) | 4.1(11.9) | 3.7(7.5) |

Table S8: The performance of BOSS compared to other methods, Sparse-Ex1, ρ =0, n=2000

| | | BOSS | BS | FS | LASSO | Gamma LASSO | SparseNet | rLASSO |
|------|-------|------------------------|--------|-----------|---------------------|----------------|-----------|--------|
| | | C_p -hdf/AICc-hdf/CV | CV | CV | AICc/CV | AICc/CV | CV | CV |
| | | | | % worse | than the best poss | sible BOSS | | |
| | p=14 | 6/6/17 | 18 | 17 | 40/40 | 12/14 | 11 | 13 |
| _ | p=30 | 3/3/20 | 21 | 21 | 72/69 | 19/16 | 12 | 15 |
| hsnr | p=60 | 2/2/23 | - | 22 | 100/96 | 30/19 | 15 | 17 |
| | p=180 | 1/1/21 | - | 21 | 136/132 | 53/20 | 14 | 16 |
| | p=14 | 6/6/17 | 18 | 17 | 41/40 | 14/17 | 12 | 13 |
| | p=30 | 3/3/20 | 21 | 21 | 72/69 | 26/18 | 12 | 15 |
| msnr | p=60 | 2/2/23 | - | 22 | 100/96 | 46/22 | 15 | 18 |
| | p=180 | 1/1/21 | - | 21 | 136/132 | 97/22 | 13 | 17 |
| | p=14 | 8/8/17 | 18 | 17 | 41/40 | 21/20 | 12 | 13 |
| | p=30 | 5/4/20 | 21 | 21 | 72/69 | 44/23 | 12 | 15 |
| lsnr | p=60 | 5/4/23 | - | 22 | 100/96 | 84/27 | 16 | 17 |
| | p=180 | 5/5/21 | - | 21 | 136/132 | 192/27 | 13 | 17 |
| | | | | | Relative efficiency | У | | |
| | p=14 | 1/1/0.9 | 0.9 | 0.91 | 0.76/0.76 | 0.95/0.92 | 0.95 | 0.94 |
| | p=30 | 1/1/0.86 | 0.85 | 0.85 | 0.6/0.61 | 0.87/0.88 | 0.92 | 0.89 |
| hsnr | p=60 | 1/1/0.83 | - | 0.83 | 0.51/0.52 | 0.78/0.85 | 0.89 | 0.87 |
| | p=180 | 1/1/0.84 | - | 0.84 | 0.43/0.44 | 0.66/0.85 | 0.89 | 0.87 |
| | p=14 | 1/1/0.9 | 0.9 | 0.91 | 0.75/0.76 | 0.93/0.91 | 0.95 | 0.94 |
| | p=30 | 1/1/0.86 | 0.85 | 0.85 | 0.6/0.61 | 0.82/0.87 | 0.92 | 0.89 |
| msnr | p=60 | 1/1/0.83 | - | 0.83 | 0.51/0.52 | 0.7/0.84 | 0.89 | 0.86 |
| | p=180 | 1/1/0.83 | - | 0.83 | 0.43/0.44 | 0.51/0.83 | 0.9 | 0.87 |
| | p=14 | 1/1/0.93 | 0.92 | 0.93 | 0.77/0.77 | 0.9/0.9 | 0.97 | 0.96 |
| , | p=30 | 1/1/0.87 | 0.86 | 0.87 | 0.61/0.62 | 0.73/0.85 | 0.93 | 0.91 |
| lsnr | p=60 | 1/1/0.85 | - | 0.85 | 0.52/0.53 | 0.57/0.82 | 0.9 | 0.89 |
| | p=180 | 1/1/0.86 | - | 0.86 | 0.44/0.45 | 0.36/0.83 | 0.93 | 0.9 |
| | | | S_1 | parsisten | cy (number of extr | ra variables) | | |
| | p=14 | 6(0.2)/6(0.2)/6(0.6) | 6(0.6) | 6(0.6) | 6(3.8)/6(4.4) | 6(0.9)/6(1.2) | 6(0.6) | 6(0.5) |
| , | p=30 | 6(0.1)/6(0.1)/6(0.5) | 6(0.6) | 6(0.6) | 6(8.5)/6(8.8) | 6(1.9)/6(1.7) | 6(1) | 6(0.5) |
| hsnr | p=60 | 6(0)/6(0)/6(0.5) | - | 6(0.5) | 6(13.4)/6(12.6) | 6(4)/6(2.2) | 6(1.6) | 6(0.6) |
| | p=180 | 6(0)/6(0)/6(0.4) | - | 6(0.3) | 6(23)/6(20.1) | 6(10.4)/6(2.5) | 6(2.1) | 6(0.4) |
| | p=14 | 6(0.2)/6(0.2)/6(0.6) | 6(0.6) | 6(0.6) | 6(3.8)/6(4.4) | 6(1)/6(1.3) | 6(0.6) | 6(0.5) |
| | p=30 | 6(0.1)/6(0.1)/6(0.5) | 6(0.6) | 6(0.6) | 6(8.5)/6(8.7) | 6(2.2)/6(1.6) | 6(0.9) | 6(0.5) |
| msnr | p=60 | 6(0)/6(0)/6(0.5) | - | 6(0.5) | 6(13.3)/6(12.6) | 6(5)/6(1.9) | 6(1.5) | 6(0.6) |
| | p=180 | 6(0)/6(0)/6(0.4) | - | 6(0.3) | 6(22.8)/6(20) | 6(15.7)/6(1.9) | 6(1.8) | 6(0.4) |
| | p=14 | 6(0.4)/6(0.4)/6(0.6) | 6(0.6) | 6(0.6) | 6(3.8)/6(4.4) | 6(1.1)/6(1.3) | 6(0.5) | 6(0.5) |
| 1 | p=30 | 6(0.1)/6(0.1)/6(0.5) | 6(0.6) | 6(0.6) | 6(8.5)/6(8.7) | 6(2.9)/6(1.4) | 6(0.7) | 6(0.5) |
| lsnr | p=60 | 6(0.1)/6(0.1)/6(0.5) | - | 6(0.5) | 6(13.4)/6(12.5) | 6(6.7)/6(1.6) | 6(1) | 6(0.6) |
| | p=180 | 6(0.1)/6(0.1)/6(0.4) | - | 6(0.3) | 6(23)/6(20) | 6(23.6)/6(1.1) | 6(1) | 6(0.4) |

Table S9: The performance of BOSS compared to other methods, Sparse-Ex1, ρ =0.5, n=200

| | | BOSS C_n -hdf/AICc-hdf/CV | BS CV | FS CV | LASSO AICc/CV | Gamma LASSO AICc/CV | SparseNet CV | rLASSO CV |
|----------|-------|--------------------------------------|----------|------------|----------------------|------------------------|-----------------|--------------|
| | | C _p -ndi/Aicc-ndi/CV | | | an the best possible | | CV | CV |
| | | | | | | | 10 | 10 |
| | p=14 | 7/5/20 | 18 | 21 | 39/39 | 16/19 | 13 | 18 |
| hsnr | p=30 | 4/2/20 | 22 | 21 | 66/65 | 34/21 | 15 | 18 |
| | p=60 | 3/2/21 | - | 23 22 | 92/89 | 57/25 | 16 16 | 18 16 |
| <u> </u> | p=180 | 65/1/19 | | | 139/134 | 136/25 | | |
| | p=14 | 19/17/20 | 15 | 20 | 34/34 | 21/20 | 12 | 21 |
| msnr | p=30 | 13/9/22 | 23 | 23 | 66/65 | 50/26 | 17 | 26 |
| mom | p=60 | 12/8/22 | - | 25 | 90/88 | 85/30 | 17 | 29 |
| | p=180 | 46/9/21 | - | 25 | 126/125 | 211/31 | 18 | 39 |
| | p=14 | 19/22/23 | 23 | 21 | -2/-2 | 12/6 | 7 | 4 |
| lomm | p=30 | 26/27/25 | 24 | 23 | -4/-5 | 9/2 | 2 | -1 |
| lsnr | p=60 | 24/26/22 | - | 20 | -4/-6 | 22/1 | 0 | -3 |
| | p=180 | 48/12/14 | - | 14 | -2/-2 | 91/2 | 1 | 0 |
| | | | | R | elative efficiency | | | |
| | p=14 | 0.98/1/0.87 | 0.89 | 0.87 | 0.75/0.75 | 0.9/0.88 | 0.93 | 0.89 |
| ١, | p=30 | 0.99/1/0.85 | 0.84 | 0.84 | 0.61/0.62 | 0.77/0.85 | 0.89 | 0.87 |
| hsnr | p=60 | 0.99/1/0.85 | - | 0.83 | 0.53/0.54 | 0.65/0.82 | 0.88 | 0.87 |
| | p=180 | 0.61/1/0.85 | - | 0.83 | 0.42/0.43 | 0.43/0.81 | 0.87 | 0.87 |
| | p=14 | 0.95/0.96/0.94 | 0.98 | 0.93 | 0.84/0.84 | 0.93/0.94 | 1 | 0.93 |
| | p=30 | 0.97/1/0.9 | 0.89 | 0.89 | 0.66/0.66 | 0.73/0.87 | 0.93 | 0.87 |
| msnr | p=60 | 0.97/1/0.88 | - | 0.87 | 0.57/0.58 | 0.59/0.83 | 0.93 | 0.84 |
| | p=180 | 0.75/1/0.9 | - | 0.88 | 0.48/0.49 | 0.35/0.83 | 0.93 | 0.79 |
| | p=14 | 0.82/0.8/0.8 | 0.8 | 0.81 | 1/1 | 0.88/0.92 | 0.91 | 0.94 |
| ١, | p=30 | 0.75/0.75/0.76 | 0.77 | 0.77 | 0.99/1 | 0.87/0.93 | 0.93 | 0.96 |
| lsnr | p=60 | 0.76/0.75/0.77 | - | 0.78 | 0.99/1 | 0.77/0.94 | 0.95 | 0.97 |
| | p=180 | 0.66/0.87/0.86 | - | 0.86 | 1/1 | 0.51/0.96 | 0.97 | 0.98 |
| | | | Sp | arsistency | (number of extra v | variables) | | |
| | p=14 | 6(0.3)/6(0.2)/6(0.8) | 6(0.6) | 6(0.8) | 6(3.8)/6(4.2) | 6(0.9)/6(1.3) | 6(0.6) | 6(1) |
| | p=30 | 6(0.1)/6(0)/6(0.6) | 6(0.7) | 6(0.6) | 6(6)/6(8.6) | 6(2.5)/6(1.5) | 6(1.1) | 6(0.8) |
| hsnr | p=60 | $\hat{6}(0)/6(\hat{0})/6(\hat{0}.5)$ | - | 6(0.6) | 6(8.8)/6(12.5) | 6(4.9)/6(1.7) | 6(1.4) | 6(0.9) |
| | p=180 | 6(9.4)/6(0)/6(0.3) | - | 6(0.4) | 6(11.7)/6(21.3) | 6(16.6)/6(1.7) | 6(1.9) | 6(0.6) |
| | p=14 | 6(1.2)/6(1)/6(1.1) | 6(0.7) | 6(1.1) | 6(3.8)/6(4.2) | 6(1.1)/6(1.5) | 6(0.7) | 6(1.7) |
| | p=30 | 6(0.4)/6(0.2)/6(0.7) | 6(0.7) | 6(0.7) | 6(6.1)/6(8.6) | 6(3.1)/6(1.6) | 6(1) | 6(1.3) |
| msnr | p=60 | 6(0.2)/6(0.2)/6(0.6) | - | 6(0.6) | 6(8.8)/6(12.4) | 6(6.3)/6(1.8) | 6(1.1) | 6(1.6) |
| | p=180 | 6(10.2)/6(0.1)/6(0.4) | - | 6(0.4) | 6(16)/6(21.1) | 6(26.5)/6(1.6) | 6(1.3) | 6(1.6) |
| | p=14 | 4.4(3.5)/4.1(3.2)/3.8(2.4) | 3.7(2) | 3.8(2.2) | 5(3.3)/5.1(3.5) | 4(1.6)/4.6(2.8) | 4.6(2.7) | 4.6(2.6) |
| 1 | p=30 | 3.7(4.4)/2.9(2.1)/3.4(2.7) | 3.3(2.3) | 3.4(2.3) | 4.8(4.8)/5.2(7.4) | 4.5(3.9)/4.7(5.2) | 4.8(5.7) | 4.6(4.5) |
| lsnr | p=60 | 2.4(2)/1.6(0.5)/2.5(1.8) | - | 2.5(1.6) | 4.4(6.4)/4.8(10) | 4.4(8.2)/4.2(7) | 4.4(7.9) | 4.1(5.7) |
| | p=180 | 1.3(14.1)/0.3(0.1)/1(0.8) | - | 1.1(0.7) | 2.5(4.9)/3.2(12) | 4.2(35.8)/2.9(9.2) | 3(9.7) | 2.7(7.5) |

Table S10: The performance of BOSS compared to other methods, Sparse-Ex1, ρ =0.5, n=2000

| | | BOSS | BS | FS | LASSO | Gamma LASSO | SparseNet | rLASSO |
|------|-------|------------------------|--------|-----------|---------------------|---------------|-----------|--------|
| | | C_p -hdf/AICc-hdf/CV | CV | CV | AICc/CV | AICc/CV | CV | CV |
| | | | | % worse | than the best poss | sible BOSS | | |
| | p=14 | 7/6/17 | 19 | 17 | 38/39 | 12/14 | 12 | 14 |
| ١, ١ | p=30 | 3/3/20 | 23 | 22 | 67/65 | 21/18 | 14 | 19 |
| hsnr | p=60 | 2/2/21 | - | 21 | 91/89 | 29/19 | 15 | 20 |
| | p=180 | 2/1/22 | - | 23 | 126/123 | 52/20 | 15 | 17 |
| | p=14 | 7/6/17 | 19 | 17 | 39/39 | 16/17 | 12 | 14 |
| | p=30 | 3/3/20 | 23 | 22 | 67/66 | 29/20 | 14 | 19 |
| msnr | p=60 | 2/2/21 | - | 21 | 91/89 | 45/21 | 14 | 20 |
| | p=180 | 2/1/22 | - | 23 | 126/123 | 95/22 | 15 | 17 |
| | p=14 | 13/13/17 | 18 | 17 | 39/39 | 23/21 | 13 | 19 |
| ١, ١ | p=30 | 6/6/20 | 23 | 22 | 67/65 | 49/25 | 15 | 21 |
| lsnr | p=60 | 5/5/21 | - | 21 | 91/89 | 83/26 | 15 | 20 |
| | p=180 | 4/4/22 | - | 23 | 126/123 | 192/28 | 15 | 17 |
| | | | | | Relative efficiency | 7 | | |
| | p=14 | 1/1/0.91 | 0.9 | 0.91 | 0.77/0.77 | 0.95/0.93 | 0.95 | 0.93 |
| | p=30 | 1/1/0.86 | 0.84 | 0.84 | 0.62/0.62 | 0.85/0.87 | 0.9 | 0.87 |
| hsnr | p=60 | 1/1/0.84 | - | 0.84 | 0.54/0.54 | 0.79/0.86 | 0.89 | 0.85 |
| | p=180 | 1/1/0.83 | - | 0.83 | 0.45/0.45 | 0.67/0.85 | 0.88 | 0.87 |
| | p=14 | 1/1/0.91 | 0.9 | 0.91 | 0.77/0.76 | 0.92/0.91 | 0.95 | 0.93 |
| | p=30 | 1/1/0.86 | 0.84 | 0.84 | 0.62/0.62 | 0.8/0.86 | 0.9 | 0.87 |
| msnr | p=60 | 1/1/0.84 | - | 0.84 | 0.54/0.54 | 0.71/0.84 | 0.89 | 0.85 |
| | p=180 | 1/1/0.83 | - | 0.83 | 0.45/0.45 | 0.52/0.83 | 0.89 | 0.87 |
| | p=14 | 1/1/0.96 | 0.95 | 0.96 | 0.81/0.81 | 0.92/0.93 | 1 | 0.95 |
| ١, ١ | p=30 | 1/1/0.88 | 0.86 | 0.87 | 0.63/0.64 | 0.71/0.85 | 0.92 | 0.88 |
| lsnr | p=60 | 1/1/0.87 | - | 0.87 | 0.55/0.56 | 0.57/0.84 | 0.91 | 0.87 |
| | p=180 | 1/1/0.85 | - | 0.85 | 0.46/0.47 | 0.36/0.82 | 0.9 | 0.89 |
| | | | Sı | parsisten | cy (number of ext | ra variables) | | |
| | p=14 | 6(0.3)/6(0.3)/6(0.6) | 6(0.6) | 6(0.6) | 6(3.8)/6(4.2) | 6(0.9)/6(1) | 6(0.6) | 6(0.6) |
| , | p=30 | 6(0.1)/6(0.1)/6(0.6) | 6(0.7) | 6(0.6) | 6(6.6)/6(8.3) | 6(2.1)/6(1.7) | 6(1) | 6(0.8) |
| hsnr | p=60 | 6(0)/6(0)/6(0.5) | - | 6(0.4) | 6(10.3)/6(12.1) | 6(3.7)/6(2) | 6(1.3) | 6(0.7) |
| | p=180 | 6(0)/6(0)/6(0.5) | - | 6(0.4) | 6(13.8)/6(18.9) | 6(9.3)/6(2.5) | 6(2.3) | 6(0.4) |
| | p=14 | 6(0.3)/6(0.3)/6(0.6) | 6(0.6) | 6(0.6) | 6(3.8)/6(4.2) | 6(1)/6(1.2) | 6(0.6) | 6(0.6) |
| | p=30 | 6(0.1)/6(0.1)/6(0.6) | 6(0.7) | 6(0.6) | 6(6.6)/6(8.3) | 6(2.5)/6(1.6) | 6(0.9) | 6(0.8) |
| msnr | p=60 | 6(0)/6(0)/6(0.5) | - | 6(0.4) | 6(10.4)/6(12) | 6(4.6)/6(1.7) | 6(1.2) | 6(0.7) |
| | p=180 | 6(0)/6(0)/6(0.5) | - | 6(0.4) | 6(14)/6(18.7) | 6(14.2)/6(2) | 6(2.1) | 6(0.5) |
| | p=14 | 6(0.6)/6(0.6)/6(0.6) | 6(0.6) | 6(0.6) | 6(3.8)/6(4.3) | 6(1.2)/6(1.3) | 6(0.5) | 6(1) |
| | p=30 | 6(0.2)/6(0.1)/6(0.6) | 6(0.7) | 6(0.6) | 6(6.6)/6(8.4) | 6(3.1)/6(1.5) | 6(0.7) | 6(0.8) |
| lsnr | p=60 | 6(0.1)/6(0.1)/6(0.5) | - | 6(0.4) | 6(10.3)/6(12) | 6(6.5)/6(1.4) | 6(0.8) | 6(0.8) |
| | p=180 | 6(0.1)/6(0)/6(0.5) | - | 6(0.4) | 6(13.8)/6(18.8) | 6(23)/6(1.4) | 6(1.4) | 6(0.5) |

Table S11: The performance of BOSS compared to other methods, Sparse-Ex1, ρ =0.9, n=200

| | | BOSS C_p -hdf/AICc-hdf/CV | BS CV | FS CV | LASSO AICc/CV | Gamma LASSO AICc/CV | SparseNet CV | rLASSO CV |
|-------|---------------|-----------------------------|----------|------------|-----------------------|------------------------|-----------------|--------------|
| | | Cp-lidi/ Micc-lidi/ C v | | | han the best possible | | | |
| | p=14 | 20/21/19 | 16 | 18 | 6/5 | 10/6 | 12 | 7 |
| | p=30 | 16/16/28 | 15 | 28 | 24/24 | 26/16 | 12 | 25 |
| hsnr | p=60 | 15/15/34 | - | 34 | 58/59 | 66/38 | 28 | 23 |
| | p=00 p=180 | 59/8/35 | - | 36 | 98/98 | 153/45 | 27 | 23 |
| | p=14 | 26/27/18 | 17 | 16 | -8/-9 | 11/1 | 3 | -3 |
| | p=30 | 24/27/20 | 19 | 15 | -11/-12 | 5/-5 | -3 | -7 |
| msnr | p=60 | 16/16/19 | - | 16 | $^{2/3}$ | 27/6 | 8 | 0 |
| | p=180 | 26/7/15 | - | 16 | 31/31 | 111/17 | 15 | 12 |
| | p=14 | 28/27/24 | 22 | 19 | -9/-13 | 9/3 | 3 | -1 |
| , | p=30 | 19/18/21 | 19 | 15 | -18/-21 | 5/-7 | -9 | -10 |
| lsnr | p=60 | 17/18/20 | - | 14 | -20/-21 | 6/-12 | -14 | -18 |
| | p=180 | 47/21/18 | - | 14 | -13/-14 | 53/-9 | -10 | -12 |
| | | | | | Relative efficiency | | | |
| | p=14 | 0.87/0.87/0.89 | 0.91 | 0.89 | 0.99/1 | 0.95/0.99 | 0.94 | 0.98 |
| , | p=30 | 0.97/0.97/0.87 | 0.98 | 0.88 | 0.91/0.91 | 0.89/0.96 | 1 | 0.89 |
| hsnr | p=60 | 1/0.99/0.85 | - | 0.85 | 0.73/0.72 | 0.69/0.83 | 0.9 | 0.93 |
| | p=180 | 0.68/1/0.8 | - | 0.79 | 0.55/0.54 | 0.43/0.74 | 0.85 | 0.88 |
| | p=14 | 0.72/0.71/0.77 | 0.77 | 0.78 | 0.98/1 | 0.82/0.9 | 0.88 | 0.93 |
| | p=30 | 0.71/0.69/0.74 | 0.74 | 0.76 | 0.99/1 | 0.84/0.93 | 0.91 | 0.95 |
| msnr | p=60 | 0.86/0.85/0.83 | - | 0.86 | 0.98/0.97 | 0.78/0.94 | 0.92 | 1 |
| | p=180 | 0.86/1/0.93 | - | 0.92 | 0.82/0.82 | 0.51/0.92 | 0.93 | 0.96 |
| | p=14 | 0.68/0.68/0.7 | 0.71 | 0.73 | 0.95/1 | 0.8/0.85 | 0.85 | 0.88 |
| lsnr | p=30 | 0.67/0.67/0.66 | 0.67 | 0.69 | 0.96/1 | 0.76/0.85 | 0.87 | 0.88 |
| 18111 | p=60 | 0.68/0.67/0.66 | - | 0.69 | 0.98/1 | 0.74/0.89 | 0.92 | 0.96 |
| | p=180 | 0.59/0.71/0.73 | - | 0.76 | 1/1 | 0.57/0.95 | 0.96 | 0.98 |
| | | | S | parsistenc | y (number of extra va | riables) | | |
| | p=14 | 5.6(2.8)/5.5(2.6)/5.7(2.8) | 5.6(1.9) | 5.6(2.6) | 5.9(4)/6(4) | 5.6(1.4)/5.8(2) | 5.6(2.2) | 5.9(3.8) |
| hsnr | p=30 | 5.6(1.5)/5.6(1.2)/5.8(3.2) | 5.8(1.5) | 5.8(2.8) | 6(7.5)/6(8.6) | 5.8(3.4)/5.8(3.4) | 5.8(2.3) | 6(7.3) |
| HSHF | p=60 | 5.9(1)/5.8(0.9)/5.9(2.8) | - | 5.9(1.9) | 6(10.2)/6(12.1) | 5.9(6.6)/5.9(4) | 5.9(3) | 6(3.1) |
| | p=180 | 6(9.9)/5.9(0.4)/6(2.4) | - | 6(1.2) | 6(13.6)/6(18) | 6(21.6)/6(4.8) | 6(4.3) | 6(2.5) |
| | p=14 | 2.9(2)/2.7(1.7)/3.7(2.9) | 3.5(2.4) | 3.6(2.7) | 4.9(3.7)/5(3.7) | 3.3(1.6)/4.2(2.6) | 4(2.6) | 4.6(3.4) |
| msnr | p=30 | 3.3(2.9)/3(2.1)/3.9(4.9) | 3.6(3.6) | 3.8(4.1) | 5.1(7.3)/5.3(8.2) | 4.1(3.8)/4.7(5.7) | 4.6(5.5) | 4.9(7.4) |
| шыш | p=60 | 4.3(2.8)/4.1(2.1)/4.4(4.3) | - | 4.4(3.2) | 5.6(10.1)/5.6(11.8) | 4.7(7.4)/5(6.9) | 5(6.8) | 5.5(7.9) |
| | p=180 | 5.1(11.7)/5(1.2)/5(2.3) | - | 5(1.7) | 5.9(14.8)/5.9(17.5) | 5.3(28.6)/5.4(6.8) | 5.4(6.3) | 5.6(5.5) |
| | p=14 | 1(1)/0.9(0.9)/1.5(1.7) | 1.4(1.4) | 1.5(1.4) | 2.6(2.5)/2.9(2.7) | 1.5(1.4)/2(1.8) | 2(1.9) | 2.1(2.1) |
| lsnr | p=30 | 0.9(1.8)/0.8(1.4)/1.2(2.9) | 1.1(2.4) | 1.2(2.2) | 2.2(4.8)/2.6(6) | 1.6(3.2)/2(4.2) | 2.1(4.5) | 1.9(4.5) |
| 18111 | p=60 | 0.9(2)/0.7(1.4)/1.1(3.2) | - | 1.1(2.4) | 2.6(7)/2.9(9) | 2(6.5)/2.3(6.6) | 2.5(7.2) | 2.6(7.3) |
| | p=180 | 1.3(14.7)/0.5(0.6)/1(2.6) | - | 1.2(1.9) | 2.8(9.7)/3.1(13.9) | 2.6(26.4)/2.6(10) | 2.8(11.4) | 2.7(9.4) |

Table S12: The performance of BOSS compared to other methods, Sparse-Ex1, ρ =0.9, n=2000

| | | BOSS C _n -hdf/AICc-hdf/CV | BS CV | FS CV | LASSO AICc/CV | Gamma LASSO AICc/CV | SparseNet CV | rLASSO CV |
|-----------------------|---------------|---|----------|----------|----------------------|------------------------|-----------------|--------------|
| | | | | | an the best possible | | CV | CV |
| | p=14 | 7/7/21 | 18 | 22 | 30/30 | 6/8 | 17 | 23 |
| | p=14 p=30 | 4/3/22 | 25 | 23 | 58/57 | 14/12 | 21 | 33 |
| hsnr | p=60 | $\frac{4/3/22}{2/2/21}$ | - | 23 | 81/82 | 34/19 | 18 | 18 |
| | p=00 p=180 | 1/1/18 | - | 22 | 114/113 | 68/18 | 15 | 17 |
| | p=14 | 15/15/21 | 14 | 21 | 22/20 | 14/12 | 14 | 23 |
| | p=30 | 4/4/28 | 23 | 28 | 54/53 | 46/22 | 21 | 50 |
| msnr | p=60 | 2/2/22 | - | 24 | 81/82 | 76/24 | 20 | 24 |
| | p=180 | 1/1/18 | - | 22 | 114/113 | 140/21 | 15 | 18 |
| | p=14 | 27/28/17 | 17 | 15 | -7/-9 | 10/2 | 4 | -2 |
| | p=30 | 22/22/20 | 16 | 17 | -7/-7 | 10/-1 | 0 | -4 |
| lsnr | p=60 | 9/9/17 | - | 16 | 15/15 | 42/13 | 16 | 12 |
| | p=180 | 3/3/13 | - | 15 | 59/58 | 146/21 | 33 | 18 |
| | | | | R | Relative efficiency | | | |
| | p=14 | 0.99/0.99/0.87 | 0.89 | 0.87 | 0.81/0.81 | 1/0.97 | 0.9 | 0.86 |
| 1 | p=30 | 1/1/0.85 | 0.83 | 0.84 | 0.65/0.66 | 0.9/0.92 | 0.86 | 0.77 |
| hsnr | p=60 | 1/1/0.84 | - | 0.83 | 0.56/0.56 | 0.76/0.86 | 0.86 | 0.86 |
| | p=180 | 1/1/0.85 | - | 0.83 | 0.47/0.47 | 0.6/0.85 | 0.88 | 0.86 |
| | p=14 | 0.98/0.98/0.93 | 0.99 | 0.93 | 0.92/0.93 | 0.99/1 | 0.98 | 0.91 |
| | p=30 | 1/1/0.81 | 0.85 | 0.81 | 0.67/0.68 | 0.71/0.85 | 0.86 | 0.69 |
| msnr | p=60 | 1/1/0.83 | - | 0.82 | 0.56/0.56 | 0.58/0.82 | 0.85 | 0.82 |
| | p=180 | 1/1/0.85 | - | 0.83 | 0.47/0.47 | 0.42/0.84 | 0.87 | 0.86 |
| | p=14 | 0.72/0.72/0.78 | 0.78 | 0.79 | 0.98/1 | 0.83/0.9 | 0.88 | 0.93 |
| lsnr | p=30 | 0.76/0.76/0.77 | 0.8 | 0.79 | 0.99/1 | 0.84/0.94 | 0.92 | 0.97 |
| 15111 | p=60 | 1/1/0.93 | - | 0.93 | 0.94/0.94 | 0.77/0.96 | 0.94 | 0.97 |
| | p=180 | 1/1/0.92 | - | 0.9 | 0.65/0.65 | 0.42/0.85 | 0.78 | 0.88 |
| | | | Sı | | (number of extra v | | | |
| | p=14 | 6(0.3)/6(0.3)/6(0.9) | 6(0.7) | 6(0.9) | 6(3.4)/6(3.4) | 6(0.2)/6(0.3) | 6(0.6) | 6(1.9) |
| hsnr | p=30 | 6(0.1)/6(0.1)/6(0.7) | 6(0.7) | 6(0.6) | 6(7.6)/6(8) | 6(0.9)/6(0.7) | 6(1.2) | 6(2.3) |
| HSIII | p=60 | 6(0)/6(0)/6(1) | - | 6(0.5) | 6(11.1)/6(12.1) | 6(2.9)/6(1.4) | 6(1.4) | 6(0.8) |
| | p=180 | 6(0)/6(0)/6(1.3) | - | 6(0.4) | 6(15.6)/6(18.5) | 6(9.5)/6(1.7) | 6(1.9) | 6(0.6) |
| | p=14 | 5.9(1.2)/5.9(1.2)/6(1.7) | 6(1) | 6(1.6) | 6(4)/6(3.9) | 6(1)/6(1.2) | 5.9(1) | 6(3.3) |
| msnr | p=30 | 6(0.2)/6(0.2)/6(1.2) | 6(0.7) | 6(1) | 6(7.8)/6(8.2) | 6(3.1)/6(1.4) | 6(1.2) | 6(4.8) |
| 1110111 | p=60 | 6(0)/6(0)/6(1.1) | - | 6(0.6) | 6(11.1)/6(12.1) | 6(6.4)/6(1.5) | 6(1.2) | 6(1.1) |
| | p=180 | 6(0)/6(0)/6(1.3) | - | 6(0.4) | 6(15.8)/6(18.5) | 6(18.7)/6(1.4) | 6(1.5) | 6(0.6) |
| | p=14 | 3.5(2.1)/3.5(2.1)/4.3(3) | 4(2.4) | 4.2(2.8) | 5.3(3.8)/5.4(3.8) | 3.9(1.8)/4.6(2.7) | 4.5(2.6) | 5(3.5) |
| lsnr | p=30 | 4.1(2.7)/4.1(2.7)/4.6(4.5) | 4.5(3.2) | 4.5(3.7) | 5.6(7.7)/5.7(8) | 4.7(4)/5.1(5.3) | 5.1(5) | 5.5(7) |
| 19111 | p=60 | 5(1.4)/5(1.4)/5.1(3.1) | - | 5.1(2.2) | 5.9(11.1)/5.9(12) | 5.3(8.2)/5.4(6) | 5.3(5.7) | 5.8(7.4) |
| | p=180 | 5.6(0.6)/5.6(0.6)/5.6(2) | - | 5.6(0.9) | 6(15.7)/6(18.4) | 5.7(26.1)/5.6(3.6) | 5.5(5.3) | 5.9(3.1) |

Table S13: The performance of BOSS compared to other methods, Sparse-Ex2, ρ =0, n=200

| | | BOSS | BS | FS | LASSO | Gamma LASSO | SparseNet | rLASSO |
|------|-------|-----------------------------|--------------------|-------------|---------------------------------|--------------------|-----------|----------|
| | | C_p -hdf/AICc-hdf/CV | CV | CV | AICc/CV | AICc/CV | CV | CV |
| | | | | % worse th | an the best possible | BOSS | | |
| | p=14 | 8/6/20 | 21 | 20 | 41/41 | 17/20 | 15 | 16 |
| ١, | p=30 | 5/3/24 | 25 | 25 | 69/68 | 32/22 | 15 | 20 |
| hsnr | p=60 | 4/2/21 | - | 23 | 95/94 | 53/23 | 16 | 19 |
| | p=180 | 34/1/19 | - | 21 | 129/130 | 139/27 | 18 | 17 |
| | p=14 | 17/14/20 | 21 | 20 | 42/41 | 23/23 | 16 | 17 |
| | p=30 | 17/13/24 | 25 | 25 | 69/68 | 48/27 | 16 | 21 |
| msnr | p=60 | 13/9/21 | - | 23 | 95/94 | 84/28 | 16 | 23 |
| | p=180 | 49/10/20 | - | 22 | 129/130 | 224/32 | 18 | 29 |
| | p=14 | 21/22/24 | 25 | 24 | 7/7 | 14/14 | 16 | 12 |
| 1 | p=30 | 29/31/26 | 25 | 26 | 1/1 | 13/8 | 8 | 6 |
| lsnr | p=60 | 26/28/23 | - | 22 | 0/0 | 25/5 | 6 | 5 |
| | p=180 | 31/18/15 | - | 16 | -2/0 | 85/4 | 3 | 3 |
| | | | | I | Relative efficiency | | | |
| | p=14 | 0.98/1/0.89 | 0.88 | 0.89 | 0.75/0.75 | 0.91/0.89 | 0.92 | 0.91 |
| ١. | p=30 | 0.98/1/0.83 | 0.82 | 0.82 | 0.61/0.61 | 0.78/0.84 | 0.9 | 0.86 |
| hsnr | p=60 | 0.99/1/0.85 | - | 0.83 | 0.52/0.53 | 0.67/0.83 | 0.88 | 0.86 |
| | p=180 | 0.75/1/0.85 | - | 0.84 | 0.44/0.44 | 0.42/0.8 | 0.86 | 0.86 |
| | p=14 | 0.98/1/0.95 | 0.94 | 0.95 | 0.8/0.81 | 0.93/0.93 | 0.98 | 0.98 |
| | p=30 | 0.96/1/0.91 | 0.9 | 0.9 | 0.67/0.67 | 0.76/0.89 | 0.97 | 0.93 |
| msnr | p=60 | 0.97/1/0.9 | - | 0.89 | 0.56/0.56 | 0.59/0.85 | 0.94 | 0.89 |
| | p=180 | 0.74/1/0.92 | - | 0.9 | 0.48/0.48 | 0.34/0.83 | 0.93 | 0.85 |
| | p=14 | 0.89/0.88/0.86 | 0.86 | 0.86 | 1/1 | 0.94/0.94 | 0.92 | 0.95 |
| 1 | p=30 | 0.78/0.77/0.8 | 0.8 | 0.8 | 1/1 | 0.89/0.93 | 0.93 | 0.95 |
| lsnr | p=60 | 0.79/0.78/0.81 | - | 0.81 | 1/0.99 | 0.8/0.95 | 0.94 | 0.95 |
| | p=180 | 0.75/0.83/0.85 | - | 0.85 | 1/0.98 | 0.53/0.94 | 0.95 | 0.95 |
| | | | S_1 | parsistency | (number of extra var | riables) | | |
| | p=14 | 6(0.3)/6(0.2)/6(0.6) | 6(0.7) | 6(0.6) | 6(3.6)/6(4.4) | 6(1)/6(1.4) | 6(0.6) | 6(0.6) |
| ١, | p=30 | 6(0.1)/6(0)/6(0.6) | 6(0.7) | 6(0.7) | 6(7.5)/6(8.4) | 6(2.4)/6(1.7) | 6(1.1) | 6(0.8) |
| hsnr | p=60 | 6(0.1)/6(0)/6(0.5) | - | 6(0.5) | 6(11.4)/6(13.2) | 6(4.8)/6(1.6) | 6(1.6) | 6(0.7) |
| | p=180 | 6(8.8)/6(0)/6(0.4) | - | 6(0.4) | 6(15.9)/6(22.1) | 6(18.5)/6(2.2) | 6(2.6) | 6(0.7) |
| | p=14 | 6(0.8)/6(0.6)/6(0.6) | 6(0.7) | 6(0.6) | 6(3.6)/6(4.4) | 6(1.1)/6(1.4) | 6(0.6) | 6(0.6) |
| | p=30 | 6(0.5)/6(0.2)/6(0.6) | 6(0.7) | 6(0.7) | 6(7.4)/6(8.5) | 6(2.9)/6(1.6) | 6(0.8) | 6(0.9) |
| msnr | p=60 | 6(0.2)/6(0.1)/6(0.5) | - | 6(0.5) | 6(11.3)/6(13.2) | 6(6.4)/6(1.5) | 6(1) | 6(0.9) |
| | p=180 | 6(9.8)/6(0.1)/6(0.4) | - | 6(0.4) | 6(15.9)/6(22) | 6(27.5)/6(2) | 6(1.6) | 6(1.3) |
| | p=14 | 5.5(4.5)/5.4(4.2)/4.8(1.8) | 4.8(1.7) | 4.8(1.8) | 5.7(3.3)/5.7(4) | 5.1(1.5)/5.3(2.9) | 5.2(2.8) | 5.2(2) |
| ١, | p=30 | 3.9(4.3)/3.1(1.8)/3.6(2.2) | $3.\dot{6}(2)^{'}$ | 3.6(2.1) | $5.3(\hat{6}.6)/5.3(\hat{7}.1)$ | 4.8(3.8)/4.7(4.9) | 4.8(5.3) | 4.5(3.6) |
| lsnr | p=60 | 2.3(1.8)/1.4(0.3)/2.7(1.4) | - | 2.7(1.4) | 4.7(8.8)/4.7(9.9) | 4.9(8.6)/4.2(6.9) | 4.3(7.5) | 4(5.5) |
| | p=180 | 1.7(14.1)/0.5(0.1)/1.4(0.6) | - | 1.4(0.7) | 3.7(10.7)/3.8(13.5) | 4.6(36.7)/3.2(9.4) | 3.3(10.3) | 3.1(8) |

Table S14: The performance of BOSS compared to other methods, Sparse-Ex2, ρ =0, n=2000

| | | BOSS C _n -hdf/AICc-hdf/CV | BS CV | FS CV | LASSO AICc/CV | Gamma LASSO AICc/CV | SparseNet CV | rLASSO CV |
|------|-------|---|----------|-----------|---------------------|------------------------|-----------------|--------------|
| | | | | | than the best poss | | CV | CV |
| | p=14 | 6/6/17 | 17 | 17 | 40/41 | 12/14 | 11 | 13 |
| | p=30 | 3/3/22 | 22 | 23 | 74/71 | 20/18 | 13 | 16 |
| hsnr | p=60 | 2/2/24 | - | 23 | 97/93 | 29/19 | 15 | 18 |
| | p=180 | 1/1/21 | - | 21 | 131/128 | 52/18 | 13 | 16 |
| | p=14 | 6/6/17 | 17 | 17 | 41/41 | 14/17 | 11 | 13 |
| | p=30 | 3/3/22 | 22 | 23 | 74/71 | 27/20 | 13 | 16 |
| msnr | p=60 | 2/2/24 | - | 23 | 97/93 | 44/21 | 15 | 18 |
| | p=180 | 1/1/21 | - | 21 | 131/127 | 97/22 | 13 | 16 |
| | p=14 | 9/8/17 | 17 | 17 | 41/41 | 21/21 | 12 | 13 |
| lsnr | p=30 | 5/5/22 | 22 | 23 | 74/71 | 46/25 | 13 | 16 |
| ISHF | p=60 | 5/4/24 | - | 23 | 97/93 | 82/26 | 15 | 18 |
| | p=180 | 5/5/21 | - | 21 | 131/128 | 192/26 | 12 | 17 |
| | | | | | Relative efficiency | У | | |
| | p=14 | 1/1/0.91 | 0.91 | 0.91 | 0.76/0.76 | 0.95/0.93 | 0.96 | 0.94 |
| ١, | p=30 | 1/1/0.84 | 0.84 | 0.84 | 0.59/0.6 | 0.86/0.87 | 0.91 | 0.89 |
| hsnr | p=60 | 1/1/0.83 | - | 0.83 | 0.52/0.53 | 0.79/0.86 | 0.89 | 0.86 |
| | p=180 | 1/1/0.83 | - | 0.84 | 0.44/0.44 | 0.66/0.86 | 0.89 | 0.87 |
| | p=14 | 1/1/0.91 | 0.91 | 0.91 | 0.75/0.75 | 0.93/0.91 | 0.96 | 0.94 |
| | p=30 | 1/1/0.84 | 0.84 | 0.84 | 0.59/0.6 | 0.81/0.86 | 0.91 | 0.89 |
| msnr | p=60 | 1/1/0.83 | - | 0.83 | 0.52/0.53 | 0.71/0.84 | 0.89 | 0.86 |
| | p=180 | 1/1/0.83 | - | 0.84 | 0.44/0.44 | 0.51/0.83 | 0.9 | 0.87 |
| | p=14 | 1/1/0.93 | 0.93 | 0.93 | 0.77/0.77 | 0.9/0.9 | 0.97 | 0.96 |
| lsnr | p=30 | 1/1/0.86 | 0.86 | 0.85 | 0.6/0.61 | 0.72/0.84 | 0.93 | 0.91 |
| ISHF | p=60 | 1/1/0.84 | - | 0.85 | 0.53/0.54 | 0.57/0.83 | 0.91 | 0.89 |
| | p=180 | 1/1/0.86 | - | 0.86 | 0.45/0.46 | 0.36/0.83 | 0.94 | 0.9 |
| | | | S_1 | parsisten | cy (number of ext | ra variables) | | |
| | p=14 | 6(0.3)/6(0.3)/6(0.6) | 6(0.6) | 6(0.6) | 6(3.8)/6(4.5) | 6(0.9)/6(1.3) | 6(0.6) | 6(0.5) |
| , | p=30 | 6(0.1)/6(0.1)/6(0.6) | 6(0.6) | 6(0.6) | 6(8.4)/6(8.7) | 6(2)/6(1.8) | 6(0.9) | 6(0.5) |
| hsnr | p=60 | 6(0)/6(0)/6(0.5) | - | 6(0.5) | 6(13.1)/6(12.2) | 6(3.8)/6(2.1) | 6(1.5) | 6(0.6) |
| | p=180 | 6(0)/6(0)/6(0.3) | - | 6(0.3) | 6(21.6)/6(19.3) | 6(10.3)/6(2.4) | 6(2.1) | 6(0.5) |
| | p=14 | 6(0.3)/6(0.3)/6(0.6) | 6(0.6) | 6(0.6) | 6(3.8)/6(4.5) | 6(0.9)/6(1.3) | 6(0.6) | 6(0.5) |
| | p=30 | 6(0.1)/6(0.1)/6(0.6) | 6(0.6) | 6(0.6) | 6(8.5)/6(8.7) | 6(2.2)/6(1.7) | 6(0.9) | 6(0.5) |
| msnr | p=60 | 6(0)/6(0)/6(0.5) | - | 6(0.5) | 6(13.1)/6(12.2) | 6(4.8)/6(1.8) | 6(1.4) | 6(0.6) |
| | p=180 | 6(0)/6(0)/6(0.3) | - | 6(0.3) | 6(21.8)/6(19.4) | 6(15.6)/6(1.9) | 6(1.9) | 6(0.5) |
| | p=14 | 6(0.4)/6(0.4)/6(0.6) | 6(0.6) | 6(0.6) | 6(3.8)/6(4.5) | 6(1.1)/6(1.4) | 6(0.5) | 6(0.5) |
| long | p=30 | 6(0.1)/6(0.1)/6(0.6) | 6(0.6) | 6(0.6) | 6(8.4)/6(8.7) | 6(3)/6(1.6) | 6(0.7) | 6(0.5) |
| lsnr | p=60 | 6(0.1)/6(0.1)/6(0.5) | - | 6(0.5) | 6(13.1)/6(12.2) | 6(6.8)/6(1.4) | 6(1) | 6(0.6) |
| | p=180 | 6(0.1)/6(0.1)/6(0.3) | - | 6(0.3) | 6(21.7)/6(19.4) | 6(23.9)/6(1.1) | 6(0.9) | 6(0.5) |

Table S15: The performance of BOSS compared to other methods, Sparse-Ex2, ρ =0.5, n=200

| | | BOSS C_n -hdf/AICc-hdf/CV | BS CV | FS CV | LASSO AICc/CV | Gamma LASSO AICc/CV | SparseNet CV | rLASSO CV |
|-----------|-------|-----------------------------|----------|------------|----------------------|------------------------|-----------------|--------------|
| | | , , , | 9 | worse that | an the best possible | BOSS | | |
| <u> </u> | p=14 | 8/6/17 | 18 | 17 | 46/44 | 15/20 | 13 | 15 |
| | p=30 | 5/3/24 | 24 | 24 | 91/88 | 28/23 | 14 | 18 |
| hsnr | p=60 | 4/2/22 | - | 23 | 123/119 | 43/24 | 16 | 17 |
| | p=180 | 34/1/19 | - | 22 | 168/165 | 100/28 | 17 | 15 |
| | p=14 | 19/16/26 | 18 | 17 | 46/44 | 21/23 | 14 | 16 |
| | p=30 | 22/18/29 | 23 | 25 | 89/87 | 42/28 | 14 | 41 |
| msnr | p=60 | 16/11/29 | - | 25 | 121/117 | 70/29 | 16 | 42 |
| | p=180 | 48/9/29 | - | 30 | 160/157 | 179/32 | 14 | 52 |
| | p=14 | 24/25/28 | 23 | 26 | 18/17 | 15/20 | 22 | 23 |
| lamm | p=30 | 33/34/26 | 20 | 30 | 17/17 | 15/19 | 18 | 22 |
| lsnr | p=60 | 28/29/23 | - | 28 | 15/16 | 23/17 | 16 | 19 |
| | p=180 | 28/14/14 | - | 17 | 8/9 | 71/11 | 10 | 12 |
| | | | | R | elative efficiency | | | |
| | p=14 | 0.98/1/0.91 | 0.9 | 0.91 | 0.73/0.74 | 0.92/0.89 | 0.94 | 0.92 |
| ١, | p=30 | 0.98/1/0.83 | 0.83 | 0.83 | 0.54/0.55 | 0.8/0.84 | 0.9 | 0.87 |
| hsnr | p=60 | 0.98/1/0.83 | - | 0.83 | 0.46/0.46 | 0.71/0.82 | 0.88 | 0.87 |
| | p=180 | 0.75/1/0.85 | - | 0.83 | 0.38/0.38 | 0.5/0.79 | 0.86 | 0.88 |
| | p=14 | 0.96/0.98/0.9 | 0.97 | 0.97 | 0.78/0.79 | 0.94/0.92 | 1 | 0.98 |
| | p=30 | 0.93/0.97/0.88 | 0.92 | 0.91 | 0.6/0.61 | 0.8/0.89 | 1 | 0.81 |
| msnr | p=60 | 0.96/1/0.86 | - | 0.89 | 0.5/0.51 | 0.66/0.87 | 0.96 | 0.78 |
| | p=180 | 0.74/1/0.84 | - | 0.83 | 0.42/0.42 | 0.39/0.83 | 0.95 | 0.71 |
| | p=14 | 0.92/0.92/0.9 | 0.94 | 0.91 | 0.97/0.98 | 1/0.96 | 0.94 | 0.94 |
| lsnr | p=30 | 0.87/0.86/0.92 | 0.96 | 0.88 | 0.99/0.98 | 1/0.96 | 0.98 | 0.94 |
| 15111 | p=60 | 0.89/0.89/0.93 | - | 0.89 | 1/0.99 | 0.93/0.98 | 0.99 | 0.96 |
| | p=180 | 0.84/0.94/0.94 | - | 0.92 | 1/0.99 | 0.63/0.97 | 0.98 | 0.96 |
| | | | Sp | arsistency | (number of extra va | riables) | | |
| | p=14 | 6(0.4)/6(0.3)/6(0.6) | 6(0.6) | 6(0.6) | 6(4.6)/6(5.5) | 6(0.9)/6(1.5) | 6(0.7) | 6(0.6) |
| la como m | p=30 | 6(0.1)/6(0)/6(0.7) | 6(0.7) | 6(0.7) | 6(11.2)/6(12.8) | 6(2.2)/6(1.5) | 6(1.1) | 6(0.7) |
| hsnr | p=60 | 6(0.1)/6(0)/6(0.5) | - | 6(0.5) | 6(16)/6(19.1) | 6(4.3)/6(1.5) | 6(1.7) | 6(0.6) |
| | p=180 | 6(9.3)/6(0)/6(0.4) | - | 6(0.4) | 6(22.5)/6(31.5) | 6(14.2)/6(2.1) | 6(2.8) | 6(0.6) |
| | p=14 | 6(0.9)/6(0.8)/6(0.6) | 6(0.6) | 6(0.6) | 6(4.6)/6(5.5) | 6(1.1)/6(1.6) | 6(0.7) | 6(0.6) |
| msnr | p=30 | 6(0.6)/6(0.4)/6(0.7) | 6(0.7) | 6(0.7) | 6(11.2)/6(12.8) | 6(2.7)/6(1.5) | 6(0.9) | 6(2) |
| msnr | p=60 | 6(0.3)/6(0.2)/6(0.5) | - | 6(0.6) | 6(16)/6(19.1) | 6(5.6)/6(1.3) | 6(1.4) | 6(1.9) |
| | p=180 | 6(10.1)/6(0.1)/6(0.5) | - | 6(0.7) | 6(22.3)/6(31.6) | 6(23.9)/6(2) | 6(2.1) | 6(2.5) |
| | p=14 | 5.7(4.8)/5.6(4.5)/5.1(1.6) | 5.1(1.4) | 5.1(1.9) | 5.7(4.3)/5.7(5.1) | 5.4(1.6)/5.5(3.7) | 5.3(2.7) | 5.4(3.2) |
| lsnr | p=30 | 3.6(5.3)/2.4(2.2)/3.9(2.4) | 3.9(1.9) | 3.5(2.8) | 4.5(8)/4.4(8.9) | 5(4.7)/4.3(6.5) | 4.2(5.3) | 3.9(6.1) |
| ISIII. | p=60 | 2.3(2.4)/1(0.3)/3.1(2.1) | - | 2.5(1.8) | 3.8(9.8)/3.7(10.9) | 5(9)/3.7(8.1) | 3.7(7) | 3.3(7.8) |
| | p=180 | 1.7(14.9)/0.4(0.1)/1.4(1.1) | - | 0.9(0.8) | 2.4(9.8)/2.4(12.9) | 4.5(35.8)/2.3(11) | 2.3(9.3) | 2.1(9.1) |

Table S16: The performance of BOSS compared to other methods, Sparse-Ex2, ρ =0.5, n=2000

| $ \begin{array}{ c c c c c } \hline & & & & & & & & & & & & & & & & & & $ | | | BOSS | BS | FS | LASSO | Gamma LASSO | SparseNet | rLASSO |
|---|------|-------|------------------------|--------|-----------|---------------------|----------------|--------------|--------|
| $\begin{array}{ c c c c c c c c c c c c c c c c c c c$ | | | C_p -hdf/AICc-hdf/CV | CV | CV | AICc/CV | AICc/CV | CV | CV |
| $\begin{array}{ c c c c c c c c c c c c c c c c c c c$ | | | | (| % worse | than the best poss | sible BOSS | | |
| $\begin{array}{ c c c c c c c }\hline hsnr & p=60 & 2/2/23 & - & 23 & 124/120 & 28/20 & 14 & 15 \\ p=180 & 1/1/21 & - & 21 & 174/171 & 46/20 & 14 & 15 \\ \hline \\ hsnr & p=30 & 4/3/23 & 22 & 23 & 85/83 & 25/20 & 12 & 16 \\ p=30 & 4/3/23 & 22 & 23 & 85/83 & 25/20 & 12 & 16 \\ p=60 & 2/2/23 & - & 23 & 125/120 & 39/22 & 14 & 15 \\ p=180 & 1/1/21 & - & 21 & 174/171 & 77/23 & 13 & 15 \\ \hline \\ hsnr & p=60 & 8/8/26 & - & 23 & 124/120 & 72/28 & 14 & 15 \\ p=60 & 8/8/26 & - & 23 & 124/120 & 72/28 & 14 & 15 \\ p=60 & 8/8/26 & - & 23 & 124/120 & 72/28 & 14 & 15 \\ p=60 & 8/8/26 & - & 23 & 124/120 & 72/28 & 14 & 15 \\ p=180 & 10/9/24 & - & 21 & 175/170 & 163/29 & 12 & 16 \\ \hline \\ hsnr & p=60 & 1/1/0.84 & 0.85 & 0.84 & 0.56/0.56 & 0.86/0.87 & 0.92 & 0.89 \\ p=60 & 1/1/0.84 & 0.85 & 0.84 & 0.37/0.37 & 0.69/0.84 & 0.89 & 0.89 \\ p=180 & 1/1/0.84 & - & 0.84 & 0.37/0.37 & 0.69/0.84 & 0.89 & 0.88 \\ \hline \\ hsnr & p=60 & 1/1/0.84 & 0.85 & 0.84 & 0.37/0.37 & 0.69/0.84 & 0.89 & 0.88 \\ \hline \\ hsnr & p=60 & 1/1/0.84 & 0.85 & 0.84 & 0.37/0.37 & 0.69/0.84 & 0.89 & 0.88 \\ \hline \\ hsnr & p=60 & 1/1/0.84 & 0.85 & 0.84 & 0.37/0.37 & 0.57/0.82 & 0.89 & 0.88 \\ \hline \\ hsnr & p=60 & 1/1/0.84 & 0.85 & 0.84 & 0.37/0.37 & 0.57/0.82 & 0.89 & 0.88 \\ \hline \\ hsnr & p=60 & 1/1/0.85 & - & 0.83 & 0.45/0.46 & 0.73/0.83 & 0.89 & 0.88 \\ \hline \\ hsnr & p=60 & 1/1/0.85 & - & 0.84 & 0.37/0.37 & 0.57/0.82 & 0.89 & 0.88 \\ \hline \\ hsnr & p=60 & 1/1/0.85 & - & 0.88 & 0.48/0.49 & 0.63/0.84 & 0.95 & 0.93 \\ \hline \\ hsnr & p=60 & 1/1/0.85 & - & 0.88 & 0.48/0.49 & 0.63/0.84 & 0.95 & 0.93 \\ \hline \\ hsnr & p=60 & 1/1/0.85 & - & 0.88 & 0.48/0.49 & 0.63/0.84 & 0.95 & 0.93 \\ \hline \\ hsnr & p=60 & 1/1/0.85 & - & 0.88 & 0.48/0.49 & 0.63/0.84 & 0.95 & 0.93 \\ \hline \\ hsnr & p=60 & 1/1/0.85 & - & 0.88 & 0.48/0.49 & 0.63/0.84 & 0.95 & 0.93 \\ \hline \\ hsnr & p=60 & 6(0)/6(0)/6(0.5) & - & 6(0.5) & 6(18.1)/6(1.7.) & 6(0.2)/6(2.4) & 6(0.1) & 6(0.5) \\ \hline \\ hsnr & p=60 & 6(0)/6(0)/6(0.5) & - & 6(0.5) & 6(18.1)/6(1.7.) & 6(3.8)/6(2.1) & 6(0.5) \\ \hline \\ hsnr & p=60 & 6(0)/6(0)/6(0.5) & - & 6(0.5) & 6(18.1)/6(1.7.) & 6(3.8)/6(2.1) & 6(0.5) \\ \hline \\ hsnr & p=60 & 6(0)/6(0)/6(0.$ | | p=14 | 7/7/18 | 19 | 18 | 48/47 | 14/18 | 13 | 15 |
| $\begin{array}{ c c c c c c c c c c c c c c c c c c c$ | ١, | p=30 | 4/3/23 | 22 | 23 | 86/83 | 20/18 | 12 | 16 |
| $\begin{array}{ c c c c c c c c c c c c c c c c c c c$ | hsnr | p=60 | | - | 23 | | | 14 | 15 |
| $\begin{array}{ c c c c c c c c c c c c c c c c c c c$ | | p=180 | 1/1/21 | - | 21 | 174/171 | 46/20 | 14 | 15 |
| $\begin{array}{ c c c c c c c c c c c c c c c c c c c$ | | p=14 | 7/7/18 | | | 49/48 | 16/19 | | 14 |
| $\begin{array}{ c c c c c c c c c c c c c c c c c c c$ | | p=30 | | 22 | 23 | 85/83 | 25/20 | 12 | 16 |
| $\begin{array}{ c c c c c c c c c c c c c c c c c c c$ | msnr | p=60 | 2/2/23 | - | 23 | 125/120 | 39/22 | 14 | 15 |
| $\begin{array}{ c c c c c c c c c c c c c c c c c c c$ | | p=180 | 1/1/21 | - | 21 | 174/171 | 77/23 | 13 | 15 |
| $ \begin{array}{ c c c c c c c c c c c c c c c c c c c$ | | p=14 | 12/12/23 | 19 | 18 | 50/48 | 21/23 | 13 | 14 |
| $\begin{array}{ c c c c c c c c c c c c c c c c c c c$ | ١, | p=30 | 9/8/27 | 22 | 23 | 85/83 | 40/25 | | 16 |
| $\begin{array}{ c c c c c c c }\hline & & & & & & & & & & & & & & & & & & &$ | Isnr | p=60 | 8/8/26 | - | 23 | 124/120 | 72/28 | 14 | 15 |
| $\begin{array}{ c c c c c c c c } & p=14 & 1/1/0.91 & 0.9 & 0.91 & 0.72/0.72 & 0.94/0.91 & 0.94 & 0.93 \\ p=30 & 1/1/0.84 & 0.85 & 0.84 & 0.56/0.56 & 0.86/0.87 & 0.92 & 0.89 \\ p=60 & 1/1/0.83 & - & 0.83 & 0.45/0.46 & 0.79/0.85 & 0.89 & 0.89 \\ p=180 & 1/1/0.84 & - & 0.84 & 0.37/0.37 & 0.69/0.84 & 0.89 & 0.88 \\ \hline & p=180 & 1/1/0.84 & - & 0.84 & 0.37/0.37 & 0.69/0.84 & 0.89 & 0.88 \\ \hline & p=30 & 1/1/0.84 & 0.85 & 0.84 & 0.56/0.56 & 0.83/0.86 & 0.92 & 0.89 \\ p=60 & 1/1/0.83 & - & 0.83 & 0.45/0.46 & 0.73/0.83 & 0.89 & 0.88 \\ \hline & p=180 & 1/1/0.84 & - & 0.84 & 0.37/0.37 & 0.57/0.82 & 0.89 & 0.88 \\ \hline & p=180 & 1/1/0.84 & - & 0.84 & 0.37/0.37 & 0.57/0.82 & 0.89 & 0.88 \\ \hline & p=180 & 1/1/0.84 & - & 0.84 & 0.37/0.37 & 0.57/0.82 & 0.89 & 0.88 \\ \hline & p=180 & 1/1/0.85 & 0.89 & 0.88 & 0.58/0.59 & 0.77/0.87 & 0.96 & 0.93 \\ \hline & p=30 & 1/1/0.85 & 0.89 & 0.88 & 0.48/0.49 & 0.63/0.84 & 0.95 & 0.93 \\ \hline & p=60 & 1/1/0.85 & - & 0.88 & 0.48/0.49 & 0.63/0.84 & 0.95 & 0.93 \\ \hline & p=180 & 0.99/1/0.88 & - & 0.9 & 0.4/0.4 & 0.41/0.85 & 0.97 & 0.94 \\ \hline & & & & & & & & & & & & & & & & & &$ | | p=180 | 10/9/24 | - | 21 | 175/170 | 163/29 | 12 | 16 |
| $\begin{array}{ c c c c c c c c c c c c c c c c c c c$ | | | | | | Relative efficiency | 7 | | |
| $ \begin{array}{ c c c c c c c c } \hline hsnr & p=60 & 1/1/0.83 & - & 0.83 & 0.45/0.46 & 0.79/0.85 & 0.89 & 0.89 \\ p=180 & 1/1/0.84 & - & 0.84 & 0.37/0.37 & 0.69/0.84 & 0.89 & 0.88 \\ \hline & p=14 & 1/1/0.91 & 0.9 & 0.91 & 0.72/0.72 & 0.92/0.89 & 0.94 & 0.93 \\ p=30 & 1/1/0.84 & 0.85 & 0.84 & 0.56/0.56 & 0.83/0.86 & 0.92 & 0.89 \\ p=60 & 1/1/0.83 & - & 0.83 & 0.45/0.46 & 0.73/0.83 & 0.89 & 0.88 \\ p=180 & 1/1/0.84 & - & 0.84 & 0.37/0.37 & 0.57/0.82 & 0.89 & 0.88 \\ \hline \\ & & p=180 & 1/1/0.84 & - & 0.84 & 0.37/0.37 & 0.57/0.82 & 0.89 & 0.88 \\ \hline \\ & & & p=30 & 1/1/0.85 & 0.89 & 0.88 & 0.58/0.59 & 0.77/0.87 & 0.96 & 0.93 \\ p=30 & 1/1/0.85 & - & 0.88 & 0.48/0.49 & 0.63/0.84 & 0.95 & 0.93 \\ p=180 & 0.99/1/0.88 & - & 0.9 & 0.4/0.4 & 0.41/0.85 & 0.97 & 0.94 \\ \hline \\ & & & & & & & & & & & & & & & & &$ | | p=14 | 1/1/0.91 | 0.9 | 0.91 | 0.72/0.72 | 0.94/0.91 | 0.94 | 0.93 |
| $\begin{array}{ c c c c c c c c } \hline & p=00 & 1/1/0.85 & - & 0.85 & 0.45/0.46 & 0.79/0.85 & 0.89 & 0.88 \\ \hline & p=180 & 1/1/0.84 & - & 0.84 & 0.37/0.37 & 0.69/0.84 & 0.89 & 0.88 \\ \hline & p=14 & 1/1/0.91 & 0.9 & 0.91 & 0.72/0.72 & 0.92/0.89 & 0.94 & 0.93 \\ \hline & p=30 & 1/1/0.84 & 0.85 & 0.84 & 0.56/0.56 & 0.83/0.86 & 0.92 & 0.89 \\ \hline & p=60 & 1/1/0.83 & - & 0.83 & 0.45/0.46 & 0.73/0.83 & 0.89 & 0.88 \\ \hline & p=180 & 1/1/0.84 & - & 0.84 & 0.37/0.37 & 0.57/0.82 & 0.89 & 0.88 \\ \hline & p=180 & 1/1/0.85 & 0.89 & 0.88 & 0.58/0.59 & 0.77/0.87 & 0.96 & 0.93 \\ \hline & lsnr & p=60 & 1/1/0.85 & - & 0.88 & 0.48/0.49 & 0.63/0.84 & 0.95 & 0.93 \\ \hline & p=180 & 0.99/1/0.88 & - & 0.9 & 0.4/0.4 & 0.41/0.85 & 0.97 & 0.94 \\ \hline & & & & & & & & & & & & & & & & & &$ | _ | p=30 | 1/1/0.84 | 0.85 | 0.84 | 0.56/0.56 | 0.86/0.87 | 0.92 | 0.89 |
| $\begin{array}{ c c c c c c c } & p=14 & 1/1/0.91 & 0.9 & 0.91 & 0.72/0.72 & 0.92/0.89 & 0.94 & 0.93 \\ p=30 & 1/1/0.84 & 0.85 & 0.84 & 0.56/0.56 & 0.83/0.86 & 0.92 & 0.89 \\ p=60 & 1/1/0.83 & - & 0.83 & 0.45/0.46 & 0.73/0.83 & 0.89 & 0.88 \\ p=180 & 1/1/0.84 & - & 0.84 & 0.37/0.37 & 0.57/0.82 & 0.89 & 0.88 \\ \hline & p=180 & 1/1/0.85 & 0.89 & 0.88 & 0.58/0.59 & 0.77/0.87 & 0.96 & 0.93 \\ lsnr & p=30 & 1/1/0.85 & 0.89 & 0.88 & 0.58/0.59 & 0.77/0.87 & 0.96 & 0.93 \\ p=180 & 0.99/1/0.85 & - & 0.88 & 0.48/0.49 & 0.63/0.84 & 0.95 & 0.93 \\ p=180 & 0.99/1/0.88 & - & 0.9 & 0.4/0.4 & 0.41/0.85 & 0.97 & 0.94 \\ \hline & & & & & & & & & & & & & & & & & &$ | hsnr | p=60 | 1/1/0.83 | - | 0.83 | 0.45/0.46 | 0.79/0.85 | 0.89 | 0.89 |
| $\begin{array}{ c c c c c c c c c c c c c c c c c c c$ | | p=180 | 1/1/0.84 | - | 0.84 | 0.37/0.37 | 0.69/0.84 | 0.89 | 0.88 |
| $\begin{array}{ c c c c c c c c c c c c c c c c c c c$ | | p=14 | 1/1/0.91 | 0.9 | 0.91 | 0.72/0.72 | 0.92/0.89 | 0.94 | 0.93 |
| $\begin{array}{ c c c c c c c c c c c c c c c c c c c$ | | p=30 | 1/1/0.84 | 0.85 | 0.84 | 0.56/0.56 | 0.83/0.86 | 0.92 | 0.89 |
| $ \begin{vmatrix} p=14 & 1/1/0.91 & 0.94 & 0.95 & 0.75/0.76 & 0.92/0.91 & 0.99 & 0.98 \\ p=30 & 1/1/0.85 & 0.89 & 0.88 & 0.58/0.59 & 0.77/0.87 & 0.96 & 0.93 \\ p=60 & 1/1/0.85 & - & 0.88 & 0.48/0.49 & 0.63/0.84 & 0.95 & 0.93 \\ p=180 & 0.99/1/0.88 & - & 0.9 & 0.4/0.4 & 0.41/0.85 & 0.97 & 0.94 \\ \hline \\ $ | msnr | p=60 | 1/1/0.83 | - | 0.83 | 0.45/0.46 | 0.73/0.83 | 0.89 | 0.88 |
| $ \begin{vmatrix} p = 30 & 1/1/0.85 & 0.89 & 0.88 & 0.58/0.59 & 0.77/0.87 & 0.96 & 0.93 \\ p = 60 & 1/1/0.85 & - & 0.88 & 0.48/0.49 & 0.63/0.84 & 0.95 & 0.93 \\ p = 180 & 0.99/1/0.88 & - & 0.9 & 0.4/0.4 & 0.41/0.85 & 0.97 & 0.94 \\ \hline \\ & & & & & & & & & & & & & & & & $ | | p=180 | 1/1/0.84 | - | 0.84 | 0.37/0.37 | 0.57/0.82 | 0.89 | 0.88 |
| $ \begin{array}{ c c c c c c c c c c c c c c c c c c c$ | | p=14 | 1/1/0.91 | 0.94 | 0.95 | 0.75/0.76 | 0.92/0.91 | 0.99 | 0.98 |
| $\begin{array}{ c c c c c c c c c c c c c c c c c c c$ | ١, | p=30 | 1/1/0.85 | 0.89 | 0.88 | 0.58/0.59 | 0.77/0.87 | 0.96 | 0.93 |
| $ \begin{array}{ c c c c c c c c c } \hline & Sparsistency (number of extra variables) \\ \hline & p=14 & 6(0.3)/6(0.3)/6(0.6) & 6(0.7) & 6(0.6) & 6(4.7)/6(5.5) & 6(1)/6(1.4) & 6(0.7) & 6(0.5) \\ p=30 & 6(0.1)/6(0.1)/6(0.6) & 6(0.6) & 6(0.6) & 6(10.9)/6(11.3) & 6(2.1)/6(1.9) & 6(0.9) & 6(0.5) \\ p=60 & 6(0)/6(0)/6(0.5) & - & 6(0.5) & 6(18.1)/6(17.7) & 6(3.8)/6(2.1) & 6(1.4) & 6(0.4) \\ p=180 & 6(0)/6(0)/6(0.3) & - & 6(0.3) & 6(32.2)/6(29.7) & 6(9.2)/6(2.4) & 6(2.1) & 6(0.3) \\ \hline & p=14 & 6(0.3)/6(0.3)/6(0.6) & 6(0.7) & 6(0.6) & 6(4.8)/6(5.5) & 6(1)/6(1.5) & 6(0.6) & 6(0.5) \\ p=30 & 6(0.1)/6(0.1)/6(0.6) & 6(0.6) & 6(0.6) & 6(11)/6(11.3) & 6(2.3)/6(1.7) & 6(0.9) & 6(0.5) \\ \hline & msnr & p=60 & 6(0)/6(0)/6(0.5) & - & 6(0.5) & 6(18.1)/6(17.7) & 6(4.6)/6(1.8) & 6(1.4) & 6(0.4) \\ \hline \end{array}$ | Isnr | p=60 | 1/1/0.85 | - | 0.88 | 0.48/0.49 | 0.63/0.84 | 0.95 | 0.93 |
| $\begin{array}{ c c c c c c c c c c c c c c c c c c c$ | | p=180 | 0.99/1/0.88 | - | 0.9 | 0.4/0.4 | 0.41/0.85 | 0.97 | 0.94 |
| $\begin{array}{ c c c c c c c c c c c c c c c c c c c$ | | | | Sı | parsisten | cy (number of exti | ra variables) | | |
| $ \begin{array}{ c c c c c c c c c c c c c c c c c c c$ | | p=14 | 6(0.3)/6(0.3)/6(0.6) | 6(0.7) | 6(0.6) | 6(4.7)/6(5.5) | 6(1)/6(1.4) | 6(0.7) | 6(0.5) |
| $\begin{array}{ c c c c c c c c c c c c c c c c c c c$ | , | p=30 | 6(0.1)/6(0.1)/6(0.6) | 6(0.6) | 6(0.6) | 6(10.9)/6(11.3) | 6(2.1)/6(1.9) | 6(0.9) | 6(0.5) |
| $ \begin{array}{ c c c c c c c c c c c c c c c c c c c$ | hsnr | p=60 | 6(0)/6(0)/6(0.5) | - | 6(0.5) | 6(18.1)/6(17.7) | 6(3.8)/6(2.1) | 6(1.4) | 6(0.4) |
| $ \begin{array}{ c c c c c c c c c c c c c c c c c c c$ | | p=180 | 6(0)/6(0)/6(0.3) | - | 6(0.3) | 6(32.2)/6(29.7) | 6(9.2)/6(2.4) | 6(2.1) | 6(0.3) |
| $ \begin{array}{ c c c c c c c c c c c c c c c c c c c$ | | p=14 | 6(0.3)/6(0.3)/6(0.6) | 6(0.7) | 6(0.6) | 6(4.8)/6(5.5) | 6(1)/6(1.5) | 6(0.6) | 6(0.5) |
| $ \begin{array}{c ccccccccccccccccccccccccccccccccccc$ | | p=30 | 6(0.1)/6(0.1)/6(0.6) | 6(0.6) | 6(0.6) | 6(11)/6(11.3) | 6(2.3)/6(1.7) | 6(0.9) | 6(0.5) |
| | msnr | p=60 | 6(0)/6(0)/6(0.5) | - | | 6(18.1)/6(17.7) | 6(4.6)/6(1.8) | 6(1.4) | 6(0.4) |
| p-100 0(0)/0(0)/0(0.3) - 0(0.3) 0(32.3)/0(29.1) 0(13.4)/0(1.8) 0(2) 0(0.3) | | p=180 | 6(0)/6(0)/6(0.3) | - | 6(0.3) | 6(32.3)/6(29.7) | 6(13.4)/6(1.8) | $\hat{6}(2)$ | 6(0.3) |
| | | p=14 | 6(0.6)/6(0.5)/6(0.6) | 6(0.7) | 6(0.6) | 6(4.8)/6(5.5) | 6(1.1)/6(1.5) | 6(0.6) | 6(0.5) |
| | | p=30 | | | | | | | 6(0.5) |
| $\begin{array}{c ccccccccccccccccccccccccccccccccccc$ | lsnr | p=60 | | . , | 6(0.5) | | | | . , |
| p=180 6(0.1)/6(0.1)/6(0.3) - 6(0.3) - 6(32.5)/6(29.7) - 6(21.7)/6(1.1) - 6(1.2) - 6(0.4) | | p=180 | 6(0.1)/6(0.1)/6(0.3) | - | 6(0.3) | 6(32.5)/6(29.7) | 6(21.7)/6(1.1) | 6(1.2) | 6(0.4) |

Table S17: The performance of BOSS compared to other methods, Sparse-Ex2, ρ =0.9, n=200

| | | BOSS C_n -hdf/AICc-hdf/CV | BS CV | FS CV | LASSO AICc/CV | Gamma LASSO AICc/CV | SparseNet CV | rLASSO CV |
|---------|-------|-------------------------------|----------|--------------|---------------------|------------------------|-----------------|--------------|
| | | | | | the best possible B | | | |
| | p=14 | 18/15/25 | 17 | 23 | 53/51 | 20/27 | 14 | 18 |
| | p=30 | 12/9/42 | 9 | 53 | 91/89 | 18/18 | 1 | 40 |
| hsnr | p=60 | 9/6/49 | - | 69 | 131/126 | 16/12 | -6 | 48 |
| | p=180 | 22/5/75 | - | 111 | 138/120 | -7/-16 | -30 | 42 |
| | p=14 | 25/23/29 | 3 | 24 | 35/34 | 10/16 | 3 | 21 |
| | p=30 | 23/20/31 | -15 | 36 | 50/48 | -1/2 | -17 | 34 |
| msnr | p=60 | 21/18/30 | - | 48 | 65/61 | -7/-7 | -26 | 46 |
| | p=180 | 23/22/20 | - | 64 | 48/35 | -16/-1 | -24 | 32 |
| | p=14 | 40/41/31 | 32 | 50 | 41/40 | 38/39 | 39 | 43 |
| lomm | p=30 | 42/42/28 | 28 | 61 | 53/53 | 44/51 | 46 | 56 |
| lsnr | p=60 | 36/35/25 | - | 50 | 45/45 | 52/47 | 45 | 48 |
| | p=180 | 25/9/11 | - | 15 | 10/11 | 59/12 | 12 | 13 |
| | | | | Rela | ative efficiency | | | |
| | p=14 | 0.97/0.99/0.91 | 0.97 | 0.93 | 0.75/0.75 | 0.95/0.89 | 1 | 0.97 |
| hsnr | p=30 | 0.9/0.92/0.71 | 0.93 | 0.66 | 0.53/0.53 | 0.86/0.85 | 1 | 0.72 |
| nsnr | p=60 | 0.87/0.89/0.63 | - | 0.56 | 0.41/0.42 | 0.81/0.84 | 1 | 0.64 |
| | p=180 | 0.58/0.67/0.4 | - | 0.33 | 0.3/0.32 | 0.76/0.84 | 1 | 0.49 |
| | p=14 | 0.82/0.83/0.79 | 0.99 | 0.83 | 0.76/0.77 | 0.94/0.88 | 1 | 0.85 |
| | p=30 | 0.68/0.69/0.63 | 0.98 | 0.61 | 0.55/0.56 | 0.84/0.82 | 1 | 0.62 |
| msnr | p=60 | 0.61/0.62/0.57 | - | 0.5 | 0.45/0.46 | 0.79/0.79 | 1 | 0.51 |
| | p=180 | 0.62/0.62/0.63 | - | 0.46 | 0.51/0.56 | 0.9/0.76 | 1 | 0.57 |
| | p=14 | 0.94/0.93/1 | 0.99 | 0.87 | 0.92/0.93 | 0.95/0.94 | 0.94 | 0.92 |
| lsnr | p=30 | 0.9/0.9/1 | 1 | 0.8 | 0.83/0.84 | 0.89/0.85 | 0.88 | 0.82 |
| 15111 | p=60 | 0.92/0.93/1 | - | 0.83 | 0.86/0.86 | 0.83/0.85 | 0.87 | 0.85 |
| | p=180 | 0.87/1/0.98 | - | 0.95 | 0.98/0.98 | 0.68/0.97 | 0.97 | 0.96 |
| | | | Spa | rsistency (r | umber of extra vari | ables) | | |
| | p=14 | 6(0.9)/6(0.7)/6(0.7) | 6(0.6) | 6(1) | 6(6.5)/6(7.2) | 6(1.3)/6(2.2) | 6(0.7) | 6(0.8) |
| hsnr | p=30 | 6(1.1)/6(0.9)/6(2.5) | 6(0.7) | 6(3.7) | 6(18.3)/6(19.9) | 6(2.9)/6(2.5) | 6(1.1) | 6(5.7) |
| nsnr | p=60 | 6(1.7)/6(1.6)/6(3.3) | - | 6(4.9) | 6(31.8)/6(36.4) | 6(4.2)/6(2.7) | 6(1.8) | 6(7.5) |
| | p=180 | 6(14.9)/6(6.8)/6(11.8) | - | 5.9(19.7) | 6(51.3)/6(76.1) | 6(8.6)/6(4.1) | 6(3.2) | 6(17.5) |
| | p=14 | 6(3)/6(2.7)/6(1.2) | 6(0.6) | 6(2.4) | 6(6.5)/6(7.2) | 6(1.5)/6(3) | 6(1.3) | 6(2.4) |
| msnr | p=30 | 6(5.1)/6(4)/6(3.5) | 6(0.7) | 6(7) | 6(18.2)/6(19.9) | 6(3.6)/6(5.3) | 6(3.4) | 6(9.8) |
| 1115111 | p=60 | 6(6.1)/6(4.7)/6(5.1) | - | 6(10.3) | 6(31.8)/6(36.3) | 6(6.5)/6(7.7) | 6(6) | 6(16.8) |
| | p=180 | 5.9(38.2)/5.5(14.8)/5.8(18.2) | - | 4.2(16.8) | 5.8(49.6)/6(75.8) | 6(23.5)/5.9(36.2) | 5.9(31.7) | 6(46.5) |
| | p=14 | 5.7(4.9)/5.6(4.6)/5.6(2.7) | 5.2(1.2) | 5.3(4) | 5.8(6.3)/5.8(6.9) | 5.4(3.7)/5.7(5.9) | 5.4(4.7) | 5.7(5.6) |
| lsnr | p=30 | 4(7.5)/2.9(4.4)/4.6(6.6) | 4.1(1.7) | 2.5(4.5) | 2.7(8.3)/2.8(9.2) | 4.4(9.7)/3.3(9.4) | 3.4(8.7) | 2.6(7.6) |
| ISIII | p=60 | 2.6(7.1)/1.4(2.5)/3.8(9.8) | - | 0.8(1.7) | 0.8(4.4)/0.9(5.7) | 3.7(16)/1.3(7.2) | 1.8(9.1) | 0.9(4.9) |
| | p=180 | 1.2(20.1)/0.3(0.5)/0.7(2.7) | - | 0.1(0.5) | 0.3(4.4)/0.3(4.6) | 2(35.8)/0.3(4.5) | 0.3(4.9) | 0.3(3.5) |

Table S18: The performance of BOSS compared to other methods, Sparse-Ex2, ρ =0.9, n=2000

| | | BOSS C _n -hdf/AICc-hdf/CV | BS CV | FS CV | LASSO AICc/CV | Gamma LASSO AICc/CV | SparseNet CV | rLASSO CV |
|----------|---------------|---|----------|-----------|---------------------|------------------------|-----------------|--------------|
| | | | | | than the best poss | | CV | CV |
| _ | p=14 | 7/7/18 | 19 | 18 | 56/55 | 22/28 | 14 | 15 |
| | p=30 | 4/3/23 | 22 | 23 | 118/116 | 29/29 | 14 | 17 |
| hsnr | p=60 | 2/2/23 | - | 23 | 186/182 | 37/33 | 15 | 15 |
| | p=00 p=180 | $\frac{2/2/23}{1/1/21}$ | _ | 21 | 299/294 | 51/41 | 15 | 13 |
| <u> </u> | p=14 | 8/8/18 | 19 | 18 | 56/55 | 23/29 | 14 | 14 |
| | p=30 | 4/4/24 | 22 | 23 | 118/115 | 31/30 | 13 | 17 |
| msnr | p=60 | 3/3/23 | _ | 23 | 185/182 | 42/36 | 16 | 15 |
| | p=180 | 3/3/22 | - | 21 | 298/293 | 61/43 | 14 | 13 |
| İ | p=14 | 36/36/42 | 15 | 19 | 52/50 | 22/30 | 12 | 23 |
| | p=30 | 37/36/43 | 12 | 32 | 100/97 | 28/26 | 7 | 40 |
| lsnr | p=60 | 39/38/47 | - | 47 | 141/138 | 35/22 | 1 | 61 |
| | p=180 | 38/38/37 | - | 72 | 178/175 | 45/16 | -12 | 100 |
| | | | | | Relative efficiency | У | | |
| | p=14 | 1/1/0.91 | 0.9 | 0.91 | 0.68/0.69 | 0.88/0.84 | 0.94 | 0.93 |
| | p=30 | 1/1/0.84 | 0.85 | 0.84 | 0.47/0.48 | 0.8/0.8 | 0.9 | 0.88 |
| hsnr | p=60 | 1/1/0.83 | - | 0.83 | 0.35/0.36 | 0.74/0.76 | 0.88 | 0.88 |
| | p=180 | 1/1/0.84 | - | 0.84 | 0.25/0.26 | 0.67/0.72 | 0.88 | 0.89 |
| | p=14 | 1/1/0.91 | 0.91 | 0.92 | 0.69/0.7 | 0.88/0.83 | 0.94 | 0.94 |
| | p=30 | 1/1/0.84 | 0.85 | 0.84 | 0.48/0.48 | 0.79/0.8 | 0.91 | 0.89 |
| msnr | p=60 | 1/1/0.84 | - | 0.84 | 0.36/0.36 | 0.72/0.76 | 0.88 | 0.9 |
| | p=180 | 1/1/0.84 | - | 0.85 | 0.26/0.26 | 0.64/0.72 | 0.9 | 0.91 |
| | p=14 | 0.83/0.83/0.79 | 0.98 | 0.94 | 0.74/0.75 | 0.92/0.87 | 1 | 0.91 |
| 1 | p=30 | 0.79/0.79/0.75 | 0.96 | 0.81 | 0.54/0.54 | 0.84/0.85 | 1 | 0.76 |
| lsnr | p=60 | 0.72/0.73/0.68 | - | 0.69 | 0.42/0.42 | 0.75/0.83 | 1 | 0.63 |
| | p=180 | 0.64/0.64/0.64 | - | 0.51 | 0.32/0.32 | 0.61/0.76 | 1 | 0.44 |
| | | | S_1 | parsisten | cy (number of extr | ra variables) | | |
| | p=14 | 6(0.3)/6(0.3)/6(0.6) | 6(0.7) | 6(0.6) | 6(6.6)/6(7.2) | 6(1.5)/6(2.1) | 6(0.7) | 6(0.5) |
| 1 | p=30 | 6(0.1)/6(0.1)/6(0.6) | 6(0.6) | 6(0.6) | 6(17.8)/6(18.9) | 6(2.7)/6(2.6) | 6(0.9) | 6(0.5) |
| hsnr | p=60 | 6(0)/6(0)/6(0.5) | - | 6(0.5) | 6(34.2)/6(35.3) | 6(4.5)/6(2.9) | 6(1.4) | 6(0.4) |
| | p=180 | 6(0)/6(0)/6(0.3) | - | 6(0.3) | 6(72.8)/6(73.6) | 6(8.7)/6(3.9) | 6(2.2) | 6(0.2) |
| | p=14 | 6(0.3)/6(0.3)/6(0.6) | 6(0.7) | 6(0.6) | 6(6.6)/6(7.2) | 6(1.5)/6(2.2) | 6(0.7) | 6(0.5) |
| | p=30 | 6(0.1)/6(0.1)/6(0.6) | 6(0.6) | 6(0.6) | 6(17.8)/6(18.8) | 6(2.8)/6(2.3) | 6(0.9) | 6(0.5) |
| msnr | p=60 | 6(0)/6(0)/6(0.5) | - | 6(0.5) | 6(34.2)/6(35.2) | 6(4.8)/6(2.6) | 6(1.4) | 6(0.4) |
| | p=180 | 6(0)/6(0)/6(0.3) | - | 6(0.3) | 6(72.8)/6(73.6) | 6(10.5)/6(3.3) | 6(2.1) | 6(0.2) |
| | p=14 | 6(2.7)/6(2.6)/6(0.6) | 6(0.7) | 6(0.9) | 6(6.6)/6(7.2) | 6(1.5)/6(2.5) | 6(0.8) | 6(1.3) |
| 1 | p=30 | 6(2.1)/6(2)/6(0.8) | 6(0.6) | 6(1.5) | 6(17.8)/6(18.8) | 6(3.2)/6(2.7) | 6(1.4) | 6(2.5) |
| lsnr | p=60 | 6(1)/6(0.9)/6(0.9) | - | 6(2.2) | 6(34.2)/6(35.1) | 6(6.3)/6(3.7) | 6(2.6) | 6(3.9) |
| | p=180 | 6(1.4)/6(1.4)/6(1.8) | - | 6(4.6) | 6(72.3)/6(73.5) | 6(17.1)/6(8.4) | 6(7.1) | 6(10.4) |

Table S19: The performance of BOSS compared to other methods, Sparse-Ex3, ρ =0, n=200

| | | BOSS C_n -hdf/AICc-hdf/CV | BS CV | FS CV | $\begin{array}{c} {\rm LASSO} \\ {\rm AICc/CV} \end{array}$ | Gamma LASSO AICc/CV | SparseNet CV | rLASSO CV |
|-------|-------|-----------------------------|----------|------------|---|------------------------|-----------------|--------------|
| | | | | | an the best possible I | , | | |
| | p=14 | 8/6/20 | 21 | 20 | 44/43 | 17/20 | 15 | 16 |
| | p=30 | 5/3/24 | 25 | 25 | 69/67 | 32/23 | 15 | 19 |
| hsnr | p=60 | 4/2/21 | - | 23 | 97/96 | 52/24 | 16 | 19 |
| | p=180 | 34/1/19 | - | 21 | 133/133 | 137/28 | 19 | 16 |
| | p=14 | 17/14/20 | 21 | 20 | 44/43 | 24/24 | 16 | 17 |
| | p=30 | 18/13/24 | 25 | 25 | 69/67 | 48/27 | 16 | 21 |
| msnr | p=60 | 14/9/21 | - | 23 | 97/95 | 84/29 | 16 | 22 |
| | p=180 | 50/11/20 | - | 22 | 132/133 | 224/33 | 19 | 29 |
| | p=14 | 22/23/26 | 26 | 26 | 8/8 | 13/15 | 17 | 15 |
| , | p=30 | 29/32/26 | 26 | 25 | 1/1 | 14/8 | 8 | 6 |
| lsnr | p=60 | 27/29/22 | - | 22 | 0/1 | 24/6 | 6 | 6 |
| | p=180 | 30/16/14 | - | 14 | -2/1 | 84/4 | 3 | 4 |
| | | | | R | telative efficiency | | | |
| | p=14 | 0.98/1/0.89 | 0.88 | 0.89 | 0.74/0.75 | 0.91/0.88 | 0.93 | 0.91 |
| 1 | p=30 | 0.98/1/0.83 | 0.82 | 0.82 | 0.61/0.61 | 0.78/0.84 | 0.89 | 0.86 |
| hsnr | p=60 | 0.99/1/0.85 | - | 0.83 | 0.52/0.52 | 0.67/0.83 | 0.88 | 0.86 |
| | p=180 | 0.75/1/0.85 | - | 0.84 | 0.43/0.43 | 0.43/0.79 | 0.85 | 0.87 |
| | p=14 | 0.98/1/0.95 | 0.95 | 0.96 | 0.8/0.8 | 0.92/0.92 | 0.99 | 0.98 |
| | p=30 | 0.96/1/0.92 | 0.91 | 0.91 | 0.67/0.68 | 0.76/0.89 | 0.98 | 0.94 |
| msnr | p=60 | 0.96/1/0.9 | - | 0.89 | 0.56/0.56 | 0.59/0.85 | 0.94 | 0.9 |
| | p=180 | 0.74/1/0.92 | - | 0.91 | 0.48/0.47 | 0.34/0.83 | 0.93 | 0.86 |
| | p=14 | 0.89/0.88/0.86 | 0.86 | 0.86 | 1/1 | 0.95/0.94 | 0.92 | 0.94 |
| lsnr | p=30 | 0.78/0.76/0.8 | 0.8 | 0.81 | 1/1 | 0.88/0.93 | 0.93 | 0.95 |
| ISIII | p=60 | 0.79/0.78/0.82 | - | 0.82 | 1/1 | 0.81/0.95 | 0.94 | 0.95 |
| | p=180 | 0.76/0.85/0.86 | - | 0.86 | 1/0.98 | 0.53/0.94 | 0.95 | 0.95 |
| | | | Sp | arsistency | (number of extra var | iables) | | |
| | p=14 | 6(0.3)/6(0.2)/6(0.6) | 6(0.7) | 6(0.6) | 6(3.7)/6(4.5) | 6(1)/6(1.3) | 6(0.6) | 6(0.6) |
| hsnr | p=30 | 6(0.1)/6(0)/6(0.6) | 6(0.7) | 6(0.7) | 6(7.4)/6(8.2) | 6(2.4)/6(1.7) | 6(1) | 6(0.7) |
| nsnr | p=60 | 6(0.1)/6(0)/6(0.5) | - | 6(0.5) | 6(11.3)/6(13.1) | 6(4.8)/6(1.7) | 6(1.5) | 6(0.7) |
| | p=180 | 6(8.8)/6(0)/6(0.4) | - | 6(0.4) | 6(16.5)/6(22.7) | 6(18)/6(2.5) | 6(2.7) | 6(0.6) |
| | p=14 | 6(0.8)/6(0.6)/6(0.6) | 6(0.7) | 6(0.6) | 6(3.7)/6(4.5) | 6(1.2)/6(1.4) | 6(0.6) | 6(0.6) |
| msnr | p=30 | 6(0.5)/6(0.3)/6(0.6) | 6(0.7) | 6(0.7) | 6(7.4)/6(8.2) | 6(2.9)/6(1.6) | 6(0.8) | 6(0.8) |
| msm | p=60 | 6(0.3)/6(0.1)/6(0.5) | - | 6(0.5) | 6(11.4)/6(13.1) | 6(6.4)/6(1.5) | 6(1.1) | 6(0.9) |
| | p=180 | 6(9.4)/6(0.1)/6(0.4) | - | 6(0.4) | 6(16.5)/6(22.8) | 6(27.4)/6(2) | 6(1.7) | 6(1.1) |
| | p=14 | 5.4(4.4)/5.2(4.1)/4.7(1.8) | 4.7(1.7) | 4.7(1.7) | 5.6(3.3)/5.6(4) | 5.1(1.5)/5.3(3) | 5.1(2.8) | 5(2.1) |
| lsnr | p=30 | 4(4.4)/3.1(1.9)/3.7(2.1) | 3.6(2.1) | 3.7(2) | 5.3(6.4)/5.4(7) | 4.9(3.8)/4.8(4.9) | 4.8(5.3) | 4.6(3.6 |
| 18111 | p=60 | 2.2(1.8)/1.2(0.2)/2.6(1.4) | - | 2.6(1.3) | 4.6(8.6)/4.6(9.6) | 4.9(8.5)/4.1(6.6) | 4.2(7.2) | 3.9(5.5 |
| | p=180 | 1.6(14.2)/0.5(0.1)/1.3(0.6) | - | 1.3(0.6) | 3.4(10.4)/3.5(13.1) | 4.6(36.9)/3(9) | 3.2(10.5) | 2.9(7.7) |

Table S20: The performance of BOSS compared to other methods, Sparse-Ex3, ρ =0, n=2000

| | | | BOSS | BS | FS | LASSO | Gamma LASSO | SparseNet | rLASSO |
|--|------|-------|------------------------|---------|-----------|---------------------|----------------|-----------|--------|
| $ \begin{array}{c ccccccccccccccccccccccccccccccccccc$ | | | C_p -hdf/AICc-hdf/CV | CV | CV | AICc/CV | AICc/CV | CV | CV |
| $\begin{array}{ c c c c c c c c c c c c c c c c c c c$ | | | | | % worse | than the best poss | sible BOSS | | |
| $\begin{array}{c ccccccccccccccccccccccccccccccccccc$ | | p=14 | 6/6/17 | 17 | 17 | 41/41 | 12/15 | 11 | 13 |
| $\begin{array}{ c c c c c c c c c c c c c c c c c c c$ | | p=30 | 3/3/22 | 22 | 23 | 72/69 | 20/18 | 13 | 16 |
| $\begin{array}{ c c c c c c c c c c c c c c c c c c c$ | hsnr | p=60 | 2/2/24 | - | 23 | 97/93 | 29/19 | 14 | 17 |
| $\begin{array}{ c c c c c c c c c c c c c c c c c c c$ | | p=180 | 1/1/21 | - | 21 | 132/129 | 53/19 | 13 | 17 |
| $\begin{array}{ c c c c c c c c c c c c c c c c c c c$ | | p=14 | 6/6/17 | | | 41/41 | 14/17 | 11 | 13 |
| $\begin{array}{c ccccccccccccccccccccccccccccccccccc$ | | p=30 | 3/3/22 | 22 | 23 | 72/69 | 26/20 | 13 | 17 |
| $ \begin{array}{ c c c c c c c c c c c c c c c c c c c$ | msnr | p=60 | 2/2/24 | - | 23 | 97/93 | 43/21 | 14 | 18 |
| $\begin{array}{ c c c c c c c c c c c c c c c c c c c$ | | p=180 | 1/1/21 | - | 21 | 132/129 | 97/22 | 13 | 17 |
| $\begin{array}{ c c c c c c c c c c c c c c c c c c c$ | | p=14 | 9/9/17 | | 17 | 42/41 | | 12 | 13 |
| $\begin{array}{ c c c c c c c c c c c c c c c c c c c$ | ١, | p=30 | 5/5/22 | 22 | 23 | 72/69 | 45/25 | 13 | 16 |
| $\begin{array}{ c c c c c c }\hline & & & & & & & & & & & & & & & & & & &$ | Isnr | p=60 | 5/4/24 | - | 23 | 97/93 | 82/26 | 15 | 18 |
| $\begin{array}{ c c c c c c c } & p=14 & 1/1/0.91 & 0.91 & 0.91 & 0.76/0.76 & 0.95/0.93 & 0.96 & 0.94 \\ p=30 & 1/1/0.84 & 0.84 & 0.84 & 0.6/0.61 & 0.86/0.87 & 0.91 & 0.88 \\ p=60 & 1/1/0.83 & - & 0.83 & 0.52/0.53 & 0.79/0.86 & 0.89 & 0.87 \\ p=180 & 1/1/0.83 & - & 0.84 & 0.44/0.44 & 0.66/0.85 & 0.89 & 0.86 \\ \hline \\ p=14 & 1/1/0.91 & 0.91 & 0.91 & 0.75/0.75 & 0.93/0.91 & 0.96 & 0.94 \\ p=30 & 1/1/0.84 & 0.84 & 0.84 & 0.6/0.61 & 0.81/0.86 & 0.91 & 0.88 \\ p=60 & 1/1/0.83 & - & 0.83 & 0.52/0.53 & 0.71/0.84 & 0.89 & 0.87 \\ p=180 & 1/1/0.83 & - & 0.83 & 0.52/0.53 & 0.71/0.84 & 0.89 & 0.87 \\ p=180 & 1/1/0.83 & - & 0.84 & 0.44/0.44 & 0.51/0.83 & 0.89 & 0.86 \\ \hline \\ p=14 & 1/1/0.93 & 0.93 & 0.93 & 0.77/0.77 & 0.9/0.9 & 0.97 & 0.96 \\ p=30 & 0.99/1/0.86 & 0.86 & 0.85 & 0.61/0.62 & 0.72/0.84 & 0.93 & 0.9 \\ p=60 & 1/1/0.84 & - & 0.85 & 0.53/0.54 & 0.57/0.83 & 0.91 & 0.89 \\ p=180 & 0.99/1/0.86 & - & 0.86 & 0.45/0.46 & 0.36/0.82 & 0.92 & 0.89 \\ \hline \\ bsnr & p=60 & 1/1/0.84 & - & 0.85 & 0.53/0.54 & 0.57/0.83 & 0.91 & 0.89 \\ p=180 & 0.99/1/0.86 & - & 0.86 & 0.45/0.46 & 0.36/0.82 & 0.92 & 0.89 \\ \hline \\ bsnr & p=60 & 6(0.1)/6(0.1)/6(0.6) & 6(0.6) & 6(0.6) & 6(3.8)/6(4.5) & 6(0.9)/6(1.3) & 6(0.6) & 6(0.5) \\ p=20 & 6(0.1)/6(0.1)/6(0.6) & 6(0.6) & 6(0.6) & 6(3.3)/6(8.5) & 6(2)/6(1.8) & 6(0.9) & 6(0.5) \\ p=180 & 6(0)/6(0)/6(0.5) & - & 6(0.5) & 6(13)/6(12.2) & 6(3.9)/6(2.1) & 6(1.5) & 6(0.5) \\ p=180 & 6(0)/6(0)/6(0.3) & - & 6(0.5) & 6(13)/6(12.2) & 6(3.9)/6(1.8) & 6(0.9) & 6(0.5) \\ p=180 & 6(0)/6(0)/6(0.3) & - & 6(0.5) & 6(13)/6(12.2) & 6(4.8)/6(1.8) & 6(1.4) & 6(0.6) \\ p=180 & 6(0)/6(0)/6(0.3) & - & 6(0.5) & 6(13)/6(12.2) & 6(4.8)/6(1.8) & 6(1.4) & 6(0.6) \\ p=180 & 6(0)/6(0)/6(0.3) & - & 6(0.5) & 6(13)/6(12.2) & 6(4.8)/6(1.8) & 6(1.4) & 6(0.5) \\ p=30 & 6(0.1)/6(0.1)/6(0.6) & 6(0.6) & 6(0.6) & 6(3.3)/6(8.5) & 6(2.2)/6(1.8) & 6(0.5) & 6(0.5) \\ p=180 & 6(0)/6(0)/6(0.3) & - & 6(0.5) & 6(13)/6(12.2) & 6(4.8)/6(1.8) & 6(1.4) & 6(0.5) \\ p=30 & 6(0.1)/6(0.1)/6(0.6) & 6(0.6) & 6(0.6) & 6(3.3)/6(8.5) & 6(3)/6(1.6) & 6(0.5) & 6(0.5) \\ p=30 & 6(0.1)/6(0.1)/6(0.5) & - &$ | | p=180 | 5/4/21 | - | 21 | 132/129 | 192/26 | 13 | 17 |
| $\begin{array}{ c c c c c c } & p=30 & 1/1/0.84 & 0.84 & 0.84 & 0.6/0.61 & 0.86/0.87 & 0.91 & 0.88 \\ p=60 & 1/1/0.83 & - & 0.83 & 0.52/0.53 & 0.79/0.86 & 0.89 & 0.87 \\ p=180 & 1/1/0.83 & - & 0.84 & 0.44/0.44 & 0.66/0.85 & 0.89 & 0.86 \\ \hline & p=14 & 1/1/0.91 & 0.91 & 0.91 & 0.75/0.75 & 0.93/0.91 & 0.96 & 0.94 \\ p=30 & 1/1/0.84 & 0.84 & 0.84 & 0.6/0.61 & 0.81/0.86 & 0.91 & 0.88 \\ p=60 & 1/1/0.83 & - & 0.83 & 0.52/0.53 & 0.71/0.84 & 0.89 & 0.87 \\ p=180 & 1/1/0.83 & - & 0.84 & 0.44/0.44 & 0.51/0.83 & 0.89 & 0.86 \\ \hline & p=14 & 1/1/0.93 & 0.93 & 0.93 & 0.77/0.77 & 0.9/0.9 & 0.97 & 0.96 \\ p=30 & 0.99/1/0.86 & 0.86 & 0.85 & 0.61/0.62 & 0.72/0.84 & 0.93 & 0.9 \\ p=60 & 1/1/0.84 & - & 0.85 & 0.63/0.54 & 0.57/0.83 & 0.91 & 0.89 \\ p=180 & 0.99/1/0.86 & - & 0.86 & 0.45/0.46 & 0.36/0.82 & 0.92 & 0.89 \\ \hline & & & & & & & & & & & & & & & & & &$ | | | | | | Relative efficiency | У | | |
| $\begin{array}{ c c c c c c } & & & & & & & & & & & & & & & & & & &$ | | p=14 | 1/1/0.91 | 0.91 | 0.91 | 0.76/0.76 | 0.95/0.93 | 0.96 | 0.94 |
| $\begin{array}{ c c c c c c c c c } \hline & p=100 & 1/1/0.83 & - & 0.84 & 0.44/0.44 & 0.66/0.85 & 0.89 & 0.86 \\ \hline & p=180 & 1/1/0.83 & - & 0.84 & 0.44/0.44 & 0.66/0.85 & 0.89 & 0.86 \\ \hline & p=30 & 1/1/0.84 & 0.84 & 0.84 & 0.6/0.61 & 0.81/0.86 & 0.91 & 0.88 \\ \hline & p=60 & 1/1/0.83 & - & 0.83 & 0.52/0.53 & 0.71/0.84 & 0.89 & 0.87 \\ \hline & p=180 & 1/1/0.83 & - & 0.84 & 0.44/0.44 & 0.51/0.83 & 0.89 & 0.86 \\ \hline & p=180 & 1/1/0.83 & - & 0.84 & 0.44/0.44 & 0.51/0.83 & 0.89 & 0.86 \\ \hline & p=30 & 0.99/1/0.86 & 0.86 & 0.85 & 0.61/0.62 & 0.72/0.84 & 0.93 & 0.9 \\ \hline & p=30 & 0.99/1/0.86 & 0.86 & 0.85 & 0.61/0.62 & 0.72/0.84 & 0.93 & 0.9 \\ \hline & p=60 & 1/1/0.84 & - & 0.85 & 0.53/0.54 & 0.57/0.83 & 0.91 & 0.89 \\ \hline & p=180 & 0.99/1/0.86 & - & 0.86 & 0.45/0.46 & 0.36/0.82 & 0.92 & 0.89 \\ \hline & & & & & & & & & & & & & & & & & &$ | | p=30 | 1/1/0.84 | 0.84 | 0.84 | 0.6/0.61 | 0.86/0.87 | 0.91 | 0.88 |
| $\begin{array}{ c c c c c c c c } & p=14 & 1/1/0.91 & 0.91 & 0.91 & 0.75/0.75 & 0.93/0.91 & 0.96 & 0.94 \\ p=30 & 1/1/0.84 & 0.84 & 0.84 & 0.6/0.61 & 0.81/0.86 & 0.91 & 0.88 \\ p=60 & 1/1/0.83 & - & 0.83 & 0.52/0.53 & 0.71/0.84 & 0.89 & 0.87 \\ p=180 & 1/1/0.83 & - & 0.84 & 0.44/0.44 & 0.51/0.83 & 0.89 & 0.86 \\ \hline \\ p=180 & 1/1/0.83 & - & 0.84 & 0.44/0.44 & 0.51/0.83 & 0.89 & 0.86 \\ \hline \\ lsnr & p=30 & 0.99/1/0.86 & 0.86 & 0.85 & 0.61/0.62 & 0.72/0.84 & 0.93 & 0.9 \\ p=60 & 1/1/0.84 & - & 0.85 & 0.53/0.54 & 0.57/0.83 & 0.91 & 0.89 \\ p=180 & 0.99/1/0.86 & - & 0.86 & 0.45/0.46 & 0.36/0.82 & 0.92 & 0.89 \\ \hline \\ \\ p=180 & 0.99/1/0.86 & - & 0.86 & 0.45/0.46 & 0.36/0.82 & 0.92 & 0.89 \\ \hline \\ \\ lsnr & p=60 & 1/1/0.84 & - & 0.85 & 0.53/0.54 & 0.57/0.83 & 0.91 & 0.89 \\ p=180 & 0.99/1/0.86 & - & 0.86 & 0.45/0.46 & 0.36/0.82 & 0.92 & 0.89 \\ \hline \\ \\ \\ \\ p=180 & 6(0.1)/6(0.1)/6(0.6) & 6(0.6) & 6(0.6) & 6(3.8)/6(4.5) & 6(0.9)/6(1.3) & 6(0.6) & 6(0.5) \\ p=30 & 6(0.1)/6(0.1)/6(0.6) & 6(0.6) & 6(0.6) & 6(8.3)/6(8.5) & 6(2)/6(1.8) & 6(0.9) & 6(0.5) \\ p=180 & 6(0)/6(0)/6(0.3) & - & 6(0.3) & 6(21.7)/6(19.1) & 6(10.3)/6(2.4) & 6(2.1) & 6(0.4) \\ \hline \\ \\ \\ msnr & p=44 & 6(0.3)/6(0.3)/6(0.6) & 6(0.6) & 6(0.6) & 6(3.9)/6(4.5) & 6(1)/6(1.3) & 6(0.6) & 6(0.5) \\ p=180 & 6(0)/6(0)/6(0.5) & - & 6(0.5) & 6(13)/6(12.2) & 6(3.9)/6(1.8) & 6(0.9) & 6(0.5) \\ p=30 & 6(0.1)/6(0.1)/6(0.6) & 6(0.6) & 6(0.6) & 6(3.9)/6(4.5) & 6(1)/6(1.8) & 6(0.9) & 6(0.5) \\ p=180 & 6(0)/6(0)/6(0.3) & - & 6(0.5) & 6(13)/6(12.2) & 6(4.8)/6(1.8) & 6(1.4) & 6(0.6) \\ p=180 & 6(0)/6(0)/6(0.3) & - & 6(0.5) & 6(13)/6(1.2) & 6(4.8)/6(1.8) & 6(1.4) & 6(0.6) \\ p=180 & 6(0)/6(0)/6(0.3) & - & 6(0.5) & 6(13)/6(1.2) & 6(4.8)/6(1.8) & 6(1.4) & 6(0.6) \\ p=180 & 6(0)/6(0)/6(0.6) & 6(0.6) & 6(0.6) & 6(0.8) & 6(3.9)/6(4.5) & 6(1.1)/6(1.4) & 6(0.5) & 6(0.5) \\ p=30 & 6(0.1)/6(0.1)/6(0.6) & 6(0.6) & 6(0.6) & 6(8.3)/6(8.5) & 6(3)/6(1.6) & 6(0.5) & 6(0.5) \\ p=30 & 6(0.1)/6(0.1)/6(0.6) & 6(0.6) & 6(0.6) & 6(8.3)/6(8.5) & 6(3)/6(1.5) & 6(1) & 6(0.5) \\ lsnr & p=60 & 6(0.1)/6(0.1)/6(0.5) & - & 6(0.5) & 6(1.32)/6(1.22) & 6$ | hsnr | p=60 | 1/1/0.83 | - | 0.83 | 0.52/0.53 | 0.79/0.86 | 0.89 | 0.87 |
| $\begin{array}{ c c c c c c c c c c c c c c c c c c c$ | | p=180 | 1/1/0.83 | - | 0.84 | 0.44/0.44 | 0.66/0.85 | 0.89 | 0.86 |
| $\begin{array}{ c c c c c c c c c c c c c c c c c c c$ | | p=14 | 1/1/0.91 | 0.91 | 0.91 | 0.75/0.75 | 0.93/0.91 | 0.96 | 0.94 |
| $\begin{array}{ c c c c c c c c c c c c c c c c c c c$ | | p=30 | 1/1/0.84 | 0.84 | 0.84 | 0.6/0.61 | 0.81/0.86 | 0.91 | 0.88 |
| $\begin{array}{ c c c c c c c c c c c c c c c c c c c$ | msnr | p=60 | 1/1/0.83 | - | 0.83 | 0.52/0.53 | 0.71/0.84 | 0.89 | 0.87 |
| $\begin{array}{ c c c c c c c c c c c c c c c c c c c$ | | p=180 | 1/1/0.83 | - | 0.84 | 0.44/0.44 | 0.51/0.83 | 0.89 | 0.86 |
| $\begin{array}{ c c c c c c c c c c c c c c c c c c c$ | | p=14 | | | | | | | |
| $\begin{array}{ c c c c c c c c c c c c c c c c c c c$ | 1 | p=30 | 0.99/1/0.86 | 0.86 | 0.85 | 0.61/0.62 | 0.72/0.84 | 0.93 | 0.9 |
| $\begin{array}{ c c c c c c c c } & Sparsistency (number of extra variables) \\ \hline & p=14 & 6(0.3)/6(0.3)/6(0.6) & 6(0.6) & 6(0.6) & 6(3.8)/6(4.5) & 6(0.9)/6(1.3) & 6(0.6) & 6(0.5) \\ p=30 & 6(0.1)/6(0.1)/6(0.6) & 6(0.6) & 6(0.6) & 6(8.3)/6(8.5) & 6(2)/6(1.8) & 6(0.9) & 6(0.5) \\ p=60 & 6(0)/6(0)/6(0.5) & - & 6(0.5) & 6(13)/6(12.2) & 6(3.9)/6(2.1) & 6(1.5) & 6(0.5) \\ p=180 & 6(0)/6(0)/6(0.3) & - & 6(0.3) & 6(21.7)/6(19.1) & 6(10.3)/6(2.4) & 6(2.1) & 6(0.4) \\ \hline \\ msnr & p=30 & 6(0.1)/6(0.1)/6(0.6) & 6(0.6) & 6(0.6) & 6(3.9)/6(4.5) & 6(1)/6(1.3) & 6(0.6) & 6(0.5) \\ p=30 & 6(0)/6(0)/6(0.5) & - & 6(0.5) & 6(13)/6(12.2) & 6(4.8)/6(1.8) & 6(0.9) & 6(0.5) \\ p=180 & 6(0)/6(0)/6(0.3) & - & 6(0.3) & 6(21.6)/6(19.1) & 6(15.6)/6(1.8) & 6(1.4) & 6(0.6) \\ p=180 & 6(0)/6(0)/6(0.3) & - & 6(0.3) & 6(21.6)/6(19.1) & 6(15.6)/6(1.8) & 6(1.8) & 6(0.4) \\ \hline \\ lsnr & p=60 & 6(0.1)/6(0.1)/6(0.6) & 6(0.6) & 6(0.6) & 6(3.9)/6(4.5) & 6(1.1)/6(1.4) & 6(0.5) & 6(0.5) \\ p=30 & 6(0.1)/6(0.1)/6(0.6) & 6(0.6) & 6(0.6) & 6(8.3)/6(8.5) & 6(3)/6(1.6) & 6(0.7) & 6(0.5) \\ lsnr & p=60 & 6(0.1)/6(0.1)/6(0.5) & - & 6(0.5) & 6(13.2)/6(12.2) & 6(6.8)/6(1.5) & 6(1) & 6(0.6) \\ \hline \\ lsnr & p=60 & 6(0.1)/6(0.1)/6(0.5) & - & 6(0.5) & 6(13.2)/6(12.2) & 6(6.8)/6(1.5) & 6(1) & 6(0.6) \\ \hline \\ \end{tabular}$ | Isnr | p=60 | | - | | 0.53/0.54 | 0.57/0.83 | | 0.89 |
| $\begin{array}{ c c c c c c c c c c c c c c c c c c c$ | | p=180 | 0.99/1/0.86 | - | 0.86 | 0.45/0.46 | 0.36/0.82 | 0.92 | 0.89 |
| $\begin{array}{ c c c c c c c c } & p=30 & 6(0.1)/6(0.1)/6(0.6) & 6(0.6) & 6(0.6) & 6(8.3)/6(8.5) & 6(2)/6(1.8) & 6(0.9) & 6(0.5) \\ p=60 & 6(0)/6(0)/6(0.5) & - & 6(0.5) & 6(13)/6(12.2) & 6(3.9)/6(2.1) & 6(1.5) & 6(0.5) \\ p=180 & 6(0)/6(0)/6(0.3) & - & 6(0.3) & 6(21.7)/6(19.1) & 6(10.3)/6(2.4) & 6(2.1) & 6(0.4) \\ \hline \\ msnr & p=30 & 6(0.1)/6(0.1)/6(0.6) & 6(0.6) & 6(0.6) & 6(3.9)/6(4.5) & 6(1)/6(1.3) & 6(0.6) & 6(0.5) \\ p=60 & 6(0)/6(0)/6(0.5) & - & 6(0.5) & 6(13)/6(12.2) & 6(4.8)/6(1.8) & 6(1.4) & 6(0.6) \\ p=180 & 6(0)/6(0)/6(0.3) & - & 6(0.3) & 6(21.6)/6(1.9) & 6(15.6)/6(1.8) & 6(1.8) & 6(0.4) \\ \hline \\ lsnr & p=30 & 6(0.1)/6(0.1)/6(0.6) & 6(0.6) & 6(0.6) & 6(3.9)/6(4.5) & 6(1.1)/6(1.4) & 6(0.5) \\ p=30 & 6(0.1)/6(0.1)/6(0.6) & 6(0.6) & 6(0.6) & 6(8.3)/6(8.5) & 6(3)/6(1.6) & 6(0.7) & 6(0.5) \\ p=30 & 6(0.1)/6(0.1)/6(0.6) & 6(0.6) & 6(0.6) & 6(8.3)/6(8.5) & 6(3)/6(1.6) & 6(0.7) & 6(0.5) \\ lsnr & p=60 & 6(0.1)/6(0.1)/6(0.5) & - & 6(0.5) & 6(13.2)/6(12.2) & 6(6.8)/6(1.5) & 6(1) & 6(0.6) \\ \hline \end{array}$ | | | | S_{I} | parsisten | cy (number of exti | ra variables) | | |
| $\begin{array}{ c c c c c c c c } \hline hsnr & p=60 & 6(0)/6(0)/6(0)/6(0.5) & - & 6(0.5) & 6(13)/6(12.2) & 6(3.9)/6(2.1) & 6(1.5) & 6(0.5) \\ \hline p=180 & 6(0)/6(0)/6(0.3) & - & 6(0.3) & 6(21.7)/6(19.1) & 6(10.3)/6(2.4) & 6(2.1) & 6(0.4) \\ \hline \\ p=30 & 6(0.1)/6(0.1)/6(0.6) & 6(0.6) & 6(0.6) & 6(3.9)/6(4.5) & 6(1)/6(1.3) & 6(0.6) & 6(0.5) \\ \hline \\ p=60 & 6(0)/6(0)/6(0.5) & - & 6(0.5) & 6(13)/6(12.2) & 6(4.8)/6(1.8) & 6(1.4) & 6(0.6) \\ \hline \\ p=180 & 6(0)/6(0)/6(0.3) & - & 6(0.3) & 6(21.6)/6(19.1) & 6(15.6)/6(1.8) & 6(1.8) & 6(0.4) \\ \hline \\ p=14 & 6(0.4)/6(0.4)/6(0.6) & 6(0.6) & 6(0.6) & 6(3.9)/6(4.5) & 6(1.1)/6(1.4) & 6(0.5) & 6(0.5) \\ \hline \\ lsnr & p=60 & 6(0.1)/6(0.1)/6(0.5) & - & 6(0.5) & 6(1.3)/6(1.2) & 6(6.8)/6(1.5) & 6(1) & 6(0.5) \\ \hline \\ lsnr & p=60 & 6(0.1)/6(0.1)/6(0.5) & - & 6(0.5) & 6(1.3)/6(1.2) & 6(6.8)/6(1.5) & 6(1) & 6(0.5) \\ \hline \\ lsnr & p=60 & 6(0.1)/6(0.1)/6(0.5) & - & 6(0.5) & 6(1.3)/6(1.2) & 6(6.8)/6(1.5) & 6(1) & 6(0.5) \\ \hline \end{array}$ | | p=14 | 6(0.3)/6(0.3)/6(0.6) | 6(0.6) | 6(0.6) | 6(3.8)/6(4.5) | 6(0.9)/6(1.3) | 6(0.6) | 6(0.5) |
| $\begin{array}{ c c c c c c c c c c c c c c c c c c c$ | , | p=30 | 6(0.1)/6(0.1)/6(0.6) | 6(0.6) | 6(0.6) | 6(8.3)/6(8.5) | 6(2)/6(1.8) | 6(0.9) | 6(0.5) |
| $\begin{array}{ c c c c c c c c c c c c c c c c c c c$ | hsnr | p=60 | 6(0)/6(0)/6(0.5) | - | 6(0.5) | 6(13)/6(12.2) | 6(3.9)/6(2.1) | 6(1.5) | 6(0.5) |
| $\begin{array}{ c c c c c c c c c c c c c c c c c c c$ | | p=180 | 6(0)/6(0)/6(0.3) | - | 6(0.3) | 6(21.7)/6(19.1) | 6(10.3)/6(2.4) | 6(2.1) | 6(0.4) |
| $ \begin{array}{ c c c c c c c c c c c c c c c c c c c$ | | p=14 | 6(0.3)/6(0.3)/6(0.6) | 6(0.6) | 6(0.6) | 6(3.9)/6(4.5) | 6(1)/6(1.3) | 6(0.6) | 6(0.5) |
| $ \begin{array}{ c c c c c c c c c c c c c c c c c c c$ | | p=30 | 6(0.1)/6(0.1)/6(0.6) | 6(0.6) | 6(0.6) | 6(8.3)/6(8.6) | 6(2.2)/6(1.8) | 6(0.9) | 6(0.5) |
| $ \begin{array}{ c c c c c c c c c c c c c c c c c c c$ | msnr | p=60 | 6(0)/6(0)/6(0.5) | - | 6(0.5) | 6(13)/6(12.2) | 6(4.8)/6(1.8) | 6(1.4) | 6(0.6) |
| $ \begin{array}{ c c c c c c c c c c c c c c c c c c c$ | | p=180 | 6(0)/6(0)/6(0.3) | - | 6(0.3) | 6(21.6)/6(19.1) | 6(15.6)/6(1.8) | 6(1.8) | 6(0.4) |
| $ \begin{array}{ c c c c c c c c c c c c c c c c c c c$ | | p=14 | 6(0.4)/6(0.4)/6(0.6) | 6(0.6) | 6(0.6) | 6(3.9)/6(4.5) | 6(1.1)/6(1.4) | 6(0.5) | 6(0.5) |
| $ \begin{array}{ c c c c c c c c c c c c c c c c c c c$ | | p=30 | | | | | | | 6(0.5) |
| $\begin{array}{ c c c c c c c c c c c c c c c c c c c$ | lsnr | p=60 | | . , | 6(0.5) | | | | |
| | | p=180 | 6(0.1)/6(0)/6(0.3) | - | 6(0.3) | 6(21.9)/6(19.1) | 6(23.7)/6(1) | 6(1) | 6(0.5) |

Table S21: The performance of BOSS compared to other methods, Sparse-Ex3, ρ =0.5, n=200

| | | BOSS | BS | FS | LASSO | Gamma LASSO | SparseNet | rLASSO |
|------|-------|----------------------------|------------------|------------|----------------------|--------------------|-----------|----------|
| | | C_p -hdf/AICc-hdf/CV | CV | CV | AICc/CV | AICc/CV | CV | CV |
| | | | Ç | % worse th | an the best possible | e BOSS | | |
| | p=14 | 7/6/18 | 19 | 18 | 40/39 | 15/18 | 14 | 15 |
| ١, | p=30 | 5/2/22 | 24 | 22 | 70/68 | 30/21 | 14 | 19 |
| hsnr | p=60 | 3/1/22 | - | 23 | 93/92 | 51/22 | 16 | 19 |
| | p=180 | 35/1/18 | - | 21 | 135/135 | 134/26 | 17 | 20 |
| | p=14 | 15/13/18 | 19 | 18 | 40/39 | 20/21 | 15 | 17 |
| | p=30 | 14/10/22 | 25 | 23 | 69/68 | 45/25 | 15 | 22 |
| msnr | p=60 | 13/9/23 | - | 24 | 91/89 | 78/26 | 15 | 27 |
| | p=180 | 48/11/20 | - | 23 | 132/133 | 218/31 | 18 | 43 |
| | p=14 | 19/21/24 | 24 | 24 | 5/4 | 11/11 | 13 | 10 |
| 1 | p=30 | 28/30/25 | 25 | 25 | 0/0 | 12/6 | 7 | 6 |
| lsnr | p=60 | 23/25/21 | - | 21 | -3/-3 | 22/3 | 3 | 2 |
| | p=180 | 27/11/13 | - | 13 | -3/-1 | 83/3 | 3 | 3 |
| | | | | R | telative efficiency | | | |
| | p=14 | 0.98/1/0.9 | 0.89 | 0.9 | 0.75/0.76 | 0.92/0.9 | 0.92 | 0.92 |
| ١, | p=30 | 0.98/1/0.84 | 0.82 | 0.84 | 0.6/0.61 | 0.79/0.85 | 0.9 | 0.86 |
| hsnr | p=60 | 0.98/1/0.83 | - | 0.83 | 0.53/0.53 | 0.67/0.83 | 0.88 | 0.85 |
| | p=180 | 0.75/1/0.85 | - | 0.84 | 0.43/0.43 | 0.43/0.8 | 0.86 | 0.84 |
| | p=14 | 0.98/1/0.95 | 0.95 | 0.95 | 0.8/0.81 | 0.93/0.93 | 0.98 | 0.96 |
| | p=30 | 0.97/1/0.9 | 0.88 | 0.89 | 0.65/0.66 | 0.76/0.88 | 0.96 | 0.9 |
| msnr | p=60 | 0.97/1/0.88 | - | 0.88 | 0.57/0.57 | 0.61/0.86 | 0.94 | 0.86 |
| | p=180 | 0.75/1/0.92 | - | 0.9 | 0.48/0.47 | 0.35/0.84 | 0.94 | 0.77 |
| | p=14 | 0.88/0.86/0.84 | 0.84 | 0.84 | 0.99/1 | 0.94/0.94 | 0.93 | 0.95 |
| lsnr | p=30 | 0.78/0.77/0.8 | 0.8 | 0.8 | 1/1 | 0.9/0.94 | 0.93 | 0.95 |
| ISHI | p=60 | 0.79/0.78/0.8 | - | 0.8 | 1/1 | 0.79/0.94 | 0.94 | 0.95 |
| | p=180 | 0.76/0.87/0.86 | - | 0.86 | 1/0.98 | 0.53/0.94 | 0.94 | 0.94 |
| | | | S_{I} | arsistency | (number of extra v | variables) | | |
| | p=14 | 6(0.4)/6(0.2)/6(0.6) | 6(0.7) | 6(0.6) | 6(3.7)/6(4.5) | 6(0.9)/6(1.3) | 6(0.7) | 6(0.6) |
| 1 | p=30 | 6(0.2)/6(0)/6(0.6) | 6(0.7) | 6(0.6) | 6(7.9)/6(9) | 6(2.4)/6(1.5) | 6(1.1) | 6(0.9) |
| hsnr | p=60 | 6(0.1)/6(0)/6(0.5) | - | 6(0.5) | 6(11.5)/6(13.3) | 6(4.9)/6(1.6) | 6(1.6) | 6(0.8) |
| | p=180 | 6(9.6)/6(0)/6(0.3) | - | 6(0.4) | 6(16.6)/6(23.8) | 6(18.1)/6(2.1) | 6(2.4) | 6(0.8) |
| | p=14 | 6(0.7)/6(0.6)/6(0.6) | 6(0.7) | 6(0.6) | 6(3.7)/6(4.5) | 6(1)/6(1.3) | 6(0.6) | 6(0.8) |
| man | p=30 | 6(0.4)/6(0.2)/6(0.7) | 6(0.8) | 6(0.7) | 6(8)/6(9) | 6(2.9)/6(1.5) | 6(0.8) | 6(1) |
| msnr | p=60 | 6(0.3)/6(0.2)/6(0.6) | - | 6(0.6) | 6(11.5)/6(13.3) | 6(6.1)/6(1.5) | 6(1.1) | 6(1.3) |
| | p=180 | 6(10)/6(0.1)/6(0.4) | - | 6(0.5) | 6(17)/6(23.8) | 6(27.9)/6(1.8) | 6(1.7) | 6(1.8) |
| | p=14 | 5.3(4.3)/5.2(4)/4.6(2.1) | 4.6(2) | 4.6(2) | 5.5(3.4)/5.6(4) | 4.9(1.4)/5.2(3) | 5.2(2.6) | 5.1(2.4) |
| lsnr | p=30 | 3.8(4.3)/2.9(2)/3.6(2.4) | 3.4(2.1) | 3.5(2.3) | 5.1(6.9)/5.2(7.5) | 4.6(3.9)/4.6(5.3) | 4.7(5.3) | 4.5(4.2) |
| ISHI | p=60 | 2.1(1.7)/1.3(0.4)/2.3(1.5) | - | 2.3(1.4) | 4.4(8.6)/4.5(9.7) | 4.4(8.3)/3.9(6.7) | 4(7.5) | 3.8(5.8) |
| | p=180 | 1.4(15.1)/0.3(0.1)/1(0.7) | - | 1(0.7) | 3(9.7)/3(12.5) | 4.3(37.2)/2.5(8.3) | 2.6(9.3) | 2.4(7.7) |

Table S22: The performance of BOSS compared to other methods, Sparse-Ex3, ρ =0.5, n=2000

| | | BOSS | BS | FS | LASSO | Gamma LASSO | SparseNet | rLASSO |
|---------|-------|------------------------|---------------|-----------|---------------------|----------------|-----------|--------|
| | | C_p -hdf/AICc-hdf/CV | CV | CV | AICc/CV | AICc/CV | CV | CV |
| | | | | % worse | than the best poss | sible BOSS | | |
| | p=14 | 7/6/18 | 19 | 19 | 43/42 | 13/16 | 13 | 15 |
| , | p=30 | 3/3/22 | 22 | 21 | 73/71 | 21/18 | 14 | 17 |
| hsnr | p=60 | 1/1/21 | - | 20 | 96/92 | 29/18 | 13 | 17 |
| | p=180 | 1/1/22 | - | 22 | 130/126 | 53/20 | 14 | 18 |
| | p=14 | 7/6/18 | 19 | 19 | 44/43 | 16/18 | 13 | 16 |
| msnr | p=30 | 3/3/22 | 22 | 21 | 73/71 | 28/20 | 14 | 17 |
| IIISIII | p=60 | 1/1/21 | - | 20 | 96/92 | 43/21 | 13 | 17 |
| | p=180 | 1/1/22 | - | 22 | 130/126 | 98/22 | 13 | 18 |
| | p=14 | 9/9/18 | 19 | 19 | 44/43 | 22/22 | 13 | 16 |
| lsnr | p=30 | 5/5/22 | 21 | 21 | 73/71 | 47/25 | 14 | 17 |
| 18111 | p=60 | 4/4/21 | - | 20 | 96/92 | 80/26 | 14 | 17 |
| | p=180 | 5/5/22 | - | 22 | 129/126 | 192/27 | 13 | 19 |
| | | | | | Relative efficiency | У | | |
| | p=14 | 1/1/0.9 | 0.9 | 0.9 | 0.75/0.75 | 0.94/0.92 | 0.95 | 0.92 |
| , | p=30 | 1/1/0.85 | 0.85 | 0.85 | 0.59/0.6 | 0.85/0.87 | 0.91 | 0.88 |
| hsnr | p=60 | 1/1/0.84 | - | 0.84 | 0.52/0.53 | 0.79/0.86 | 0.89 | 0.86 |
| | p=180 | 1/1/0.83 | - | 0.83 | 0.44/0.45 | 0.66/0.84 | 0.89 | 0.86 |
| | p=14 | 1/1/0.9 | 0.9 | 0.9 | 0.74/0.75 | 0.92/0.9 | 0.94 | 0.92 |
| | p=30 | 1/1/0.85 | 0.85 | 0.85 | 0.59/0.6 | 0.8/0.85 | 0.9 | 0.88 |
| msnr | p=60 | 1/1/0.84 | - | 0.84 | 0.52/0.53 | 0.71/0.84 | 0.9 | 0.87 |
| | p=180 | 1/1/0.83 | - | 0.83 | 0.44/0.45 | 0.51/0.83 | 0.89 | 0.86 |
| | p=14 | 1/1/0.92 | 0.92 | 0.92 | 0.75/0.76 | 0.89/0.89 | 0.96 | 0.94 |
| lsnr | p=30 | 1/1/0.86 | 0.86 | 0.86 | 0.61/0.61 | 0.71/0.84 | 0.92 | 0.9 |
| 18111 | p=60 | 1/1/0.86 | - | 0.86 | 0.53/0.54 | 0.58/0.83 | 0.91 | 0.88 |
| | p=180 | 1/1/0.86 | - | 0.86 | 0.46/0.46 | 0.36/0.82 | 0.93 | 0.88 |
| | | | $S_{\bar{i}}$ | parsisten | cy (number of ext | ra variables) | | |
| | p=14 | 6(0.3)/6(0.3)/6(0.6) | 6(0.6) | 6(0.6) | 6(3.9)/6(4.4) | 6(0.9)/6(1.3) | 6(0.6) | 6(0.6) |
| , | p=30 | 6(0.1)/6(0.1)/6(0.6) | 6(0.6) | 6(0.6) | 6(8.4)/6(8.6) | 6(2.1)/6(1.7) | 6(1) | 6(0.6) |
| hsnr | p=60 | 6(0)/6(0)/6(0.5) | - | 6(0.5) | 6(13.2)/6(12.3) | 6(3.9)/6(2.1) | 6(1.6) | 6(0.6) |
| | p=180 | 6(0)/6(0)/6(0.4) | - | 6(0.4) | 6(21.5)/6(18.7) | 6(10.4)/6(2.6) | 6(2.3) | 6(0.6) |
| | p=14 | 6(0.3)/6(0.3)/6(0.6) | 6(0.6) | 6(0.6) | 6(3.9)/6(4.5) | 6(1)/6(1.4) | 6(0.6) | 6(0.6) |
| | p=30 | 6(0.1)/6(0.1)/6(0.6) | 6(0.6) | 6(0.6) | 6(8.3)/6(8.6) | 6(2.4)/6(1.6) | 6(0.9) | 6(0.6) |
| msnr | p=60 | 6(0)/6(0)/6(0.5) | - | 6(0.5) | 6(13)/6(12.3) | 6(4.7)/6(1.8) | 6(1.4) | 6(0.6) |
| | p=180 | 6(0)/6(0)/6(0.4) | - | 6(0.4) | 6(21.5)/6(18.7) | 6(15.7)/6(1.9) | 6(2.1) | 6(0.5) |
| | p=14 | 6(0.4)/6(0.4)/6(0.6) | 6(0.6) | 6(0.6) | 6(3.9)/6(4.5) | 6(1.1)/6(1.4) | 6(0.5) | 6(0.6) |
| 1 | p=30 | 6(0.1)/6(0.1)/6(0.6) | 6(0.6) | 6(0.6) | 6(8.3)/6(8.6) | 6(3)/6(1.4) | 6(0.7) | 6(0.6) |
| lsnr | p=60 | 6(0.1)/6(0.1)/6(0.5) | - | 6(0.5) | 6(13.1)/6(12.2) | 6(6.5)/6(1.5) | 6(1) | 6(0.6) |
| | p=180 | 6(0.1)/6(0.1)/6(0.4) | - | 6(0.4) | 6(21.2)/6(18.7) | 6(23.5)/6(1.2) | 6(0.9) | 6(0.5) |

Table S23: The performance of BOSS compared to other methods, Sparse-Ex3, ρ =0.9, n=200

| | | BOSS | BS CV | FS CV | LASSO | Gamma LASSO | SparseNet | rLASSO |
|---------|-------|-----------------------------|----------|------------|-----------------------|---------------------|-----------|----------|
| | | C_p -hdf/AICc-hdf/CV | CV | | AICc/CV | AICc/CV | CV | CV |
| | | | | % worse t. | han the best possible | | | |
| | p=14 | 7/6/24 | 13 | 24 | 33/33 | 14/16 | 12 | 16 |
| homm | p=30 | 7/5/41 | 17 | 41 | 66/64 | 26/29 | 12 | 23 |
| hsnr | p=60 | 6/4/43 | - | 43 | 84/83 | 44/38 | 13 | 19 |
| | p=180 | 35/3/27 | - | 29 | 126/126 | 132/35 | 16 | 18 |
| | p=14 | 14/13/19 | 16 | 19 | 18/17 | 17/17 | 6 | 9 |
| msnr | p=30 | 15/13/24 | 8 | 25 | 30/29 | 29/24 | 0 | 8 |
| IIISIII | p=60 | 12/10/20 | - | 20 | 43/42 | 50/25 | -6 | 6 |
| | p=180 | 35/7/16 | - | 18 | 87/87 | 164/23 | 2 | 13 |
| | p=14 | 17/20/22 | 22 | 21 | -2/-3 | 5/3 | 5 | 4 |
| lsnr | p=30 | 26/28/24 | 23 | 23 | -2/-2 | 8/6 | 5 | 3 |
| ISH | p=60 | 23/26/22 | - | 22 | -3/-3 | 20/3 | 4 | 2 |
| | p=180 | 29/16/16 | - | 15 | -5/-3 | 79/1 | 1 | 0 |
| | | | | | Relative efficiency | | | |
| | p=14 | 0.99/1/0.85 | 0.93 | 0.85 | 0.79/0.79 | 0.92/0.91 | 0.95 | 0.91 |
| ١, | p=30 | 0.98/1/0.74 | 0.9 | 0.74 | 0.63/0.64 | 0.83/0.81 | 0.93 | 0.86 |
| hsnr | p=60 | 0.98/1/0.73 | - | 0.73 | 0.57/0.57 | 0.73/0.75 | 0.92 | 0.87 |
| | p=180 | 0.76/1/0.8 | - | 0.79 | 0.45/0.45 | 0.44/0.76 | 0.88 | 0.87 |
| | p=14 | 0.93/0.94/0.9 | 0.92 | 0.9 | 0.9/0.91 | 0.91/0.91 | 1 | 0.97 |
| | p=30 | 0.87/0.88/0.8 | 0.93 | 0.8 | 0.77/0.77 | 0.77/0.8 | 1 | 0.92 |
| msnr | p=60 | 0.84/0.85/0.78 | - | 0.78 | 0.66/0.66 | 0.63/0.75 | 1 | 0.89 |
| | p=180 | 0.75/0.95/0.88 | - | 0.87 | 0.55/0.55 | 0.39/0.83 | 1 | 0.9 |
| | p=14 | 0.83/0.81/0.8 | 0.8 | 0.81 | 0.99/1 | 0.93/0.94 | 0.93 | 0.94 |
| lsnr | p=30 | 0.78/0.76/0.79 | 0.8 | 0.8 | 1/1 | 0.91/0.93 | 0.93 | 0.95 |
| ISH | p=60 | 0.78/0.77/0.79 | - | 0.8 | 1/1 | 0.8/0.94 | 0.93 | 0.95 |
| | p=180 | 0.74/0.82/0.82 | - | 0.83 | 1/0.98 | 0.53/0.94 | 0.95 | 0.95 |
| | | | S | parsistenc | y (number of extra va | riables) | | |
| | p=14 | 6(0.6)/6(0.5)/6(1.4) | 6(0.6) | 6(1.4) | 6(3.9)/6(4.5) | 6(1)/6(1.4) | 6(0.7) | 6(1.2) |
| , | p=30 | 6(0.7)/6(0.6)/6(2.1) | 6(0.8) | 6(2.1) | 6(9.2)/6(10.3) | 6(2.5)/6(3.4) | 6(1.6) | 6(2.3) |
| hsnr | p=60 | 6(0.8)/6(0.7)/6(2) | - 1 | 6(1.9) | 6(12.4)/6(14.2) | 6(5.1)/6(4.7) | 6(2.5) | 6(2.1) |
| | p=180 | 6(9.2)/6(0.1)/6(0.6) | - | 6(0.6) | 6(16.2)/6(22.2) | 6(18.1)/6(3.4) | 6(2.4) | 6(0.8) |
| | p=14 | 5.6(1.2)/5.6(1.1)/5.8(2.1) | 5.8(1.8) | 5.8(2.1) | 6(4)/6(4.5) | 5.7(1.5)/5.8(2.6) | 5.8(1) | 5.9(1.9) |
| | p=30 | 5.1(1.5)/5.1(1.2)/5.3(2.6) | 5.5(1.4) | 5.3(2.6) | 6(9.1)/6(10.2) | 5.2(4.1)/5.4(5.8) | 5.7(1.8) | 5.7(3.2) |
| msnr | p=60 | 5.2(1.2)/5.2(1)/5.2(1.7) | - | 5.2(1.6) | 5.9(12.4)/6(14.1) | 5.2(7.5)/5.3(5.2) | 5.8(1.7) | 5.7(2.8) |
| | p=180 | 5.6(10)/5.6(0.5)/5.6(0.8) | - | 5.6(0.8) | 6(16.2)/6(22.2) | 5.6(27.5)/5.6(3.1) | 5.9(1.7) | 5.9(1.9) |
| | p=14 | 4.4(4)/4.2(3.6)/3.7(2.5) | 3.6(2.4) | 3.7(2.3) | 4.8(3.6)/4.9(4.1) | 3.9(2.1)/4.4(3.2) | 4.5(2.5) | 4.5(3) |
| , | p=30 | 2.6(4.4)/1.9(2.3)/2.4(3) | 2.5(2.8) | 2.4(2.9) | 3.9(7.5)/4(8.2) | 3.3(4.9)/3.3(6.3) | 3.7(6.1) | 3.4(5.3) |
| lsnr | p=60 | 1.7(2)/1.1(0.8)/1.8(2) | - | 1.8(1.9) | 3.7(9.4)/3.8(10.4) | 3.4(8.9)/3.2(7.6) | 3.4(7.7) | 3.2(6.5) |
| | p=180 | 1.4(14.4)/0.5(0.2)/1.1(1.1) | - | 1.1(1.1) | 3.2(11.1)/3.3(14.7) | 3.5(36.7)/2.8(10.2) | 3(10.8) | 2.8(9.1) |

Table S24: The performance of BOSS compared to other methods, Sparse-Ex3, ρ =0.9, n=2000

| | | BOSS C_v -hdf/AICc-hdf/CV | BS CV | FS CV | LASSO AICc/CV | Gamma LASSO AICc/CV | SparseNet CV | rLASSO CV |
|-------|-------|-----------------------------|----------|------------|----------------------|------------------------|-----------------|-----------|
| | | | | | in the best possible | | | |
| - | p=14 | 6/6/19 | 19 | 19 | 40/39 | 12/14 | 13 | 15 |
| | p=30 | 2/2/21 | 21 | 22 | 74/72 | 20/18 | 13 | 17 |
| hsnr | p=60 | $\frac{2/2/21}{1/1/22}$ | - | 22 | 101/97 | 29/19 | 14 | 19 |
| | p=180 | 1/1/21 | - | 22 | 135/131 | 52/18 | 14 | 21 |
| | p=14 | 6/6/19 | 19 | 19 | 42/40 | 18/18 | 14 | 15 |
| | p=30 | 2/2/21 | 21 | 22 | 74/72 | 27/20 | 14 | 17 |
| msnr | p=60 | 1/1/22 | - | 22 | 101/97 | 43/21 | 14 | 19 |
| | p=180 | 1/1/21 | - | 22 | 135/132 | 96/21 | 13 | 21 |
| | p=14 | 9/9/19 | 19 | 19 | 27/26 | 17/18 | 6 | 14 |
| ١, | p=30 | 5/5/21 | 20 | 21 | 53/51 | 34/23 | 3 | 14 |
| lsnr | p=60 | 4/4/20 | - | 20 | 75/71 | 62/22 | 1 | 12 |
| | p=180 | 4/4/17 | - | 17 | 92/89 | 145/23 | -5 | 11 |
| | | | | Re | elative efficiency | | | |
| | p=14 | 1/1/0.89 | 0.89 | 0.89 | 0.76/0.76 | 0.95/0.93 | 0.94 | 0.92 |
| ١, | p=30 | 1/1/0.84 | 0.85 | 0.84 | 0.59/0.6 | 0.85/0.87 | 0.9 | 0.87 |
| hsnr | p=60 | 1/1/0.83 | - | 0.83 | 0.5/0.51 | 0.79/0.85 | 0.89 | 0.85 |
| | p=180 | 1/1/0.84 | - | 0.83 | 0.43/0.44 | 0.67/0.86 | 0.89 | 0.84 |
| | p=14 | 1/1/0.89 | 0.89 | 0.89 | 0.75/0.76 | 0.9/0.9 | 0.93 | 0.92 |
| | p=30 | 1/1/0.84 | 0.85 | 0.84 | 0.59/0.6 | 0.81/0.85 | 0.9 | 0.87 |
| msnr | p=60 | 1/1/0.83 | - | 0.83 | 0.5/0.51 | 0.71/0.84 | 0.89 | 0.85 |
| | p=180 | 1/1/0.84 | - | 0.83 | 0.43/0.44 | 0.52/0.83 | 0.9 | 0.84 |
| | p=14 | 0.97/0.97/0.89 | 0.89 | 0.89 | 0.83/0.84 | 0.91/0.89 | 1 | 0.93 |
| lsnr | p=30 | 0.98/0.98/0.85 | 0.86 | 0.85 | 0.67/0.68 | 0.77/0.83 | 1 | 0.9 |
| ISIII | p=60 | 0.97/0.97/0.84 | - | 0.84 | 0.58/0.59 | 0.62/0.82 | 1 | 0.9 |
| | p=180 | 0.91/0.91/0.81 | - | 0.81 | 0.49/0.5 | 0.39/0.77 | 1 | 0.85 |
| | | | Spa | arsistency | (number of extra | variables) | | |
| | p=14 | 6(0.3)/6(0.3)/6(0.7) | 6(0.6) | 6(0.6) | 6(4.1)/6(4.6) | 6(0.8)/6(1) | 6(0.7) | 6(0.6) |
| 1 | p=30 | 6(0)/6(0)/6(0.6) | 6(0.6) | 6(0.6) | 6(9.2)/6(9.5) | 6(2)/6(1.8) | 6(1) | 6(0.7) |
| hsnr | p=60 | 6(0)/6(0)/6(0.5) | - | 6(0.5) | 6(14)/6(13.3) | 6(3.7)/6(2.1) | 6(1.5) | 6(0.8) |
| | p=180 | 6(0)/6(0)/6(0.4) | - | 6(0.4) | 6(23.2)/6(20.6) | 6(10.1)/6(2.4) | 6(2.2) | 6(0.7) |
| | p=14 | 6(0.3)/6(0.3)/6(0.7) | 6(0.6) | 6(0.6) | 6(4.2)/6(4.6) | 6(1.1)/6(1.3) | 6(0.7) | 6(0.6) |
| menr | p=30 | 6(0)/6(0)/6(0.6) | 6(0.6) | 6(0.6) | 6(9.2)/6(9.5) | 6(2.3)/6(1.7) | 6(1) | 6(0.7) |
| msnr | p=60 | 6(0)/6(0)/6(0.5) | - | 6(0.5) | 6(14.1)/6(13.3) | 6(4.7)/6(1.8) | 6(1.4) | 6(0.7) |
| | p=180 | 6(0)/6(0)/6(0.4) | - | 6(0.4) | 6(23.2)/6(20.5) | 6(15.3)/6(1.9) | 6(1.9) | 6(0.7) |
| | p=14 | 5.8(0.4)/5.8(0.4)/5.9(1.4) | 5.9(1.5) | 5.9(1.5) | 6(4.2)/6(4.6) | 5.9(1.2)/5.9(2.1) | 6(0.8) | 6(1.6) |
| lsnr | p=30 | 5.8(0.3)/5.8(0.3)/5.8(1.1) | 5.8(1.1) | 5.8(1.1) | 6(9.2)/6(9.5) | 5.8(2.8)/5.9(3) | 6(0.8) | 6(1.6) |
| ISIII | p=60 | 5.8(0.3)/5.8(0.3)/5.8(0.8) | - | 5.8(0.8) | 6(14)/6(13.3) | 5.8(6.3)/5.8(2.3) | 6(1.1) | 6(1.4) |
| | p=180 | 5.7(0.3)/5.7(0.3)/5.7(0.7) | - | 5.7(0.7) | 6(23)/6(20.6) | 5.7(23.2)/5.7(2.6) | 6(1) | 5.9(1.7) |

Table S25: The performance of BOSS compared to other methods, Sparse-Ex4, ρ =0, n=200

| | | BOSS C_p -hdf/AICc-hdf/CV | BS CV | FS CV | LASSO AICc/CV | Gamma LASSO AICc/CV | SparseNet CV | rLASSO CV |
|---------|-------|---------------------------------|----------|------------|---|------------------------|-----------------|--------------|
| | | C _p -ndi/Alcc-ndi/CV | CV | | han the best possible | | CV | CV |
| | | 20.100.100 | | | * | | | |
| | p=14 | 30/30/22 | 22 | 22 | 19/19 | 16/18 | 20 | 20 |
| hsnr | p=30 | 24/21/24 | 25 | 25 | 29/28 | 32/19 | 16 | 20 |
| 11.5111 | p=60 | 16/15/20 | - | 21 | 37/36 | 57/17 | 13 | 21 |
| | p=180 | 29/5/14 | - | 15 | 50/51 | 168/14 | 11 | 16 |
| | p=14 | 25/22/22 | 23 | 22 | 31/31 | 26/21 | 18 | 18 |
| msnr | p=30 | 26/20/27 | 28 | 28 | 52/51 | 43/24 | 21 | 26 |
| 1113111 | p=60 | 18/14/24 | - | 25 | 69/68 | 72/25 | 21 | 27 |
| | p=180 | 55/16/26 | - | 27 | 97/99 | 237/29 | 27 | 36 |
| | p=14 | 34/34/29 | 30 | 29 | 16/16 | 19/25 | 25 | 19 |
| lsnr | p=30 | 37/34/31 | 31 | 31 | 20/18 | 33/25 | 24 | 22 |
| ISHF | p=60 | 32/33/29 | - | 29 | 20/20 | 55/24 | 22 | 22 |
| | p=180 | 49/29/27 | - | 26 | 18/20 | 142/23 | 21 | 17 |
| | | | | | Relative efficiency | | | |
| | p=14 | 0.89/0.89/0.95 | 0.95 | 0.95 | 0.98/0.98 | 1/0.98 | 0.97 | 0.97 |
| | p=30 | 0.94/0.96/0.94 | 0.93 | 0.93 | 0.9/0.91 | 0.88/0.98 | 1 | 0.97 |
| hsnr | p=60 | 0.97/0.99/0.94 | - | 0.94 | 0.83/0.83 | 0.72/0.97 | 1 | 0.93 |
| | p=180 | 0.82/1/0.92 | - | 0.92 | 0.7/0.7 | 0.39/0.92 | 0.94 | 0.91 |
| | p=14 | 0.95/0.96/0.97 | 0.96 | 0.97 | 0.9/0.9 | 0.94/0.98 | 1 | 1 |
| | p=30 | 0.96/1/0.95 | 0.94 | 0.94 | 0.79/0.8 | 0.84/0.97 | 0.99 | 0.95 |
| msnr | p=60 | 0.96/1/0.92 | - | 0.92 | 0.68/0.68 | 0.66/0.91 | 0.95 | 0.9 |
| | p=180 | 0.74/1/0.92 | - | 0.91 | 0.59/0.58 | 0.34/0.9 | 0.91 | 0.85 |
| | p=14 | 0.86/0.87/0.9 | 0.89 | 0.9 | 1/1 | 0.97/0.93 | 0.93 | 0.97 |
| , | p=30 | 0.87/0.89/0.9 | 0.91 | 0.9 | 0.99/1 | 0.89/0.95 | 0.96 | 0.97 |
| lsnr | p=60 | 0.91/0.9/0.93 | - | 0.93 | 1/1 | 0.77/0.97 | 0.98 | 0.98 |
| | p=180 | 0.78/0.91/0.92 | - | 0.92 | 0.99/0.97 | 0.48/0.95 | 0.96 | 1 |
| | | | S | parsistenc | y (number of extra va | riables) | | |
| | p=14 | 5(1.7)/4.9(1.3)/5.2(0.9) | 5.2(0.9) | 5.2(0.9) | 5.8(3.4)/5.9(4.2) | 5.5(1.3)/5.3(1.5) | 5.3(1.3) | 5.2(1.1) |
| , | p=30 | 4.6(0.7)/4.4(0.2)/4.9(0.9) | 4.9(1.1) | 4.9(1) | 5.7(7)/5.8(8) | 5.4(3.3)/5(1.9) | 5(2) | 5(1.4) |
| hsnr | p=60 | 4.3(0.2)/4.2(0)/4.6(0.7) | - | 4.6(0.7) | 5.5(10.4)/5.6(12.1) | 5.4(7.5)/4.8(2.2) | 4.9(2.8) | 4.6(1.6) |
| | p=180 | 4.3(10.2)/4.1(0)/4.2(0.4) | - | 4.3(0.5) | 5.2(14)/5.3(19) | 5.4(35.4)/4.4(2.3) | 4.5(3.9) | 4.3(1.5) |
| | p=14 | 4.5(1.3)/4.4(1)/4.4(0.6) | 4.4(0.7) | 4.4(0.7) | 5.2(3.1)/5.2(3.6) | 4.6(1.1)/4.5(1) | 4.4(0.8) | 4.4(0.7 |
| | p=30 | 4.2(0.8)/4.1(0.4)/4.2(0.8) | 4.2(0.8) | 4.2(0.8) | 5(6.5)/5(7.1) | 4.6(2.9)/4.3(1.3) | 4.3(1.3) | 4.3(1.2) |
| msnr | p=60 | 4(0.3)/4(0.2)/4.1(0.6) | - | 4.1(0.6) | 4.7(9.5)/4.7(10.7) | 4.5(6.5)/4.1(1.3) | 4.2(1.7) | 4.1(1.2) |
| | p=180 | 4.1(10.4)/3.9(0.1)/4(0.5) | - | 4(0.5) | 4.4(13.1)/4.5(17.1) | 4.6(31.6)/4(1.6) | 4.1(2.6) | 4(1.7) |
| | p=14 | 3.9(2.4)/3.7(2)/3.3(0.9) | 3.3(1.1) | 3.2(0.9) | 4.4(2.7)/4.5(3) | 3.7(1.3)/3.6(1.5) | 3.6(1.6) | 3.6(1.2) |
| , | p=30 | 2.6(1.8)/2.2(0.7)/2.5(1.1) | 2.5(1.1) | 2.5(1.1) | $3.8(\hat{5}.3)/3.9(\hat{5}.\acute{5})$ | 3.4(3.5)/2.9(2.5) | $3(2.9)^{'}$ | 3(2.4) |
| lsnr | p=60 | 2(0.8)/1.7(0.2)/2.2(0.8) | - | 2.2(0.8) | 3.4(7.3)/3.5(8.1) | 3.5(7.8)/2.7(3.3) | 2.8(3.9) | 2.7(3.1) |
| | p=180 | 1.8(12)/1.3(0.1)/1.6(0.6) | - | 1.7(0.6) | 2.9(9.7)/2.9(11.2) | 3.7(34)/2.2(5) | 2.4(6.2) | 2.2(3.8) |

Table S26: The performance of BOSS compared to other methods, Sparse-Ex4, ρ =0, n=2000

| | | BOSS C_n -hdf/AICc-hdf/CV | BS CV | FS CV | LASSO AICc/CV | Gamma LASSO AICc/CV | SparseNet CV | rLASSO CV |
|-------------|-------|-----------------------------|----------|------------|-----------------------|------------------------|-----------------|--------------|
| | | | | | han the best possible | , | | |
| | p=14 | 9/9/17 | 17 | 17 | 41/41 | 19/15 | 12 | 13 |
| | p=30 | 5/5/22 | 22 | 23 | 74/71 | 45/22 | 13 | 16 |
| hsnr | p=60 | 4/4/24 | - | 23 | 97/93 | 83/23 | 16 | 17 |
| | p=180 | 4/4/21 | - | 21 | 131/127 | 200/23 | 13 | 17 |
| | p=14 | 31/31/21 | 21 | 22 | 34/33 | 20/20 | 22 | 22 |
| | p=30 | 40/40/29 | 31 | 29 | 52/50 | 42/29 | 28 | 34 |
| msnr | p=60 | 40/40/32 | - | 32 | 64/61 | 76/29 | 29 | 33 |
| | p=180 | 39/40/31 | - | 32 | 67/64 | 157/27 | 27 | 30 |
| | p=14 | 19/19/19 | 19 | 19 | 28/28 | 24/18 | 16 | 16 |
| lsnr | p=30 | 11/11/21 | 22 | 21 | 49/47 | 57/20 | 14 | 17 |
| ISIII | p=60 | 10/9/20 | - | 20 | 64/61 | 102/19 | 13 | 17 |
| | p=180 | 9/8/20 | - | 20 | 91/88 | 235/21 | 14 | 18 |
| | | | | : | Relative efficiency | | | |
| | p=14 | 1/1/0.93 | 0.93 | 0.93 | 0.77/0.77 | 0.91/0.95 | 0.97 | 0.96 |
| homm | p=30 | 1/1/0.86 | 0.86 | 0.86 | 0.6/0.61 | 0.72/0.86 | 0.93 | 0.91 |
| hsnr | p=60 | 1/1/0.84 | - | 0.84 | 0.53/0.54 | 0.57/0.85 | 0.9 | 0.89 |
| | p=180 | 1/1/0.86 | - | 0.86 | 0.45/0.46 | 0.35/0.85 | 0.92 | 0.89 |
| | p=14 | 0.91/0.91/0.99 | 0.99 | 0.98 | 0.9/0.9 | 1/0.99 | 0.98 | 0.98 |
| | p=30 | 0.91/0.91/0.99 | 0.97 | 0.99 | 0.84/0.85 | 0.9/0.99 | 1 | 0.95 |
| msnr | p=60 | 0.92/0.92/0.97 | - | 0.98 | 0.78/0.8 | 0.73/1 | 1 | 0.97 |
| | p=180 | 0.91/0.91/0.96 | - | 0.96 | 0.76/0.77 | 0.49/1 | 1 | 0.97 |
| | p=14 | 0.97/0.97/0.97 | 0.97 | 0.97 | 0.9/0.91 | 0.93/0.98 | 1 | 1 |
| lsnr | p=30 | 1/1/0.92 | 0.91 | 0.92 | 0.74/0.76 | 0.71/0.93 | 0.98 | 0.95 |
| 15111 | p=60 | 1/1/0.91 | - | 0.91 | 0.67/0.68 | 0.54/0.92 | 0.97 | 0.93 |
| | p=180 | 1/1/0.9 | - | 0.9 | 0.57/0.58 | 0.32/0.9 | 0.95 | 0.92 |
| | | | S | parsistenc | y (number of extra va | riables) | | |
| | p=14 | 6(0.4)/6(0.4)/6(0.6) | 6(0.6) | 6(0.6) | 6(3.8)/6(4.5) | 6(1.1)/6(0.8) | 6(0.5) | 6(0.5) |
| homm | p=30 | 6(0.1)/6(0.1)/6(0.6) | 6(0.6) | 6(0.6) | 6(8.4)/6(8.7) | 6(2.9)/6(1.3) | 6(0.7) | 6(0.5) |
| hsnr | p=60 | 6(0.1)/6(0.1)/6(0.5) | - | 6(0.5) | 6(13)/6(12.2) | 6(6.8)/6(1.5) | 6(1.1) | 6(0.6) |
| | p=180 | 6(0)/6(0)/6(0.3) | - | 6(0.3) | 6(21.7)/6(19.4) | 6(24.4)/6(1.5) | 6(1.2) | 6(0.5) |
| | p=14 | 5.8(1.9)/5.8(1.8)/5.8(0.8) | 5.8(0.8) | 5.8(0.8) | 6(3.8)/6(4.4) | 5.9(1.2)/5.9(1.5) | 5.8(1.1) | 5.8(0.9) |
| menr | p=30 | 5.4(1)/5.4(0.9)/5.6(0.9) | 5.6(0.9) | 5.6(0.9) | 6(8.5)/6(8.6) | 5.9(3.4)/5.7(2.2) | 5.7(1.9) | 5.6(1.5) |
| msnr | p=60 | 5.2(0.3)/5.2(0.3)/5.6(0.8) | - | 5.6(0.8) | 6(13)/6(12.1) | 5.9(7.8)/5.7(2.6) | 5.7(2.7) | 5.6(1.4) |
| | p=180 | 4.7(0.1)/4.7(0.1)/5.2(0.6) | - | 5.2(0.6) | 5.9(21.7)/5.9(19) | 5.9(26.9)/5.4(2.9) | 5.4(4.5) | 5.2(1.4) |
| | p=14 | 4.5(1)/4.5(1)/4.5(0.6) | 4.5(0.6) | 4.5(0.6) | 5.3(3.4)/5.4(3.8) | 4.8(1.3)/4.6(1) | 4.5(0.7) | 4.5(0.6) |
| lsnr | p=30 | 4.1(0.3)/4.1(0.3)/4.3(0.6) | 4.3(0.6) | 4.3(0.6) | 5.1(7.2)/5.1(7.3) | 4.8(3.6)/4.3(1.2) | 4.3(1) | 4.2(0.9) |
| ISIII | p=60 | 4.1(0.2)/4.1(0.2)/4.2(0.5) | - | 4.2(0.5) | 5(11.2)/4.9(10.1) | 4.8(8)/4.2(1.2) | 4.2(1.2) | 4.2(0.8) |
| | p=180 | 4(0.1)/4(0.1)/4.1(0.4) | - | 4.1(0.4) | 4.7(18.7)/4.6(15.6) | 4.8(27)/4.1(1) | 4.1(1.4) | 4.1(0.8) |

Table S27: The performance of BOSS compared to other methods, Sparse-Ex4, ρ =0.5, n=200

| | | BOSS C_n -hdf/AICc-hdf/CV | BS CV | FS CV | LASSO AICc/CV | Gamma LASSO AICc/CV | SparseNet CV | rLASSO CV |
|----------|-------|-----------------------------|----------|------------|-----------------------|------------------------|-----------------|--------------|
| ! | | | | | han the best possible | | | |
| <u> </u> | p=14 | 34/33/25 | 22 | 26 | 29/28 | 17/25 | 25 | 33 |
| | p=30 | 23/19/24 | 23 | 28 | 49/47 | 34/26 | 21 | 32 |
| hsnr | p=60 | 18/17/21 | _ | 24 | 56/54 | 52/21 | 17 | 28 |
| | p=180 | 29/4/15 | - | 16 | 82/81 | 170/16 | 13 | 15 |
| | p=14 | 27/25/29 | 20 | 21 | 38/37 | 25/20 | 17 | 24 |
| | p=30 | 24/19/34 | 24 | 30 | 74/72 | 52/26 | 16 | 52 |
| msnr | p=60 | 17/13/33 | - | 28 | 90/89 | 78/26 | 14 | 62 |
| | p=180 | 52/14/37 | - | 29 | 137/137 | 263/29 | 17 | 91 |
| | p=14 | 37/35/31 | 24 | 30 | 30/29 | 23/29 | 26 | 33 |
| lsnr | p=30 | 37/35/32 | 23 | 34 | 35/35 | 30/31 | 23 | 38 |
| ISH | p=60 | 37/38/32 | - | 36 | 38/40 | 53/34 | 24 | 42 |
| | p=180 | 49/31/26 | - | 34 | 33/35 | 120/31 | 20 | 38 |
| | | | | | Relative efficiency | | | |
| | p=14 | 0.88/0.88/0.94 | 0.97 | 0.93 | 0.91/0.92 | 1/0.94 | 0.94 | 0.89 |
| hsnr | p=30 | 0.97/1/0.96 | 0.97 | 0.93 | 0.8/0.81 | 0.89/0.95 | 0.99 | 0.9 |
| HSHF | p=60 | 0.99/1/0.96 | - | 0.94 | 0.75/0.76 | 0.77/0.96 | 1 | 0.91 |
| | p=180 | 0.81/1/0.91 | - | 0.9 | 0.57/0.58 | 0.39/0.9 | 0.92 | 0.91 |
| | p=14 | 0.92/0.94/0.91 | 0.97 | 0.96 | 0.84/0.85 | 0.93/0.97 | 1 | 0.94 |
| | p=30 | 0.93/0.98/0.87 | 0.93 | 0.89 | 0.66/0.67 | 0.76/0.92 | 1 | 0.76 |
| msnr | p=60 | 0.97/1/0.85 | - | 0.88 | 0.6/0.6 | 0.64/0.9 | 1 | 0.7 |
| | p=180 | 0.74/1/0.83 | - | 0.88 | 0.48/0.48 | 0.31/0.88 | 0.97 | 0.59 |
| | p=14 | 0.9/0.91/0.94 | 0.99 | 0.95 | 0.95/0.95 | 1/0.95 | 0.98 | 0.92 |
| lsnr | p=30 | 0.9/0.91/0.93 | 1 | 0.92 | 0.91/0.91 | 0.94/0.93 | 1 | 0.89 |
| 15111 | p=60 | 0.91/0.9/0.94 | - | 0.91 | 0.9/0.89 | 0.81/0.93 | 1 | 0.87 |
| | p=180 | 0.81/0.92/0.96 | - | 0.9 | 0.91/0.89 | 0.55/0.92 | 1 | 0.87 |
| | | | S | parsistenc | y (number of extra va | riables) | | |
| | p=14 | 5.2(1.9)/5.1(1.4)/5.5(0.9) | 5.5(0.9) | 5.4(1) | 5.9(4.6)/6(5.4) | 5.7(1.3)/5.4(1.9) | 5.4(1.4) | 5.2(1.4) |
| hsnr | p=30 | 4.5(0.9)/4.4(0.2)/5(1) | 5(1) | 4.8(1.1) | 5.7(10.4)/5.7(12) | 5.4(3.6)/4.8(2.3) | 4.8(2.1) | 4.5(1.8) |
| nsnr | p=60 | 4.4(0.3)/4.2(0.1)/4.7(0.8) | - | 4.6(0.8) | 5.6(15)/5.7(17.8) | 5.5(7.4)/4.7(2.3) | 4.8(2.8) | 4.4(1.6) |
| | p=180 | 4.3(11.4)/4(0)/4.2(0.5) | - | 4.1(0.5) | 5.1(20.2)/5.3(27.9) | 5.2(35.3)/4.2(2.1) | 4.2(3.5) | 4.1(0.8) |
| | p=14 | 4.7(1.6)/4.6(1.3)/4.4(0.6) | 4.5(0.7) | 4.5(0.7) | 5.4(4.2)/5.5(5) | 4.7(1.1)/4.6(1.2) | 4.5(0.8) | 4.6(1.1) |
| msnr | p=30 | 4.2(1)/4.1(0.5)/4.2(0.7) | 4.2(0.7) | 4.2(1) | 5(9.3)/5.1(10.7) | 4.5(3.1)/4.2(1.4) | 4.2(1.2) | 4.3(2.9) |
| msnr | p=60 | 4.1(0.4)/4(0.2)/4.1(0.6) | - | 4.1(0.8) | 4.8(13.6)/4.9(15.9) | 4.5(6.8)/4.1(1.6) | 4.1(1.8) | 4.1(3.8) |
| | p=180 | 4.1(10.7)/4(0.1)/4(0.4) | - | 4(0.6) | 4.5(19.3)/4.6(26.2) | 4.5(35.4)/4(1.7) | 4.1(2.6) | 4(5.2) |
| | p=14 | 4(2.7)/3.8(2.2)/3.3(0.8) | 3.3(0.8) | 3.3(1) | 4.5(3.6)/4.7(4.1) | 3.7(1.4)/3.5(1.7) | 3.4(1.4) | 3.7(2) |
| lsnr | p=30 | 2.7(2.3)/2.3(1)/2.7(1.3) | 2.6(1) | 2.6(1.5) | 3.6(6.9)/3.6(7.5) | 3.4(3.7)/2.9(3.3) | 2.8(2.9) | 2.9(4) |
| 15111 | p=60 | 1.9(1.1)/1.5(0.3)/2.3(1.2) | - | 2(1.1) | 2.9(8.5)/2.9(9.5) | 3.4(7.8)/2.4(4) | 2.5(3.9) | 2.4(5.2) |
| | p=180 | 1.7(12.7)/1(0.2)/1.6(0.9) | - | 1.3(0.8) | 2.2(10.7)/2.1(13.3) | 3.5(32.4)/1.9(6.4) | 2.1(6.5) | 1.9(8) |

Table S28: The performance of BOSS compared to other methods, Sparse-Ex4, ρ =0.5, n=2000

| | | BOSS C_n -hdf/AICc-hdf/CV | BS CV | FS CV | LASSO AICc/CV | Gamma LASSO AICc/CV | SparseNet CV | rLASSO CV |
|-------|-------|-----------------------------|----------|-------------|----------------------|------------------------|-----------------|--------------|
| İ | | | - | % worse th | an the best possible | BOSS | | |
| i | p=14 | 12/11/25 | 19 | 18 | 48/47 | 19/16 | 13 | 14 |
| | p=30 | 8/7/29 | 21 | 23 | 86/83 | 39/20 | 12 | 16 |
| hsnr | p=60 | 7/7/28 | - | 23 | 125/120 | 73/22 | 14 | 15 |
| | p=180 | 7/6/28 | - | 21 | 174/171 | 171/23 | 12 | 18 |
| | p=14 | 33/33/26 | 18 | 20 | 44/42 | 20/23 | 18 | 34 |
| | p=30 | 40/39/33 | 21 | 31 | 71/69 | 43/35 | 26 | 54 |
| msnr | p=60 | 42/43/35 | - | 42 | 93/90 | 76/44 | 31 | 69 |
| | p=180 | 41/42/33 | - | 46 | 105/102 | 153/48 | 37 | 67 |
| | p=14 | 22/22/30 | 21 | 21 | 36/35 | 24/20 | 17 | 19 |
| 1 | p=30 | 14/13/30 | 22 | 23 | 61/59 | 55/20 | 15 | 19 |
| lsnr | p=60 | 11/10/28 | - | 21 | 89/85 | 104/21 | 13 | 20 |
| | p=180 | 8/8/27 | - | 20 | 125/121 | 242/19 | 10 | 26 |
| | | | | I | Relative efficiency | | | |
| | p=14 | 1/1/0.89 | 0.94 | 0.95 | 0.75/0.76 | 0.94/0.96 | 0.99 | 0.98 |
| ١, | p=30 | 1/1/0.83 | 0.89 | 0.87 | 0.58/0.59 | 0.77/0.89 | 0.96 | 0.93 |
| hsnr | p=60 | 1/1/0.83 | - | 0.87 | 0.47/0.48 | 0.62/0.87 | 0.93 | 0.92 |
| | p=180 | 1/1/0.83 | - | 0.88 | 0.39/0.39 | 0.39/0.87 | 0.95 | 0.9 |
| | p=14 | 0.88/0.88/0.93 | 1 | 0.98 | 0.82/0.83 | 0.99/0.96 | 1 | 0.88 |
| | p=30 | 0.87/0.87/0.91 | 1 | 0.93 | 0.71/0.72 | 0.85/0.9 | 0.97 | 0.79 |
| msnr | p=60 | 0.92/0.92/0.98 | - | 0.92 | 0.68/0.69 | 0.75/0.91 | 1 | 0.77 |
| | p=180 | 0.94/0.94/1 | - | 0.91 | 0.65/0.66 | 0.53/0.9 | 0.97 | 0.8 |
| | p=14 | 0.96/0.96/0.9 | 0.97 | 0.96 | 0.86/0.87 | 0.94/0.98 | 1 | 0.98 |
| lsnr | p=30 | 0.99/1/0.87 | 0.93 | 0.92 | 0.7/0.71 | 0.73/0.95 | 0.99 | 0.95 |
| ISIII | p=60 | 1/1/0.86 | - | 0.91 | 0.58/0.59 | 0.54/0.91 | 0.98 | 0.92 |
| | p=180 | 0.99/1/0.85 | - | 0.9 | 0.48/0.49 | 0.32/0.91 | 0.98 | 0.86 |
| | | | S_1 | parsistency | (number of extra var | riables) | | |
| | p=14 | 6(0.6)/6(0.5)/6(0.6) | 6(0.7) | 6(0.6) | 6(4.7)/6(5.5) | 6(1)/6(1) | 6(0.6) | 6(0.5) |
| hsnr | p=30 | 6(0.2)/6(0.2)/6(0.6) | 6(0.6) | 6(0.6) | 6(10.9)/6(11.3) | 6(2.7)/6(1.4) | 6(0.8) | 6(0.5) |
| IISHF | p=60 | 6(0.1)/6(0.1)/6(0.5) | - | 6(0.5) | 6(18)/6(17.7) | 6(6.4)/6(1.5) | 6(1.1) | 6(0.4) |
| | p=180 | 6(0.1)/6(0.1)/6(0.3) | - | 6(0.3) | 6(32.2)/6(29.8) | 6(22.3)/6(1.3) | 6(1.3) | 6(0.4) |
| | p=14 | 5.9(2.1)/5.9(2)/6(0.7) | 5.9(0.7) | 5.9(0.9) | 6(4.8)/6(5.5) | 6(1.2)/5.9(1.9) | 5.9(1.1) | 5.9(1.7) |
| menr | p=30 | 5.6(1.1)/5.6(1)/5.9(0.8) | 5.9(0.7) | 5.8(1) | 6(10.9)/6(11.3) | 6(3.3)/5.8(2.8) | 5.8(2) | 5.6(2.2) |
| msnr | p=60 | 5.4(0.4)/5.3(0.3)/5.8(0.8) | - | 5.6(1.1) | 6(18)/6(17.6) | 6(7.7)/5.6(3.7) | 5.7(3.1) | 5.3(2.3) |
| | p=180 | 4.8(0.2)/4.8(0.2)/5.5(1) | - | 5.1(0.8) | 5.9(31.7)/5.9(29) | 6(26.5)/5.1(4.5) | 5.2(4.7) | 4.7(2) |
| | p=14 | 4.6(1.4)/4.6(1.3)/4.6(0.7) | 4.6(0.7) | 4.6(0.8) | 5.5(4.4)/5.5(5) | 4.9(1.3)/4.6(1.2) | 4.5(0.8) | 4.4(0.8) |
| lsnr | p=30 | 4.2(0.5)/4.2(0.4)/4.3(0.7) | 4.3(0.6) | 4.2(0.7) | 5.2(9.6)/5.3(9.9) | 4.8(3.6)/4.3(1.1) | 4.3(1) | 4.2(0.8) |
| ISIII | p=60 | 4.1(0.2)/4.1(0.2)/4.2(0.5) | - | 4.1(0.5) | 5(15.5)/5(14.7) | 4.8(8.2)/4.1(1.2) | 4.1(1.2) | 4.1(0.9) |
| | p=180 | 4(0.1)/4(0.1)/4(0.4) | - | 4(0.4) | 4.6(26.1)/4.6(23.6) | 4.8(27.9)/4(1) | 4.1(1.3) | 4(0.9) |

Table S29: The performance of BOSS compared to other methods, Sparse-Ex4, ρ =0.9, n=200

| | | BOSS C_p -hdf/AICc-hdf/CV | BS CV | FS CV | LASSO AICc/CV | Gamma LASSO AICc/CV | SparseNet CV | rLASSO CV |
|----------|-------|-----------------------------|----------|------------|-----------------------|------------------------|-----------------|--------------|
| | | | | | han the best possible | , | | |
| <u>'</u> | p=14 | 34/33/29 | 24 | 46 | 45/44 | 33/43 | 40 | 53 |
| | p=30 | 25/21/33 | 21 | 56 | 73/71 | 40/36 | 28 | 58 |
| hsnr | p=60 | 23/22/37 | - | 57 | 95/91 | 50/31 | 22 | 64 |
| | p=180 | 27/7/34 | - | 68 | 123/110 | 91/2 | -10 | 62 |
| | p=14 | 29/27/28 | 15 | 33 | 41/39 | 23/28 | 16 | 39 |
| | p=30 | 25/19/30 | -4 | 52 | 61/60 | 29/23 | 3 | 56 |
| msnr | p=60 | 22/14/24 | - | 83 | 90/86 | 57/38 | 16 | 91 |
| | p=180 | 31/17/26 | - | 66 | 78/66 | 78/26 | 6 | 70 |
| | p=14 | 41/39/31 | 27 | 54 | 51/50 | 46/47 | 38 | 55 |
| lsnr | p=30 | 39/32/27 | 18 | 78 | 71/72 | 58/66 | 44 | 75 |
| ISIII | p=60 | 29/28/23 | - | 81 | 80/80 | 79/79 | 57 | 84 |
| | p=180 | 37/17/18 | - | 36 | 33/33 | 110/37 | 35 | 36 |
| | | | | | Relative efficiency | | | |
| | p=14 | 0.93/0.94/0.96 | 1 | 0.85 | 0.86/0.86 | 0.94/0.87 | 0.89 | 0.81 |
| hsnr | p=30 | 0.97/1/0.91 | 1 | 0.78 | 0.7/0.71 | 0.87/0.9 | 0.95 | 0.77 |
| nsnr | p=60 | 0.99/1/0.89 | - | 0.77 | 0.62/0.64 | 0.81/0.93 | 0.99 | 0.74 |
| | p=180 | 0.71/0.84/0.68 | - | 0.54 | 0.41/0.43 | 0.47/0.88 | 1 | 0.56 |
| | p=14 | 0.89/0.91/0.9 | 1 | 0.87 | 0.82/0.83 | 0.93/0.9 | 0.99 | 0.83 |
| | p=30 | 0.77/0.81/0.74 | 1 | 0.63 | 0.6/0.6 | 0.75/0.78 | 0.93 | 0.62 |
| msnr | p=60 | 0.93/1/0.92 | - | 0.62 | 0.6/0.61 | 0.73/0.83 | 0.99 | 0.6 |
| | p=180 | 0.81/0.9/0.84 | - | 0.64 | 0.59/0.64 | 0.59/0.84 | 1 | 0.62 |
| | p=14 | 0.9/0.91/0.97 | 1 | 0.83 | 0.84/0.84 | 0.87/0.86 | 0.92 | 0.82 |
| lsnr | p=30 | 0.85/0.89/0.93 | 1 | 0.66 | 0.69/0.69 | 0.75/0.71 | 0.82 | 0.67 |
| 15111 | p=60 | 0.95/0.97/1 | - | 0.68 | 0.69/0.68 | 0.69/0.69 | 0.78 | 0.67 |
| | p=180 | 0.86/1/0.99 | - | 0.86 | 0.88/0.88 | 0.56/0.86 | 0.87 | 0.86 |
| | | | S | parsistenc | y (number of extra va | ariables) | | |
| | p=14 | 5.8(2.9)/5.7(2.5)/5.6(1.6) | 5.6(0.8) | 5.3(2) | 6(6.5)/6(7.2) | 5.5(2.3)/5.4(3.4) | 5.3(2.4) | 5.4(3.2) |
| hsnr | p=30 | 5.2(3.7)/5.1(2.8)/5.3(3.8) | 5(1) | 4.8(4.1) | 5.8(17.8)/5.8(19.5) | 4.9(4.5)/4.5(3.4) | 4.4(2.7) | 4.8(6.8) |
| nsnr | p=60 | 5(4.2)/4.8(3)/4.9(4.7) | - | 4.5(4.3) | 5.6(30.2)/5.7(35.1) | 4.9(8.8)/4.3(3.6) | 4.3(3.3) | 4.3(8.7) |
| | p=180 | 4.4(13.2)/4.2(2.4)/4.3(4.3) | - | 4.3(8) | 4.6(44.2)/4.8(64.9) | 4.4(29.2)/4.1(4) | 4.1(3.1) | 4.1(15.4) |
| | p=14 | 5(2.5)/4.9(2.2)/4.7(1.4) | 4.6(0.7) | 4.9(2.4) | 5.6(6.3)/5.7(7) | 4.6(1.8)/4.9(3.3) | 4.6(2.4) | 5(3.9) |
| msnr | p=30 | 4.5(4.5)/4.4(3.6)/4.5(3.7) | 4.2(0.7) | 4.6(6.5) | 5.2(16.9)/5.3(18.5) | 4.4(4.7)/4.5(7) | 4.4(5.8) | 4.8(11.2) |
| 1115111 | p=60 | 4.3(5.9)/4.2(5.1)/4.3(5.7) | - | 3.7(6.3) | 4.8(28.3)/5(32.8) | 4.4(10.4)/4.2(11.8) | 4.3(11.7) | 4.1(17.8) |
| | p=180 | 4.1(24.5)/3.6(7.6)/3.7(9.2) | - | 3(8.8) | 3.8(37.7)/4.3(59.6) | 4.3(37.5)/3.6(20.4) | 3.8(22.8) | 3.2(26) |
| | p=14 | 4.2(3)/4(2.7)/3.8(1.9) | 3.3(0.7) | 3.9(2.9) | 4.9(5.9)/5.1(6.5) | 3.8(2.6)/4.1(4.1) | 3.7(3.2) | 4.4(4.7) |
| lsnr | p=30 | 3.1(5.5)/2.7(3.9)/3.2(5) | 2.7(0.9) | 2.2(4.4) | 3(10.1)/3(11) | 3.3(7.6)/2.8(8) | 2.9(8) | 2.6(8.5) |
| 15111 | p=60 | 2.2(5.3)/1.9(3.9)/2.6(6.8) | - | 0.9(2) | 1.2(7.4)/1.2(8.4) | 2.8(12.8)/1.3(6.6) | 2(10) | 1.1(6.4) |
| | p=180 | 1.4(18.2)/0.7(1.7)/1.1(5.5) | - | 0.2(0.6) | 0.3(4.8)/0.3(5.4) | 2.3(40.2)/0.3(4.4) | 0.6(9) | 0.3(4.4) |

Table S30: The performance of BOSS compared to other methods, Sparse-Ex4, ρ =0.9, n=2000

| | | BOSS C_n -hdf/AICc-hdf/CV | BS CV | FS CV | LASSO AICc/CV | Gamma LASSO AICc/CV | SparseNet CV | rLASSO CV |
|-------|-------|-------------------------------|------------------|-------------|------------------------|------------------------|-----------------|--------------|
| | | P / / | Ç | % worse th | an the best possible I | BOSS | | |
| | p=14 | 33/33/27 | 16 | 20 | 53/51 | 17/20 | 15 | 27 |
| | p=30 | 33/32/33 | 16 | 33 | 108/106 | 26/22 | 12 | 46 |
| hsnr | p=60 | 27/26/30 | - | 48 | 157/154 | 37/22 | 9 | 73 |
| | p=180 | 15/15/25 | - | 90 | 226/223 | 68/33 | 10 | 140 |
| | p=14 | 28/28/22 | 18 | 45 | 53/51 | 26/39 | 30 | 57 |
| | p=30 | 22/22/26 | 23 | 89 | 108/105 | 56/75 | 55 | 109 |
| msnr | p=60 | 21/21/27 | - | 114 | 166/162 | 100/107 | 92 | 124 |
| | p=180 | 25/25/30 | - | 107 | 253/250 | 190/110 | 105 | 106 |
| | p=14 | 33/33/32 | 20 | 29 | 45/44 | 24/28 | 19 | 37 |
| 1 | p=30 | 28/27/34 | 16 | 40 | 85/82 | 44/30 | 12 | 57 |
| lsnr | p=60 | 19/19/30 | - | 59 | 122/119 | 75/32 | 9 | 89 |
| | p=180 | 15/14/27 | - | 104 | 179/176 | 167/48 | 20 | 159 |
| | | | | F | Relative efficiency | | | |
| | p=14 | 0.86/0.86/0.9 | 0.99 | 0.96 | 0.75/0.76 | 0.98/0.95 | 1 | 0.91 |
| ١, | p=30 | 0.84/0.84/0.84 | 0.96 | 0.84 | 0.54/0.54 | 0.89/0.92 | 1 | 0.77 |
| hsnr | p=60 | 0.86/0.86/0.84 | - | 0.74 | 0.42/0.43 | 0.8/0.89 | 1 | 0.63 |
| | p=180 | 0.95/0.96/0.88 | - | 0.58 | 0.34/0.34 | 0.65/0.82 | 1 | 0.46 |
| | p=14 | 0.92/0.92/0.97 | 1 | 0.81 | 0.77/0.78 | 0.94/0.85 | 0.91 | 0.76 |
| | p=30 | 0.99/1/0.96 | 0.99 | 0.64 | 0.58/0.59 | 0.78/0.7 | 0.78 | 0.58 |
| msnr | p=60 | 1/1/0.95 | - | 0.56 | 0.45/0.46 | 0.6/0.58 | 0.63 | 0.54 |
| | p=180 | 1/1/0.96 | - | 0.6 | 0.35/0.36 | 0.43/0.6 | 0.61 | 0.61 |
| | p=14 | 0.9/0.9/0.9 | 1 | 0.92 | 0.82/0.83 | 0.96/0.93 | 1 | 0.87 |
| lsnr | p=30 | 0.87/0.88/0.83 | 0.97 | 0.8 | 0.61/0.61 | 0.78/0.86 | 1 | 0.71 |
| 15111 | p=60 | 0.92/0.92/0.84 | - | 0.69 | 0.49/0.5 | 0.62/0.83 | 1 | 0.58 |
| | p=180 | 1/1/0.9 | - | 0.56 | 0.41/0.41 | 0.43/0.77 | 0.95 | 0.44 |
| | | | S_{I} | parsistency | (number of extra var | riables) | | |
| | p=14 | 6(1.4)/6(1.4)/6(0.6) | 6(0.7) | 6(0.9) | 6(6.6)/6(7.2) | 6(1.2)/6(1.8) | 6(0.9) | 6(1.4) |
| 1 | p=30 | 6(0.5)/6(0.4)/6(0.7) | 6(0.6) | 6(1.3) | 6(17.8)/6(18.9) | 6(2.6)/6(2.5) | 6(1.6) | 6(2.4) |
| hsnr | p=60 | 6(0.4)/6(0.4)/6(0.8) | - | 6(2) | 6(34.2)/6(35.3) | 6(5.8)/6(3.9) | 6(3.1) | 6(4.1) |
| | p=180 | 6(1.4)/6(1.4)/6(1.7) | - | 5.9(3.8) | 6(72.7)/6(73.8) | 6(17.2)/6(9.4) | 6(8.7) | 5.9(9.4) |
| | p=14 | 6(2)/6(2)/6(1.3) | 6(0.7) | 5.9(2.4) | 6(6.6)/6(7.2) | 6(2.4)/5.9(4.1) | 5.9(2.9) | 5.8(3.9) |
| msnr | p=30 | 5.9(2.4)/5.9(2.4)/5.9(2.6) | 5.9(0.7) | 5.4(3.4) | 6(17.8)/6(18.8) | 5.9(5.9)/5.6(7.2) | 5.6(6.2) | 5.1(5.6) |
| msnr | p=60 | 5.8(4.8)/5.8(4.8)/5.9(5.6) | - | 4.7(1.9) | 6(34)/6(35.1) | 5.8(12.4)/4.9(7.7) | 5(8.3) | 4.3(2.6) |
| | p=180 | 5.5(12.9)/5.5(12.7)/5.7(16.2) | - | 4.2(0.6) | 5.7(68.6)/5.7(69.3) | 5.4(31.9)/4.2(3.4) | 4.3(5) | 4(0.3) |
| | p=14 | 5(2.5)/5(2.4)/4.7(1.1) | 4.6(0.7) | 4.6(1.5) | 5.7(6.4)/5.7(7) | 4.6(1.5)/4.7(2.4) | 4.5(1.5) | 4.7(2.6) |
| lsnr | p=30 | 4.5(2.1)/4.4(1.9)/4.4(1.7) | 4.3(0.6) | 4.3(2.2) | 5.4(16.6)/5.4(17.6) | 4.5(3.7)/4.3(3.5) | 4.2(2.5) | 4.4(4.6) |
| 15111 | p=60 | 4.2(1.9)/4.2(1.8)/4.3(2.3) | - | 4.2(3.2) | 5.1(30.6)/5.1(31.3) | 4.3(8.1)/4.2(5.8) | 4.2(5) | 4.3(8.8) |
| | p=180 | 4.1(3.7)/4.1(3.6)/4.1(4.4) | - | 3.7(3.7) | 4.6(60.3)/4.6(60.5) | 4.3(26.8)/4.1(14.8) | 4.2(14.2) | 3.6(13.7) |

Table S31: The performance of BOSS compared to other methods, Dense, ρ =0, n=200

| | | $\begin{array}{ c c c c c c c c c c c c c c c c c c c$ | BS CV | FS CV | LASSO AICc/CV | Gamma LASSO AICc/CV | SparseNet CV | rLASSO CV |
|----------|-------|--|----------|----------|------------------|------------------------|-----------------|-----------|
| | | | | | | possible BOSS | | |
| <u> </u> | p=14 | 0/0/0 | 0 | 0 | 0/0 | 0/1 | 0 | 0 |
| | p=30 | 2/2/7 | 8 | 7 | 1/1 | 8/2 | 4 | 4 |
| hsnr | p=60 | 9/11/11 | - | 11 | 0/-2 | -1/-1 | 1 | 2 |
| | p=180 | 18/13/11 | - | 12 | 18/12 | 5/5 | 3 | 13 |
| | p=14 | 0/0/6 | 6 | 6 | 1/1 | 7/1 | 3 | 3 |
| | p=30 | 4/5/10 | 10 | 10 | 0/-1 | 8/2 | 4 | 3 |
| msnr | p=60 | 11/12/12 | - | 12 | -3/-5 | -1/-2 | -1 | -1 |
| | p=180 | 19/14/13 | - | 12 | 3/0 | 13/1 | 2 | 5 |
| | p=14 | 7/9/20 | 19 | 20 | 3/3 | 17/8 | 10 | 10 |
| lsnr | p=30 | 15/19/16 | 16 | 16 | -8/-8 | 5/-1 | -3 | -3 |
| ISIII | p=60 | 16/14/14 | - | 14 | -9/-8 | 11/-4 | -4 | -4 |
| | p=180 | 22/7/8 | - | 9 | -5/-3 | 65/0 | -1 | 0 |
| | | | | | Relative effic | iency | | |
| | p=14 | 1/1/1 | 1 | 1 | 1/1 | 1/0.99 | 1 | 1 |
| homm | p=30 | 0.99/0.99/0.95 | 0.94 | 0.94 | 1/1 | 0.93/0.99 | 0.97 | 0.98 |
| hsnr | p=60 | 0.9/0.88/0.89 | - | 0.89 | 0.98/1 | 1/0.99 | 0.98 | 0.96 |
| | p=180 | 0.88/0.91/0.93 | - | 0.93 | 0.88/0.93 | 0.99/0.99 | 1 | 0.92 |
| | p=14 | 1/1/0.95 | 0.95 | 0.95 | 1/1 | 0.94/0.99 | 0.97 | 0.98 |
| | p=30 | 0.96/0.95/0.91 | 0.9 | 0.91 | 0.99/1 | 0.92/0.98 | 0.96 | 0.96 |
| msnr | p=60 | 0.86/0.85/0.85 | - | 0.85 | 0.98/1 | 0.96/0.97 | 0.96 | 0.96 |
| | p=180 | 0.84/0.88/0.89 | - | 0.89 | 0.97/1 | 0.88/0.98 | 0.98 | 0.95 |
| | p=14 | 0.96/0.94/0.86 | 0.86 | 0.85 | 0.99/1 | 0.88/0.95 | 0.93 | 0.93 |
| ١, | p=30 | 0.8/0.77/0.79 | 0.79 | 0.79 | 1/1 | 0.88/0.93 | 0.94 | 0.94 |
| lsnr | p=60 | 0.79/0.8/0.8 | - | 0.8 | 1/1 | 0.83/0.95 | 0.96 | 0.96 |
| | p=180 | 0.78/0.89/0.88 | - | 0.88 | 1/0.98 | 0.58/0.95 | 0.96 | 0.95 |
| | | | Spar | sistenc | y (number o | f extra variables) | | |
| | p=14 | 14/14/14 | 14 | 14 | 14/14 | 14/14 | 14 | 14 |
| ١, | p=30 | 29.2/29/26 | 25.7 | 25.9 | 28.6/29.2 | 25.3/28.6 | 27.2 | 26.8 |
| hsnr | p=60 | 35.8/24.3/28 | - | 27.6 | 40.5/44.9 | 29.8/38.4 | 36.8 | 32.8 |
| | p=180 | 36.9/17/19.3 | - | 19.2 | 47.5/67.6 | 38.7/36.4 | 32.4 | 36.5 |
| | p=14 | 14/14/13.4 | 13.4 | 13.4 | 13.9/13.9 | 13.4/13.9 | 13.6 | 13.7 |
| | p=30 | 26.9/26/21.1 | 20.7 | 20.9 | 25.1/26.3 | 18.8/24.9 | 23.7 | 22.6 |
| msnr | p=60 | 26/14.9/18.4 | - | 18.3 | 32.2/36.4 | 22.7/29.2 | 29.6 | 25 |
| | p=180 | 30.7/7.9/9.9 | - | 9.9 | 33.8/49.1 | 40.6/30.1 | 27.9 | 25.8 |
| | p=14 | 12.2/11.8/8.3 | 8.4 | 8.2 | 10.6/11.2 | 7.6/10.4 | 10 | 9.1 |
| lsnr | p=30 | 13/7.8/8 | 7.5 | 7.8 | 14/15.1 | 10.3/12.3 | 12.7 | 10.6 |
| ISIII | p=60 | 5.4/1/4.2 | - | 4.1 | 15.2/16.6 | 15.3/13.7 | 14.6 | 12.2 |
| | p=180 | 16.6/0.3/1.4 | - | 1.5 | 12.4/15.8 | 41.6/12.2 | 13.5 | 11.3 |

Table S32: The performance of BOSS compared to other methods, Dense, ρ =0, n=2000

| | | BOSS C _p -hdf/AICc-hdf/CV | BS CV | FS CV | LASSO AICc/CV | Gamma LASSO AICc/CV | SparseNet CV | rLASSO CV |
|------|-------|---|----------|----------|------------------|------------------------|-----------------|-----------|
| i | | | % v | worse t | han the best | possible BOSS | | |
| | p=14 | 0/0/0 | 0 | 0 | 2/2 | 1/4 | 0 | 0 |
| | p=30 | 0/0/1 | 1 | 1 | 1/1 | 3/6 | 1 | 1 |
| hsnr | p=60 | 5/5/7 | - | 7 | 1/0 | 0/0 | 3 | 4 |
| | p=180 | 7/7/9 | - | 9 | 15/14 | 3/5 | 2 | 9 |
| | p=14 | 0/0/0 | 0 | 0 | 0/0 | 0/2 | 0 | 0 |
| | p=30 | 1/1/5 | 5 | 5 | 1/1 | 4/2 | 3 | 3 |
| msnr | p=60 | 8/8/9 | - | 9 | 1/0 | -1/0 | 3 | 4 |
| | p=180 | 8/8/10 | - | 10 | 13/12 | 3/4 | 3 | 7 |
| | p=14 | 0/0/4 | 4 | 4 | 0/0 | 3/1 | 3 | 3 |
| 1, | p=30 | 3/3/10 | 10 | 9 | 1/0 | 7/2 | 5 | 5 |
| lsnr | p=60 | 13/13/12 | - | 12 | 0/-1 | 0/1 | 3 | 3 |
| | p=180 | 9/9/12 | - | 13 | 9/8 | 14/5 | 4 | 7 |
| | | | | | Relative effic | eiency | | |
| | p=14 | 1/1/1 | 1 | 1 | 0.98/0.98 | 0.99/0.96 | 1 | 1 |
| , | p=30 | 1/1/0.99 | 0.99 | 0.99 | 0.99/0.99 | 0.97/0.94 | 0.99 | 0.99 |
| hsnr | p=60 | 0.95/0.95/0.93 | - | 0.93 | 0.99/0.99 | 1/1 | 0.97 | 0.96 |
| | p=180 | 0.95/0.96/0.94 | - | 0.94 | 0.89/0.9 | 0.99/0.98 | 1 | 0.94 |
| | p=14 | 1/1/1 | 1 | 1 | 1/1 | 1/0.99 | 1 | 1 |
| | p=30 | 1/1/0.96 | 0.96 | 0.96 | 1/1 | 0.97/0.99 | 0.97 | 0.97 |
| msnr | p=60 | 0.92/0.92/0.91 | - | 0.91 | 0.98/0.99 | 1/0.99 | 0.96 | 0.96 |
| | p=180 | 0.95/0.95/0.93 | - | 0.93 | 0.91/0.92 | 1/0.99 | 1 | 0.96 |
| | p=14 | 1/1/0.96 | 0.96 | 0.96 | 1/1 | 0.98/0.99 | 0.98 | 0.97 |
| lsnr | p=30 | 0.97/0.97/0.91 | 0.91 | 0.92 | 1/1 | 0.94/0.98 | 0.96 | 0.96 |
| Isnr | p=60 | 0.88/0.88/0.88 | - | 0.88 | 0.99/1 | 0.99/0.99 | 0.96 | 0.96 |
| | p=180 | 0.95/0.96/0.93 | - | 0.93 | 0.96/0.97 | 0.91/1 | 1 | 0.97 |
| | | | Spar | sistenc | y (number o | f extra variables) | | |
| | p=14 | 14/14/14 | 14 | 14 | 14/14 | 14/14 | 14 | 14 |
| ١, | p=30 | 30/30/29.8 | 29.8 | 29.8 | 30/30 | 30/30 | 29.9 | 29.9 |
| hsnr | p=60 | 50.1/49.6/39.8 | - | 39.7 | 53.1/54.3 | 46.4/50.2 | 44.8 | 42.6 |
| | p=180 | 32.5/31.6/32.3 | - | 32.1 | 88.1/88.8 | 62.2/60.9 | 46.4 | 38.7 |
| | p=14 | 14/14/14 | 14 | 14 | 14/14 | 14/14 | 14 | 14 |
| | p=30 | 29.8/29.8/28.1 | 28.2 | 28.1 | 29.6/29.8 | 28.9/29.7 | 28.7 | 28.7 |
| msnr | p=60 | 42/41.1/31.3 | - | 31.1 | 48.1/49.1 | 37.1/43.5 | 37.5 | 34.2 |
| | p=180 | 23.9/23.2/24.1 | - | 24.1 | 75.1/74.9 | 51.3/44.6 | 38.9 | 29.6 |
| | p=14 | 14/14/13.7 | 13.7 | 13.7 | 14/14 | 13.8/14 | 13.8 | 13.8 |
| Ι, | p=30 | 27.8/27.8/22.1 | 21.9 | 22.1 | 26.8/27.5 | 21/26.2 | 24.6 | 23.4 |
| lsnr | p=60 | 30/28.5/19.9 | - | 19.5 | 38.5/38.9 | 25.4/31.4 | 29.1 | 25.3 |
| | p=180 | 14.1/13.5/14.1 | - | 14 | 55.3/53.9 | 42/31.8 | 29.7 | 23.4 |

Table S33: The performance of BOSS compared to other methods, Dense, ρ =0.5, n=200

| | | BOSS C _p -hdf/AICc-hdf/CV | BS CV | FS CV | LASSO AICc/CV | Gamma LASSO AICc/CV | SparseNet CV | rLASSO CV |
|-------|-------|---|----------|----------|------------------|------------------------|-----------------|-----------|
| İ | | | % v | worse t | han the best | possible BOSS | | |
| | p=14 | 0/0/4 | 0 | 0 | 0/0 | 1/2 | 0 | -1 |
| | p=30 | 1/1/8 | 9 | 8 | 2/1 | 6/2 | 5 | 1 |
| hsnr | p=60 | 13/13/12 | - | 12 | 10/7 | 5/5 | 7 | 4 |
| | p=180 | 37/14/13 | - | 16 | 47/27 | 10/13 | 8 | 7 |
| | p=14 | 0/0/5 | 5 | 4 | 0/0 | 2/1 | 2 | 1 |
| | p=30 | 4/5/10 | 11 | 10 | 4/3 | 8/4 | 8 | 3 |
| msnr | p=60 | 16/15/14 | - | 14 | 11/6 | 4/6 | 7 | 4 |
| | p=180 | 43/14/14 | - | 17 | 37/21 | 18/18 | 11 | 14 |
| | p=14 | 5/7/17 | 19 | 17 | 9/7 | 16/8 | 14 | 12 |
| lsnr | p=30 | 18/18/17 | 16 | 18 | 10/7 | 10/10 | 11 | 7 |
| 15111 | p=60 | 17/13/13 | - | 14 | 6/5 | 19/8 | 8 | 5 |
| | p=180 | 47/4/8 | - | 9 | 2/4 | 79/6 | 6 | 4 |
| | | | | | Relative effic | eiency | | |
| | p=14 | 0.99/0.99/0.95 | 0.99 | 0.99 | 0.99/0.99 | 0.99/0.97 | 0.99 | 1 |
| , | p=30 | 0.98/0.98/0.93 | 0.91 | 0.93 | 0.98/0.98 | 0.94/0.98 | 0.94 | 0.98 |
| hsnr | p=60 | 0.92/0.92/0.93 | - | 0.93 | 0.95/0.98 | 0.99/0.99 | 0.97 | 1 |
| | p=180 | 0.78/0.94/0.95 | - | 0.92 | 0.73/0.84 | 0.97/0.95 | 0.99 | 1 |
| | p=14 | 1/1/0.95 | 0.95 | 0.96 | 1/1 | 0.98/0.99 | 0.98 | 0.99 |
| | p=30 | 0.98/0.98/0.93 | 0.92 | 0.93 | 0.99/1 | 0.95/0.98 | 0.95 | 0.99 |
| msnr | p=60 | 0.89/0.9/0.91 | - | 0.91 | 0.93/0.98 | 1/0.98 | 0.97 | 1 |
| | p=180 | 0.77/0.97/0.97 | - | 0.95 | 0.81/0.91 | 0.94/0.94 | 1 | 0.97 |
| | p=14 | 0.97/0.96/0.87 | 0.86 | 0.87 | 0.93/0.96 | 0.88/0.94 | 0.9 | 0.91 |
| lsnr | p=30 | 0.9/0.9/0.92 | 0.92 | 0.91 | 0.97/1 | 0.98/0.97 | 0.96 | 1 |
| ISH | p=60 | 0.9/0.93/0.93 | - | 0.93 | 0.99/1 | 0.88/0.98 | 0.97 | 1 |
| | p=180 | 0.69/0.97/0.94 | - | 0.94 | 1/0.98 | 0.57/0.96 | 0.96 | 0.98 |
| | | | Spar | sistenc | y (number o | f extra variables) | | |
| | p=14 | 14/14/14 | 14 | 14 | 14/14 | 14/14 | 14 | 14 |
| , | p=30 | 29.7/29.6/26.1 | 25.1 | 26 | 29.1/29.7 | 27/29.2 | 27 | 28 |
| hsnr | p=60 | 42/29.1/29.4 | - | 28.6 | 44.7/50.7 | 33.7/43.1 | 35 | 42 |
| | p=180 | 43.6/17/20.2 | - | 19.6 | 52.2/87.1 | 40.3/42.5 | 32.4 | 63.5 |
| | p=14 | 14/14/13.7 | 13.6 | 13.7 | 14/14 | 13.8/14 | 13.8 | 13.9 |
| | p=30 | 28.3/27.8/21.1 | 18.8 | 20.9 | 26.7/28.2 | 20.3/26.2 | 22.6 | 25.1 |
| msnr | p=60 | 34.4/17.9/19.9 | - | 19.6 | 34.7/43.5 | 24.7/33.7 | 27.1 | 35.8 |
| | p=180 | 36.7/8.3/11 | - | 9.7 | 24.5/61.4 | 39.6/28.9 | 22.1 | 47.6 |
| | p=14 | 13.1/12.7/9.4 | 8.7 | 9.3 | 10.8/12 | 8.7/11.4 | 10.3 | 10.6 |
| lame | p=30 | 13.4/5.7/7.5 | 6.6 | 7.1 | 5.3/12.9 | 11.8/11.8 | 10.3 | 11.4 |
| lsnr | p=60 | 4.8/0.6/3.5 | - | 3 | 3.7/11.2 | 15.7/9.4 | 8.9 | 8.7 |
| | p=180 | 19/0.2/1.1 | - | 0.9 | 2.7/8.6 | 38.9/7.2 | 6.9 | 5.9 |

Table S34: The performance of BOSS compared to other methods, Dense, ρ =0.5, n=2000

| $ \begin{array}{ c c c c c c c c c c c c c c c c c c c$ | | | BOSS | BS | FS | LASSO | Gamma LASSO | SparseNet | rLASSO |
|--|--------|-------|---------------------------------------|------|---------|-----------------|------------------|-----------|--------|
| $ \begin{array}{ c c c c c c c c c c c c c c c c c c c$ | | | | | | | | | |
| $\begin{array}{c ccccccccccccccccccccccccccccccccccc$ | l I | | · · · · · · · · · · · · · · · · · · · | | | | | | |
| $\begin{array}{ c c c c c c c c c c c c c c c c c c c$ | - | | 0.10.10 | | | | | | |
| $\begin{array}{c ccccccccccccccccccccccccccccccccccc$ | | 1 * | | | | , | , | | |
| $\begin{array}{ c c c c c c c c c c c c c c c c c c c$ | hsnr | 1 * | / / | | | , | , | | |
| $\begin{array}{ c c c c c c c c c c c c c c c c c c c$ | 110111 | 1 * | | | | | | | |
| $\begin{array}{ c c c c c c c c c c c c c c c c c c c$ | | p=180 | | | | · ' | | | |
| $\begin{array}{ c c c c c c c c c c c c c c c c c c c$ | | 1 * | , , | | | | , | | |
| $\begin{array}{ c c c c c c c c c c c c c c c c c c c$ | menr | * | , , | | | | , | | |
| $ \begin{array}{ c c c c c c c c c c c c c c c c c c c$ | mom | 1 * | , , | | | | | | |
| $\begin{array}{ c c c c c c c c c c c c c c c c c c c$ | | p=180 | 9/9/11 | - | 14 | 36/34 | 16/18 | 9 | 33 |
| $\begin{array}{ c c c c c c c c c c c c c c c c c c c$ | | 1 * | | | | , | | | |
| $\begin{array}{ c c c c c c c c c c c c c c c c c c c$ | lown | 1 * | , , | | | , | | | |
| $\begin{array}{ c c c c c c c c c }\hline & & & & & & & & & & & & & & & & & & &$ | ISH | 1 * | ' ' | - | | , | , | | |
| $\begin{array}{ c c c c c c c c c c } \hline & p=14 & 1/1/1 & 1 & 1 & 0.98/0.98 & 0.98/0.95 & 1 & 1 \\ p=30 & 0.98/0.98/0.96 & 0.98 & 0.98 & 0.97/0.97 & 0.9/0.89 & 0.98 & 0.99 \\ p=60 & 0.98/0.98/0.96 & - & 0.96 & 1/1 & 0.99/0.98 & 0.98 & 0.98 \\ p=180 & 1/1/0.99 & - & 0.96 & 0.79/0.79 & 0.9/0.89 & 1 & 0.81 \\ \hline & p=30 & 0.98/0.98/0.94 & 0.93 & 0.94 & 0.98/0.98 & 0.95/0.94 & 0.96 & 0.97 \\ msnr & p=60 & 0.95/0.95/0.95 & - & 0.95 & 0.98/0.98 & 1/1 & 0.98 & 0.96 \\ p=180 & 0.99/1/0.98 & - & 0.95 & 0.98/0.98 & 1/1 & 0.98 & 0.96 \\ p=180 & 0.99/1/0.98 & - & 0.95 & 0.8/0.81 & 0.93/0.92 & 1 & 0.81 \\ \hline & p=30 & 0.98/0.98/0.91 & 0.99 & 0.99 & 0.99 & 0.99 \\ p=180 & 0.99/1/0.97 & - & 0.95 & 0.8/0.81 & 0.93/0.97 & 0.93 & 0.96 \\ p=60 & 0.91/0.91/0.93 & - & 0.93 & 0.95/0.96 & 1/0.98 & 0.98 & 0.94 \\ p=180 & 0.99/1/0.97 & - & 0.95 & 0.83/0.85 & 0.93/0.93 & 1 & 0.85 \\ \hline & & & & & & & & & & & & & & & & & &$ | | p=180 | 11/11/13 | - | 16 | 32/30 | 19/18 | 10 | 30 |
| $\begin{array}{ c c c c c c c c c c c c c c c c c c c$ | | | | | | Relative effici | ency | | |
| $ \begin{array}{ c c c c c c c c } \hline hsnr & p=60 & 0.98/0.98/0.96 & - & 0.96 & 1/1 & 0.99/0.98 & 0.98 & 0.98 \\ p=180 & 1/1/0.99 & - & 0.96 & 0.79/0.79 & 0.9/0.89 & 1 & 0.81 \\ \hline & p=30 & 0.98/0.98/0.94 & 0.93 & 0.94 & 0.98/0.98 & 0.95/0.94 & 0.96 & 0.97 \\ p=60 & 0.95/0.95/0.95 & - & 0.95 & 0.98/0.98 & 1/1 & 0.98 & 0.96 \\ p=180 & 0.99/1/0.98 & - & 0.95 & 0.8/0.81 & 0.93/0.92 & 1 & 0.81 \\ \hline & p=30 & 0.98/0.98/0.91 & 0.9 & 0.91 & 0.98/0.98 & 0.93/0.97 & 0.93 & 0.96 \\ p=180 & 0.99/1/0.97 & - & 0.93 & 0.95/0.96 & 1/0.98 & 0.98 & 0.94 \\ p=180 & 0.99/1/0.97 & - & 0.95 & 0.83/0.85 & 0.93/0.93 & 1 & 0.85 \\ \hline & & & & & & & & & & & & & & & & & &$ | | p=14 | 1/1/1 | 1 | 1 | 0.98/0.98 | 0.98/0.95 | 1 | 1 |
| $\begin{array}{ c c c c c c c c c c c c c c c c c c c$ | ١, | p=30 | 0.98/0.98/0.96 | 0.98 | 0.98 | 0.97/0.97 | 0.9/0.89 | 0.98 | 0.99 |
| $\begin{array}{ c c c c c c c c c c c c c c c c c c c$ | hsnr | p=60 | 0.98/0.98/0.96 | - | 0.96 | 1/1 | 0.99/0.98 | 0.98 | 0.98 |
| $\begin{array}{ c c c c c c c c c c c c c c c c c c c$ | | p=180 | 1/1/0.99 | - | 0.96 | 0.79/0.79 | 0.9/0.89 | 1 | 0.81 |
| $\begin{array}{ c c c c c c c c c c c c c c c c c c c$ | | p=14 | 1/1/0.98 | 1 | 1 | 1/1 | 0.99/0.96 | 1 | 1 |
| $\begin{array}{ c c c c c c c c c c c c c c c c c c c$ | | p=30 | 0.98/0.98/0.94 | 0.93 | 0.94 | 0.98/0.98 | 0.95/0.94 | 0.96 | 0.97 |
| $ \begin{array}{ c c c c c c c c c c c c c c c c c c c$ | msnr | p=60 | 0.95/0.95/0.95 | - | 0.95 | 0.98/0.98 | 1/1 | 0.98 | 0.96 |
| $ \begin{array}{ c c c c c c c c c c c c c c c c c c c$ | | p=180 | 0.99/1/0.98 | - | 0.95 | 0.8/0.81 | 0.93/0.92 | 1 | 0.81 |
| $ \begin{array}{ c c c c c c c c c c c c c c c c c c c$ | | p=14 | 1/1/0.95 | 0.98 | 0.98 | 1/1 | 0.99/0.99 | 0.99 | 0.99 |
| $\begin{array}{ c c c c c c c c c c c c c c c c c c c$ | | p=30 | 0.98/0.98/0.91 | 0.9 | 0.91 | 0.98/0.98 | 0.93/0.97 | 0.93 | 0.96 |
| $\begin{array}{ c c c c c c c c c c c c c c c c c c c$ | Isnr | p=60 | 0.91/0.91/0.93 | - | 0.93 | | 1/0.98 | 0.98 | 0.94 |
| $\begin{array}{ c c c c c c c c c c c c c c c c c c c$ | | p=180 | 0.99/1/0.97 | - | 0.95 | 0.83/0.85 | 0.93/0.93 | 1 | 0.85 |
| $ \begin{array}{ c c c c c c c c c c c c c c c c c c c$ | | | | Spa | rsisten | cy (number of | extra variables) | | |
| $ \begin{array}{ c c c c c c c c c c c c c c c c c c c$ | | p=14 | 14/14/14 | 14 | 14 | 14/14 | 14/14 | 14 | 14 |
| $ \begin{array}{ c c c c c c c c c c c c c c c c c c c$ | | 1 * | , , | 30 | 30 | | 30/30 | 30 | 30 |
| $ \begin{array}{ c c c c c c c c c c c c c c c c c c c$ | hsnr | p=60 | 53.6/53.3/40.3 | - | 40 | , | | 43.8 | 49 |
| $\begin{array}{ c c c c c c c c c c c c c c c c c c c$ | | p=180 | 36/34.5/35.1 | - | 32.6 | 106.5/113.5 | 76.5/77.1 | 43 | 66.3 |
| $\begin{array}{ c c c c c c c c c c c c c c c c c c c$ | | p=14 | 14/14/14 | 14 | 14 | 14/14 | 14/14 | 14 | 14 |
| p=00 | | 1 * | , , | | | , | , | | |
| p=14 14/14/13.9 13.9 13.9 14/14 14/14 13.9 1 | msnr | p=60 | 47.5/46.6/31.6 | - | 31.2 | 51.5/53.4 | 42.1/48.1 | 36.3 | 43.6 |
| p=30 $29.1/29/22.7$ 21.2 22.1 $28/28.9$ $23/27.6$ 24.1 26.2 | | p=180 | 27.3/26.2/27.1 | - | 24.1 | 90.5/98.9 | 60/54.4 | 35.2 | 54.9 |
| p=30 $29.1/29/22.7$ 21.2 22.1 $28/28.9$ $23/27.6$ 24.1 26.2 | | p=14 | 14/14/13.9 | 13.9 | 13.9 | 14/14 | 14/14 | 13.9 | 13.9 |
| | | p=30 | 29.1/29/22.7 | 21.2 | 22.1 | 28/28.9 | 23/27.6 | | 26.2 |
| $\begin{array}{ c c c c c c c c c c c c c c c c c c c$ | lsnr | p=60 | 36.1/34.7/21.1 | - | 19.8 | 42.2/45.5 | 28.3/34.9 | 26.5 | 35.2 |
| p=180 17/16/17 - 14.3 61.8/72 43.7/33.1 25.3 46.9 | | p=180 | 17/16/17 | - | 14.3 | 61.8/72 | 43.7/33.1 | 25.3 | 46.9 |

Table S35: The performance of BOSS compared to other methods, Dense, ρ =0.9, n=200

| | | BOSS | BS | FS | LASSO | Gamma LASSO | SparseNet | rLASSO |
|---------|-------|------------------------|------|----------|----------------|--------------------|-----------|---------|
| | | C_p -hdf/AICc-hdf/CV | CV | CV | AICc/CV | AICc/CV | CV | CV |
| 1 | | | | | | possible BOSS | | |
| | | 1 0/0/2 | | | | * | | |
| | p=14 | 0/0/5 | 0 | 0 | 0/0 | 6/7 | 1 | 1 |
| hsnr | p=30 | 2/2/9 | 10 | 8 | 2/2 | 14/15 | 8 | 3 |
| 110111 | p=60 | 15/19/14 | - | 12 12 | 12/11 | 12/13 | 14 20 | 6 23 |
| | p=180 | 46/15/12 | - | | 71/43 | 23/24 | | |
| | p=14 | 1/1/7 | 8 | 6 | 2/1 | 8/8 | 5 | 5 |
| msnr | p=30 | 4/5/12 | 12 | 10 | 4/3 | 8/5 | 9 | 7 |
| 1115111 | p=60 | 20/23/16 | - | 13 | 30/17 | 12/15 | 15 | 18 |
| | p=180 | 58/26/15 | - | 17 | 61/46 | 31/37 | 26 | 44 |
| | p=14 | 11/13/18 | 19 | 18 | 11/10 | 13/12 | 18 | 16 |
| lsnr | p=30 | 19/15/14 | 15 | 13 | 10/11 | 19/12 | 12 | 15 |
| ISIII | p=60 | 14/11/12 | - | 12 | 9/12 | 34/13 | 12 | 4 |
| | p=180 | 59/12/10 | - | 10 | 15/17 | 106/12 | 9 | 10 |
| | | | | | Relative effic | iency | | |
| | p=14 | 0.99/0.99/0.95 | 0.99 | 0.99 | 0.99/0.99 | 0.94/0.93 | 0.99 | 0.99 |
| ١, | p=30 | 0.98/0.98/0.91 | 0.9 | 0.92 | 0.98/0.98 | 0.87/0.87 | 0.93 | 0.97 |
| hsnr | p=60 | 0.87/0.84/0.87 | - | 0.89 | 0.89/0.9 | 0.89/0.88 | 0.88 | 0.94 |
| | p=180 | 0.77/0.97/1 | - | 1 | 0.65/0.78 | 0.91/0.9 | 0.93 | 0.91 |
| | p=14 | 0.99/0.99/0.94 | 0.93 | 0.94 | 0.98/0.99 | 0.93/0.93 | 0.95 | 0.96 |
| | p=30 | 0.99/0.98/0.92 | 0.92 | 0.93 | 0.99/1 | 0.95/0.98 | 0.95 | 0.96 |
| msnr | p=60 | 0.93/0.92/0.97 | - | 0.99 | 0.86/0.96 | 1/0.97 | 0.98 | 0.95 |
| | p=180 | 0.73/0.91/1 | - | 0.98 | 0.71/0.79 | 0.88/0.84 | 0.91 | 0.8 |
| | p=14 | 0.93/0.91/0.87 | 0.87 | 0.88 | 0.94/0.94 | 0.91/0.93 | 0.88 | 0.89 |
| | p=30 | 0.92/0.96/0.97 | 0.96 | 0.97 | 1/1 | 0.92/0.98 | 0.98 | 0.96 |
| lsnr | p=60 | 0.91/0.94/0.93 | - | 0.93 | 0.96/0.93 | 0.78/0.93 | 0.93 | 1 |
| | p=180 | 0.69/0.97/0.99 | - | 1 | 0.95/0.93 | 0.53/0.98 | 1 | 1 |
| | | | Spar | sistenc | y (number o | f extra variables) | | |
| | p=14 | 14/14/14 | 14 | 14 | 14/14 | 14/14 | 14 | 14 |
| ١. | p=30 | 29.5/29.3/25.2 | 23 | 24.6 | 28.9/29.5 | 24.4/24.8 | 26.2 | 27.6 |
| hsnr | p=60 | 44.3/26.1/27.4 | - | 23.6 | 46.5/49.8 | 31.6/34.4 | 32.9 | 41.2 |
| | p=180 | 46.7/15.6/21.3 | - | 17.2 | 54.4/93.4 | 44.8/46.9 | 37.7 | 67.6 |
| | p=14 | 14/14/13.5 | 13.2 | 13.4 | 13.9/14 | 13.4/13.7 | 13.5 | 13.6 |
| | p=30 | 28.6/28/20.2 | 16.6 | 19 | 26.4/27.9 | 19.3/24.4 | 22.3 | 24.5 |
| msnr | p=60 | 33/13/18.4 | - | 14.9 | 30.3/42.2 | 24.7/32.3 | 25.8 | 34.3 |
| | p=180 | 41.6/5.8/14.1 | - | 9.3 | 4.8/42.5 | 46.7/30.9 | 26 | 29.2 |
| | p=14 | 10.6/9.8/7.1 | 6.4 | 6.6 | 8.9/9.3 | 7.5/8.6 | 7 | 7.6 |
| 1, | p=30 | 8.6/4.1/5.2 | 4.3 | 4.5 | 8.4/9.2 | 10.3/7.6 | 5.9 | 6.8 |
| lsnr | p=60 | 3.7/1.4/4 | - | 2.7 | 2.7/8.1 | 14.5/6.2 | 5 | 4.2 |
| | p=180 | 18/1/2.1 | - | 1.6 | 3.9/6.8 | 37.7/4 | 3.3 | 2.7 |

Table S36: The performance of BOSS compared to other methods, Dense, ρ =0.9, n=2000

| | | BOSS | BS | FS | LASSO | Gamma LASSO | SparseNet | rLASSO |
|--------|-------|------------------------|------|---------|-----------------|------------------|-----------|--------|
| | | C_p -hdf/AICc-hdf/CV | CV | CV | AICc/CV | AICc/CV | CV | CV |
| l I | | | | | | possible BOSS | | |
| - | | 1 0/0/0 | | | | | | |
| | p=14 | 0/0/0 | 0 | 0 | 3/4 | 27/27 | 2 | 0 |
| hsnr | p=30 | 0/0/3 | 1 | 1 | 2/2 | 106/106 | 1 | 3 |
| 110111 | p=60 | 7/8/9 | - | 6 | 6/6 | 74/74 | 8 | 7 |
| | p=180 | 10/10/10 | | 9 | 39/38 | 56/56 | 17 | 35 |
| | p=14 | 0/0/3 | 0 | 0 | 1/1 | 8/8 | 1 | 0 |
| msnr | p=30 | 0/0/5 | 7 | 5 | 1/1 | 25/25 | 3 | 6 |
| msm | p=60 | 12/12/10 | - | 8 | 9/8 | 11/11 | 9 | 10 |
| | p=180 | 10/11/12 | - | 9 | 41/39 | 22/23 | 16 | 38 |
| | p=14 | 1/1/7 | 5 | 4 | 1/1 | 5/8 | 3 | 3 |
| lomm | p=30 | 3/3/11 | 11 | 9 | 3/2 | 7/6 | 8 | 8 |
| lsnr | p=60 | 19/18/14 | - | 10 | 14/13 | 8/11 | 12 | 15 |
| | p=180 | 12/12/13 | - | 11 | 40/38 | 27/26 | 18 | 37 |
| | | | | | Relative effici | ency | | |
| | p=14 | 1/1/1 | 1 | 1 | 0.97/0.97 | 0.79/0.79 | 0.98 | 1 |
| | p=30 | 1/1/0.97 | 0.99 | 0.99 | 0.98/0.98 | 0.49/0.49 | 0.99 | 0.98 |
| hsnr | p=60 | 0.98/0.98/0.97 | - | 1 | 1/1 | 0.61/0.61 | 0.97 | 0.99 |
| | p=180 | 0.99/0.99/0.99 | - | 1 | 0.78/0.79 | 0.7/0.7 | 0.93 | 0.8 |
| | p=14 | 1/1/0.97 | 1 | 1 | 0.99/0.99 | 0.92/0.92 | 0.99 | 1 |
| | p=30 | 1/1/0.96 | 0.94 | 0.95 | 1/1 | 0.8/0.8 | 0.97 | 0.95 |
| msnr | p=60 | 0.96/0.96/0.98 | - | 1 | 0.99/0.99 | 0.97/0.97 | 0.99 | 0.98 |
| | p=180 | 0.98/0.98/0.98 | - | 1 | 0.77/0.78 | 0.89/0.88 | 0.94 | 0.79 |
| | p=14 | 1/1/0.94 | 0.95 | 0.97 | 1/1 | 0.96/0.93 | 0.98 | 0.98 |
| | p=30 | 0.99/0.99/0.92 | 0.92 | 0.94 | 1/1 | 0.96/0.96 | 0.94 | 0.95 |
| lsnr | p=60 | 0.91/0.92/0.95 | - | 0.99 | 0.95/0.96 | 1/0.98 | 0.97 | 0.95 |
| | p=180 | 1/0.99/0.99 | - | 1 | 0.8/0.81 | 0.88/0.88 | 0.94 | 0.81 |
| | | | Spa | rsisten | ey (number of | extra variables) | | |
| | p=14 | 14/14/14 | 14 | 14 | 14/14 | 14/14 | 14 | 14 |
| | p=30 | 30/30/29.9 | 29.9 | 29.9 | 30/30 | 26.1/26.1 | 30 | 29.9 |
| hsnr | p=60 | 53.2/52.7/39.2 | - | 36.3 | 55.5/57.2 | 29.4/29.4 | 46 | 49.5 |
| | p=180 | 37/35/38.6 | - | 30.2 | 109.6/118.6 | 43.1/43.1 | 52.4 | 74.3 |
| i | p=14 | 14/14/14 | 14 | 14 | 14/14 | 14/14 | 14 | 14 |
| | p=30 | 29.9/29.9/28.2 | 27.3 | 27.9 | 29.7/29.9 | 26.3/26.3 | 28.8 | 28.7 |
| msnr | p=60 | 47.5/46.6/31.3 | _ | 27.4 | 51.1/53.4 | 35.5/35.6 | 37.2 | 44 |
| | p=180 | 30.8/28.4/32 | - | 23 | 95.1/104.1 | 62.7/59 | 44.6 | 71.3 |
| | p=14 | 14/14/13.8 | 13.6 | 13.7 | 14/14 | 13.8/13.9 | 13.8 | 13.8 |
| | p=30 | 28.8/28.8/21.2 | 18.5 | 20.2 | 27.6/28.4 | 21.7/24.8 | 23.5 | 24.8 |
| lsnr | p=60 | 35.3/33.6/20.6 | - | 16.3 | 41/43.9 | 28.5/33.1 | 26.4 | 35.4 |
| | p=180 | 18.5/16.6/21.4 | - | 11.8 | 65.3/76.1 | 49.6/41.2 | 32.3 | 60.8 |
| | 1 * | 1 / / | | | ' | , | | |

Table S37: The performance of BOSS for high dimensional data, Sparse-Ex1, ρ =0, n=200

| P=200 | | | BOSS C _v /AICc/CV | FS EBIC/HDBIC/HDHQ/CV | FSstop EBIC/HDBIC/HDHQ | FStrim HDBIC | FSstoptrim HDBIC | lasso AICc/CV | Gamma lasso AICc/CV | SparseNet CV | rlasso CV |
|--|-------|---------|---------------------------------|--------------------------|---------------------------|-----------------|---------------------|------------------|------------------------|-----------------|--------------|
| $ \begin{array}{c c c c c c c c c c c c c c c c c c c $ | İ | | | , , , | % worse than the | best possi | ible BOSS | , | , | | |
| $ \begin{array}{c c c c c c c c c c c c c c c c c c c $ | i – | p=250 | 6/1/17 | 502/502/502/18 | 1/0/1 | 502 | 0 | 141/142 | 183/142 | 17 | 16 |
| $\begin{array}{ c c c c c c c c c c c c c c c c c c c$ | ١. | | | | | 511 | 0 | | | | 18 |
| $ \begin{array}{ c c c c c c c c c c c c c c c c c c c$ | hsnr | p=1000 | 86/13/21 | 512/512/512/22 | 2/0/0 | 512 | 0 | 184/192 | 424/192 | | 17 |
| $\begin{array}{c c c c c c c c c c c c c c c c c c c $ | | p=1500 | 122/44/19 | 505/505/505/21 | 2/0/0 | 505 | 0 | 206/209 | 433/209 | 26 | 15 |
| $\begin{array}{c c c c c c c c c c c c c c c c c c c $ | | | | | | | | | | | |
| $\begin{array}{ c c c c c c } \hline p_{p} = 1000 & 150/128/23 & 499/499/489/25 & 11/601/53 & 499 & 604 & 20/206 & 472/206 & 26 & 63 \\ \hline p_{p} = 250 & 161/51/3 & 166/166/166/13 & 15/16/15 & 166 & 16 & -3/0 & 122/0 & 3 & 3 \\ p_{p} = 1000 & 22/12/12 & 149/149/149/12 & 149/12 & 149 & 12 & -3/0 & 143/0 & 3 & 3 \\ p_{p} = 1000 & 33/16/9 & 138/138/189/6 & 9/9/9 & 136 & 9 & -3/2 & 133/2 & 3 & 4 \\ p_{p} = 1000 & 33/16/9 & 138/138/189/6 & 33/3/3 & 138 & 3 & -3/1 & 133/2 & 3 & 4 \\ p_{p} = 1000 & 33/16/9 & 138/138/189/6 & 3/3/3 & 138 & 3 & -3/1 & 133/2 & 3 & 4 \\ p_{p} = 1000 & 0.54/0.89/188 & 0.17/0.17/0.185 & 0.99/1/0.99 & 0.17 & 1 & 0.42/0.41 & 0.35/0.41 & 0.85 & 0.87 \\ p_{p} = 000 & 0.59/0.99/0.85 & 0.16/0.16/0.16/0.82 & 0.98/1/0.99 & 0.16 & 1 & 0.38/0.38 & 0.21/0.38 & 0.81 & 0.85 \\ p_{p} = 1000 & 0.54/0.89/0.88 & 0.16/0.16/0.16/0.82 & 0.98/1/1 & 0.16 & 1 & 0.35/0.34 & 0.19/0.32 & 0.79 & 0.86 \\ p_{p} = 1000 & 0.54/0.93/0.88 & 0.17/0.17/0.17/0.87 & 1/0.28/0.08 & 0.17 & 0.28 & 0.43/0.33 & 0.21/0.32 & 0.79 & 0.86 \\ p_{p} = 0.00 & 0.66/0.85/0.89 & 0.17/0.17/0.17/0.87 & 1/0.28/0.08 & 0.17 & 0.28 & 0.43/0.33 & 0.21/0.32 & 0.79 & 0.86 \\ p_{p} = 0.00 & 0.38/0.48/0.89 & 0.17/0.17/0.17/0.87 & 1/0.28/0.08 & 0.17 & 0.28 & 0.43/0.33 & 0.21/0.32 & 0.89 \\ p_{p} = 0.00 & 0.38/0.48/0.89 & 0.17/0.17/0.17/0.88 & 1/0.21/0.9 & 0.17 & 0.21 & 0.41/0.4 & 0.19/0.4 & 0.85 & 0.83 \\ p_{p} = 0.00 & 0.38/0.48/0.89 & 0.17/0.17/0.17/0.88 & 1/0.21/0.9 & 0.17 & 0.21 & 0.41/0.4 & 0.19/0.4 & 0.85 & 0.83 \\ p_{p} = 0.00 & 0.38/0.48/0.89 & 0.18/0.18/0.18/0.366 & 1/0.16/0.91 & 0.18 & 0.16 & 0.36/0.36 & 0.19/0.36 & 0.87 \\ p_{p} = 0.00 & 0.38/0.88/0.89 & 0.18/0.18/0.18/0.86 & 1/0.16/0.91 & 0.18 & 0.16 & 0.36/0.36 & 0.19/0.36 & 0.87 \\ p_{p} = 0.00 & 0.79/0.87/0.87 & 0.39/0.39/0.39/0.87 & 0.39/0.88/0.89 & 0.18 & 0.18/0.18/0.18 & 0.16 & 0.36/0.36 & 0.19/0.36 & 0.87 \\ p_{p} = 0.00 & 0.73/0.81/0.89 & 0.41/0.41/0.41/0.99 & 0.94/0.95/0.95 & 0.41 & 0.95 & 1/0.96 & 0.41/0.97 & 0.94 & 0.94 \\ p_{p} = 0.00 & 0.73/0.81/0.89 & 0.41/0.41/0.31/0.99 & 0.89/0.99 & 0.41 & 0.95 & 1/0.96 & 0.41/0.$ | menr | | | | | | | | | | |
| $ \begin{array}{ c c c c c c c c c c c c c c c c c c c$ | mam | | | | | | | | | | |
| $\begin{array}{ c c c c c c c c c c c c c c c c c c c$ | | | , , | , , , | , , | | | , | | | |
| $\begin{array}{ c c c c c c c c c c c c c c c c c c c$ | | | | | | | | | | | |
| $ \begin{array}{ c c c c c c c c c c c c c c c c c c c$ | lsnr | | | | | | | | | | |
| $ \begin{array}{ c c c c c c c c c c c c c c c c c c c$ | | | | | | | | | | | |
| $\begin{array}{ c c c c c c c c c c c c c c c c c c c$ | | p-1000 | 1 04/20/0 | 100/100/100/0 | , , | | | -0/1 | 100/1 | | - |
| $\begin{array}{ c c c c c c c c c c c c c c c c c c c$ | | l n=250 | 1 0 0 0 0 0 0 0 0 | 0.17/0.17/0.17/0.05 | | | | 0.49/0.41 | 0.25/0.41 | 0.05 | 0.97 |
| $ \begin{array}{ c c c c c c c c c c c c c c c c c c c$ | | | | | | | | | | | |
| $\begin{array}{ c c c c c c c c c c c c c c c c c c c$ | hsnr | | | | | | | | | | |
| $\begin{array}{ c c c c c c c c c c c c c c c c c c c$ | | | | | | | | | | | |
| $\begin{array}{ c c c c c c c c c c c c c c c c c c c$ | i | p=250 | 0.84/0.93/0.88 | 0.17/0.17/0.17/0.87 | 1/0.28/0.98 | 0.17 | 0.28 | 0.43/0.43 | 0.25/0.43 | 0.88 | 0.81 |
| $\begin{array}{ c c c c c c c c c c c c c c c c c c c$ | | | | | | 0.17 | | | | 0.85 | |
| $ \begin{array}{ c c c c c c c c c c c c c c c c c c c$ | msnr | p=1000 | 0.46/0.69/0.87 | 0.18/0.18/0.18/0.86 | 1/0.16/0.91 | 0.18 | 0.16 | 0.38/0.37 | 0.18/0.37 | 0.84 | 0.8 |
| $ \begin{array}{ c c c c c c c c c c c c c c c c c c c$ | | p=1500 | 0.38/0.48/0.89 | 0.18/0.18/0.18/0.88 | 1/0.16/0.72 | 0.18 | 0.16 | 0.36/0.36 | 0.19/0.36 | 0.87 | 0.68 |
| $ \begin{array}{ c c c c c c c c c c c c c c c c c c c$ | | p=250 | 0.84/0.85/0.86 | 0.37/0.37/0.37/0.86 | 0.85/0.84/0.84 | | 0.84 | | | | 0.94 |
| $\begin{array}{ c c c c c c c c c c c c c c c c c c c$ | lonn | | | | | | | | | | |
| $ \begin{array}{ c c c c c c c c c c c c c c c c c c c$ | ISIII | | | | | | | | | | |
| $\begin{array}{ c c c c c c c c c c c c c c c c c c c$ | | p=1500 | 0.73/0.81/0.92 | 0.41/0.41/0.41/0.92 | , , | | 0.95 | 1/0.96 | 0.41/0.96 | 0.94 | 0.93 |
| $\begin{array}{ c c c c c c c c c c c c c c c c c c c$ | | | | | | | | | | | |
| $ \begin{array}{ c c c c c c } \hline hsnr & p=1000 & 6/6/6 & 6/6/6/6/$ | | | | | | | | | | | |
| $\begin{array}{ c c c c c c c c c c c c c c c c c c c$ | hsnr | | | | | | | | | | |
| $\begin{array}{ c c c c c c c c c c c c c c c c c c c$ | | | | | | | | | | | |
| $\begin{array}{ c c c c c c c c c c c c c c c c c c c$ | | | | | | | | | | | |
| $\begin{array}{ l c c c c c c c c c c c c c c c c c c $ | | | | | | | | | | | |
| $ \begin{array}{ c c c c c c c c c c c c c c c c c c c$ | msnr | | | | | | | | | | |
| $ \begin{array}{ c c c c c c c c c c c c c c c c c c c$ | | p=1500 | | | | 6 | 0.1 | 6/6 | 6/6 | 6 | 5.9 |
| $ \begin{array}{ c c c c c c c c c c c c c c c c c c c$ | | p=250 | 0.8/0.4/1.1 | 5.6/5.6/5.6/1.1 | 0.3/0/0.1 | 5.6 | 0 | 3.3/3.3 | 4.6/3.3 | 2.9 | 2.6 |
| $\begin{array}{ c c c c c c c c c c c c c c c c c c c$ | ١, | p=500 | 1.1/0.4/0.8 | 4.3/4.3/4.3/0.8 | 0.2/0/0.1 | | 0 | 3/3 | | | |
| $ \begin{array}{ c c c c c c c c c c c c c c c c c c c$ | Isnr | | | | | | | | | | |
| $ \begin{array}{c ccccccccccccccccccccccccccccccccccc$ | | p=1500 | 0.8/0.5/0.3 | 2.3/2.3/2.3/0.3 | , , | | | 1.5/1.6 | 2.4/1.6 | 1.4 | 1.3 |
| $ \begin{array}{c ccccccccccccccccccccccccccccccccccc$ | | | | | | | | | | | |
| $ \begin{array}{c ccccccccccccccccccccccccccccccccccc$ | | | | | | | | | | | |
| $ \begin{array}{ c c c c c c c c c c c c c c c c c c c$ | hsnr | | | | | | | | | | |
| $ \begin{array}{ c c c c c c c c c c c c c c c c c c c$ | | | | | | | | | | | |
| $ \begin{array}{ c c c c c c c c c c c c c c c c c c c$ | | | , , | . , , , | | | | | | | |
| $ \begin{array}{ c c c c c c c c c c c c c c c c c c c$ | | | | | | | | | | | |
| $ \begin{vmatrix} p = 1500 & 8.1/4/0.3 & 193/193/193/0.3 & 0/0/0 & 192.9 & 0 & 21.3/44.1 & 99/44.1 & 2.6 & 2.5 \\ p = 250 & 0.7/0.1/0.5 & 193.4/193.4/193.4/0.5 & 0/0/0 & 193.4 & 0 & 10.1/13.1 & 70/13.1 & 9.6 & 7.2 \\ p = 500 & 2.8/0.2/0.5 & 194.7/194.7/0.4 & 0/0/0 & 194.7 & 0 & 11.3/15.9 & 113.7/15.9 & 12.4 & 8.9 \\ p = 1000 & 5.8/1.5/0.4 & 195.8/195.8/195.8/0.3 & 0/0/0 & 195.8 & 0 & 10.7/20 & 113/20 & 14.1 & 11.5 \\ \end{vmatrix} $ | msnr | | | | | | | | | | |
| $ \begin{vmatrix} p = 250 & 0.7/0.1/0.5 & 193.4/193.4/193.4/0.5 & 0/0/0 & 193.4 & 0 & 10.1/13.1 & 70/13.1 & 9.6 & 7.2 \\ p = 500 & 2.8/0.2/0.5 & 194.7/194.7/0.4 & 0/0/0 & 194.7 & 0 & 11.3/15.9 & 113.7/15.9 & 12.4 & 8.9 \\ lsnr & p = 1000 & 5.8/1.5/0.4 & 195.8/195.8/195.8/195.8/0.3 & 0/0/0 & 195.8 & 0 & 10.7/20 & 113/20 & 14.1 & 11.5 \\ \end{vmatrix} $ | | | | | | | | | | | |
| $ \begin{vmatrix} p = 500 \\ lsnr \end{vmatrix} = \begin{vmatrix} 2.8/0.2/0.5 & 194.7/194.7/0.4 & 0/0/0 & 194.7 & 0 & 11.3/15.9 & 113.7/15.9 & 12.4 & 8.9 \\ p = 1000 & 5.8/1.5/0.4 & 195.8/195.8/195.8/195.8/0.3 & 0/0/0 & 195.8 & 0 & 10.7/20 & 113/20 & 14.1 & 11.5 \end{vmatrix} $ | _ | 1 * | , , , | , , , | , , | | 0 | | , | 9.6 | 7.2 |
| $ \begin{vmatrix} \text{lsnr} \\ \text{p} = 1000 \end{vmatrix} = 5.8/1.5/0.4 + 195.8/195.8/195.8/195.8/0.3 + 0/0/0 + 195.8 + 0 + 10.7/20 + 113/20 + 14.1 + 11.5 $ | | 1 * | | | | | | | | | |
| $ \begin{array}{ c c c c c c c c c c c c c c c c c c c$ | lsnr | | | | | | | | | | |
| | | p=1500 | 6.1/3.2/0.3 | 196.7/196.7/196.7/0.3 | 0/0/0 | 196.6 | 0 | 9.5/15.6 | 111.9/15.6 | 12.8 | 10.7 |

Table S38: The performance of BOSS for high dimensional data, Sparse-Ex1, ρ =0.5, n=200

| | | BOSS $C_p/AICc/CV$ | FS EBIC/HDBIC/HDHQ/CV | FSstop EBIC/HDBIC/HDHQ | FStrim HDBIC | FSstoptrim HDBIC | lasso AICc/CV | Gamma lasso AICc/CV | SparseNet CV | rlasso CV |
|----------|------------------|----------------------------------|--|----------------------------------|-----------------|---------------------|------------------------|---------------------------------------|-----------------|--------------|
| i | | | | % worse than the | best possi | ible BOSS | | | | |
| | p=250 | 4/1/17 | 495/495/495/20 | 1/0/1 | 495 | 0 | 139/138 | 177/138 | 17 | 16 |
| hsnr | p=500 | 21/2/18 | 507/507/507/18 | 3/0/1 | 507 | 0 | 161/161 | 359/161 | 20 | 19 |
| nsnr | p=1000 | 70/9/20 | 513/513/513/21 | 3/0/0 | 513 | 0 | 184/186 | 425/186 | 24 | 20 |
| | p=1500 | 113/30/16 | 502/502/502/19 | 3/0/0 | 502 | 0 | 208/209 | 428/209 | 23 | 14 |
| | p=250 | 22/13/19 | 490/490/490/22 | 4/303/8 | 490 | 304 | 137/136 | 293/136 | 18 | 37 |
| msnr | p=500 p=1000 | 53/24/20 116/52/23 | 498/498/498/20 506/506/506/25 | 8/412/20 8/570/26 | 498 506 | 414 570 | 157/158 180/184 | 450/158 475/184 | 21 24 | 35 39 |
| | p=1500 | 182/113/22 | 491/491/491/24 | 11/584/61 | 491 | 584 | 203/204 | 465/204 | 26 | 73 |
| | p=250 | 13/12/11 | 165/165/165/12 | 12/13/13 | 165 | 13 | -4/-2 | 117/-2 | 1 | 1 |
| ١, | p=500 | 20/12/11 | 150/150/150/11 | 11/12/12 | 150 | 12 | -3/-1 | 144/-1 | 2 | 2 |
| lsnr | p=1000 | 30/14/9 | 136/136/136/9 | 8/8/8 | 136 | 8 | -4/0 | 133/0 | 2 | 3 |
| | p=1500 | 31/17/6 | 141/141/141/6 | 3/2/2 | 141 | 2 | -3/0 | 138/0 | 3 | 4 |
| | | | | | efficiency | | | | | |
| | p=250 | 0.96/0.99/0.85 | 0.17/0.17/0.17/0.83 | 0.99/1/0.99 | 0.17 | 1 | 0.42/0.42 | 0.36/0.42 | 0.85 | 0.86 |
| hsnr | p=500 p=1000 | 0.83/0.98/0.84 0.59/0.92/0.84 | 0.16/0.16/0.16/0.85 0.16/0.16/0.16/0.82 | 0.97/1/0.99 0.97/1/1 | 0.16 0.16 | 1 1 | 0.38/0.38 0.35/0.35 | 0.22/0.38 0.19/0.35 | 0.83 0.81 | 0.84 0.83 |
| | p=1000 p=1500 | 0.47/0.77/0.86 | 0.17/0.17/0.17/0.84 | 0.98/1/1 | 0.10 | 1 | 0.32/0.32 | 0.19/0.33 | 0.81 | 0.88 |
| | p=250 | 0.85/0.92/0.87 | 0.18/0.18/0.18/0.85 | 1/0.26/0.96 | 0.18 | 0.26 | 0.44/0.44 | 0.26/0.44 | 0.88 | 0.76 |
| | p=500 | 0.7/0.87/0.89 | 0.18/0.18/0.18/0.9 | 1/0.21/0.9 | 0.18 | 0.21 | 0.42/0.42 | 0.2/0.42 | 0.89 | 0.8 |
| msnr | p=1000 | 0.5/0.71/0.88 | 0.18/0.18/0.18/0.87 | 1/0.16/0.86 | 0.18 | 0.16 | 0.39/0.38 | 0.19/0.38 | 0.87 | 0.78 |
| | p=1500 | 0.4/0.52/0.91 | 0.19/0.19/0.19/0.9 | 1/0.16/0.69 | 0.19 | 0.16 | 0.37/0.37 | 0.2/0.37 | 0.89 | 0.64 |
| | p=250 | 0.85/0.86/0.86 | 0.36/0.36/0.36/0.86 | 0.86/0.85/0.85 | 0.36 | 0.85 | 1/0.98 | 0.44/0.98 | 0.95 | 0.95 |
| lsnr | p=500 | 0.8/0.86/0.87 | 0.39/0.39/0.39/0.87 | 0.87/0.86/0.86 | 0.39 | 0.86 | 1/0.97 | 0.4/0.97 | 0.94 | 0.94 |
| 13111 | p=1000 | 0.74/0.84/0.88 0.74/0.83/0.92 | 0.41/0.41/0.41/0.88 0.4/0.4/0.4/0.92 | 0.89/0.88/0.88 0.95/0.95/0.95 | 0.41 | 0.88 0.95 | 1/0.96 1/0.97 | 0.41/0.96 0.41/0.97 | 0.94 0.94 | 0.93 0.94 |
| | p=1500 | 0.74/0.83/0.92 | 0.4/0.4/0.4/0.92 | , , | sistency | 0.95 | 1/0.97 | 0.41/0.97 | 0.94 | 0.94 |
| | l 050 | 6/6/6 | 6/6/6/6 | 6/6/6 | 6 | 6 | 6/6 | 6/6 | 6 | 6 |
| | p=250 p=500 | 6/6/6 | 6/6/6/6 | 6/6/6 | 6 | 6 | 6/6 | 6/6 | 6 | 6 |
| hsnr | p=300 p=1000 | 6/6/6 | 6/6/6/6 | 6/6/6 | 6 | 6 | 6/6 | 6/6 | 6 | 6 |
| | p=1500 | 6/6/6 | 6/6/6/6 | 6/6/6 | 6 | 6 | 6/6 | 6/6 | 6 | 6 |
| | p=250 | 6/6/6 | 6/6/6/6 | 6/3.1/5.9 | 6 | 3.1 | 6/6 | 6/6 | 6 | 6 |
| msnr | p=500 | 6/6/6 | 6/6/6/6 | 6/2.3/5.9 | 6 | 2.3 | 6/6 | 6/6 | 6 | 6 |
| msm | p=1000 | 6/6/6 | 6/6/6/6 | 6/1/5.8 | 6 | 1 | 6/6 | 6/6 | 6 | 6 |
| | p=1500 | 6/6/6 | 6/6/6/6 | 5.9/0/5.5 | 6 | 0 | 6/6 | 6/6 | 6 | 5.9 |
| | p=250 | 0.7/0.3/1 1/0.4/0.8 | 5.5/5.5/5.5/1 4.2/4.2/4.2/0.8 | 0.2/0/0.1 0.2/0/0.1 | 5.5 4.2 | 0 | 3/3.1 2.9/2.9 | 4.3/3.1 3.7/2.9 | 2.7 2.5 | 2.5 2.4 |
| lsnr | p=500 p=1000 | 1.2/0.6/0.6 | 3.1/3.1/3.1/0.6 | 0.2/0/0.1 | 3.1 | 0 | 2.5/2.5 | 3/2.5 | 2.5 | 2.4 |
| | p=1500 | 0.7/0.4/0.2 | 2.1/2.1/2.1/0.2 | 0/0/0 | 2.1 | ő | 1.3/1.3 | 2.1/1.3 | 1.2 | 1.1 |
| <u> </u> | | | | Number of | extra varia | bles | , | · · · · · · · · · · · · · · · · · · · | | |
| | p=250 | 0.2/0/0.3 | 193/193/193/0.3 | 0/0/0 | 193 | 0 | 17/23.7 | 26.6/23.7 | 2 | 0.5 |
| ١, | p=500 | 1/0/0.3 | 193/193/193/0.3 | 0/0/0 | 193 | 0 | 18.3/28.3 | 71.3/28.3 | 3 | 0.8 |
| hsnr | p=1000 | 3.6/0.3/0.2 | 193/193/193/0.3 | 0/0/0 | 193 | 0 | 18.7/35.2 | 87.8/35.2 | 3.6 | 0.6 |
| | p=1500 | 5.9/1.3/0.2 | 193/193/193/0.2 | 0/0/0 | 192.9 | 0 | 22.5/44.6 | 89.1/44.6 | 3.9 | 0.5 |
| | p=250 | 0.5/0.2/0.3 | 193/193/193/0.4 | 0/0/0 | 193 | 0 | 16.7/23.7 | 46.2/23.7 | 1.2 | 1.2 |
| msnr | p=500 | 1.7/0.3/0.3 | 193/193/193/0.3 | 0/0/0 | 193 193 | 0 | 18.4/28.3 | 98.4/28.3 101/35.2 | 1.8 2 | 1.3 |
| | p=1000 p=1500 | 4.6/1/0.3 7.6/3.2/0.3 | 193/193/193/0.3 193/193/193/0.3 | 0/0/0 0/0/0 | 193 | 0 | 18.9/35.2 22.4/44.6 | 101/35.2 | 2.4 | 1.4 2.9 |
| | | 0.4/0.1/0.5 | | 0/0/0 | 193.5 | 0 | 9.4/12.1 | 67.6/12.1 | 8.7 | 6.7 |
| | p=250 p=500 | 0.4/0.1/0.5 2.4/0.2/0.5 | 193.5/193.5/193.5/0.6 194.8/194.8/194.8/0.5 | 0/0/0 | 193.5 | 0 | 9.4/12.1 10.8/15.6 | 114.8/15.6 | 12.2 | 9.3 |
| lsnr | p=1000 | 5.2/1.3/0.4 | 195.9/195.9/195.9/0.4 | 0/0/0 | 195.8 | 0 | 10.8/18 | 115.1/18 | 12.8 | 10.6 |
| | p=1500 | 5.2/2.3/0.3 | 196.9/196.9/196.9/0.3 | 0/0/0 | 196.8 | 0 | 9/13.3 | 113.5/13.3 | 11.4 | 9.6 |
| | | , , , | , | , , | | | | , - | | |

Table S39: The performance of BOSS for high dimensional data, Sparse-Ex1, ρ =0.9, n=200

| | | BOSS $C_p/AICc/CV$ | FS EBIC/HDBIC/HDHQ/CV | FSstop EBIC/HDBIC/HDHQ | FStrim HDBIC | FSstoptrim HDBIC | lasso AICc/CV | Gamma lasso AICc/CV | SparseNet CV | rlasso CV |
|---------|------------------|----------------------------------|--|----------------------------------|-----------------|---------------------|--------------------------------------|------------------------|-----------------|--------------|
| ĺ | | | | % worse than the | best possi | ible BOSS | | | | |
| | p=250 | 5/4/39 | 447/447/447/39 | 3/25/4 | 447 | 22 | 108/107 | 201/107 | 22 | 25 |
| 1 | p=500 | 7/5/40 | 473/473/473/42 | 4/17/6 | 473 | 16 | 135/134 | 341/134 | 31 | 26 |
| hsnr | p=1000 | 18/7/50 | 447/447/447/51 | 3/46/6 | 447 | 43 | 143/141 | 360/141 | 30 | 22 |
| | p=1500 | 37/9/48 | 459/459/459/49 | 5/27/7 | 459 | 26 | 176/173 | 389/173 | 54 | 30 |
| | p=250 | 10/9/19 | 272/272/272/19 | 14/199/18 | 272 | 199 | 41/40 | 170/40 | 25 | 20 |
| msnr | p=500 p=1000 | 12/8/13 21/12/13 | 262/262/262/14 242/242/242/15 | 7/232/14 7/291/18 | 262 242 | 232 291 | 48/47 52/50 | 239/47 226/50 | 27 26 | 11 5 |
| | p=1500 | 41/21/14 | 237/237/237/15 | 11/273/58 | 237 | 273 | 66/64 | 223/64 | 26 | 31 |
| | p=250 | 11/11/11 | 164/164/164/10 | 11/11/11 | 164 | 11 | -13/-12 | 97/-12 | -8 | -8 |
| ١. | p=500 | 14/12/12 | 155/155/155/12 | 13/13/13 | 155 | 13 | -9/-9 | 149/-9 | -5 | -5 |
| lsnr | p=1000 | 18/11/10 | 139/139/139/10 | 9/9/9 | 139 | 9 | -9/-8 | 136/-8 | -5 | -4 |
| | p=1500 | 19/7/6 | 151/151/151/6 | 2/2/2 | 151 | 2 | -5/-3 | 147/-3 | -1 | 0 |
| | | | | | efficiency | | | | | |
| | p=250 | 0.98/0.99/0.74 | 0.19/0.19/0.19/0.74 | 1/0.82/0.99 | 0.19 | 0.85 | 0.49/0.5 | 0.34/0.5 | 0.84 | 0.83 |
| hsnr | p=500 p=1000 | 0.97/0.99/0.75 0.87/0.96/0.69 | 0.18/0.18/0.18/0.74 0.19/0.19/0.19/0.68 | 1/0.89/0.99 1/0.71/0.97 | 0.18 0.19 | 0.9 0.72 | 0.44/0.45 0.42/0.43 | 0.24/0.45 0.22/0.43 | 0.8 0.8 | 0.83 0.84 |
| | p=1000 p=1500 | 0.77/0.97/0.71 | 0.19/0.19/0.19/0.08 | 1/0.83/0.99 | 0.19 | 0.72 | 0.42/0.43 | 0.22/0.43 | 0.68 | 0.84 |
| | p=250 | 0.99/1/0.91 | 0.29/0.29/0.29/0.91 | 0.96/0.36/0.92 | 0.29 | 0.36 | 0.77/0.78 | 0.4/0.78 | 0.87 | 0.9 |
| | p=500 | 0.96/0.99/0.95 | 0.3/0.3/0.3/0.94 | 1/0.32/0.94 | 0.23 | 0.32 | 0.72/0.73 | 0.32/0.73 | 0.85 | 0.97 |
| msnr | p=1000 | 0.87/0.93/0.93 | 0.31/0.31/0.31/0.91 | 0.98/0.27/0.89 | 0.31 | 0.27 | 0.69/0.7 | 0.32/0.7 | 0.83 | 1 |
| | p=1500 | 0.79/0.92/0.98 | 0.33/0.33/0.33/0.97 | 1/0.3/0.71 | 0.33 | 0.3 | 0.67/0.68 | 0.34/0.68 | 0.88 | 0.85 |
| | p=250 | 0.78/0.78/0.78 | 0.33/0.33/0.33/0.79 | 0.78/0.78/0.78 | 0.33 | 0.78 | 1/0.99 | 0.44/0.99 | 0.95 | 0.95 |
| lsnr | p=500 | 0.79/0.81/0.81 | 0.36/0.36/0.36/0.81 | 0.81/0.8/0.8 | 0.36 | 0.8 | 1/0.99 | 0.36/0.99 | 0.95 | 0.95 |
| 13111 | p=1000 | 0.77/0.82/0.83 0.8/0.89/0.9 | 0.38/0.38/0.38/0.82 0.38/0.38/0.38/0.9 | 0.83/0.83/0.83 0.93/0.94/0.94 | 0.38 0.38 | 0.83 0.94 | 1/0.98 1/0.98 | 0.39/0.98 0.38/0.98 | 0.95 0.96 | 0.95 0.95 |
| | p=1500 | 0.8/0.89/0.9 | 0.38/0.38/0.38/0.9 | , , | | 0.94 | 1/0.98 | 0.38/0.98 | 0.96 | 0.95 |
| | 1 050 | 0.10.10 | 0.10.10.10 | | sistency | F 0 | 0.10 | 0.10 | | |
| | p=250 p=500 | 6/6/6 6/6/6 | 6/6/6/6 6/6/6/6 | 6/5.8/6 6/5.9/6 | 6 | 5.8 5.9 | 6/6 6/6 | 6/6 6/6 | 6 6 | 6 |
| hsnr | p=300 p=1000 | 6/6/6 | 6/6/6/6 | 6/5.7/5.9 | 6 | 5.7 | 6/6 | 5.9/6 | 6 | 6 |
| | p=1500 | 6/6/6 | 6/6/6/6 | 6/5.8/5.9 | 6 | 5.8 | 6/6 | 5.9/6 | 5.9 | 6 |
| | p=250 | 5/5/5 | 5.9/5.9/5.9/5.1 | 4.9/2.1/4.8 | 5.9 | 2.1 | 5.9/5.9 | 5.2/5.9 | 5 | 5.6 |
| | p=500 | 5/5/5 | 5.6/5.6/5.6/5 | 4.9/1.8/4.8 | 5.6 | 1.7 | 5.9/5.9 | 4.9/5.9 | 4.8 | 5.7 |
| msnr | p=1000 | 4.9/4.9/4.9 | 5.4/5.4/5.4/4.9 | 4.8/0.6/4.7 | 5.4 | 0.6 | 5.9/5.9 | 4.9/5.9 | 4.7 | 5.7 |
| | p=1500 | 4.9/4.9/4.8 | 5.2/5.2/5.2/4.8 | 4.7/0/3.9 | 5.2 | 0 | 5.8/5.8 | 4.9/5.8 | 4.6 | 5.4 |
| | p=250 | 0.4/0.2/0.6 | 5.3/5.3/5.3/0.7 | 0.1/0/0.1 | 5.3 | 0 | 2.4/2.5 | 2.9/2.5 | 2.2 | 2.1 |
| lsnr | p=500 p=1000 | 0.6/0.3/0.6 0.7/0.3/0.4 | 3.6/3.6/3.6/0.6 2.6/2.6/2.6/0.4 | 0.1/0/0.1 0.1/0/0 | 3.6 2.6 | 0 | $\frac{2.2}{2.4}$ $\frac{2}{2.2}$ | 2.6/2.4 2.2/2.2 | 2 1.8 | 1.9 1.7 |
| | p=1000 p=1500 | 0.4/0.1/0.2 | 1.9/1.9/1.9/0.2 | 0.1/0/0 | 1.9 | 0 | 1/1 | 1.6/1 | 0.9 | 0.8 |
| _ | p-1000 | 0.1/0.1/0.2 | 1.0/1.0/1.0/0.2 | Number of | | | -/- | 1.0, 1 | 0.0 | 0.0 |
| | p=250 | 0.5/0.5/2.8 | 193/193/193/1.3 | 0.5/0.5/0.5 | 193 | 0.2 | 17.9/21.4 | 35.7/21.4 | 3.9 | 2.7 |
| ١. | p=500 | 0.3/0.2/1.4 | 193/193/193/0.9 | 0.2/0.2/0.2 | 193 | 0.1 | 19.5/25.2 | 72.1/25.2 | 5.1 | 1.6 |
| hsnr | p=1000 | 1.2/0.6/1.6 | 193/193/193/1.3 | 0.6/0.5/0.5 | 193 | 0.3 | 21.2/29.9 | 85.1/29.9 | 7 | 2.3 |
| | p=1500 | 2/0.3/1.1 | 193/193/193/1 | 0.2/0.2/0.2 | 193 | 0.2 | 25.2/40.1 | 91.9/40.1 | 10 | 1.9 |
| | p=250 | 1.6/1.4/2.9 | 193.1/193.1/193.1/2 | 1.2/0.5/1.2 | 193.1 | 0.5 | 17.9/21.4 | 57/21.4 | 6.9 | 6.8 |
| msnr | p=500 | 1.7/1.3/1.7 | 193.4/193.4/193.4/1.6 | 1.1/0.3/1 | 193.4 | 0.3 | 19.4/25 | 103.4/25 | 7.3 | 5.3 |
| 1113111 | p=1000 p=1500 | 2.5/1.7/1.7 4.6/2.2/1.7 | 193.6/193.6/193.6/1.7 | 1.2/0.2/1.2 1.2/0/0.9 | 193.6 193.7 | 0.2 | 21.1/29.8 25.1/39.7 | 107/29.8 107.2/39.7 | 7.8 7.5 | 4.7 8.5 |
| | | | 193.7/193.7/193.7/1.7 | | | | | • | | |
| | p=250 | 0.9/0.4/1.6 | 193.7/193.7/193.7/1.5 | 0.2/0/0.1 0.1/0/0 | 193.7 195.4 | 0 | 12.2/13.8 12.7/16 | 62.3/13.8 | 11.5 12.9 | 9.6 10.2 |
| lsnr | p=500 p=1000 | 1.7/0.5/1.5 3.3/0.9/1 | 195.4/195.4/195.4/1.2 196.4/196.4/196.4/0.9 | 0.1/0/0 | 195.4 | 0 | 13.8/18 | 119.1/16 120.8/18 | 12.9 | 10.2 |
| | p=1500 | 3.3/0.8/0.5 | 197.1/197.1/197.1/0.5 | 0/0/0 | 197 | 0 | 10.8/14.5 | 119.7/14.5 | 12.4 | 9.2 |
| | 1 * | -// | , , , | -1-1- | | - | , | / | | |

Table S40: The performance of BOSS for high dimensional data, Sparse-Ex2, ρ =0, n=200

| | | $\begin{array}{c c} \operatorname{BOSS} \\ \operatorname{C}_p/\operatorname{AICc/CV} \end{array}$ | FS EBIC/HDBIC/HDHQ/CV | FSstop EBIC/HDBIC/HDHQ | FStrim HDBIC | FSstoptrim HDBIC | lasso AICc/CV | Gamma lasso AICc/CV | SparseNet CV | rlasso CV |
|----------|------------------|---|--|--------------------------------|-----------------|---------------------|------------------------|------------------------------------|-----------------|--------------|
| ĺ | | | | % worse than the | best possi | ble BOSS | | | | |
| | p=250 | 5/1/18 | 501/501/501/18 | 2/0/1 | 501 | 0 | 152/152 | 189/152 | 18 | 16 |
| hsnr | p=500 | 30/3/18 | 501/501/501/19 | 2/0/1 | 501 | 0 | 178/179 | 366/179 | 23 | 17 |
| nsnr | p=1000 | 86/11/20 | 501/501/501/20 | 2/0/0 | 501 | 0 | 203/204 | 420/204 | 25 | 14 |
| | p=1500 | 132/40/19 | 501/501/501/21 | 2/0/0 | 501 | 0 | 218/218 | 432/218 | 26 | 15 |
| | p=250 | 29/16/19 | 498/498/498/20 | 5/419/13 | 498 | 419 | 151/151 | 311/151 | 18 | 60 |
| msnr | p=500 | 83/38/22 | 495/495/495/23 | 10/514/39 | 495 | 514 | 175/176 | 448/176 | 23 | 87 |
| moni | p=1000 p=1500 | 162/88/26 214/151/27 | 491/491/491/27 485/485/485/29 | 18/538/89 26/536/142 | 491 485 | 538 536 | 197/200 210/211 | 462/200 460/211 | 27 26 | 117 140 |
| | 1 * | , , | , , , | , , | | | | | | |
| | p=250 p=500 | 10/8/9 16/6/8 | 169/169/169/9 162/162/162/8 | 8/7/8 5/4/5 | 169 162 | 7 4 | -3/0 -2/1 | $\frac{125}{0}$ $\frac{156}{1}$ | 3 4 | 3 4 |
| lsnr | p=500 p=1000 | 27/9/6 | 158/158/158/6 | 3/3/3 | 158 | 3 | -2/1 -1/3 | 155/3 | 5 | 5 |
| | p=1500 | 36/20/6 | 156/156/156/6 | 2/2/2 | 156 | 2 | -2/2 | 153/2 | 4 | 6 |
| <u> </u> | 1 | | | , , | e efficiency | | , | , | | |
| | p=250 | 0.95/0.99/0.85 | 0.17/0.17/0.17/0.85 | 0.98/1/0.99 | 0.17 | 1 | 0.4/0.4 | 0.35/0.4 | 0.84 | 0.86 |
| hsnr | p=500 | 0.77/0.97/0.85 | 0.17/0.17/0.17/0.84 | 0.98/1/0.99 | 0.17 | 1 | 0.36/0.36 | 0.21/0.36 | 0.81 | 0.86 |
| nsnr | p=1000 | 0.54/0.9/0.84 | 0.17/0.17/0.17/0.83 | 0.98/1/1 | 0.17 | 1 | 0.33/0.33 | 0.19/0.33 | 0.8 | 0.87 |
| | p=1500 | 0.43/0.72/0.84 | 0.17/0.17/0.17/0.83 | 0.98/1/1 | 0.17 | 1 | 0.31/0.31 | 0.19/0.31 | 0.79 | 0.87 |
| | p=250 | 0.81/0.9/0.88 | 0.18/0.18/0.18/0.88 | 1/0.2/0.93 | 0.18 | 0.2 | 0.42/0.42 | 0.26/0.42 | 0.89 | 0.66 |
| msnr | p=500 | 0.6/0.8/0.9 | 0.18/0.18/0.18/0.89 | 1/0.18/0.79 | 0.18 | 0.18 | 0.4/0.4 | 0.2/0.4 | 0.89 | 0.59 |
| mani | p=1000 | 0.45/0.63/0.94 0.4/0.5/0.99 | 0.2/0.2/0.2/0.93 0.22/0.22/0.22/0.98 | 1/0.19/0.63 1/0.2/0.52 | 0.2 0.22 | 0.19 0.2 | 0.4/0.39 0.41/0.4 | 0.21/0.39 0.22/0.4 | 0.93 1 | 0.54 0.52 |
| | p=1500 | | | | | | | | | |
| | p=250 | 0.88/0.9/0.89 0.85/0.93/0.91 | 0.36/0.36/0.36/0.89 0.38/0.38/0.38/0.91 | 0.9/0.91/0.9 0.94/0.94/0.94 | 0.36 | 0.91 0.94 | 1/0.98 1/0.97 | 0.43/0.98 0.38/0.97 | 0.95 0.94 | 0.95 |
| lsnr | p=500 p=1000 | 0.85/0.93/0.91 | 0.38/0.38/0.38/0.93 | 0.94/0.94/0.94 | 0.38 | 0.94 | 1/0.97 | 0.39/0.96 | 0.94 | 0.94 |
| | p=1500 | 0.73/0.82/0.93 | 0.38/0.38/0.38/0.93 | 0.96/0.97/0.96 | 0.38 | 0.97 | 1/0.96 | 0.39/0.96 | 0.95 | 0.93 |
| | P | | 3130, 3130, 3130, 3130 | , , | sistency | | -7 0100 | 0.007 0.00 | | |
| | p=250 | 6/6/6 | 6/6/6/6 | 6/6/6 | 6 | 6 | 6/6 | 6/6 | 6 | 6 |
| ١. | p=500 | 6/6/6 | 6/6/6/6 | 6/6/6 | 6 | 6 | 6/6 | 6/6 | 6 | 6 |
| hsnr | p=1000 | 6/6/6 | 6/6/6/6 | 6/6/6 | 6 | 6 | 6/6 | 6/6 | 6 | 6 |
| | p=1500 | 6/6/6 | 6/6/6/6 | 6/6/6 | 6 | 6 | 6/6 | 6/6 | 6 | 6 |
| | p=250 | 6/6/6 | 6/6/6/6 | 6/1.7/5.9 | 6 | 1.7 | 6/6 | 6/6 | 6 | 6 |
| msnr | p=500 | 6/6/6 | 6/6/6/6 | 5.9/0.5/5.7 | 6 | 0.5 | 6/6 | 6/6 | 6 | 5.9 |
| | p=1000 p=1500 | 6/6/6 6/6/6 | 6/6/6/6 6/6/6/6 | 5.8/0.1/5.2 5.8/0/4.6 | 6 | 0.1 | 6/6 6/6 | 6/6 6/6 | 6 | 5.8 5.7 |
| - | 1 * | | | | | | | | | |
| | p=250 p=500 | 0.4/0.2/0.7 0.5/0.2/0.4 | 5.5/5.5/5.5/0.7 4/4/4/0.4 | 0.1/0/0.1 0.1/0/0 | 5.5 4 | 0 | 2.4/2.3 1.7/1.8 | 4.3/2.3 3.5/1.8 | 2.1 1.6 | 1.9 1.5 |
| lsnr | p=300 p=1000 | 0.5/0.2/0.4 | 2.7/2.7/2.7/0.3 | 0.1/0/0 | 2.7 | 0 | 1.3/1.3 | 2.6/1.3 | 1.0 | 1.2 |
| | p=1500 | 0.6/0.3/0.2 | 2.1/2.1/2.1/0.2 | 0/0/0 | 2.1 | ő | 1.1/1.1 | 2.1/1.1 | 1 | 0.9 |
| <u> </u> | | ' ' | , , , | Number of | extra varia | bles | | , | | |
| | p=250 | 0.2/0/0.3 | 193/193/193/0.3 | 0/0/0 | 193 | 0 | 18.2/26.6 | 29.1/26.6 | 2.5 | 0.6 |
| hsnr | p=500 | 1.7/0/0.3 | 193/193/193/0.3 | 0/0/0 | 193 | 0 | 20.5/35 | 75/35 | 3.5 | 0.5 |
| Inshr | p=1000 | 4.7/0.3/0.3 | 193/193/193/0.3 | 0/0/0 | 193 | 0 | 22.3/44.2 | 88.9/44.2 | 4.2 | 0.4 |
| | p=1500 | 7.1/1.9/0.2 | 193/193/193/0.3 | 0/0/0 | 192.9 | 0 | 23/48.8 | 90.4/48.8 | 4.4 | 0.4 |
| | p=250 | 0.5/0.2/0.3 | 193/193/193/0.3 | 0/0/0 | 193 | 0 | 18.2/26.6 | 49.3/26.6 | 1.6 | 2.3 |
| msnr | p=500 p=1000 | 3/0.6/0.3 6.6/1.9/0.4 | 193/193/193/0.4 193/193/193/0.4 | 0/0/0 0/0/0 | 193 193 | 0 | 20.7/34.9 22.4/44.3 | 98.2/34.9 100.9/44.3 | 2.1 2.6 | 3.7 4.6 |
| | p=1000 p=1500 | 9.3/4.8/0.4 | 193/193/193/0.4 | 0/0/0 | 193 | 0 | 23/48.6 | 100.9/44.3 | 2.6 | 6.2 |
| | p=1500 p=250 | | | 0/0/0 | 193.5 | 0 | 8.9/11 | | 8.1 | 6.5 |
| | p=250 p=500 | 0.5/0/0.4 2.1/0.1/0.3 | 193.5/193.5/193.5/0.4 195/195/195/0.3 | 0/0/0 0/0/0 | 193.5 195 | 0 | 8.9/11 8.5/11.9 | 69.1/11 114.5/11.9 | 8.1 9.6 | 6.5 7.6 |
| lsnr | p=300 p=1000 | 3.9/0.7/0.3 | 196.3/196.3/196.3/0.3 | 0/0/0 | 196.3 | 0 | 8.5/13.5 | 114/13.5 | 10.6 | 8.7 |
| | p=1500 | 5.6/2.6/0.2 | 196.9/196.9/196.9/0.3 | 0/0/0 | 196.9 | 0 | 8.2/12.9 | 112.5/12.9 | 10.4 | 8.9 |
| | | | | | | | | | | |

Table S41: The performance of BOSS for high dimensional data, Sparse-Ex2, ρ =0.5, n=200

| | | BOSS $C_p/AICc/CV$ | FS EBIC/HDBIC/HDHQ/CV | FSstop EBIC/HDBIC/HDHQ | FStrim HDBIC | FSstoptrim HDBIC | lasso AICc/CV | Gamma lasso AICc/CV | SparseNet CV | rlasso CV |
|----------|------------------|----------------------------------|--|---------------------------|-----------------|---------------------|------------------------|------------------------|-----------------|--------------|
| ĺ | | | | % worse than the | best possi | ble BOSS | | | | |
| | p=250 | 6/1/18 | 501/501/501/18 | 2/0/1 | 501 | 0 | 214/206 | 125/206 | 18 | 27 |
| homm | p=500 | 40/3/18 | 501/501/501/19 | 2/0/1 | 501 | 0 | 259/245 | 269/245 | 24 | 37 |
| hsnr | p=1000 | 110/16/20 | 501/501/501/22 | 2/0/0 | 501 | 0 | 304/285 | 373/285 | 26 | 55 |
| | p=1500 | 154/49/21 | 501/501/501/25 | 2/0/0 | 501 | 0 | 337/306 | 391/306 | 27 | 75 |
| | p=250 | 30/13/34 | 457/457/457/43 | 3/382/6 | 457 | 382 | 191/184 | 232/184 | 12 | 140 |
| msnr | p=500 p=1000 | 74/26/41 113/57/44 | 412/412/412/62 331/331/331/66 | 8/437/27 20/368/73 | 412 331 | 437 368 | 206/195 195/179 | 347/195 298/179 | 9 | 177 180 |
| | p=1500 | 104/80/42 | 263/263/263/67 | 29/296/96 | 263 | 296 | 172/153 | 240/153 | -2 | 157 |
| | p=250 | 7/5/8 | 162/162/162/9 | 5/5/5 | 162 | 5 | 3/4 | 113/4 | 7 | 7 |
| ١, | p=500 | 9/3/6 | 155/155/155/6 | 2/2/2 | 155 | 2 | 1/3 | 147/3 | 5 | 5 |
| lsnr | p=1000 | 16/5/5 | 153/153/153/5 | 1/1/1 | 153 | 1 | 1/3 | 148/3 | 4 | 5 |
| | p=1500 | 26/13/4 | 152/152/152/5 | 1/0/0 | 152 | 0 | 0/2 | 148/2 | 3 | 5 |
| | | | | | e efficiency | | | | | |
| | p=250 | 0.94/0.99/0.85 | 0.17/0.17/0.17/0.85 | 0.98/1/0.99 | 0.17 | 1 | 0.32/0.33 | 0.44/0.33 | 0.85 | 0.79 |
| hsnr | p=500 p=1000 | 0.72/0.97/0.85 0.48/0.86/0.83 | 0.17/0.17/0.17/0.84 0.17/0.17/0.17/0.82 | 0.98/1/0.99 0.98/1/1 | 0.17 0.17 | 1 1 | 0.28/0.29 0.25/0.26 | 0.27/0.29 0.21/0.26 | 0.8 0.79 | 0.73 0.65 |
| | p=1500 | 0.39/0.67/0.83 | 0.17/0.17/0.17/0.02 | 0.98/1/1 | 0.17 | 1 | 0.23/0.25 | 0.2/0.25 | 0.79 | 0.57 |
| <u> </u> | p=250 | 0.8/0.91/0.77 | 0.19/0.19/0.19/0.72 | 1/0.21/0.97 | 0.19 | 0.21 | 0.36/0.36 | 0.31/0.36 | 0.92 | 0.43 |
| | p=500 | 0.62/0.86/0.76 | 0.21/0.21/0.21/0.67 | 1/0.2/0.85 | 0.21 | 0.2 | 0.35/0.37 | 0.24/0.37 | 0.99 | 0.39 |
| msnr | p=1000 | 0.48/0.66/0.72 | 0.24/0.24/0.24/0.62 | 0.86/0.22/0.6 | 0.24 | 0.22 | 0.35/0.37 | 0.26/0.37 | 1 | 0.37 |
| | p=1500 | 0.48/0.54/0.69 | 0.27/0.27/0.27/0.59 | 0.76/0.25/0.5 | 0.27 | 0.25 | 0.36/0.39 | 0.29/0.39 | 1 | 0.38 |
| | p=250 | 0.97/0.98/0.96 | 0.39/0.39/0.39/0.95 | 0.98/0.99/0.98 | 0.39 | 0.99 | 1/0.99 | 0.49/0.99 | 0.97 | 0.97 |
| lsnr | p=500 | 0.93/0.99/0.96 | 0.4/0.4/0.4/0.95 | 0.99/0.99/0.99 1/1/1 | $0.4 \\ 0.4$ | 0.99 1 | 1/0.99 1/0.98 | 0.41/0.99 | 0.96 0.96 | 0.96 0.96 |
| | p=1000 p=1500 | 0.87/0.96/0.96 0.8/0.89/0.96 | 0.4/0.4/0.4/0.96 0.4/0.4/0.4/0.96 | 0.99/1/1 | 0.4 | 1 | 1/0.98 | 0.41/0.98 0.4/0.98 | 0.96 | 0.96 |
| | p-1000 | 0.070.0070.00 | 0.1/0.1/0.1/0.00 | , , | sistency | 1 | 1/0.50 | 0.4/0.50 | 0.51 | |
| - | p=250 | 6/6/6 | 6/6/6/6 | 6/6/6 | 6 | 6 | 6/6 | 6/6 | 6 | 6 |
| | p=500 | 6/6/6 | 6/6/6/6 | 6/6/6 | 6 | 6 | 6/6 | 6/6 | 6 | 6 |
| hsnr | p=1000 | 6/6/6 | 6/6/6/6 | 6/6/6 | 6 | 6 | 6/6 | 6/6 | 6 | 6 |
| | p=1500 | 6/6/6 | 6/6/6/6 | 6/6/6 | 6 | 6 | 6/6 | 6/6 | 6 | 6 |
| | p=250 | 6/6/6 | 6/6/6/6 | 6/1.5/5.9 | 6 | 1.5 | 6/6 | 6/6 | 6 | 5.9 |
| msnr | p=500 p=1000 | 6/6/6 | 6/6/6/5.9 6/6/6/5.7 | 5.9/0.3/5.6 5.6/0/4.7 | 6 | 0.3 0 | 5.9/6 | 6/6 6/5.9 | 6 | 5.8 5.6 |
| | p=1000 p=1500 | 5.9/5.9/5.9 5.8/5.8/5.7 | 5.9/5.9/5.9/5.3 | 5.1/0/3.8 | 5.9 | 0 | 5.7/5.9 5.3/5.6 | 5.9/5.6 | 6 | 5.0 |
| | p=250 | 0.2/0.1/0.5 | 5.5/5.5/5.5/0.3 | 0/0/0 | 5.5 | 0 | 1/1 | 4/1 | 1 | 0.9 |
| | p=500 | 0.2/0.1/0.2 | 3.6/3.6/3.6/0.2 | 0/0/0 | 3.6 | ő | 0.7/0.7 | 2.8/0.7 | 0.7 | 0.6 |
| lsnr | p=1000 | 0.2/0.1/0.1 | 2.1/2.1/2.1/0.1 | 0/0/0 | 2.1 | 0 | 0.5/0.5 | 1.8/0.5 | 0.5 | 0.4 |
| | p=1500 | 0.2/0.1/0.1 | 1.5/1.5/1.5/0.1 | 0/0/0 | 1.5 | 0 | 0.4/0.4 | 1.3/0.4 | 0.4 | 0.3 |
| | | | | Number of | extra varia | bles | | | | |
| | p=250 | 0.2/0/0.3 | 193/193/193/0.3 | 0/0/0 | 193 | 0 | 27.9/43.8 | 19.2/43.8 | 2.7 | 1 |
| hsnr | p=500 | 2.5/0/0.3 | 193/193/193/0.3 | 0/0/0 | 193 | 0 | 31.8/58.1 | 53.8/58.1 | 3.9 | 1.3 |
| 110111 | p=1000 p=1500 | 6.9/0.7/0.3 8.6/2.4/0.3 | 193/193/193/0.3 193/193/193/0.3 | 0/0/0 0/0/0 | 193 192.9 | 0 | 35.4/76.2 36.9/86 | 80.3/76.2 83.5/86 | 4.5 5 | 3.2 |
| _ | p=250 | 0.9/0.3/0.6 | 193/193/193/1 | 0.1/0/0.1 | 193 | 0 | 27.7/43.8 | 39.5/43.8 | 2.4 | 10.9 |
| | p=500 | 4.3/0.8/0.9 | 193/193/193/1.6 | 0.2/0/0.1 | 193 | 0 | 31.4/57.4 | 89.5/57.4 | 4.1 | 20.8 |
| msnr | p=1000 | 9.2/3/1.3 | 193/193/193/2.1 | 0.3/0/0.1 | 193 | 0 | 32/71.9 | 97.2/71.9 | 7.6 | 35.4 |
| | p=1500 | 10.9/6.7/1.7 | 193.1/193.1/193.1/2.2 | 0.3/0/0.1 | 193 | 0 | 29.5/74.2 | 97.6/74.2 | 11.5 | 42.2 |
| | p=250 | 0.3/0/0.6 | 193.5/193.5/193.5/0.4 | 0/0/0 | 193.5 | 0 | 6.1/7.2 | 65.5/7.2 | 6.3 | 5.1 |
| lsnr | p=500 | 1.2/0.1/0.3 | 195.4/195.4/195.4/0.3 | 0/0/0 | 195.4 | 0 | 6.6/7.7 | 111.7/7.7 | 7.1 | 5.6 |
| | p=1000 p=1500 | 2.5/0.5/0.3 4/1.7/0.2 | 196.9/196.9/196.9/0.3 197.5/197.5/197.5/0.3 | 0/0/0 0/0/0 | 196.9 197.4 | 0 | 6.5/9.2 6.8/9.4 | 112.7/9.2 111/9.4 | $7.9 \\ 7.4$ | 5.9 6.5 |
| | P-1900 | 4/1.1/0.2 | 101.0/101.0/101.0/0.0 | 0/0/0 | 131.4 | 0 | 0.0/ 3.4 | 111/ 3.4 | 1.4 | 0.0 |

Table S42: The performance of BOSS for high dimensional data, Sparse-Ex2, ρ =0.9, n=200

| | | $\begin{array}{c} {\rm BOSS} \\ {\rm C}_p/{\rm AICc/CV} \end{array}$ | FS EBIC/HDBIC/HDHQ/CV | FSstop EBIC/HDBIC/HDHQ | FStrim HDBIC | FSstoptrim HDBIC | lasso AICc/CV | Gamma lasso AICc/CV | SparseNet CV | rlasso CV |
|------|------------------|--|--|----------------------------------|-----------------|---------------------|-----------------------------|------------------------|-----------------|----------------|
| | | | | % worse than the | best possi | ible BOSS | | | | |
| | p=250 | 18/13/68 | 225/225/225/128 | 37/137/49 | 225 | 116 | 186/147 | -7/147 | -36 | 116 |
| hsnr | p=500 | 106/69/105 | 70/70/70/141 | 96/180/111 | 70 | 174 | 275/234 | -31/234 | -30 | 221 |
| nsnr | p=1000 | 97/68/108 | 22/22/22/129 | 91/159/106 | 22 | 158 | 177/178 | 21/178 | 158 | 176 |
| | p=1500 | 91/84/116 | 7/7/7/132 | 111/147/122 | 7 | 147 | 137/133 | 8/133 | 134 | 131 |
| | p=250 | 23/21/18 | 68/68/68/61 | 57/82/64 | 68 | 82 | 75/70 | -4/70 | -9 | 70 |
| msnr | p=500 | 14/14/15 | 21/21/21/26 | 24/32/27 | 21 | 32 | 27/27 | 6/27 | 27 | 27 |
| mam | p=1000 p=1500 | 11/11/13 10/10/12 | 11/11/11/19 7/7/7/15 | 18/22/20 | 11 7 | 22 17 | 18/18 12/12 | 2/18 -2/12 | 19 12 | 18 12 |
| | • | , , | , , , | 15/17/16 | | | | | | |
| | p=250 p=500 | 3/3/6 | 157/157/157/7 153/153/153/5 | $\frac{3/3/3}{1/1/1}$ | 157 153 | 3 1 | $\frac{3}{4}$ $\frac{2}{2}$ | 83/4 132/2 | 5 4 | 6 5 |
| lsnr | p=500 p=1000 | 5/1/5 12/2/4 | 153/153/153/5 | 0/0/0 | 153 | 0 | 1/2 | 138/2 | 4 | 5 5 |
| | p=1500 | 21/9/4 | 151/151/151/5 | 0/0/0 | 151 | 0 | 1/2 | 140/2 | 3 | 5 |
| | 1 | 7-7 | .,.,.,. | , , | e efficiency | | | -/ | | |
| | p=250 | 0.54/0.56/0.38 | 0.2/0.2/0.2/0.28 | 0.47/0.27/0.43 | 0.2 | 0.3 | 0.22/0.26 | 0.69/0.26 | 1 | 0.3 |
| hsnr | p=500 | 0.34/0.41/0.34 | 0.41/0.41/0.41/0.29 | 0.35/0.25/0.33 | 0.41 | 0.25 | 0.18/0.21 | 1/0.21 | 0.98 | 0.21 |
| nsnr | p=1000 | 0.61/0.72/0.58 | 0.99/0.99/0.99/0.53 | 0.63/0.47/0.59 | 0.99 | 0.47 | 0.44/0.43 | 1/0.43 | 0.47 | 0.44 |
| | p=1500 | 0.56/0.58/0.49 | 1/1/1/0.46 | 0.51/0.43/0.48 | 1 | 0.43 | 0.45/0.46 | 0.98/0.46 | 0.45 | 0.46 |
| | p=250 | 0.74/0.76/0.77 | 0.54/0.54/0.54/0.57 | 0.58/0.5/0.56 | 0.54 | 0.5 | 0.52/0.54 | 0.95/0.54 | 1 | 0.54 |
| msnr | p=500 | 0.93/0.93/0.92 | 0.88/0.88/0.88/0.84 | 0.85/0.8/0.83 | 0.88 | 0.8 | 0.83/0.83 | 1/0.83 | 0.84 | 0.83 |
| | p=1000 p=1500 | 0.92/0.91/0.9 0.89/0.89/0.87 | 0.91/0.91/0.91/0.86 0.92/0.92/0.92/0.85 | 0.86/0.83/0.85 0.85/0.84/0.84 | 0.91 0.92 | 0.83 0.84 | 0.86/0.86 0.87/0.87 | 1/0.86 1/0.87 | 0.86 0.87 | 0.86 0.87 |
| | | | | | | | | , | | |
| | p=250 p=500 | 0.99/1/0.97 0.96/1/0.96 | 0.4/0.4/0.4/0.96 0.4/0.4/0.4/0.96 | $\frac{1}{1}$ $\frac{1}{1}$ | 0.4 | 1 1 | 0.99/0.99 0.99/0.99 | 0.56/0.99 0.43/0.99 | 0.97 0.97 | 0.97 0.96 |
| lsnr | p=300 p=1000 | 0.9/0.98/0.96 | 0.4/0.4/0.4/0.96 | 1/1/1 | 0.4 | 1 | 0.99/0.99 | 0.42/0.98 | 0.97 | 0.96 |
| | p=1500 | 0.83/0.92/0.96 | 0.4/0.4/0.4/0.96 | 1/1/1 | 0.4 | 1 | 1/0.98 | 0.42/0.98 | 0.97 | 0.95 |
| | - | | , , , | Spar | sistency | | | , | | |
| | p=250 | 6/6/6 | 6/6/6/5.8 | 5.6/4.7/5.5 | 6 | 4.7 | 6/6 | 6/6 | 6 | 6 |
| hsnr | p=500 | 4.7/4.7/4.7 | 5.4/5.4/5.4/3.4 | 3.9/2.2/3.6 | 5.4 | 2.2 | 1.4/2.2 | 6/2.2 | 6 | 2.3 |
| nsm | p=1000 | 3.7/3.7/3.5 | 4.3/4.3/4.3/1.9 | 2.9/0.8/2.5 | 4.3 | 0.8 | 0.8/0.7 | 3.1/0.7 | 1.2 | 0.8 |
| | p=1500 | 2.4/2.4/2.1 | 3/3/3/0.8 | 1.5/0.1/1.1 | 3 | 0.1 | 0.8/0.8 | 1.9/0.8 | 0.8 | 0.8 |
| | p=250 | 4.1/3.9/4.5 | 5.8/5.8/5.8/1.6 | 1.5/0.1/1.1 | 5.8 | 0.1 | 1/1.5 | 5.8/1.5 | 5.7 | 1.5 |
| msnr | p=500 p=1000 | 1.9/1.8/1.9 1.3/1.2/1.1 | 4/4/4/0.6 2.6/2.6/2.6/0.4 | 0.7/0/0.4 0.4/0/0.2 | 4 2.6 | 0 | 0.7/0.6 0.4/0.4 | 2.5/0.6 1.7/0.4 | 0.7 0.4 | 0.5 0.4 |
| | p=1500 | 0.8/0.8/0.6 | 1.8/1.8/1.8/0.2 | 0.2/0/0.1 | 1.8 | 0 | 0.4/0.4 | 1.3/0.4 | 0.4 | 0.4 |
| | p=250 | 0.1/0.1/0.2 | 4.9/4.9/4.9/0.1 | 0/0/0 | 4.9 | 0 | 0.2/0.2 | 1.4/0.2 | 0.2 | 0.2 |
| | p=500 | 0.1/0.1/0.2 | 2.5/2.5/2.5/0 | 0/0/0 | 2.5 | 0 | 0.2/0.2 | 1.3/0.1 | 0.2 | 0.2 |
| lsnr | p=1000 | 0.1/0/0 | 1.3/1.3/1.3/0 | 0/0/0 | 1.3 | ő | 0.1/0.1 | 0.8/0.1 | 0.1 | 0.1 |
| | p=1500 | 0/0/0 | 0.9/0.9/0.9/0 | 0/0/0 | 0.9 | 0 | 0.1/0.1 | 0.5/0.1 | 0.1 | 0.1 |
| | | | | Number of | extra varia | bles | | | | |
| | p=250 | 9.4/6.3/11.3 | 193/193/193/23.8 | 4/2/3.6 | 193 | 0 | 68.2/108.6 | 9.5/108.6 | 4.2 | 49.7 |
| hsnr | p=500 | 12.7/9/11.2 | 193.6/193.6/193.6/10.4 | 3.4/1/2.6 | 193.6 | 0 | 9.6/35.3 | 33.7/35.3 | 56.3 | 36.3 |
| | p=1000 p=1500 | 6.3/6.8/5.8 6.4/5.7/3.7 | 194.7/194.7/194.7/3.5 196/196/196/1.1 | 2.3/0.3/1.5 1.1/0/0.6 | 194.6 195.9 | 0 | 6.1/6.3 8.6/13.4 | 89/6.3 94/13.4 | 16.4 11.3 | 4.9 9.9 |
| | • | , , | , , , | , , | | | | , | | |
| | p=250 p=500 | 13.6/10.4/16.5 3.8/3.2/4.4 | 193.2/193.2/193.2/2.9 195/195/195/0.9 | 0.5/0/0.2 0.2/0/0.1 | 193.2 195 | 0 | 6.8/19.3 5.9/7.3 | 52.7/19.3 82.8/7.3 | 65.4 7.7 | 16.7 5.1 |
| msnr | p=300 p=1000 | 2.9/2.1/1.8 | 196.4/196.3/196.4/0.4 | 0.1/0/0 | 196.3 | 0 | 5.5/6.2 | 95.5/6.2 | 5.2 | 4.8 |
| | p=1500 | 3.9/2.7/1 | 197.2/197.2/197.2/0.4 | 0/0/0 | 197.1 | 0 | 6.8/8.8 | 97.8/8.8 | 7.3 | 6.1 |
| | p=250 | 0.2/0.1/0.6 | 194.1/194.1/194.1/0.3 | 0/0/0 | 194.1 | 0 | 4.5/4.4 | 51.1/4.4 | 4.2 | 3.3 |
| | p=500 | 0.7/0.1/0.3 | 196.5/196.5/196.5/0.3 | 0/0/0 | 196.5 | ő | 5.5/5.6 | 102.5/5.6 | 5.4 | 4.5 |
| lsnr | p=1000 | 1.9/0.3/0.3 | 197.7/197.7/197.7/0.3 | 0/0/0 | 197.7 | 0 | 5.6/7.5 | 105.8/7.5 | 6 | 5.2 |
| | p=1500 | 3.4/1.3/0.2 | 198.1/198.1/198.1/0.3 | 0/0/0 | 198.1 | 0 | 6.1/7.7 | 105.5/7.7 | 6.3 | 6 |

Table S43: The performance of BOSS for high dimensional data, Sparse-Ex3, ρ =0, n=200

| | | $\begin{array}{c c} \operatorname{BOSS} \\ \operatorname{C}_p/\operatorname{AICc/CV} \end{array}$ | FS EBIC/HDBIC/HDHQ/CV | FSstop EBIC/HDBIC/HDHQ | FStrim HDBIC | FSstoptrim HDBIC | lasso AICc/CV | Gamma lasso AICc/CV | SparseNet CV | rlasso CV |
|--------|---------------------------|---|---|---------------------------------|-------------------------|---------------------|------------------------|--------------------------------------|--------------------|--------------|
| | | | | % worse than the | best possi | ble BOSS | | | | |
| | p=250 | 6/1/18 | 501/501/501/18 | 2/0/1 | 501 | 0 | 131/134 | 189/134 | 18 | 15 |
| hsnr | p = 500 | 24/2/18 | 501/501/501/19 | 2/0/1 | 501 | 0 | 151/155 | 364/155 | 23 | 17 |
| nsnr | p=1000 | 74/12/20 | 501/501/501/20 | 2/0/0 | 501 | 0 | 173/179 | 417/179 | 24 | 16 |
| | p=1500 | 128/40/19 | 501/501/501/21 | 2/0/0 | 501 | 0 | 185/193 | 430/193 | 27 | 15 |
| | p=250 | 21/10/19 | 498/498/498/19 | 6/221/10 | 498 | 223 | 130/133 | 313/133 | 20 | 20 |
| msnr | p=500 | 57/24/20 | 496/496/496/21 | 9/383/21 | 496 | 385 | 149/153 | 448/153 | 25 | 26 |
| mom | p=1000 p=1500 | 134/63/24 194/121/24 | 494/494/494/24 493/493/493/26 | 13/509/45 17/553/64 | 494 493 | 510 553 | 170/177 181/190 | 464/177 467/190 | 29 29 | 36 42 |
| | • | , , | , , , | , , | | | | | | |
| . | p=250 p=500 | 18/18/15 24/14/13 | 168/168/168/15 154/154/154/12 | 19/24/21 14/18/16 | 168 154 | 24 18 | -4/0 | 124/0 148/0 | 3 4 | 2 3 |
| lsnr | p=500 p=1000 | 37/18/10 | 144/144/144/10 | 11/13/12 | 144 | 13 | -3/0 -3/2 | 140/2 | 4 | 4 |
| . | p=1500 | 46/29/9 | 139/139/139/10 | 9/11/10 | 139 | 11 | -3/3 | 137/3 | 5 | 5 |
| | 1 | -7 -7- | | , , | efficiency | | -,- | , | | |
| T | p=250 | 0.95/0.99/0.85 | 0.17/0.17/0.17/0.85 | 0.98/1/0.99 | 0.17 | 1 | 0.43/0.43 | 0.35/0.43 | 0.85 | 0.87 |
| hsnr | p=500 | 0.81/0.98/0.85 | 0.17/0.17/0.17/0.84 | 0.98/1/0.99 | 0.17 | 1 | 0.4/0.39 | 0.22/0.39 | 0.81 | 0.86 |
| IISIII | p=1000 | 0.58/0.9/0.84 | 0.17/0.17/0.17/0.83 | 0.98/1/1 | 0.17 | 1 | 0.37/0.36 | 0.19/0.36 | 0.8 | 0.86 |
| | p=1500 | 0.44/0.72/0.84 | 0.17/0.17/0.17/0.83 | 0.98/1/1 | 0.17 | 1 | 0.35/0.34 | 0.19/0.34 | 0.79 | 0.87 |
| . | p=250 | 0.88/0.96/0.89 | 0.18/0.18/0.18/0.89 | 1/0.33/0.96 | 0.18 | 0.33 | 0.46/0.46 | 0.26/0.46 | 0.88 | 0.88 |
| msnr | p=500 | 0.69/0.88/0.91 | 0.18/0.18/0.18/0.91 | 1/0.23/0.91 | 0.18 | 0.23 | 0.44/0.43 | 0.2/0.43 | 0.88 | 0.87 |
| | p=1000 p=1500 | 0.48/0.69/0.91 0.4/0.53/0.94 | 0.19/0.19/0.19/0.91 0.2/0.2/0.2/0.93 | 1/0.19/0.78 1/0.18/0.71 | 0.19 | 0.19 0.18 | 0.42/0.41 0.42/0.4 | 0.2/0.41 0.21/0.4 | 0.88 0.91 | 0.83 0.83 |
| | p=1500 p=250 | | | | 0.36 | 0.78 | 1/0.97 | 0.43/0.97 | 0.94 | 0.94 |
| . | p=250 p=500 | 0.82/0.82/0.84 0.78/0.84/0.86 | 0.36/0.36/0.36/0.84 0.38/0.38/0.38/0.86 | 0.81/0.78/0.8 0.84/0.82/0.83 | 0.36 | 0.78 | 1/0.97 | 0.43/0.97 | 0.94 | 0.94 |
| lsnr | p=1000 | 0.71/0.82/0.88 | 0.4/0.4/0.4/0.88 | 0.88/0.86/0.87 | 0.36 | 0.86 | 1/0.95 | 0.4/0.95 | 0.94 | 0.94 |
| . 1 | p=1500 | 0.67/0.75/0.89 | 0.41/0.41/0.41/0.89 | 0.89/0.88/0.88 | 0.41 | 0.88 | 1/0.95 | 0.41/0.95 | 0.93 | 0.93 |
| | | | | Spars | sistency | | - | | | i |
| | p=250 | 6/6/6 | 6/6/6/6 | 6/6/6 | 6 | 6 | 6/6 | 6/6 | 6 | 6 |
| hsnr | p=500 | 6/6/6 | 6/6/6/6 | 6/6/6 | 6 | 6 | 6/6 | 6/6 | 6 | 6 |
| 115111 | p=1000 | 6/6/6 | 6/6/6/6 | 6/6/6 6/6/6 | 6 6 | 6 6 | 6/6 | 6/6 6/6 | 6 6 | 6 |
| | p=1500 | 6/6/6 | 6/6/6/6 | , , | | | 6/6 | | | |
| . | p=250 p=500 | 6/6/6 6/6/6 | 6/6/6/6 | 6/4.2/5.9 5.9/2.7/5.9 | 6 6 | 4.2 2.7 | 6/6 | 6/6 6/6 | 6 6 | 6 |
| msnr | p=500 p=1000 | 6/6/6 | 6/6/6/6 6/6/6/6 | 5.9/2.1/5.9 5.9/1.4/5.7 | 6 | 1.4 | 6/6 6/6 | 6/6 | 6 | 6 |
| . | p=1500 | 6/6/6 | 6/6/6/6 | 5.9/0.9/5.5 | 6 | 0.9 | 6/6 | 6/6 | 6 | 6 |
| | p=250 | 1.2/0.7/1.4 | 5.6/5.6/5.6/1.4 | 0.5/0/0.3 | 5.6 | 0 | 3.9/3.9 | 4.5/3.9 | 3.3 | 3.1 |
| . | p=500 | 1.3/0.7/1 | 4.4/4.4/4.4/1 | 0.3/0/0.1 | 4.4 | 0 | 3.3/3.4 | 4/3.4 | 2.8 | 2.6 |
| lsnr | p=1000 | 1.3/0.8/0.7 | 3.2/3.2/3.2/0.7 | 0.2/0/0.1 | 3.2 | 0 | 2.6/2.8 | 3.1/2.8 | 2.3 | 2.2 |
| . | p=1500 | 1.3/0.9/0.6 | 2.6/2.6/2.6/0.6 | 0.2/0/0.1 | 2.6 | 0 | 2.4/2.4 | 2.7/2.4 | 2 | 2 |
| | | | | Number of | extra varia | bles | | | | |
| . | p=250 | 0.4/0/0.3 | 193/193/193/0.3 | 0/0/0 | 193 | 0 | 15.1/22.3 | 29.1/22.3 | 2.5 | 0.5 |
| hsnr | p=500 | 1.4/0/0.3 | 193/193/193/0.3 | 0/0/0 | 193 | 0 | 17.1/27.7 | 74.4/27.7 | 3.6 | 0.8 |
| | p=1000 p=1500 | 3.9/0.4/0.3 6.8/1.9/0.2 | 193/193/193/0.3 193/193/193/0.3 | 0/0/0 0/0/0 | 193 192.9 | 0 | 19.2/35.4 19.3/40.1 | 87.2/35.4 89.7/40.1 | 4.2 4.7 | 0.8 0.8 |
| | • | , , | | 0/0/0 | | 0 | | , | 1.7 | |
| . | p=250 p=500 | 0.6/0.1/0.3 2/0.3/0.3 | 193/193/193/0.3 193/193/193/0.3 | 0/0/0 | 193 193 | 0 | 15.1/22.3 17.2/27.7 | 49.9/22.3 97.2/27.7 | 2.4 | 0.6 1.2 |
| msnr | p=300 p=1000 | 5.4/1.4/0.3 | 193/193/193/0.3 | 0/0/0 | 193 | 0 | 18.9/35.8 | 100.1/35.8 | 2.4 | 1.3 |
| . | p=1500 | 8.3/3.8/0.3 | 193/193/193/0.3 | 0/0/0 | 192.9 | 0 | 19.4/40.4 | 99.6/40.4 | 2.6 | 1.8 |
| - | p=250 | 1/0.1/0.5 | 193.4/193.4/193.4/0.5 | 0/0/0 | 193.4 | 0 | 10.8/14.6 | 69.8/14.6 | 10.3 | 7 |
| | | | | | | | | | | 8.2 |
| ' , | p=500 | 2.6/0.2/0.5 | 194.6/194.6/194.6/0.4 | 0/0/0 | 194.6 | 0 | 11.3/15.7 | 113.8/15.7 | 11 | 8.2 |
| lsnr | p=500 p=1000 p=1500 | 2.6/0.2/0.5 6.1/1.5/0.3 8/4/0.3 | 194.6/194.6/194.6/0.4 195.8/195.8/195.8/0.3 196.3/196.3/196.3/0.3 | 0/0/0 0/0/0 0/0/0 | 194.6 195.8 196.3 | 0 0 0 | 11.2/18.9 11.1/20 | 113.8/15.7 113.7/18.9 111.8/20 | 11 13.5 14.5 | 10.2 11.4 |

Table S44: The performance of BOSS for high dimensional data, Sparse-Ex3, ρ =0.5, n=200

| | | $\frac{\mathrm{BOSS}}{\mathrm{C}_p/\mathrm{AICc/CV}}$ | FS EBIC/HDBIC/HDHQ/CV | FSstop EBIC/HDBIC/HDHQ | FStrim HDBIC | FSstoptrim HDBIC | lasso AICc/CV | Gamma lasso AICc/CV | SparseNet CV | rlasso CV |
|-------|------------------|---|--|-----------------------------|-----------------|---------------------|------------------------|--------------------------|-----------------|--------------|
| | | | | % worse than the | best possi | ible BOSS | | | | |
| | p=250 p=500 | 6/1/16 24/2/18 | 495/495/495/19 495/495/495/20 | 2/0/1 2/0/1 | 495 495 | 0 | 135/137 156/159 | 182/137 356/159 | 19 24 | 16 16 |
| hsnr | p=1000 | 79/11/19 | 495/495/495/20 | 2/0/0 | 495 | 0 | 179/185 | 412/185 | 25 | 15 |
| | p=1500 | 124/44/18 | 495/495/495/20 | 2/0/0 | 495 | 0 | 191/199 | 425/199 | 26 | 14 |
| | p=250 p=500 | 22/11/18 61/26/19 | 492/492/492/20 490/490/490/22 | 4/234/8 7/408/19 | 492 490 | 236 409 | 134/136 153/157 | 304/136 441/157 | 19 24 | 24 33 |
| msnr | p=500 p=1000 | 133/62/23 | 488/488/488/24 | 11/515/41 | 488 | 409 515 | 176/182 | 458/182 | 27 | 33 46 |
| | p=1500 | 190/122/22 | 486/486/486/24 | 15/549/63 | 486 | 549 | 187/195 | 460/195 | 27 | 56 |
| | p=250 | 17/17/14 | 166/166/166/14 | 17/21/19 | 166 | 21 | -3/0 | 122/0 | 4 | 3 |
| lsnr | p=500 | 23/13/12 | 153/153/153/12 | 13/15/14 | 153 | 15 | -3/1 | 148/1 | 4 | 3 |
| | p=1000 p=1500 | 35/17/10 44/28/9 | 144/144/144/10 140/140/140/9 | 9/11/10 8/9/9 | 144 140 | 11 9 | -3/2 -2/3 | 141/2 138/3 | 4 5 | 4 6 |
| | | | | Relative | efficiency | | , | | | |
| | p=250 | 0.95/0.99/0.86 | 0.17/0.17/0.17/0.84 | 0.98/1/0.99 | 0.17 | 1 | 0.43/0.42 | 0.35/0.42 | 0.84 | 0.86 |
| hsnr | p=500 p=1000 | 0.8/0.98/0.85 0.56/0.9/0.84 | 0.17/0.17/0.17/0.83 0.17/0.17/0.17/0.84 | 0.98/1/0.99 0.98/1/1 | 0.17 0.17 | 1 1 | 0.39/0.39 0.36/0.35 | 0.22/0.39 0.2/0.35 | 0.81 0.8 | 0.86 0.87 |
| | p=1000 p=1500 | 0.45/0.7/0.85 | 0.17/0.17/0.17/0.84 | 0.98/1/1 | 0.17 | 1 | 0.34/0.33 | 0.2/0.33 | 0.8 | 0.88 |
| | p=250 | 0.86/0.94/0.89 | 0.18/0.18/0.18/0.87 | 1/0.31/0.96 | 0.18 | 0.31 | 0.45/0.44 | 0.26/0.44 | 0.87 | 0.84 |
| msnr | p=500 | 0.67/0.85/0.9 | 0.18/0.18/0.18/0.88 | 1/0.21/0.9 | 0.18 | 0.21 | 0.42/0.42 | 0.2/0.42 | 0.87 | 0.81 |
| msnr | p=1000 | 0.48/0.68/0.9 0.39/0.52/0.94 | 0.19/0.19/0.19/0.9 0.2/0.2/0.2/0.92 | 1/0.18/0.79 | 0.19 | 0.18 0.18 | 0.4/0.39 0.4/0.39 | 0.2/0.39 0.2/0.39 | 0.88 | 0.76 |
| | p=1500 p=250 | 0.83/0.83/0.85 | 0.2/0.2/0.2/0.92 | 1/0.18/0.7 0.83/0.8/0.82 | 0.2 | 0.18 | 1/0.97 | 0.2/0.39 | 0.94 | 0.73 |
| | p=250 p=500 | 0.83/0.83/0.83 | 0.38/0.38/0.38/0.87 | 0.86/0.84/0.85 | 0.38 | 0.8 | 1/0.97 | 0.39/0.96 | 0.94 | 0.95 |
| lsnr | p=1000 | 0.72/0.83/0.89 | 0.4/0.4/0.4/0.89 | 0.89/0.88/0.88 | 0.4 | 0.88 | 1/0.96 | 0.41/0.96 | 0.94 | 0.93 |
| | p=1500 | 0.68/0.76/0.9 | 0.41/0.41/0.41/0.9 | 0.9/0.89/0.9 | 0.41 | 0.89 | 1/0.95 | 0.41/0.95 | 0.93 | 0.92 |
| | | | | Spar | sistency | | | | | |
| | p=250 | 6/6/6 | 6/6/6/6 | 6/6/6 | 6 | 6 | 6/6 | 6/6 | 6 | 6 |
| hsnr | p=500 p=1000 | 6/6/6 6/6/6 | 6/6/6/6 6/6/6/6 | 6/6/6 6/6/6 | 6 | 6 6 | 6/6 6/6 | 6/6 6/6 | 6 6 | 6 6 |
| | p=1500 | 6/6/6 | 6/6/6/6 | 6/6/6 | 6 | 6 | 6/6 | 6/6 | 6 | 6 |
| | p=250 | 6/6/6 | 6/6/6/6 | 6/4/5.9 | 6 | 4 | 6/6 | 6/6 | 6 | 6 |
| msnr | p=500 | 6/6/6 | 6/6/6/6 | 6/2.3/5.9 | 6 | 2.3 | 6/6 | 6/6 | 6 | 6 |
| mom | p=1000 p=1500 | 6/6/6 6/6/6 | 6/6/6/6 6/6/6/6 | 5.9/1.2/5.7 5.9/0.8/5.5 | 6 | 1.2 0.8 | 6/6 6/6 | 6/6 6/6 | 6 | 6 5.9 |
| | p=250 | 1.1/0.6/1.2 | 5.5/5.5/5.5/1.3 | 0.4/0/0.2 | 5.5 | 0 | 3.6/3.6 | 4.3/3.6 | 3 | 2.9 |
| | p=500 | 1.2/0.5/0.9 | 4.2/4.2/4.2/0.9 | 0.3/0/0.1 | 4.2 | 0 | 3/3 | 3.8/3 | 2.6 | 2.4 |
| lsnr | p=1000 | 1.1/0.7/0.6 | 3/3/3/0.6 | 0.2/0/0.1 | 3 | 0 | 2.3/2.4 | 2.9/2.4 | 2.1 | 2 |
| | p=1500 | 1.2/0.8/0.5 | 2.5/2.5/2.5/0.5 | 0.2/0/0 | 2.5 | 0 | 2.1/2.2 | 2.5/2.2 | 1.9 | 1.7 |
| | p=250 | 0.3/0/0.3 | 193/193/193/0.3 | Number of 0/0/0 | extra varia | bles 0 | 15.8/23.3 | 28.2/23.3 | 2.6 | 0.5 |
| | p=250 p=500 | 1.4/0/0.3 | 193/193/193/0.3 | 0/0/0 | 193 | 0 | 17.7/29.6 | 73.4/29.6 | 3.7 | 0.6 |
| hsnr | p=1000 | 4.4/0.4/0.3 | 193/193/193/0.3 | 0/0/0 | 193 | 0 | 19.6/37.8 | 87.6/37.8 | 4.1 | 0.6 |
| | p=1500 | 6.7/2.2/0.2 | 193/193/193/0.3 | 0/0/0 | 192.9 | 0 | 20.4/42.7 | 89.5/42.7 | 4.6 | 0.5 |
| | p=250 | 0.5/0.1/0.3 | 193/193/193/0.3 | 0/0/0 | 193 | 0 | 15.9/23.3 | 48.6/23.3 | 1.6 | 0.8 |
| msnr | p=500 p=1000 | 2.3/0.4/0.3 5.5/1.4/0.3 | 193/193/193/0.3 193/193/193/0.3 | 0/0/0 0/0/0 | 193 193 | 0 | 18/29.7 19.6/37.9 | 96.8/29.7 100.4/37.9 | 2.2 2.5 | 1.7 1.8 |
| | p=1000 p=1500 | 8.4/3.9/0.3 | 193/193/193/0.3 | 0/0/0 | 193 | 0 | 20.6/43 | 99.7/43 | 2.5 | 2.4 |
| | p=250 | 0.8/0.1/0.5 | 193.5/193.5/193.5/0.5 | 0/0/0 | 193.5 | 0 | 10.3/14.4 | 69.3/14.4 | 10.3 | 7.1 |
| lsnr | p=500 | 2.9/0.2/0.4 | 194.8/194.8/194.8/0.4 | 0/0/0 | 194.8 | 0 | 11.2/15.8 | 114.6/15.8 | 11.2 | 8.6 |
| ıSIII | p=1000 p=1500 | 5.7/1.5/0.4 7.6/3.8/0.3 | 196/196/196/0.4 196.5/196.5/196.5/0.3 | 0/0/0 0/0/0 | 196 196.4 | 0 | 10.9/18.1 10.7/18.8 | 113.7/18.1 112.5/18.8 | 13.8 14.1 | 10.1 12 |
| | h=1900 | 1.0/3.8/0.3 | 190.0/190.0/190.0/0.3 | 0/0/0 | 190.4 | U | 10.7/18.8 | 112.0/18.8 | 14.1 | 12 |

Table S45: The performance of BOSS for high dimensional data, Sparse-Ex3, ρ =0.9, n=200

| | | BOSS $C_p/AICc/CV$ | FS EBIC/HDBIC/HDHQ/CV | FSstop EBIC/HDBIC/HDHQ | FStrim HDBIC | FSstoptrim HDBIC | lasso AICc/CV | Gamma lasso AICc/CV | SparseNet CV | rlasso CV |
|---------|------------------|---------------------------------|--|---------------------------------|-----------------|---------------------|------------------------|------------------------|-----------------|--------------|
| i | | | | % worse than the | best possi | ible BOSS | | | | |
| | p=250 | 8/3/30 | 477/477/477/33 | 3/13/4 | 477 | 13 | 135/137 | 167/137 | 17 | 16 |
| hsnr | p=500 | 28/6/33 | 476/476/476/34 | 4/13/7 | 476 | 13 | 156/159 | 334/159 | 22 | 17 |
| nsnr | p=1000 | 85/17/34 | 475/475/475/35 | 6/13/9 | 475 | 13 | 179/183 | 393/183 | 22 | 17 |
| | p=1500 | 123/52/32 | 474/474/474/34 | 6/13/10 | 474 | 13 | 191/196 | 405/196 | 24 | 18 |
| | p=250 | 15/7/12 | 367/367/367/13 | 2/172/4 | 367 | 172 | 91/92 | 217/92 | 3 | 13 |
| msnr | p=500 p=1000 | 44/17/13 103/44/15 | 366/366/366/13 365/365/365/17 | 4/315/11 7/401/27 | 366 365 | 315 401 | 107/110 126/130 | 327/110 342/130 | 5 10 | 21 37 |
| | p=1500 | 140/92/16 | 364/364/364/17 | 9/426/42 | 364 | 426 | 135/139 | 343/139 | 11 | 45 |
| | p=250 | 16/15/14 | 164/164/164/14 | 16/18/17 | 164 | 18 | -3/0 | 118/0 | 3 | 3 |
| ١, ١ | p=500 | 21/12/11 | 151/151/151/11 | 11/12/12 | 151 | 12 | -3/0 | 145/0 | 2 | 3 |
| lsnr | p=1000 | 33/15/9 | 142/142/142/9 | 8/9/8 | 142 | 9 | -3/2 | 139/2 | 4 | 4 |
| | p=1500 | 41/27/8 | 139/139/139/8 | 7/7/7 | 139 | 7 | -3/2 | 136/2 | 4 | 6 |
| | | | | | efficiency | | | | | |
| | p=250 | 0.96/1/0.79 0.81/0.99/0.79 | 0.18/0.18/0.18/0.77 | 1/0.91/0.99 | 0.18 | 0.91 | 0.44/0.43 | 0.39/0.43 | 0.88 | 0.89 |
| hsnr | p=500 p=1000 | 0.81/0.99/0.79 | 0.18/0.18/0.18/0.78 0.18/0.18/0.18/0.78 | 1/0.92/0.98 1/0.94/0.97 | 0.18 0.18 | 0.92 0.94 | 0.41/0.4 0.38/0.37 | 0.24/0.4 0.21/0.37 | 0.86 0.87 | 0.89 0.91 |
| | p=1500 | 0.47/0.7/0.8 | 0.18/0.18/0.18/0.79 | 1/0.94/0.96 | 0.18 | 0.94 | 0.36/0.36 | 0.21/0.36 | 0.85 | 0.91 |
| | p=250 | 0.89/0.96/0.91 | 0.22/0.22/0.22/0.9 | 1/0.38/0.98 | 0.22 | 0.38 | 0.54/0.53 | 0.32/0.53 | 0.99 | 0.91 |
| | p=500 | 0.72/0.88/0.92 | 0.22/0.22/0.22/0.91 | 1/0.25/0.93 | 0.22 | 0.25 | 0.5/0.49 | 0.24/0.49 | 0.99 | 0.86 |
| msnr | p=1000 | 0.53/0.74/0.93 | 0.23/0.23/0.23/0.92 | 1/0.21/0.84 | 0.23 | 0.21 | 0.47/0.47 | 0.24/0.47 | 0.98 | 0.78 |
| | p=1500 | 0.45/0.57/0.94 | 0.23/0.23/0.23/0.93 | 1/0.21/0.77 | 0.23 | 0.21 | 0.46/0.46 | 0.25/0.46 | 0.98 | 0.75 |
| | p=250 | 0.83/0.84/0.85 | 0.37/0.37/0.37/0.85 | 0.84/0.82/0.83 | 0.37 | 0.82 | 1/0.97 | 0.45/0.97 | 0.94 | 0.94 |
| lsnr | p=500 | 0.8/0.87/0.87 | 0.38/0.38/0.38/0.87 | 0.87/0.86/0.86 | 0.38 | 0.86 | 1/0.97 | 0.39/0.97 | 0.94 | 0.94 |
| | p=1000 p=1500 | 0.73/0.84/0.89 0.69/0.76/0.9 | 0.4/0.4/0.4/0.89 0.41/0.41/0.41/0.9 | 0.9/0.89/0.89 0.91/0.91/0.91 | 0.4 0.41 | 0.89 0.91 | 1/0.95 1/0.95 | 0.41/0.95 0.41/0.95 | 0.93 0.93 | 0.93 0.92 |
| | p=1000 | 0.09/0.10/0.9 | 0.41/0.41/0.41/0.9 | , , | sistency | 0.31 | 1/0.55 | 0.41/0.55 | 0.55 | 0.92 |
| _ | p=250 | 6/6/6 | 6/6/6/6 | 6/5.9/6 | 6 | 5.9 | 6/6 | 6/6 | 6 | 6 |
| | p=500 | 6/6/6 | 6/6/6/6 | 6/5.9/6 | 6 | 5.9 | 6/6 | 6/6 | 6 | 6 |
| hsnr | p=1000 | 6/6/6 | 6/6/6/6 | 6/5.9/5.9 | 6 | 5.9 | 6/6 | 5.9/6 | 6 | 6 |
| | p=1500 | 6/6/6 | 6/6/6/6 | 6/5.9/5.9 | 6 | 5.9 | 6/6 | 5.9/6 | 6 | 6 |
| | p=250 | 5.5/5.5/5.5 | 5.9/5.9/5.9/5.5 | 5.5/3.7/5.5 | 5.9 | 3.7 | 6/6 | 5.6/6 | 5.8 | 5.9 |
| msnr | p=500 | 5.5/5.5/5.5 | 5.8/5.8/5.8/5.5 | 5.5/2/5.4 | 5.8 | 2 | 6/6 | 5.6/6 | 5.8 | 5.9 |
| 1110111 | p=1000 p=1500 | 5.5/5.5/5.5 5.5/5.5/5.5 | 5.6/5.6/5.6/5.5 5.6/5.6/5.6/5.5 | 5.5/0.9/5.3 5.5/0.6/5.1 | 5.6 5.6 | 0.9 0.6 | 6/6 5.9/6 | 5.5/6 5.5/6 | 5.8 5.8 | 5.8 5.8 |
| | 1 * | 0.8/0.5/1 | 5.2/5.2/5.2/1 | 0.3/0/0.2 | 5.2 | 0.0 | 3/3 | 3.5/3 | 2.6 | 2.4 |
| | p=250 p=500 | 0.8/0.5/1 | 3.7/3.7/3.7/0.7 | 0.3/0/0.2 | 3.7 | 0 | 2.4/2.4 | 3.1/2.4 | 2.0 | 2.4 |
| lsnr | p=1000 | 0.9/0.5/0.5 | 2.6/2.6/2.6/0.5 | 0.1/0/0 | 2.6 | 0 | 1.9/1.9 | 2.3/1.9 | 1.8 | 1.6 |
| | p=1500 | 0.9/0.7/0.4 | 2.1/2.1/2.1/0.4 | 0.1/0/0 | 2.1 | 0 | 1.6/1.7 | 2/1.7 | 1.5 | 1.4 |
| | | | | Number of | extra varia | bles | | | | |
| | p=250 | 0.3/0.1/0.6 | 193/193/193/0.7 | 0.1/0.1/0.1 | 193 | 0.1 | 17.2/25.2 | 26.8/25.2 | 2.8 | 0.8 |
| hsnr | p=500 | 1.6/0.1/0.7 | 193/193/193/0.6 | 0.1/0.1/0.1 | 193 | 0.1 | 19.1/32.2 | 71.2/32.2 | 4 | 0.8 |
| 115111 | p=1000 p=1500 | 5/0.7/0.6 7.3/2.8/0.5 | 193/193/193/0.6 193/193/193/0.5 | 0.1/0.1/0.1 0.1/0.1/0.1 | 193 192.9 | 0.1 0.1 | 21.2/40.2 22/45 | 87.3/40.2 89.8/45 | 4.6 5.4 | 0.8 |
| | 1 * | | | | | | , | , | | |
| | p=250 p=500 | 1/0.6/0.8 2.7/0.8/0.8 | 193.1/193.1/193.1/0.8 193.2/193.2/193.2/0.8 | 0.5/0.3/0.5 0.5/0.1/0.5 | 193.1 193.2 | 0.3 0.1 | 17.2/25.1 19.1/32.2 | 47.5/25.1 97.3/32.2 | 2 2.2 | 2 2.6 |
| msnr | p=500 p=1000 | 6.6/1.9/0.8 | 193.2/193.2/193.2/0.8 193.4/193.3/193.4/0.8 | 0.5/0.1/0.5 | 193.2 | 0.1 | 21.1/40.6 | 100.4/40.6 | 3 | 3.4 |
| | p=1500 | 9.1/4.8/0.8 | 193.4/193.4/193.4/0.8 | 0.5/0/0.4 | 193.3 | 0 | 21.8/44.9 | 100.5/44.9 | 3.3 | 4 |
| | p=250 | 1/0.2/0.8 | 193.8/193.8/193.8/0.9 | 0.1/0/0 | 193.8 | 0 | 11.2/14.5 | 68.1/14.5 | 10.9 | 8.1 |
| , | p=500 | 2.9/0.3/0.6 | 195.3/195.3/195.3/0.6 | 0/0/0 | 195.3 | 0 | 11.3/15.9 | 114.2/15.9 | 11.5 | 8.8 |
| lsnr | p=1000 | 5.9/1.4/0.5 | 196.4/196.4/196.4/0.5 | 0/0/0 | 196.4 | 0 | 11.2/18.2 | 114.5/18.2 | 14 | 11 |
| | p=1500 | 7.6/4.2/0.4 | 196.9/196.9/196.9/0.4 | 0/0/0 | 196.8 | 0 | 10.9/19.3 | 112.4/19.3 | 14.3 | 12.6 |

Table S46: The performance of BOSS for high dimensional data, Sparse-Ex4, ρ =0, n=200

| | | BOSS C _n /AICc/CV | FS EBIC/HDBIC/HDHQ/CV | FSstop EBIC/HDBIC/HDHQ | FStrim HDBIC | FSstoptrim HDBIC | lasso AICc/CV | Gamma lasso AICc/CV | SparseNet CV | rlasso CV |
|----------|------------------|----------------------------------|--|----------------------------------|-----------------|---------------------|--|--------------------------|-----------------|--------------|
| i | | | | % worse than the | best possi | ible BOSS | | , | | |
| i — | p=250 | 10/6/13 | 302/302/302/13 | 6/5/6 | 302 | 5 | 63/63 | 234/63 | 11 | 16 |
| ١. | p=500 | 23/6/11 | 294/294/294/12 | 4/3/4 | 294 | 3 | 73/75 | 281/75 | 12 | 16 |
| hsnr | p=1000 | 56/13/12 | 289/289/289/12 | 3/2/2 | 289 | 2 | 84/87 | 280/87 | 13 | 12 |
| | p=1500 | 78/31/11 | 286/286/286/11 | 3/1/2 | 286 | 1 | 90/93 | 278/93 | 13 | 12 |
| | p=250 | 33/30/29 | 452/452/452/29 | 39/153/58 | 452 | 153 | 108/109 | 363/109 | 29 | 74 |
| msnr | p=500 | 65/36/31 | 427/427/427/31 | 46/155/75 | 427 399 | 155 | 115/119 | 421/119 | 35 38 | 86 |
| | p=1000 p=1500 | 116/62/36 153/109/38 | 399/399/399/37 386/386/386/37 | 51/150/89 55/146/95 | 386 | 150 146 | $\frac{119}{127}$ $\frac{122}{131}$ | 396/127 383/131 | 38 41 | 95 100 |
| _ | p=250 | 35/35/28 | 275/275/275/28 | 38/47/42 | 275 | 47 | 19/22 | 201/22 | 21 | 23 |
| 1 | p=500 | 39/27/23 | 244/244/244/23 | 29/35/32 | 244 | 35 | 14/19 | 242/19 | 19 | 21 |
| lsnr | p=1000 | 51/27/19 | 217/217/217/19 | 21/24/23 | 217 | 24 | 10/16 | 217/16 | 16 | 19 |
| | p=1500 | 63/40/17 | 207/207/207/18 | 18/20/20 | 207 | 20 | 9/15 | 206/15 | 14 | 19 |
| | | | | | e efficiency | | | | | |
| | p=250 p=500 | 0.96/0.99/0.93 0.84/0.98/0.93 | 0.26/0.26/0.26/0.93 0.26/0.26/0.26/0.92 | 0.99/1/1 0.99/1/1 | 0.26 0.26 | 1 1 | 0.65/0.65 0.6/0.59 | 0.32/0.65 0.27/0.59 | 0.95 0.92 | 0.91 0.89 |
| hsnr | p=500 p=1000 | 0.65/0.9/0.91 | 0.26/0.26/0.26/0.92 | 0.99/1/1 | 0.26 | 1 | 0.6/0.59 | 0.27/0.59 | 0.92 | 0.89 |
| | p=1500 | 0.57/0.78/0.91 | 0.26/0.26/0.26/0.91 | 0.99/1/1 | 0.26 | 1 | 0.53/0.52 | 0.27/0.52 | 0.89 | 0.91 |
| | p=250 | 0.97/0.99/1 | 0.23/0.23/0.23/1 | 0.93/0.51/0.81 | 0.23 | 0.51 | 0.62/0.62 | 0.28/0.62 | 0.99 | 0.74 |
| | p=500 | 0.79/0.96/1 | 0.25/0.25/0.25/1 | 0.89/0.51/0.75 | 0.25 | 0.51 | 0.61/0.59 | 0.25/0.59 | 0.97 | 0.7 |
| msnr | p=1000 | 0.63/0.84/1 | 0.27/0.27/0.27/0.99 | 0.9/0.54/0.72 | 0.27 | 0.54 | 0.62/0.6 | 0.27/0.6 | 0.99 | 0.69 |
| | p=1500 | 0.54/0.66/0.99 | 0.28/0.28/0.28/1 | 0.88/0.56/0.7 | 0.28 | 0.56 | 0.62/0.59 | 0.28/0.59 | 0.97 | 0.69 |
| | p=250 | 0.88/0.88/0.93 | 0.32/0.32/0.32/0.93 | 0.86/0.81/0.84 | 0.32 | 0.81 | 1/0.97 | 0.39/0.97 | 0.98 | 0.96 |
| lsnr | p=500 p=1000 | 0.82/0.9/0.93 0.73/0.87/0.93 | 0.33/0.33/0.33/0.93 0.35/0.35/0.35/0.93 | 0.89/0.85/0.86 0.91/0.89/0.89 | 0.33 0.35 | 0.85 0.89 | 1/0.96 1/0.95 | 0.33/0.96 0.35/0.95 | 0.96 0.95 | 0.95 0.93 |
| | p=1500 | 0.67/0.78/0.93 | 0.35/0.35/0.35/0.92 | 0.92/0.9/0.91 | 0.35 | 0.9 | 1/0.94 | 0.35/0.94 | 0.95 | 0.91 |
| | 1 | | , , , | | sistency | | , | , | | |
| <u> </u> | p=250 | 4.1/4.1/4.3 | 5.8/5.8/5.8/4.2 | 4.1/4/4 | 5.8 | 4 | 5/5.2 | 5.4/5.2 | 4.5 | 4.2 |
| ١. | p=500 | 4.2/4.1/4.2 | 5.3/5.3/5.3/4.2 | 4/4/4 | 5.3 | 4 | 4.8/4.9 | 5.1/4.9 | 4.4 | 4.1 |
| hsnr | p=1000 | 4.2/4.1/4.1 | 4.9/4.9/4.9/4.1 | 4/4/4 | 4.9 | 4 | 4.6/4.8 | 4.8/4.8 | 4.3 | 4 |
| | p=1500 | 4.2/4.1/4.1 | 4.7/4.7/4.1 | 4/4/4 | 4.7 | 4 | 4.5/4.6 | 4.6/4.6 | 4.3 | 4 |
| | p=250 | 3.8/3.7/3.9 | 5.6/5.6/5.6/3.9 | 3.6/2.3/3.4 | 5.6 4.9 | 2.3 | 4.3/4.3 | 4.8/4.3 | 4 | 3.8 3.6 |
| msnr | p=500 p=1000 | 3.9/3.7/3.8 3.9/3.7/3.7 | 4.9/4.9/4.9/3.8 4.5/4.5/4.5/3.7 | 3.4/2.2/3.1 3.3/2/2.8 | 4.9 | 2.2 | 4.1/4.2 $4/4.1$ | 4.6/4.2 4.3/4.1 | 3.9 3.9 | 3.4 |
| | p=1500 | 3.9/3.8/3.6 | 4.3/4.3/4.3/3.6 | 3.2/2/2.7 | 4.3 | 2 | 3.8/4 | 4.1/4 | 3.8 | 3.3 |
| <u> </u> | p=250 | 0.8/0.5/1.2 | 5.3/5.3/5.3/1.2 | 0.4/0/0.2 | 5.3 | 0 | 2.2/2.2 | 3.7/2.2 | 2 | 1.8 |
| ١, | p=500 | 0.9/0.5/0.9 | 3.8/3.8/3.8/0.9 | 0.3/0/0.1 | 3.8 | 0 | 1.9/1.8 | 3.3/1.8 | 1.7 | 1.6 |
| lsnr | p=1000 | 0.9/0.6/0.6 | 2.7/2.7/2.7/0.6 | 0.2/0/0.1 | 2.7 | 0 | 1.6/1.5 | 2.5/1.5 | 1.4 | 1.3 |
| | p=1500 | 1/0.7/0.5 | 2.3/2.3/2.3/0.5 | 0.2/0/0 | 2.3 | 0 | 1.4/1.4 | 2.1/1.4 | 1.3 | 1.2 |
| | | | | Number of | | | | | | |
| | p=250 | 0.2/0/0.4 | 193.2/193.2/193.2/0.3 | 0/0/0 | 193.2 | 0 | 16.1/22.7 | 67.5/22.7 | 3.2 | 1.1 |
| hsnr | p=500 p=1000 | 2/0.1/0.3 5.1/0.7/0.3 | 193.7/193.7/193.7/0.3 194.1/194.1/194.1/0.3 | 0/0/0 0/0/0 | 193.7 194.1 | 0 | 17.9/29.1 19.2/36.7 | 101.9/29.1 96.1/36.7 | 4.2 5.1 | 1.6 0.9 |
| | p=1000 p=1500 | 7.3/2.4/0.3 | 194.3/194.3/194.3/0.3 | 0/0/0 | 194.1 | 0 | 20.2/40.2 | 92.2/40.2 | 5.7 | 1 |
| | p=250 | 0.5/0.1/0.4 | 193.4/193.4/193.4/0.4 | 0/0/0 | 193.4 | 0 | 15/20.1 | 73/20.1 | 2.7 | 3.1 |
| mon- | p=500 | 2.4/0.3/0.4 | 194.1/194.1/194.1/0.4 | 0/0/0 | 194.1 | 0 | 16.8/26.3 | 117/26.3 | 4.2 | 4.1 |
| msnr | p=1000 | 5.9/1.5/0.4 | 194.5/194.5/194.5/0.4 | 0/0/0 | 194.5 | 0 | 18.1/32.9 | 111.4/32.9 | 5 | 5.3 |
| <u></u> | p=1500 | 8.2/4.3/0.4 | 194.7/194.7/194.7/0.4 | 0/0/0 | 194.7 | 0 | 18.2/35.6 | 106.8/35.6 | 6.1 | 5.6 |
| | p=250 | 0.4/0.1/0.5 | 193.7/193.7/193.7/0.5 | 0/0/0 | 193.7 | 0 | 9.1/11 | 67/11 | 6.8 | 5.6 |
| lsnr | p=500 p=1000 | 1.9/0.1/0.4 4.6/1/0.3 | 195.2/195.2/195.2/0.4 196.2/196.2/196.2/0.3 | 0/0/0 0/0/0 | 195.2 196.2 | 0 | 10.2/12.8 10.3/15.7 | 128.2/12.8 126.3/15.7 | 8.4 10.6 | 6.8 9.1 |
| | p=1000 p=1500 | 4.6/1/0.3 6.6/2.9/0.3 | 196.2/196.2/196.2/0.3 | 0/0/0 | 196.2 | 0 | 10.3/15.7 | 126.3/15.7 | 10.6 | 10.8 |
| | P-1000 | 1 5.0/2.0/0.0 | | 0/0/0 | 100.1 | | 10/10.0 | -21.0/10.0 | 11.0 | 10.0 |

Table S47: The performance of BOSS for high dimensional data, Sparse-Ex4, ρ =0.5, n=200

| | | $\begin{array}{c c} \operatorname{BOSS} \\ \operatorname{C}_p/\operatorname{AICc/CV} \end{array}$ | FS EBIC/HDBIC/HDHQ/CV | FSstop EBIC/HDBIC/HDHQ | FStrim HDBIC | FSstoptrim HDBIC | lasso AICc/CV | Gamma lasso AICc/CV | SparseNet CV | rlasso CV |
|-----------------------|---------------------------|---|---|-----------------------------------|----------------------|---------------------|--------------------------------------|-------------------------------|---------------------|-----------------|
| | | | | % worse than the | best possi | ible BOSS | | | | |
| | p=250 p=500 | 9/5/12 26/4/11 | 292/292/292/13 283/283/283/12 | 5/5/5 3/2/2 | 292 283 | 5 2 | 95/93 112/107 | 215/93 268/107 | 13 12 | 19 21 |
| hsnr | p=1000 p=1500 | 59/13/11 84/37/11 | 278/278/278/12 277/277/277/12 | $\frac{2/1/1}{1/0/1}$ | 278 277 | 1 0 | 132/125 145/135 | 268/125 268/135 | 12 12 | 30 39 |
| | p=250 | 26/22/31 | 374/374/374/44 | 29/117/44 | 374 | 118 | 123/121 | 306/121 | 15 | 115 |
| msnr | p=500 p=1000 p=1500 | 48/22/28 72/36/27 78/56/26 | 314/314/314/47 267/267/267/45 235/235/235/39 | 30/100/49 30/83/47 26/72/42 | 314 267 235 | 100 84 73 | 117/115 112/110 102/101 | 308/115 264/110 232/101 | 20 24 23 | 102 87 72 |
| | p=250 | 25/24/21 | 251/251/251/33 | 32/37/35 | 251 | 37 | 30/32 | 180/32 | 25 | 35 |
| lsnr | p=500 p=1000 | 26/17/17 30/14/12 | 216/216/216/24 187/187/187/15 | 21/24/23 11/12/12 | 216 187 | 24 12 | 20/23 11/14 | 214/23 186/14 | 21 14 | 26 17 |
| | p=1500 | 36/22/11 | 177/177/177/12 | 8/9/8 | 177 e efficiency | 9 | 7/11 | 177/11 | 12 | 15 |
| | l - 050 | 1 0 00 /0 00 /0 03 | 0.07/0.07/0.07/0.00 | | 0.27 | 1 | 0.52/0.54 | 0.33/0.54 | 0.93 | 0.88 |
| hsnr | p=250 p=500 p=1000 | 0.96/0.99/0.93 0.81/0.98/0.92 0.63/0.89/0.91 | 0.27/0.27/0.27/0.92 0.27/0.27/0.27/0.91 0.27/0.27/0.27/0.9 | 0.99/1/1 0.99/1/1 | 0.27 0.27 0.27 | 1 1 | 0.53/0.54 0.48/0.49 0.43/0.45 | 0.28/0.49 0.27/0.45 | 0.93 0.91 0.9 | 0.84 0.77 |
| | p=1000 p=1500 | 0.55/0.73/0.91 | 0.27/0.27/0.27/0.9 | 0.99/1/1 $0.99/1/1$ | 0.27 | 1 | 0.43/0.45 $0.41/0.43$ | 0.27/0.43 | 0.9 | 0.77 |
| | p=250 p=500 | 0.91/0.94/0.88 0.81/0.98/0.94 | 0.24/0.24/0.24/0.8 0.29/0.29/0.29/0.82 | 0.89/0.53/0.8 0.93/0.6/0.81 | 0.24 0.29 | 0.53 0.6 | 0.52/0.52 0.55/0.56 | 0.28/0.52 0.29/0.56 | 1 1 | 0.54 0.6 |
| msnr | p=1000 p=1500 | 0.72/0.91/0.97 0.69/0.79/0.98 | 0.34/0.34/0.34/0.85 0.37/0.37/0.37/0.88 | 0.95/0.67/0.84 0.98/0.71/0.87 | $0.34 \\ 0.37$ | $0.67 \\ 0.71$ | 0.58/0.59 $0.61/0.61$ | 0.34/0.59 0.37/0.61 | 1 1 | $0.66 \\ 0.71$ |
| | p=250 p=500 | 0.97/0.98/1 0.93/1/1 | 0.35/0.35/0.35/0.91 0.37/0.37/0.37/0.94 | 0.92/0.88/0.9 0.97/0.95/0.95 | 0.35 0.37 | 0.88 0.95 | 0.94/0.92 0.97/0.95 | 0.43/0.92 0.37/0.95 | 0.97 0.97 | 0.9 |
| lsnr | p=300 p=1000 p=1500 | 0.85/0.97/0.98 0.79/0.88/0.97 | 0.37/0.37/0.37/0.94 0.39/0.39/0.39/0.96 0.39/0.39/0.39/0.96 | 1/0.99/0.99 1/0.99/0.99 | 0.39 | 0.99 0.99 | 1/0.97 1/0.96 | 0.39/0.97 0.39/0.96 | 0.97 0.96 | 0.94 0.93 |
| | p=1300 | 1 0.79/0.88/0.97 | 0.39/0.39/0.39/0.90 | | sistency | 0.99 | 1/0.90 | 0.39/0.90 | 0.90 | 0.93 |
| | p=250 | 4.1/4.1/4.2 | 5.8/5.8/5.8/4.1 | 4/4/4 | 5.8 | 4 | 4.8/5 | 5.3/5 | 4.3 | 4 |
| | p=500 | 4.1/4.1/4.1 | 5.2/5.2/5.2/4.1 | 4/4/4 | 5.2 | 4 | 4.5/4.7 | 5/4.7 | 4.2 | 4 |
| hsnr | p=1000 p=1500 | 4.1/4.1/4 4.1/4.1/4 | 4.7/4.7/4.7/4 4.5/4.5/4.5/4 | $\frac{4/4/4}{4/4/4}$ | $\frac{4.7}{4.5}$ | 4 | 4.3/4.5 $4.2/4.4$ | 4.6/4.5 4.4/4.4 | 4.1 4.1 | 4 4 |
| | p=250 | 3.9/3.9/3.9 | 5.6/5.6/5.6/3.7 | 3.5/2.3/3.3 | 5.6 | 2.3 | 4.1/4.3 | 4.8/4.3 | 4 | 3.3 |
| msnr | p=500 p=1000 | 3.8/3.7/3.7 3.7/3.6/3.5 | 4.8/4.8/4.8/3.3 4.2/4.2/4.2/3.1 | 3.2/2.2/2.9 3/2.1/2.7 | 4.8 4.2 | 2.1 | $\frac{3.8}{4}$ $\frac{3.4}{3.7}$ | 4.4/4 $4.1/3.7$ | 3.8 3.6 | 2.9 2.6 |
| | p=1500 | 3.5/3.5/3.3 | 4/4/4/2.9 | 2.9/2/2.5 | 4 | 2 | 3.2/3.4 | 3.8/3.4 | 3.4 | 2.5 |
| | p=250 | 0.8/0.6/1.2 | 5.3/5.3/5.3/0.7 | 0.3/0/0.1 | 5.3 | 0 | 1.4/1.2 | 3.4/1.2 | 1.4 | 1.1 |
| lsnr | p=500 p=1000 | 0.7/0.5/0.7 0.5/0.3/0.3 | 3.6/3.6/3.6/0.4 2.3/2.3/2.3/0.2 | 0.1/0/0.1 0.1/0/0 | 3.6 2.3 | 0 | 0.9/0.9 0.6/0.6 | 2.8/0.9 1.7/0.6 | 1 0.6 | 0.7 0.5 |
| | p=1000 p=1500 | 0.4/0.4/0.2 | 1.7/1.7/1.7/0.2 | 0.1/0/0 | 1.7 | 0 | 0.5/0.5 | 1.3/0.5 | 0.5 | 0.3 |
| | | | | Number of | extra varia | bles | | | | i |
| | p=250 | 0.4/0/0.4 | 193.2/193.2/193.2/0.3 | 0/0/0 | 193.2 | 0 | 23.7/36.4 | 63.8/36.4 | 3.4 | 1.1 |
| hsnr | p=500 | 2.7/0.1/0.3 | 193.8/193.8/193.8/0.3 | 0/0/0 | 193.8 | 0 | 26.1/46.1 | 104.6/46.1 | 4.1 | 1.4 |
| 110111 | p=1000 p=1500 | 6.2/0.8/0.3 8.3/3.1/0.3 | 194.3/194.3/194.3/0.3 194.5/194.5/194.5/0.3 | 0/0/0 0/0/0 | 194.2 194.4 | 0 | 28.5/59.2 29.8/66 | 103.1/59.2 100.1/66 | 5.1 5.3 | 2.3 3.7 |
| | p=250 | 0.9/0.4/0.8 | 193.4/193.4/193.4/0.9 | 0.1/0/0 | 193.4 | 0 | 21.7/32.8 | 74.5/32.8 | 4.6 | 6.5 |
| msnr | p=500 | 3.4/0.7/0.9 | 194.2/194.2/194.2/0.9 | 0.1/0/0 | 194.2 | 0 | 22.8/39.7 | 116.2/39.7 | 7.4 | 5.5 |
| | p=1000 p=1500 | 6.6/1.9/1 8.2/4.6/0.9 | 194.8/194.7/194.8/0.8 195/195/195/0.7 | 0.1/0/0 0.1/0/0 | 194.7 194.9 | 0 | 22.9/46.5 22.5/47.9 | 114.4/46.5 111.5/47.9 | 9.3 10.8 | 5.1 4.2 |
| | p=250 | 0.6/0.2/1.1 | 193.7/193.7/193.7/0.6 | 0/0/0 | 193.7 | 0 | 8.6/10.2 | 68.8/10.2 | 6.8 | 7 |
| lsnr | p=500 | 1.7/0.3/0.7 3.3/0.8/0.4 | 195.4/195.4/195.4/0.4 196.7/196.7/196.7/0.3 | 0/0/0 0/0/0 | 195.4 196.7 | 0 | 7.9/9.8 7.6/11.5 | 126.8/9.8 126.4/11.5 | 8.1 8.5 | 6.8 7.6 |
| | p=1000 p=1500 | 3.3/0.8/0.4 4.7/2.3/0.3 | 196.7/196.7/196.7/0.3 | 0/0/0 | 196.7 | 0 | 7.5/11.5 | 126.4/11.5 122.8/12.2 | 8.5 9.4 | 9.2 |

Table S48: The performance of BOSS for high dimensional data, Sparse-Ex4, ρ =0.9, n=200

| | | ${}^{\mathrm{BOSS}}_{\mathrm{C}_p/\mathrm{AICc/CV}}$ | FS EBIC/HDBIC/HDHQ/CV | FSstop EBIC/HDBIC/HDHQ | FStrim HDBIC | FSstoptrim HDBIC | lasso AICc/CV | Gamma lasso AICc/CV | SparseNet CV | rlasso CV |
|--------|------------------|--|--|---------------------------|-----------------|---------------------|-------------------------------|------------------------------------|-----------------|--------------|
| | | | | % worse than the | best poss | ible BOSS | | | | |
| | p=250 | 13/5/35 | 249/249/249/75 | 6/10/6 | 249 | 3 | 182/149 | 140/149 | 4 | 151 |
| hsnr | p=500 | 26/8/48 | 196/196/196/90 | 8/32/12 | 196 | 22 | 254/169 | 170/169 | 10 | 196 |
| | p=1000 | 15/60/119 | 51/51/51/147 | 105/146/115 | 51 | 144 | 105/58 | 47/58 | 4 | 50 |
| | p=1500 | 26/48/123 | 23/23/23/146 | 114/141/124 | 23 | 140 | 97/39 | 21/39 | 3 | 36 |
| | p=250 | 19/21/23 | 144/144/144/79 | 51/102/60 | 144 | 101 | 86/72 | 100/72 | 20 | 67 |
| msnr | p=500 | 16/14/17 | 66/66/66/53 | 34/60/40 | 66 | 60 | 60/50 | 62/50 | -11 | 48 |
| mam | p=1000 | 12/12/15 | 22/22/22/25 | 19/27/22 | 22 | 27 | 24/25 | 21/25 | 15 | 25 |
| | p=1500 | 10/10/13 | 13/13/13/18 | 15/19/16 | 13 | 19 | 15/15 | 12/15 | 14 | 15 |
| | p=250 | 11/10/14 | 197/197/197/20 | 16/16/16 | 197 | 16 | 17/17 | 160/17 | 20 | 20 |
| lsnr | p=500 | 8/5/9 | 173/173/173/11 | 7/7/7 | 173 162 | 7 2 | 8/9 | 170/9 | 10 6 | 11 8 |
| | p=1000 p=1500 | 15/4/6 23/10/5 | 162/162/162/7 158/158/158/6 | $\frac{2/2/2}{1/1/1}$ | 158 | 1 | $\frac{3}{5}$ $\frac{2}{3}$ | $\frac{160}{5}$ $\frac{157}{3}$ | 5 | 7 |
| | p-1000 | 20/10/0 | 100/100/100/0 | , , | e efficiency | | 2/0 | 101/0 | | |
| - | p=250 | 0.92/0.99/0.77 | 0.3/0.3/0.3/0.59 | 0.98/0.94/0.98 | 0.3 | 1 | 0.37/0.42 | 0.43/0.42 | 1 | 0.41 |
| | p=500 | 0.85/1/0.73 | 0.36/0.36/0.36/0.57 | 1/0.82/0.96 | 0.36 | 0.88 | 0.37/0.42 | 0.4/0.4 | 0.98 | 0.36 |
| hsnr | p=1000 | 0.91/0.65/0.48 | 0.69/0.69/0.69/0.42 | 0.51/0.42/0.49 | 0.69 | 0.43 | 0.51/0.66 | 0.71/0.66 | 1 | 0.7 |
| | p=1500 | 0.81/0.69/0.46 | 0.83/0.83/0.83/0.42 | 0.48/0.43/0.46 | 0.83 | 0.43 | 0.52/0.74 | 0.85/0.74 | 1 | 0.76 |
| | p=250 | 1/0.99/0.97 | 0.49/0.49/0.49/0.67 | 0.79/0.59/0.75 | 0.49 | 0.6 | 0.64/0.69 | 0.6/0.69 | 1 | 0.72 |
| | p=500 | 0.76/0.78/0.76 | 0.53/0.53/0.53/0.58 | 0.66/0.55/0.63 | 0.53 | 0.55 | 0.55/0.59 | 0.55/0.59 | 1 | 0.6 |
| msnr | p=1000 | 1/1/0.97 | 0.92/0.92/0.92/0.89 | 0.94/0.88/0.92 | 0.92 | 0.88 | 0.9/0.9 | 0.93/0.9 | 0.97 | 0.9 |
| | p=1500 | 1/0.99/0.97 | 0.97/0.97/0.97/0.93 | 0.95/0.92/0.94 | 0.97 | 0.92 | 0.95/0.95 | 0.98/0.95 | 0.96 | 0.95 |
| 1 | p=250 | 0.99/1/0.97 | 0.37/0.37/0.37/0.91 | 0.95/0.95/0.95 | 0.37 | 0.95 | 0.94/0.94 | 0.42/0.94 | 0.92 | 0.92 |
| lsnr | p=500 | 0.98/1/0.96 | 0.39/0.39/0.39/0.95 | 0.98/0.98/0.99 | 0.39 | 0.98 | 0.97/0.97 | 0.39/0.97 | 0.95 | 0.95 |
| 15111 | p=1000 | 0.89/0.98/0.97 | 0.39/0.39/0.39/0.96 | 1/1/1 | 0.39 | 1 | 0.99/0.97 | 0.39/0.97 | 0.96 | 0.95 |
| | p=1500 | 0.82/0.92/0.96 | 0.39/0.39/0.39/0.95 | 1/1/1 | 0.39 | 1 | 0.99/0.98 | 0.39/0.98 | 0.96 | 0.95 |
| | | | | | sistency | | | | | |
| | p=250 | 4.1/4.1/4.2 | 5.6/5.6/5.6/4.1 | 4/3.9/4 | 5.6 | 3.9 | 4.3/4.6 | 4.5/4.6 | 4.2 | 4.1 |
| hsnr | p=500 | 4/4/4 | 4.8/4.8/4.8/4 | 3.9/3.7/3.8 | 4.8 | 3.7 | $\frac{3.2}{4}$ $\frac{3}{3}$ | 4.3/4 2.5/3 | 4.2 | 3.1 |
| | p=1000 p=1500 | 3.1/3/2.8 2.2/2.1/1.7 | 3.6/3.6/3.6/1.9 2.6/2.6/2.6/0.8 | 2/1.4/1.8 1.2/0.7/1 | 3.6 2.6 | 1.4 0.7 | 2.5/2.8 | 1.9/2.8 | 3.9 3.3 | 3 2.8 |
| | 1 * | , , | | 2.2/1/1.9 | 5.4 | 1 | 2.9/3.2 | 3.9/3.2 | 2.9 | 2.9 |
| | p=250 p=500 | 3.5/3.3/3.5 2.6/2.4/2.5 | 5.4/5.4/5.4/2.3 4/4/4/1 | 1.3/0.4/1 | 5.4 4 | 0.4 | 1.3/1.6 | 3.9/3.2 2.8/1.6 | 2.9 | 1.7 |
| msnr | p=1000 | 1.1/1/1 | 2.4/2.4/2.4/0.4 | 0.5/0.1/0.4 | 2.4 | 0.1 | 0.6/0.6 | 1.5/0.6 | 1 | 0.5 |
| | p=1500 | 0.8/0.7/0.5 | 1.6/1.6/1.6/0.2 | 0.3/0.1/0.2 | 1.6 | 0.1 | 0.5/0.5 | 1/0.5 | 0.5 | 0.4 |
| | p=250 | 0.3/0.3/0.4 | 4.7/4.7/4.7/0.1 | 0.1/0/0 | 4.7 | 0 | 0.2/0.2 | 1.9/0.2 | 0.2 | 0.2 |
| | p=500 | 0.2/0.1/0.1 | 2.5/2.5/2.5/0 | 0/0/0 | 2.5 | 0 | 0.2/0.1 | 1.3/0.1 | 0.1 | 0.1 |
| lsnr | p=1000 | 0.1/0.1/0 | 1.3/1.3/1.3/0 | 0/0/0 | 1.3 | 0 | 0.1/0.1 | 0.7/0.1 | 0.1 | 0.1 |
| | p=1500 | 0.1/0/0 | 0.8/0.8/0.8/0 | 0/0/0 | 0.8 | 0 | 0.1/0.1 | 0.5/0.1 | 0.1 | 0.1 |
| | | | | Number of | extra varia | bles | | | | |
| | p=250 | 2.9/1.2/3.6 | 193.4/193.4/193.4/7.3 | 0.8/0.7/0.8 | 193.4 | 0 | 55.7/90.9 | 49.1/90.9 | 9.3 | 39.6 |
| hsnr | p=500 | 7.8/2.5/4.9 | 194.2/194.2/194.2/11.5 | 1.8/1.2/1.6 | 194.2 | 0 | 44.1/104.6 | 96/104.6 | 33.9 | 18.9 |
| lisiii | p=1000 | 24.7/10.1/6.6 | 195.4/195.4/195.4/5.9 | 2.5/0.9/2 | 195.4 | 0 | 50.1/93.8 | 108.1/93.8 | 87.7 | 40.7 |
| | p=1500 | 28.5/18.4/4.5 | 196.4/196.4/196.4/2.1 | 1.7/0.5/1.1 | 196.3 | 0 | 43/101.4 | 109.6/101.4 | 84.5 | 61.6 |
| | p=250 | 9.9/7.2/9.2 | 193.6/193.6/193.6/6.6 | 1.6/0.2/1.2 | 193.6 | 0 | 33.4/55.5 | 68.7/55.5 | 24.4 | 27.8 |
| msnr | p=500 | 11.9/6.4/7.4 | 195/195/195/2 | 1.1/0.1/0.6 | 195 | 0 | 15.2/36.7 | 112.9/36.7 | 41 25.6 | 24.6 |
| | p=1000 p=1500 | 4.7/2.9/2.7 5.4/3.3/1.4 | 196.6/196.6/196.6/0.8 197.4/197.4/197.4/0.6 | 0.4/0/0.2 0.2/0/0.1 | 196.5 197.3 | 0 | 8.2/11 8.6/11.9 | 115.1/11 113.4/11.9 | 25.6 10.1 | 7.5 7.8 |
| | | | | | | | | • | | |
| | p=250 | 0.7/0.6/1.5 | 194.3/194.3/194.3/0.3 | 0/0/0 | 194.3 196.5 | 0 | 4.2/3.8 | 79.1/3.8 | 4.2 4.7 | 2.8 3.9 |
| lsnr | p=500 p=1000 | 0.6/0.2/0.5 2.1/0.3/0.3 | 196.5/196.5/196.5/0.3 197.7/197.7/197.7/0.3 | 0/0/0 0/0/0 | 196.5 | 0 | 4.7/5.2 5.9/8.1 | 123.5/5.2 121.3/8.1 | 6.3 | 5.5 |
| | p=1000 p=1500 | 3.6/1.3/0.3 | 198.2/198.2/198.2/0.3 | 0/0/0 | 198.1 | 0 | 6.5/8.5 | 119.2/8.5 | 7 | 6.6 |
| | 1 . 2000 | ,, 0.00 | ,,, 0.0 | ~/ ~/ ~ | | | 0.0,0.0 | | • | 0.0 |

Table S49: The performance of BOSS for high dimensional data, Dense, ρ =0, n=200

| | | BOSS $C_p/AICc/CV$ | FS EBIC/HDBIC/HDHQ/CV | FSstop EBIC/HDBIC/HDHQ | FStrim HDBIC | FSstoptrim HDBIC | lasso AICc/CV | Gamma lasso AICc/CV | SparseNet CV | rlasso CV |
|------|--|--|---|---|-----------------------------|------------------------------|--|---|------------------------------|------------------------------|
| | | | | % worse than the | best poss | ible BOSS | | | | |
| hsnr | p=250 p=500 p=1000 p=1500 | 11/14/14 15/9/12 18/9/10 20/13/10 | 68/68/68/13 55/55/55/12 45/45/45/10 41/41/41/10 | 35/166/50 33/147/74 38/132/101 46/126/109 | 68 55 45 41 | 166 147 132 126 | 18/9 25/12 32/13 36/15 | 5/9 23/12 27/13 26/15 | 3 3 1 1 | 16 19 20 18 |
| | p=250 | 13/19/16 | 76/76/76/16 | 32/69/35 | 76 | 69 | 5/1 | 27/1 | 3 | 7 |
| msnr | p=500 p=1000 p=1500 | 15/11/13 17/10/9 18/13/8 | 60/60/60/13 49/49/49/9 44/44/44/8 | 21/68/26 $14/66/21$ $12/64/22$ | 60 49 44 | 68 66 64 | 5/1 5/1 5/1 | 47/1 41/1 38/1 | 3 2 1 | 7 7 6 |
| lsnr | p=250 p=500 p=1000 p=1500 | 11/9/9 16/7/8 26/11/7 35/21/6 | $\begin{array}{c} 156/156/156/9 \\ 150/150/150/8 \\ 145/145/145/7 \\ 143/143/143/6 \end{array}$ | 8/9/9 $6/6/6$ $4/4/4$ $4/3/3$ | 156 150 145 143 | 9 6 4 3 | -3/0 -2/1 -2/2 -2/3 | 112/0 $143/1$ $141/2$ $140/3$ | 2 3 4 4 | 3 3 5 6 |
| | | | | Relativ | e efficiency | 7 | | | | |
| hsnr | p=250 p=500 p=1000 p=1500 | 0.93/0.91/0.91 0.89/0.94/0.91 0.86/0.93/0.92 0.84/0.89/0.92 | 0.62/0.62/0.62/0.91 0.66/0.66/0.66/0.92 0.7/0.7/0.70.92 0.72/0.72/0.72/0.92 | 0.76/0.39/0.69 0.77/0.42/0.59 0.74/0.44/0.5 0.69/0.45/0.48 | 0.62 0.66 0.7 0.72 | 0.39 0.42 0.44 0.45 | 0.88/0.95 0.82/0.92 0.76/0.89 0.74/0.88 | 0.99/0.95 0.84/0.92 0.8/0.89 0.8/0.88 | 1 1 1 1 | 0.89 0.87 0.85 0.85 |
| msnr | p=250 p=500 p=1000 p=1500 | 0.9/0.85/0.87 0.87/0.9/0.89 0.86/0.92/0.92 0.86/0.89/0.94 | 0.57/0.57/0.57/0.87 0.63/0.63/0.63/0.89 0.68/0.68/0.68/0.92 0.7/0.7/0.7/0.94 | 0.77/0.6/0.75 0.83/0.6/0.8 0.88/0.61/0.83 0.9/0.62/0.83 | 0.57 0.63 0.68 0.7 | 0.6 0.6 0.61 0.62 | 0.97/1 0.96/1 0.96/1 0.96/1 | 0.8/1 $0.68/1$ $0.72/1$ $0.73/1$ | 0.98 0.98 0.99 | 0.95 0.94 0.95 0.96 |
| lsnr | p=250 p=500 p=1000 p=1500 | 0.88/0.89/0.89 0.85/0.91/0.91 0.78/0.88/0.92 0.73/0.81/0.93 | 0.38/0.38/0.38/0.89 0.39/0.39/0.39/0.9 0.4/0.4/0.4/0.92 0.4/0.4/0.4/0.92 | 0.9/0.89/0.89 0.92/0.92/0.92 0.94/0.94/0.94 0.95/0.95/0.95 | 0.38 0.39 0.4 0.4 | 0.89 0.92 0.94 0.95 | 1/0.97 1/0.97 1/0.96 1/0.95 | 0.46/0.97 0.4/0.97 0.41/0.96 0.41/0.95 | 0.95 0.95 0.95 0.94 | 0.95 0.95 0.93 0.93 |
| | | | | Spar | sistency | | | | | |
| hsnr | p=250 p=500 p=1000 p=1500 | 21.3/14.8/16.5 26.8/15.6/14.8 29.9/19.2/13.7 29.3/23.6/13.5 | 199/199/199/16.3 199/199/199/14.5 199/199/199/13.6 199/199/199/13.3 | 11.3/3.1/10.1 10.7/3/7.8 9.6/3/5.1 8.8/3/4.1 | 199 199 199 198.9 | 3.1 3 3 3 | 47.7/74.1 47.2/87.8 45.9/99 45.4/106.3 | 47.2/74.1 80.7/87.8 96.1/99 98/106.3 | 32.1 30.9 27.7 27.1 | 35.5 34.5 34 36.8 |
| msnr | p=250 p=500 p=1000 p=1500 | 12/5.9/7.9 16.3/6.4/5.7 18.6/9.8/4.4 19.6/13.9/3.9 | $\begin{array}{c} 199/199/199/7.6 \\ 199/199/199/5.6 \\ 199/199/199/4.4 \\ 199/199/199/3.9 \end{array}$ | 3.2/1.5/3 3.1/0.8/2.7 2.9/0.3/2.5 2.9/0.2/2.3 | 199 199 199 198.9 | 1.5 0.8 0.3 0.2 | 32.7/49.7 30.5/54.7 27.7/57.1 27.2/59 | 57.8/49.7 103.2/54.7 106.3/57.1 106.4/59 | 27.7 26.2 22.8 20.7 | 27.8 25.8 20.7 19.8 |
| lsnr | p=250 p=500 p=1000 p=1500 | 1.1/0.3/1.1 2.6/0.4/0.8 5/1.5/0.6 6.5/3.4/0.5 | 199/199/199/1.1 199/199/199/0.8 199/199/199/0.6 199/199/199/0.5 | 0.2/0/0.1 0.1/0/0.1 0.1/0/0 0.1/0/0 | 199 199 199 198.9 | 0 0 0 0 | 11.1/14.7 11.1/14.8 10.6/16.6 10/17.6 | 72.2/14.7 117.1/14.8 114.9/16.6 113.5/17.6 | 11.3 12.5 12.5 12.8 | 9.5 9.1 10.5 11.8 |
| | | | | Number of | extra varia | ables | | | | |
| hsnr | p=250 p=500 p=1000 p=1500 | -/-/- -/-/- -/-/- -/-/- | -/-/-/- -/-/-/- -/-/-/- -/-/-/- | -/-/- -/-/- -/-/- -/-/- | - | - - - | -/- -/- -/- -/- | -/- -/- -/- -/- | - - - - | - - - |
| msnr | p=250 p=500 p=1000 | -/-/- -/-/- -/-/- | -/-/-/- -/-/- -/-/- | -/-/- -/-/- -/-/- | - - - | - - - | -/- -/- -/- | -/- -/- -/- | - - - | - - - |
| lsnr | p=1500 p=250 p=500 p=1000 p=1500 | -/-/- -/-/- -/-/- -/-/- | -/-/- -/-/- -/-/-/- -/-/- | -/-/- -/-/- -/-/- -/-/- | - - - - | - - - | -/- -/- -/- -/- | -/- -/- -/- -/- | - - - - | - - - |

Table S50: The performance of BOSS for high dimensional data, Dense, ρ =0.5, n=200

| | | $\frac{\mathrm{BOSS}}{\mathrm{C}_p/\mathrm{AICc/CV}}$ | FS EBIC/HDBIC/HDHQ/CV | FSstop EBIC/HDBIC/HDHQ | FStrim HDBIC | FSstoptrim HDBIC | lasso AICc/CV | Gamma lasso AICc/CV | SparseNet CV | rlasso CV |
|----------|------------------------------------|--|---|--|--|------------------------------|---|---|------------------------------|------------------------------|
| | | | | % worse than the | best poss | ible BOSS | | | | |
| hsnr | p=250 p=500 p=1000 p=1500 | 9/11/11 10/7/13 15/10/24 18/13/35 | 62/62/62/13 47/47/47/14 32/32/32/28 21/21/21/38 | 34/147/59 45/127/87 51/104/89 53/88/79 | 62 47 32 21 | 147 127 104 88 | 44/23 71/29 100/52 89/57 | 6/23 9/29 11/52 8/57 | 5 1 3 21 | 27 45 90 79 |
| msnr | p=250 p=500 p=1000 p=1500 | 13/14/13 8/6/8 10/5/5 12/8/4 | 66/66/66/15 52/52/52/8 46/46/46/5 44/44/44/4 | 19/49/21 10/54/13 7/61/11 6/63/13 | 66 52 46 44 | 49 54 61 63 | 24/17 21/15 22/15 24/17 | 15/17 32/15 34/15 34/17 | 10 6 3 2 | 20 16 18 21 |
| lsnr | p=250 p=500 p=1000 p=1500 | 10/9/10 10/6/7 17/6/6 24/12/5 | $\begin{array}{c} 156/156/156/11 \\ 147/147/147/7 \\ 142/142/142/6 \\ 140/140/140/6 \end{array}$ | 9/10/9 5/5/5 4/3/4 3/2/2 | 156 147 142 140 e efficiency | 10 5 3 2 | 4/6 2/3 1/2 0/2 | 99/6 135/3 135/2 134/2 | 7 5 4 4 | 8 5 5 4 |
| <u> </u> | p=250 | 0.96/0.95/0.95 | 0.65/0.65/0.65/0.93 | 0.78/0.43/0.66 | e emciency 0.65 | 0.43 | 0.73/0.86 | 0.99/0.86 | 1 | 0.83 |
| hsnr | p=250 p=500 p=1000 p=1500 | 0.92/0.94/0.89 0.9/0.94/0.83 0.92/0.96/0.8 | 0.69/0.69/0.69/0.88 0.69/0.78/0.78/0.81 0.89/0.89/0.89/0.79 | 0.78/0.43/0.66 0.7/0.44/0.54 0.68/0.51/0.55 0.71/0.58/0.6 | 0.69 0.78 0.89 | 0.43 0.44 0.51 0.58 | 0.73/0.86 0.59/0.78 0.52/0.68 0.57/0.69 | 0.99/0.86 0.92/0.78 0.93/0.68 1/0.69 | 1 1 0.89 | 0.69 0.54 0.61 |
| msnr | p=250 p=500 p=1000 p=1500 | 0.98/0.96/0.98 0.98/0.99/0.98 0.94/0.98/0.98 0.91/0.94/0.98 | $\begin{array}{c} 0.66/0.66/0.66/0.96 \\ 0.7/0.7/0.7/0.98 \\ 0.71/0.71/0.71/0.99 \\ 0.71/0.71/0.71/0.99 \end{array}$ | 0.92/0.74/0.91 0.96/0.69/0.94 0.97/0.64/0.93 0.96/0.63/0.9 | 0.66 0.7 0.71 0.71 | 0.74 0.69 0.64 0.63 | 0.89/0.94 0.88/0.92 0.85/0.89 0.82/0.87 | 0.96/0.94 0.8/0.92 0.77/0.89 0.76/0.87 | 1 1 1 1 | 0.92 0.91 0.88 0.84 |
| lsnr | p=250 p=500 p=1000 p=1500 | 0.95/0.96/0.95 0.92/0.96/0.95 0.86/0.95/0.95 0.81/0.89/0.95 | $\begin{array}{c} 0.41/0.41/0.41/0.94 \\ 0.41/0.41/0.41/0.95 \\ 0.42/0.42/0.42/0.95 \\ 0.42/0.42/0.42/0.95 \end{array}$ | 0.96/0.95/0.95 0.97/0.96/0.96 0.97/0.97/0.97 0.97/0.98/0.97 | 0.41 0.41 0.42 0.42 | 0.95 0.96 0.97 0.98 | 1/0.99 1/0.99 1/0.98 1/0.98 | 0.52/0.99 0.43/0.99 0.43/0.98 0.43/0.98 | 0.98 0.97 0.97 0.96 | 0.97 0.97 0.96 0.96 |
| | | | | Spar | sistency | | | | | |
| hsnr | p=250 p=500 p=1000 p=1500 | 21.5/15.1/17.4 22.6/15.5/15.7 20.8/15.7/12.5 16.1/16.1/9.8 | 199/199/199/16.5 199/199/199/15.6 199/199/199/11.5 199/199/199/8.6 | $\begin{array}{c} 10.9/3.2/9 \\ 9.1/3.1/5.8 \\ 7.3/3/4.1 \\ 6/3/3.6 \end{array}$ | 199 199 199 198.9 | 3.2 3.1 3 3 | 58.7/96.1 52.3/106.6 30.2/92.9 29.4/71.9 | 44.4/96.1 63/106.6 87/92.9 94.5/71.9 | 27.1 30.3 38.3 28.8 | 63 66.7 19.8 11 |
| msnr | p=250 p=500 p=1000 p=1500 | 9.2/5/6.6 7.7/4.8/4.4 10.2/5.4/3.8 11.1/8/3.7 | 199/199/199/5.2 199/199/199/4.1 199/199/199/3.8 199/199/199/3.7 | 3.2/1.8/3.1 3.1/1.1/2.9 3/0.4/2.8 3/0.3/2.6 | 199 199 199 198.9 | 1.8 1.1 0.4 0.3 | 28.2/49 26.1/43.2 25.9/47 24.9/48.7 | 52.3/49 93.3/43.2 103.5/47 103.2/48.7 | 15.2 10.4 9.2 10.1 | 25 18.5 21.1 22.5 |
| lsnr | p=250 p=500 p=1000 p=1500 | 0.6/0.2/1.1 1.4/0.2/0.7 3.3/0.6/0.5 4.2/1.6/0.4 | $\begin{array}{c} 199/199/199/0.9 \\ 199/199/199/0.6 \\ 199/199/199/0.5 \\ 199/199/199/0.4 \end{array}$ | 0.1/0/0.1 0.1/0/0 0.1/0/0 0/0/0 | 199 199 199 198.9 | 0 0 0 0 | 8.3/9.2 8.1/9.6 8/10.1 8.1/10.6 | 65.2/9.2 112.3/9.6 112.4/10.1 110.5/10.6 | 7.2 7.7 8.4 9.3 | 6.2 5.8 7.2 7.2 |
| | | | | Number of | extra varia | ables | | | | |
| hsnr | p=250 p=500 p=1000 p=1500 | -/-/- -/-/- -/-/- -/-/- | -/-/-/ -/-/-/ -/-/-/ -/-/-/ | -/-/- -/-/- -/-/- -/-/- | - - - | - - - | -/- -/- -/- -/- | -/- -/- -/- -/- | - - - | - - - |
| msnr | p=250 p=500 p=1000 p=1500 | -/-/- -/-/- -/-/- | -/-/-/- -/-/-/- -/-/-/- | -/-/- -/-/- -/-/- -/-/- | - - - | - - - | -/- -/- -/- -/- | -/- -/- -/- -/- | - - - | - - - - |
| lsnr | p=250 p=500 p=1000 p=1500 | -/-/- -/-/- -/-/- | -/-/-/- -/-/-/- -/-/- -/-/- | -/-/- -/-/- -/-/- -/-/- | - - - | - - - | -/- -/- -/- -/- | -/- -/- -/- -/- | - - - | - - - |

Table S51: The performance of BOSS for high dimensional data, Dense, ρ =0.9, n=200

| | | BOSS C _v /AICc/CV | FS EBIC/HDBIC/HDHQ/CV | FSstop EBIC/HDBIC/HDHQ | FStrim HDBIC | FSstoptrim HDBIC | lasso AICc/CV | Gamma lasso AICc/CV | SparseNet CV | rlasso CV |
|----------|------------------|----------------------------------|--|----------------------------------|-----------------|---------------------|--|---------------------------------------|-----------------|--------------|
| i | | | | % worse than the | best possi | ible BOSS | - | | | |
| | p=250 p=500 | 10/21/12 27/24/18 | 79/79/79/12 61/61/61/21 | 68/113/90 68/95/82 | 79 61 | 113 95 | 75/39 113/71 | 19/39 32/71 | 14 52 | 42 80 |
| hsnr | p=1000 p=1500 | 45/21/26 34/17/25 | 37/37/37/29 22/22/22/26 | 51/67/58 37/51/42 | 37 22 | 67 51 | $\frac{129}{123}$ $\frac{101}{103}$ | $\frac{30/123}{17/103}$ | 55 36 | 125 106 |
| | p=250 | 14/13/9 | 94/94/94/9 | 17/49/23 | 94 | 49 | 46/43 | 33/43 | 15 | 46 |
| msnr | p=500 p=1000 | 10/9/7 8/7/7 | 85/85/85/7 79/79/79/7 | 15/46/22 15/43/25 | 85 79 | 46 43 | $\frac{49}{50}$ $\frac{45}{46}$ | 49/50 53/46 | 18 25 | 48 44 |
| | p=1500 p=1500 | 7/7/7 | 76/76/76/7 | 15/41/26 | 76 | 41 | 41/42 | 55/42 | 33 | 41 |
| | p=250 p=500 | 15/16/11 15/15/11 | 227/227/227/11 220/220/220/11 | 15/38/20 15/37/22 | 227 220 | 38 37 | 14/14 13/13 | 143/14 200/13 | 10 9 | 11 10 |
| lsnr | p=500 p=1000 | 19/15/11 | 213/213/213/12 | 16/36/24 | 213 | 36 | 12/13 | 198/13 | 9 | 10 |
| | p=1500 | 24/17/13 | 209/209/209/13 | 17/34/24 | 209 | 34 | 12/14 | 194/14 | 10 | 10 |
| | | | | Relative | efficiency | | | | | |
| | p=250 p=500 | 1/0.91/0.99 0.93/0.95/1 | 0.62/0.62/0.62/0.99 0.73/0.73/0.73/0.98 | 0.66/0.52/0.58 0.71/0.61/0.65 | 0.62 | 0.52 0.61 | 0.63/0.8 0.56/0.69 | 0.92/0.8 0.9/0.69 | 0.97 0.78 | 0.78 0.66 |
| hsnr | p=300 p=1000 | 0.83/1/0.97 | 0.89/0.89/0.89/0.94 | 0.8/0.73/0.77 | 0.73 | 0.01 | 0.53/0.59 $0.53/0.54$ | 0.93/0.54 | 0.78 | 0.54 |
| | p=1500 | 0.87/1/0.94 | 0.96/0.96/0.96/0.93 | 0.85/0.77/0.82 | 0.96 | 0.77 | 0.58/0.58 | 1/0.58 | 0.86 | 0.57 |
| | p=250 | 0.96/0.96/1 | 0.56/0.56/0.56/1 | 0.93/0.73/0.89 | 0.56 | 0.73 | 0.75/0.76 | 0.82/0.76 | 0.95 | 0.75 |
| msnr | p=500 | 0.97/0.98/1 0.99/1/1 | 0.58/0.58/0.58/1 0.6/0.6/0.6/1 | 0.93/0.73/0.87 0.93/0.75/0.85 | 0.58 | 0.73 0.75 | 0.71/0.71 0.74/0.73 | 0.72/0.71 0.7/0.73 | 0.91 0.86 | 0.72 0.74 |
| | p=1000 p=1500 | 1/1/1 | 0.61/0.61/0.61/1 | 0.93/0.76/0.85 | 0.61 | 0.76 | 0.74/0.75 $0.76/0.75$ | 0.69/0.75 | 0.81 | 0.74 |
| | p=250 | 0.96/0.95/0.99 | 0.34/0.34/0.34/0.99 | 0.96/0.8/0.92 | 0.34 | 0.8 | 0.97/0.97 | 0.45/0.97 | 1 | 1 |
| lsnr | p=500 | 0.95/0.95/0.98 0.92/0.95/0.98 | 0.34/0.34/0.34/0.99 | 0.95/0.8/0.89 | 0.34 0.35 | 0.8 0.81 | 0.97/0.96 0.97/0.96 | 0.36/0.96 | 1 1 | 0.99 |
| | p=1000 p=1500 | 0.88/0.94/0.97 | 0.35/0.35/0.35/0.98 0.35/0.35/0.35/0.98 | 0.94/0.81/0.89 0.94/0.82/0.88 | 0.35 | 0.81 | 0.97/0.96 | 0.37/0.96 0.37/0.97 | 1 | 1 |
| <u> </u> | | | . , , | Spars | sistency | | , | · · · · · · · · · · · · · · · · · · · | | = |
| | p=250 | 17.2/13.2/19.3 | 199/199/199/16.3 | 6.4/3.2/4.7 | 199 | 3.2 | 55.8/93.9 | 49.7/93.9 | 42.5 | 77.7 |
| hsnr | p=500 | 13.1/11.7/16.3 | 199/199/199/13.6 | 5/3.1/3.8 | 199 | 3.1 | 38.3/79.6 | 71.1/79.6 | 36.1 | 55.5 |
| | p=1000 p=1500 | 6.6/9.7/10.4 4.9/7.9/6.9 | 199/199/199/8 199/199/199/5.8 | 4.2/3/3.6 3.9/2.9/3.5 | 199 199 | 3 2.9 | 9.8/19.2 12.5/12.6 | 62.7/19.2 63.7/12.6 | 15.1 20.8 | 9.2 3.2 |
| <u> </u> | p=250 | 5.1/3.8/6.7 | 199/199/199/4.6 | 2.8/1.3/2.5 | 199 | 1.3 | 17/28.6 | 52.8/28.6 | 14.9 | 17.2 |
| msnr | p=500 | 3.6/3.6/4.6 | 199/199/199/4 | 2.7/1.1/2.3 | 199 | 1.1 | 7.4/8.9 | 82/8.9 | 16.8 | 3.5 |
| 1110111 | p=1000 p=1500 | 3.6/3.6/3.8 3.9/3.9/3.6 | 199/199/199/3.6 199/199/199/3.5 | 2.5/1/1.9 2.4/1/1.8 | 199 199 | 1 1 | 8.3/8.3 10.4/10.5 | 93.8/8.3 97.2/10.5 | 17.8 11.8 | 2.3 2.6 |
| <u> </u> | p=250 | 0.9/0.8/2 | 199/199/199/1.6 | 0.7/0.1/0.6 | 199 | 0.1 | 6.6/6.8 | 64.6/6.8 | 3.8 | 3.1 |
| lsnr | p=500 | 1/0.8/1.5 | 199/199/199/1.3 | 0.6/0.1/0.4 | 199 | 0.1 | 7.5/7.3 | 112.2/7.3 | 3.9 | 3.2 |
| 15111 | p=1000 p=1500 | 1.5/0.9/1.2 2.2/1/1.1 | 199/199/199/1.2 199/199/199/1.1 | 0.5/0/0.3 0.5/0/0.3 | 199 199 | 0 | 9.1/9.2 9.3/10.3 | 115.1/9.2 112.6/10.3 | 4.9 5.6 | 3.9 4.7 |
| <u> </u> | 1 | | ,,, | Number of | extra varia | bles | / | -/ | | |
| <u> </u> | p=250 | -/-/- | -/-/- | -/-/- | - | - | -/- | -/- | - | <u> </u> |
| hsnr | p=500 | -/-/- | -/-/- | -/-/- | - | - | -/- | -/- | - | - |
| 110111 | p=1000 p=1500 | -/-/- -/-/- | -/-/- -/-/- | -/-/- -/-/- | - | - | -/- -/- | -/- -/- | - | - |
| <u> </u> | p=250 | -/-/- | -/-/- | -/-/- | - | - | -/- | -/- | - | |
| msnr | p=500 | -/-/- | -/-/- | -/-/- | - | - | -/- | -/,- | - | - |
| 1115111 | p=1000 p=1500 | -/-/- -/-/- | -/-/- -/-/- | -/-/- -/-/- | - | - | -/- -/- | -/- -/- | - | - |
| <u> </u> | p=250 | -/-/- | -/-/- | -/-/- | _ | - | -/- | -/- | - | |
| lsnr | p=500 | -/-/- | -/-/-/- | -/-/- | - | - | -/- | -/- | - | - |
| ism | p=1000 p=1500 | -/-/- | -/-/- | -/-/- | - | - | -/- -/- | -/- -/- | - | - |
| | h=1900 | -/-/- | -/-/- | -/-/- | - | - | -/- | -/- | - | - |

References

- Ing, C.-K. and T. L. Lai (2011). A stepwise regression method and consistent model selection for high-dimensional sparse linear models. *Statistica Sinica*, 1473–1513.
- Taddy, M. (2017). One-step estimator paths for concave regularization. *Journal of Computational and Graphical Statistics* 26(3), 525–536.
- Wang, H. (2009). Forward regression for ultra-high dimensional variable screening. *Journal of the American Statistical Association* 104 (488), 1512–1524.
- Zou, H., T. Hastie, and R. Tibshirani (2007). On the "degrees of freedom" of the lasso. *The Annals of Statistics* 35(5), 2173–2192.