

Example

Let's look at an LED illuminating the human eye. Rather than treat the LED as an extended source (like it really is), let's treat it as a perfect point source.

LED specifications: 70 cd

No need for LED area or cone angle

Eye diameter outside $L = 10^2 \text{ cd/m}^2 \rightarrow D = 3 \text{ mm}$, $f = 60$
Distance from LED to eye 3m

$$\Omega = \pi \left(\frac{1.5 \times 10^{-3}}{3} \right)^2 = 0.785 \mu \text{Sr}$$

Total luminous flux $\Phi = (70)(0.785 \times 10^{-6})$
 $= 55 \mu \text{lm}$

At this distance the field should be very uniform

$$e(r) = E_0 \text{ circ} \left(\frac{r}{1.5 \text{ mm}} \right)$$

$$E(fr) = \mathcal{F}\{e(r)\} \Big|_{fr = \frac{r}{\lambda f}}$$

$$E(fr) = E_0 \frac{J_1((2\pi)(1.5 \times 10^{-3}) fr)}{fr} \quad \text{ignore any amplitude factors}$$

Substitute in $fr = \frac{r}{\lambda f}$

$$E(r) = E_0 \frac{J_1((2\pi)(1.5 \times 10^{-3}) (\frac{r}{620 \times 10^{-9}}) (16.67 \times 10^{-3}))}{r}$$

$$= E_0 \frac{J_1(9.12 \times 10^5 r)}{r}$$

convert to illuminance

$$I = I_0 \frac{J_1^2(9.12 \times 10^5 r)}{r^2}$$

Use conservation of power to find I_0

$$\Phi = 55 \times 10^{-6} = \int_0^{2\pi} \int_0^\infty I_0 \frac{J_1^2(9.12 \times 10^5 r)}{r^2} r dr d\theta$$

$$= I_0 2\pi \int_0^\infty \frac{J_1^2(9.12 \times 10^5 r)}{r} dr$$

$$u = 9.12 \times 10^5 r \quad du = 9.12 \times 10^5 dr$$

$$\Phi = 2\pi I_0 \int_0^\infty \frac{J_1^2(u)}{\left(\frac{u}{9.12 \times 10^5}\right)} \left(\frac{1}{9.12 \times 10^5}\right) du$$

$$= 2\pi I_0 \int_0^\infty \frac{J_1^2(u)}{u} du = (2\pi)(I_0) \left(\frac{1}{2}\right) = I_0 \pi$$

$$I_0 = \frac{55 \times 10^{-6}}{\pi} = 1.75 \times 10^{-5} \frac{\text{lm}}{\text{m}^2}$$

$$I = 1.75 \times 10^{-5} \frac{J_1^2(9.12 \times 10^5 r)}{r^2}$$

To find the maximum I : $I_{\max} = 1.75 \times 10^{-5} \lim_{r \rightarrow 0} \frac{J_1^2(9.12 \times 10^5 r)}{r^2}$

look up small angle approximation for bessel function

$$J_n \sim \frac{x^n}{2^n n!} \quad J_1 \sim \frac{x}{2}$$

$$I_{\max} = 1.75 \times 10^{-5} \lim_{r \rightarrow 0} \frac{(9.12 \times 10^5 r)^2}{4 r^2}$$

$$= (1.75 \times 10^{-5}) \frac{(9.12 \times 10^5)^2}{4}$$

$$I_{\max} = 3.64 \times 10^6 \frac{\text{lm}}{\text{m}^2} = 3.64 \times 10^6 \text{ lux}$$

This is much higher than reality because it assumes the lens is perfect.

Let's go to OSLO to look at a single lens

Main lobe of pattern is called the Airy Disk. It is when

$$J_1(9.12 \times 10^5 r) = 0$$

$$J_1(3.8317) = 0$$

$$r = \frac{3.8317}{9.12 \times 10^5} = 4.2 \text{ } \mu\text{m}$$

$$I \propto \frac{55 \times 10^{-6} \text{ lm}}{(\pi) (0.0043 \times 10^{-3})^2} = 9.36 \times 10^5 \frac{\text{lm}}{\text{m}^2} = 0.94 \times 10^6 \text{ lux}$$

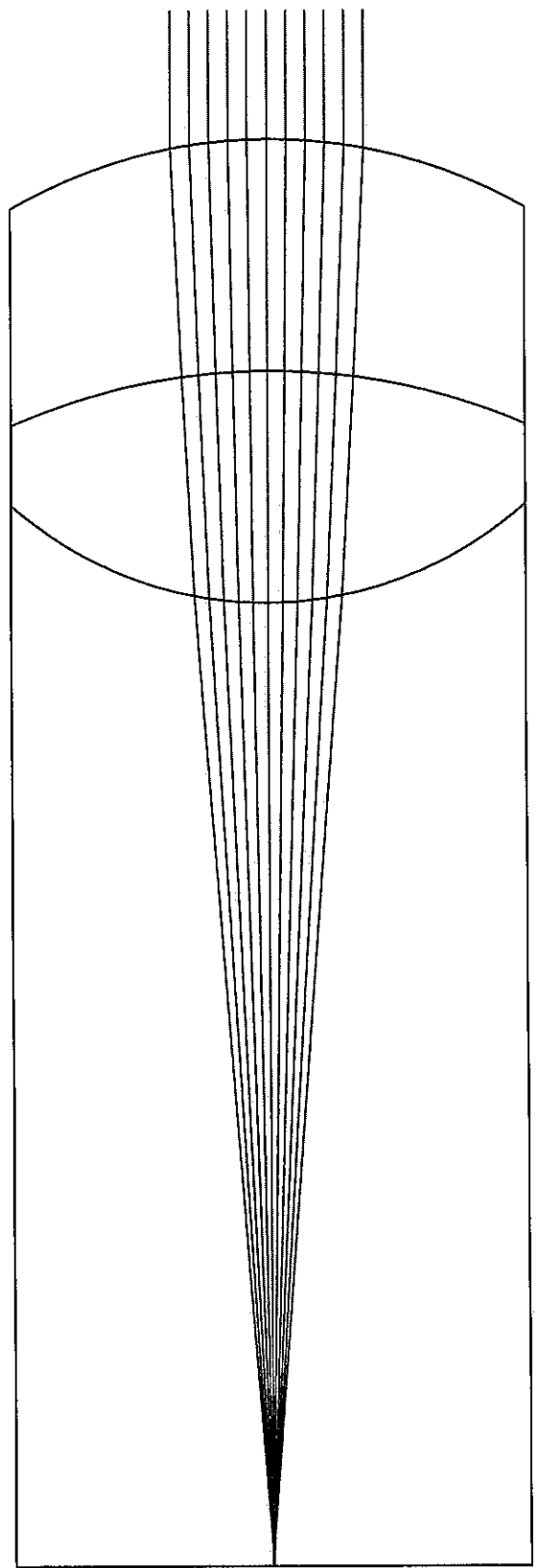
No name

FOCAL LENGTH = 14.97 NA = 0.1002

UNITS: MM
DES: OSLO

2.69

Human Eye model
with D=3mm

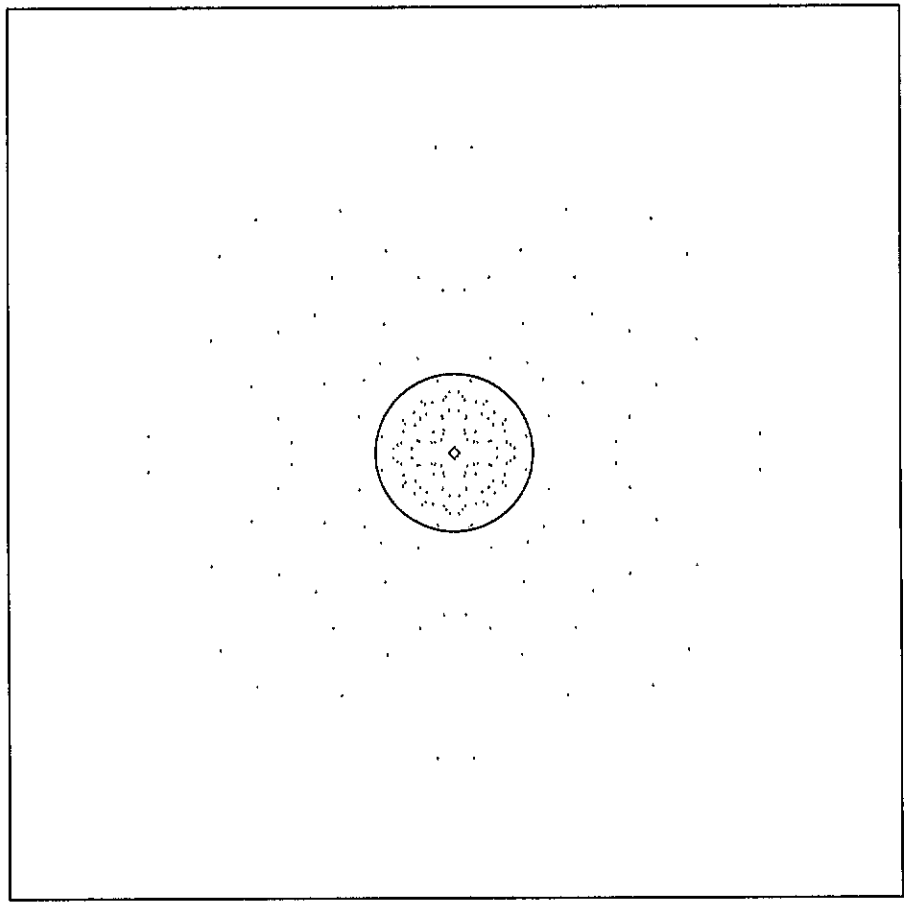


No name SPOT DIAGRAM	FBY 0 FBX 0 FOCUS 0	REFHT 0 UNITS: mm
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GEOMETRICAL
RMS R SIZE
0.005965

Geometrical optics
dominates

DIFFRACTION
LIMIT
0.003541



GEOMETRICAL
RMS Y SIZE
0.004218

GEOMETRICAL
RMS X SIZE
0.004218

0.02
-0.02