Features of dual-purpose structure for heavy ion and light particles

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The different charge-to-mass ratio is essential in magneto-optics design. To achieve high luminosity sufficient beam lifetime must be guaranteed. Transition energy crossing must also be solved. The NICA collider will be used for both collider experiments with heavy ions and light polarized nuclei.

Keywords: Transition energy, Intra-beam scattering, Stochastic cooling, Resonant structure, Dual-purpose structure

I. INTRODUCTION

Regardless of the purpose of the synchrotron, always in the case of two modes, when multiply charged heavy particles and one or two charged light particles are accelerated, the problem arises of what the magneto-optical structure should look like to satisfy all the conditions of stable motion for both types of particles. Obviously, compared to light particles, multiply charged particles have a prevailing heating effect due to intra-beam scattering, and light particles have a greater chance of crossing through transition energy. All these effects are of great importance for colliders, where luminosity plays a decisive role. When developing a structure that meets all the requirements for differently charged partiticles, it is fundamentally important to have a retunable structure without introducing design differences. We called such a structure – dual-purpose or simple, dual.

In NICA complex the dual magneto-optical structure opens up the prospect of accelerating both heavy ions, such as gold, and light particles like protons and deuterons. The design of this structure requires a different approach due to the varying charge-to-mass ratios involved.

II. LIGHT PARTICLES

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In a classical regular structure, the transition energy is approximately equal to the betatron tune $\gamma_{\rm tr} \simeq \nu_{\rm s}$ [1]. For the same magnetic rigidity $B\rho$, the maximum energy for light particles is greater than for heavy ions due to their charge-to-mass ratio. This means that a heavy-ion structure optimized for operating up to a certain transition energy would require overcoming that energy in order to operate with light particles. For this reason, a structure with varying transition energy can be considered.

A. Transition energy

In general, the transition energy is determined by the momentum compaction factor

$$\alpha = \frac{1}{\gamma_{\text{tr}}^2} = \frac{1}{C} \int_0^C \frac{D(s)}{\rho(s)} ds \tag{1}$$

where C – orbit length, D(s) – dispersion function, $\rho(s)$ – radius of orbit curvature. It is a characteristic of the structure and remains constant regardless of the particle type. In the first order the slip-factor $\eta=\eta_0=1/\gamma_{\rm tr}^2-1/\gamma^2$, and thus the frequency of synchrotron oscillations $\omega_s\sim\eta$ tends to zero when the beam energy approaches the transition value. In this case, the adiabaticity of the longitudinal phase motion is violated, which leads to instabilities, as well as the influence of nonlinear effect higher orders of momentum spread δ . The introduction of modulation into the D(s) or $\rho(s)$, function leads to variations in the momentum compaction factor and, consequently, the transition energy.

B. Superperiodic modulation

The equation for the dispersion function with biperiodic variable focusing [2]

$$\frac{\mathrm{d}^2 D}{\mathrm{d}s^2} + \left[K(s) + \varepsilon k(s) \right] D = \frac{1}{\rho(s)},\tag{2}$$

52 where $K(s)=\frac{e}{p}G(s), \varepsilon k\left(s\right)=\frac{e}{p}\Delta G(s), G\left(s\right)$ – gradient 53 of magneto-optical lenses, $\Delta G\left(s\right)$ – superperiodic gradient 54 modulation. Here is considered an additional perturbation to 55 regular one $\varepsilon k\left(s\right)=\sum_{k=0}^{\infty}g_{k}\cos(k\phi)$, where $g_{k}-k$ -th harmonic of the gradient modulation in the Fourier series expansion of the function. The solution for momentum compaction 58 factor as follows for only gradient modulation

$$\alpha_{\rm s} = \frac{1}{\nu^2} \left\{ 1 + \frac{1}{4(1 - kS/\nu)} \left(\frac{\bar{R}}{\nu} \right)^4 \frac{g_k^2}{\left[1 - (1 - kS/\nu)^2 \right]^2} \right\}.$$

where $\overline{R}_{\rm arc}$ – the average value of the curvature, ν_x – betatron tune in horizontal plane on arc, S – number of superperiods per arc length. Eq. (3) considered without introducing curvature modulation due to the possibility of introducing a variation of transition energy into a stationary lattice. To raise the transition energy, it is necessary to reduce $\alpha_s=1/\gamma_{\rm tr}^{\rm arc}$, this means that the expression under the sum sign must be negative, this is realizable under the condition $kS/\nu_{x,{\rm arc}}>1$. First harmonic k=1 has a dominant influence the condition is implemented for S=4, $\nu_{x,{\rm arc}}=3$. Fig. 1 shows 12

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73 For structure with the missing magnet technique introduced 93 derivatives become zero, then ⁷⁴ for one reason or another it can be also implemented (Fig. 2), ₇₅ but need to suppress dispersion at the edge of arc [4].

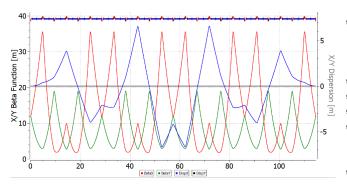


Fig. 1. (Color online) "Resonant" magneto-optic structure with dispersion modulation and increased transition energy.

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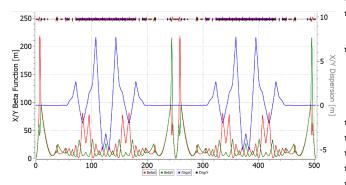


Fig. 2. (Color online) "Resonant" NICA magneto-optic adapted structure with increased transition energy and missing magnet.

III. HEAVY ION MODE

The lifetime of the beam luminosity in a collider exper-82 iment is achieved through the reduction of intra-beam scat-83 tering effects, coupled with the application of stochastic and 84 electron beam cooling techniques. This approach assumes particular significance when dealing with high-intensity ion 86 beams. The temporal evolution of emittance and momentum 87 spread in the presence of cooling processes is governed by a 88 set of equations

$$\frac{\mathrm{d}\varepsilon}{\mathrm{d}t} = \underbrace{-\frac{1}{\tau_{\mathrm{tr}}} \cdot \varepsilon}_{\text{cooling}} + \underbrace{\left(\frac{\mathrm{d}\varepsilon}{\mathrm{d}t}\right)_{\mathrm{IBS}}}_{\text{heating}}$$

$$\frac{\mathrm{d}\delta^{2}}{\mathrm{d}t} = \underbrace{-\frac{1}{\tau_{\mathrm{long}}} \cdot \delta^{2}}_{\text{cooling}} + \underbrace{\left(\frac{\mathrm{d}\delta^{2}}{\mathrm{d}t}\right)_{\mathrm{IBS}}}_{\text{heating}} \tag{4}$$

FODO cells per arc, 3 FODO cells are combined into one supprepried [3]. Thus, due to the tune of betatron tune a multiple of 2π , the arc has the properties of a first-order achromat. So where ε – transverse emittance, $\tau_{\rm tr}$ – transverse cooling time, $\tau_{\rm tr}$ – transverse cooling time, $\tau_{\rm tr}$ – momentum spread, $\tau_{\rm long}$ – longitudinal cooling time, $\tau_{\rm tr}$ – momentum spread, $\tau_{\rm long}$ – longitudinal cooling time, $\tau_{\rm tr}$ – transverse emittance, $\tau_{\rm tr}$ – transverse cooling time, $\tau_{\rm tr}$ – transverse emittance, $\tau_{\rm tr}$ – transverse cooling time, $\tau_{\rm tr}$ – transverse emittance, $\tau_{\rm tr}$ – transverse cooling time, $\tau_{\rm tr}$ – transverse emittance, $\tau_{\rm tr}$ – transverse cooling time, $\tau_{\rm tr}$ – transverse emittance, $\tau_{\rm tr}$ – transverse cooling time, $\tau_{\rm tr}$ – transverse emittance, $\tau_{\rm tr}$ – transverse emittance, $\tau_{\rm tr}$ – transverse emittance, $\tau_{\rm tr}$ – transverse cooling time, $\tau_{\rm tr}$ – transverse emittance, $\tau_{\rm tr}$

$$\varepsilon_{\rm st} = \tau_{\rm tr} \cdot \left(\frac{\mathrm{d}\varepsilon}{\mathrm{d}t}\right)_{\rm IBS}\Big|_{\varepsilon = \varepsilon_{\rm st}}$$

$$\delta_{\rm st}^2 = \tau_{\rm long} \cdot \left(\frac{\mathrm{d}\delta^2}{\mathrm{d}t}\right)_{\rm IBS}\Big|_{\delta^2 = \delta_+^2}$$
(5)

95 The benchmark for evaluating the effectiveness of a cooling 96 technique can be determined by comparing the timescales of 97 stochastic or electron cooling processes to the beam lifetime due to IBS over the entire energy spectrum.

Stochastic cooling

Let's consider stochastic cooling using the approximate theory developed by D.Mohl [5, 6]. Based on his main find-102 ings, the cooling rate can be determined using the following 103 expression

$$\frac{1}{\tau_{\text{tr, 1}}} = \frac{W}{N} \left[\underbrace{2g\cos\theta \left(1 - 1/M_{\text{pk}}^2\right)}_{\text{coherent}} - \underbrace{g^2 \left(M_{\text{kp}} + U\right)}_{\text{incoherent}} \right] \quad (6)$$
effect(cooling)

where $W=f_{\rm max}-f_{\rm min}$ – system bandwidth, N – effective number of particles, recalculated based on the ratio of orbit $_{107}$ length to the beam length, considering its distribution, g – 108 fraction of observed sample error corrected per turn, U – the $_{\rm 109}$ ratio of noise to signal, $M_{\rm pk},\,M_{\rm kp}$ – mixing factors between $_{\rm 110}$ the pickup-kicker and the kicker-pickup, respectively. Eq. (6) in the absence of noise at $g=g_0=\frac{1-M_{
m pk}^2}{M_{
m kp}}$ reaches the 112 maximum

$$\frac{1}{\tau_{\text{tr}}} = \frac{W}{N} \frac{\left(1 - 1/M_{\text{pk}}^2\right)^2}{M_{\text{kp}}}$$

$$\frac{1}{\tau_{\text{l}}} = 2\frac{W}{N} \frac{\left(1 - 1/M_{\text{pk}}^2\right)^2}{M_{\text{kp}}}$$
(7)

114 The mixing coefficients are defined as

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$$M_{\rm pk} = \frac{1}{2 \left(f_{\rm max} + f_{\rm min} \right) \eta_{\rm pk} T_{\rm pk} \frac{\Delta p}{p}},$$

$$M_{\rm kp} = \frac{1}{2 \left(f_{\rm max} - f_{\rm min} \right) \eta_{\rm kp} T_{\rm kp} \frac{\Delta p}{p}}$$
(8)

where $\eta_{\rm pk}T_{\rm pk}\delta,\,\eta_{\rm kp}T_{\rm kp}\delta$ – relative particle displacement times (mixing), $\eta_{\rm pk}$, $\eta_{\rm kp}$ – slip-factor, as a first approximation $\eta_{\rm pk}$ = 118 $\alpha_{\rm pk}$ – $1/\gamma^2$, $\eta_{\rm kp}$ = $\alpha_{\rm kp}$ – $1/\gamma^2$, $\alpha_{\rm pk}$, $\alpha_{\rm kp}$ – first-order of local momentum compaction factors, $T_{\rm pk}$, $T_{\rm kp}$ – the absolute 120 times between the pickup-kicker and kicker-pickup, respec-121 tively. The stochastic cooling times of Eq. (7) depend on the

122 ratio of the effective particle density to the cooling system 167 bandwidth and the properties of magneto-optics, local mo- 168 mentum compaction factors α_{pk} , α_{kp} .

by the requirement that the "Schottky" beam bands do not overlap. In the simplest case, this can be expressed:

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$$f_{\text{max}} < \frac{1}{\eta_{\text{pk}} T_{\text{pk}} \frac{\Delta p}{p}} \tag{9}$$

thus, a mixing factor $M_{\rm pk}>1$. Otherwise, the cooling effi-130 ciency becomes zero. Thus, for a given number of particles, it is desirable to achieve the highest possible frequency band. 132 From an electron perspective, modern technologies allow for the implementation of a 10 GHz frequency band [7], however, 134 its use is not always feasible due to the large magnitude of the 135 slip-factor $\eta_{\rm pk}$ and momentum spread δ .

Eq. (6) has been derived for coasting beam. Particle den-137 sity for a single harmonic RF resonator is described by a Gaussian distribution

$$\rho(s) = \frac{N_{\text{bunch}}}{\sigma_{\text{bunch}} \sqrt{2\pi}} \cdot e^{-\frac{s^2}{2\sigma_{\text{bunch}}^2}}$$
(10)

 $_{\text{140}}$ where s – the distance from the beam center, σ_{bunch} – the dis- $^{\text{186}}$ persion of the particle distribution, and N_{bunch} – the number 187 across the entire "regular" ring illustrates at Fig. 3. The 142 of particles. Assuming that cooling is at its minimum at the 188 143 center (s=0), the effective particle number at orbit length 189 C_{orb} can be calculated as follows:

$$N = \frac{N_{\text{bunch}}}{4\sigma_{\text{bunch}}} \cdot C_{\text{orb}} \tag{11}$$

146 For a beam generated by a multiharmonic barrier-type RF 147 system, so-called "Barrier Bucket", the particles distribution 148 in the beam can be considered approximately uniform along 149 its entire length. The effective particles number is determined 150 by a simple ratio of the beam length to the total orbit length: 151 To summarize, the effective value of particles depends on 152 their distribution and is determined by their form-factor 153 $F_{\text{bunch}} = \sqrt{2\pi \div 4}$

$$N = N_{\text{bunch}} \cdot \frac{C_{\text{orb}}}{F_{\text{bunch}} \cdot \sigma_{\text{bunch}}}$$
 (12)

As example let us consider the case of NICA with maximal ₁₅₆ form-factor $F_{\rm bunch}=4$ with $C_{\rm orb}=503.04$ m, $\sigma_{\rm bunch}=0.6$ m, $N_{\text{bunch}} = 2.2 \cdot 10^9$. Considering the accumulated FNAL [8] 158 experience, quite realistic values for the frequency band are 159 $f_{
m max}=8$ GHz and $f_{
m min}=2$ GHz. For NICA $f_{
m max}=4$ GHz and $f_{\min} = 2$ GHz. With these parameters, the maximum achievable cooling rate is $1/\tau_{tr} = 1/230 \text{ s}^{-1}$.

Based on Eq. (8), it is evident that asymptotic growth may 162 163 occur in two scenarios:

1. slip-factor approaches the value $\eta \to \frac{1}{2(f_{\max} + f_{\min})T_{\text{pk}}\delta}$, 203 The case of a "combined" structure, one arc operates in a reg- $M_{\rm pk} \rightarrow 1;$

2. slip-factor approaches zero, mixing between the kicker to the pickup does not occur and $M_{\rm kp} \to \infty$.

The maximum value of the frequency band is determined 169 The efficiency of stochastic cooling depends on the properties of magneto-optical structure. In classical "regular" structures, 171 transition energy is acquired through the horizontal frequency 172 $\gamma_{\rm tr} \approx \nu_x$ and slip-factor $\eta=1/\gamma_{\rm tr}^2-1/\gamma^2$ can achieve zero. 173 To avoid asymptotic growth, it is necessary to vary the slip-(9) 174 factor which means $\gamma_{\rm tr}$. This is possible in "resonant" struc-175 ture, where transition energy can be increased or even reach 176 complex value. In more exotic case, can be used "combined" 177 structure then $\eta_{\rm pk}$ (pickup-kicker) with real transition energy 178 at one arc

$$\eta_{\rm pk} = 1/\gamma_{\rm tr}^2 - 1/\gamma^2 \tag{13}$$

180 compensated by $\eta_{\rm kp}$ (kicker-pickup) with complex transition 181 energy at another

$$\eta_{\rm kp} = -1/\gamma_{\rm tr}^2 - 1/\gamma^2 \tag{14}$$

183 for the whole ring. Such structure achieves the required ratio (10) 184 of mixing factors for a maximum cooling rate close to ideal 185 [9]. Let us delve deeper declared structures in more detail.

The behaviour of the β -functions and D the dispersion straight sections, which remain constant in all structures, are essential for analyzing of the resonant characteristics of the 190 entire structure. Their arrangement does not affect the intra-191 beam scattering and transition energy. To suppress dispersion 192 in the "regular" structure, 'missing magnets' technic imple-(11) 193 mented on both sides of the arc. The "resonant" structure is based on the principle of resonant modulation of the dispersion function and can be obtained from a "regular" one by introducing additional family of focusing quadrupoles. To suppress dispersion can be used either two edge focusing quadrupoles on both sides of the arc or only two families of 199 focusing quadrupoles on the arc, when an integer number of betatron oscillations is reached.

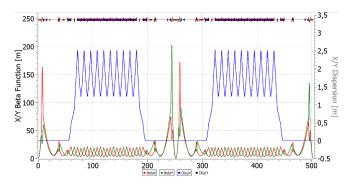


Fig. 3. (Color online) "Regular" FODO NICA magneto-optic structure with missing magnets.

the beam Schottky spectrum becomes continuous and 204 ular mode, while the other employs resonant modulation (Fig. 205 4). Such choice is based on the principle of compensation, ²⁰⁶ as described by Eqs. 13, 14, which requires a greater mod-²⁰⁷ ulation depth of the quadrupoles than in purely "resonant" ²⁰⁸ structure with increased transition energy. As illustrated in

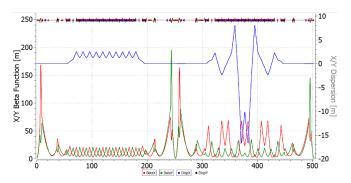


Fig. 4. (Color online) "Combined" NICA magneto-optic structure with real and complex transition energies in arcs.

²¹¹ Fig. 5, "resonant" optics with increased transition energy, the ²¹² second asymptotic is at higher energy compared to the "regular" structure. In "combined" magneto-optics, the cooling ²¹⁴ efficiency is closer to the ideal value in a large energy range ²¹⁵ from 2.5 to 4.5 GeV, while in "regular" optics the cooling rate ²¹⁶ is almost two times lower at the most optimal point ~ 3 GeV. ²¹⁷ This behaviour is explained by absence of the second point of ²¹⁸ asymptotic growth.

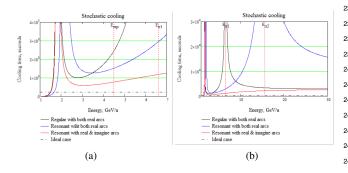


Fig. 5. (Color online) The dependence of stochastic cooling time on the energy for various structures. Energy range (a) 1-7, (b) 0-30 GeV.

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B. Intrabeam Scattering

Intra-beam scattering represents a fundamental limitation on the beam lifetime in the collider. Consequently, the selection of an appropriate cooling technique hinges on comparing its characteristic time scales with the rate at which the beam heated due to intra-beam scattering. This is derived from the fundamental principles governing this process

$$\frac{1}{\tau_{\text{IBS}}} = \frac{\sqrt{\pi}}{4} \frac{cZ^2 r_p^2 L_C}{A} \cdot \frac{N}{C_{\text{orb}}} \cdot \frac{\langle \beta_x \rangle}{\beta^3 \gamma^3 \varepsilon_x^{5/2} \langle \sqrt{\beta_x} \rangle} \times \left(\left\langle \frac{D_x^2 + \dot{D}_x^2}{\beta_x^2} \right\rangle - \frac{1}{\gamma^2} \right) \tag{15}$$

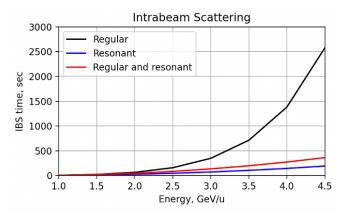


Fig. 6. (Color online) The dependence of the beam lifetime due to intra-beam scattering in "regular", "resonant" and "combined" structures on the beam energy for heavy ion beam.

229 Unlike stochastic cooling, the IBS rate increases as decreasing energy $1/\gamma^3$. In addition, the expression in parentheses is proportional to the slip-factor η . Therefore, it should be ex-232 pected that in optics with a value η close to zero, the heating 233 rate should decrease. Fig. 6 shows the dependences of the 234 heating time constant in the three above-mentioned structures 235 calculated using MADX programs [10] for the parameters of the heavy ion beam $^{197}_{79}$ Au of the NICA collider with maximum luminosity 10^{27} sm $^{-2}$ s $^{-1}$. In the context of light nuclei, such as protons and deuterons, the IBS time experiences a significant increase as the charge decreases. Consequently, 240 the issue of intra-beam scattering becomes critical for heavy-241 ion beam. From the comparison of the IBS lifetime with the 242 cooling time it can be concluded that in a regular structure, stochastic cooling is able to balance intra-beam scattering in the energy range $W \geq 4.5$ GeV. In order to apply stochas-245 tic cooling over the entire energy range, it is obvious that we 246 must sacrifice the luminosity of the beam at low energies by 247 increasing the emittance. In resonant structures, the IBS time 248 is notably reduced. This is explained by the fact that the structure has a greater ratio $\left\langle \frac{D_x^2 + \hat{D}_x^2}{\beta_x^2} \right\rangle$ between the dispersion and 250 the beam β -function than in the case of a regular. Thus, for 251 the case of heavy ions, the configuration should be regular and 252 minimally modulated. Electron cooling is used in the regular 253 structure to cool the beam lower 4.5 GeV [11, 12].

TABLE 1. Main structure parameters.

	_		
Structure	Regular	Resonant	Combined
Energy, GeV per nuclon	4.5	12.6	12.6
Transition energy $\gamma_{\rm tr}$	7	15	i50
Modulation depth	_	25%	45%
Stochastic cooling at 4.5 GeV, s	2500	1500	800
IBS time at 4.5 GeV, s	2500	400	250

IV. SUMMARY

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The dual magneto-optical structure is proposed for acceler-255 256 ating both heavy ion and light particle beams, exemplified by the NICA facility. For light particles, due to charge-to-mass ratio, experiment energy can rise more than transition energy of the lattice, which is optimal for heavy ions. Using dispersion modulation, transition energy increases or even reaches a 270 ever, due to modulation of β -function and D dispersion, the 272 a separate family of quadrupoles

263 time of intra-beam scattering decreases, which is crucial for 264 multiply charged heavy particles. For this reason, a "regu-265 lar" magneto-optic structure with minimally modulated dispersion and β -function is optimal in the heavy-ion mode. Despite the fact that stochastic cooling in "regular" structures is significantly weaker than in "resonant" and "combined" ones, 269 it can compensate IBS effect.

No special changes are required to convert the "regular" complex value in a "resonant" magneto-optic structure. How- 271 structure into a "resonant" one. It is enough only to introduce

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