

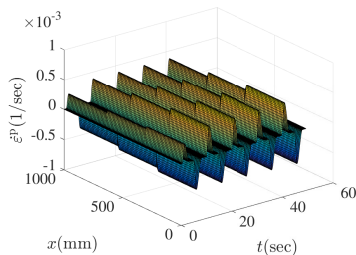
Model order reduction for fatigue analysis

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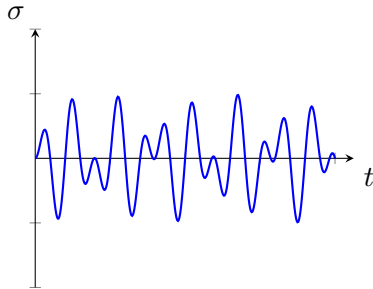
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DFG Deutsche
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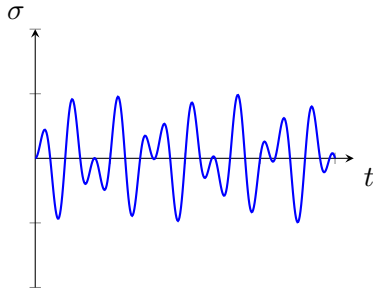
Fatigue damage

■ Cyclic loading



Fatigue damage

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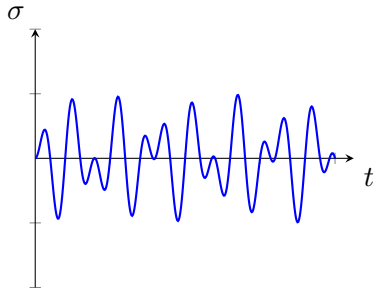
■ Damage



Image by alegri / 4freephotos.com

Fatigue damage

■ Cyclic loading



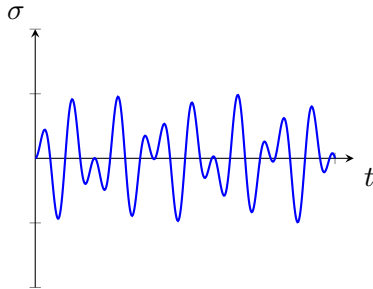
■ Damage



Image by alegri / 4freepotos.com

Fatigue damage

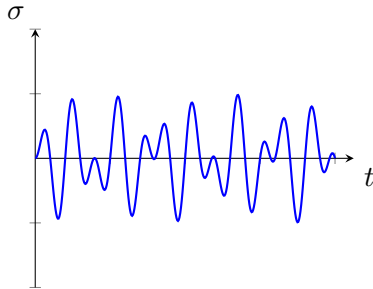
■ Cyclic loading



- Virtual experiments
- Continuum damage model
- Millions of cycles
- Computationally expensive

Fatigue damage

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Model order reduction (MOR) techniques

LATIN overview

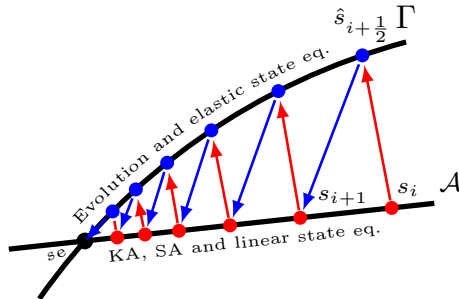
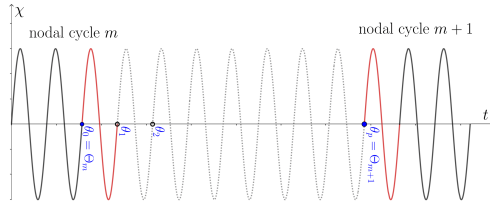


Illustration of the LATIN iterations

LATIN with two-time scale for ductile damage

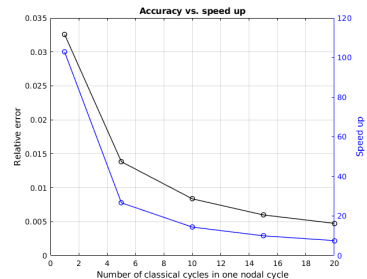
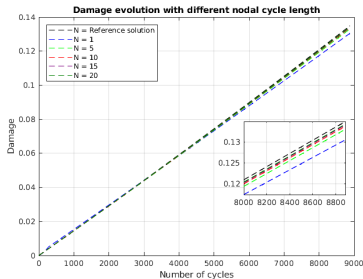
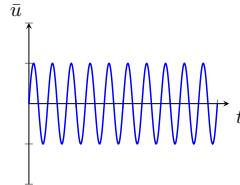
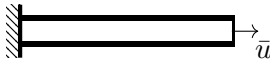
- The first and second nodal cycles are computed



- The initial condition QoI are interpolated between the nodal cycles

$$\chi(t) = \frac{\Theta_{m+1} - \theta_k}{\Theta_{m+1} - \Theta_m} \chi(\tau_m) + \frac{\theta_k - \Theta_m}{\Theta_{m+1} - \Theta_m} \chi(\tau_{m+1})$$

Ductile damage example



LATIN for brittle damage

■ Assumptions

- Free energy function $\psi_e = 1/2 (1 - D) E (\varepsilon^e)^2$
- Damage dissipation potential

$$\varphi_d = \frac{k_d}{n_d + 1} \langle f^d \rangle_+^{n_d + 1}, \quad f^d = Y - Y_0$$

Y_0 is the initial damage limit and k_d and n_d are the damage viscous parameters.

LATIN scheme for brittle damage

- The strain and displacement are initialised by the given B.C. only
- Global stage
Purely elastic and the displacement is written in PGD form
 - The static admissibility

$$\int \sigma \varepsilon^* \, d\Omega \, dt = \int b u^* \, d\Omega \, dt + \int_{\partial\Omega_N} \bar{t} u^* \, ds \, dt.$$

- In terms of corrections it becomes

$$\int \Delta\sigma \varepsilon^* \, d\Omega \, dt = 0.$$

LATIN scheme for brittle damage

■ Global search direction

$$\begin{aligned}
 (\varepsilon_{i+1}^e - \hat{\varepsilon}_{i+1/2}^e) - E^{-1}(\sigma_{i+1} - \hat{\sigma}_{i+1/2}) &= 0, \\
 \Delta \varepsilon_{i+1}^e - E^{-1} \Delta \sigma_{i+1} - \hat{f}^e &= 0, \\
 \hat{f}^e &= -E^{-1}(\hat{\sigma}_{i+1/2} - \sigma_i) + (\hat{\varepsilon}_{i+1/2}^e - \varepsilon_i^e).
 \end{aligned}$$

■ Separate representation of the displacement

$$\Delta u = \lambda v, \quad \Delta \varepsilon = \lambda \bar{\varepsilon} = \lambda \nabla v,$$

leads to the following variations

$$\Delta u^* = \lambda^* v + \lambda v^*, \quad \Delta \varepsilon^* = \lambda^* \nabla v + \lambda \nabla v^*.$$

LATIN scheme for brittle damage

- Static admissibility as a space and a time problems

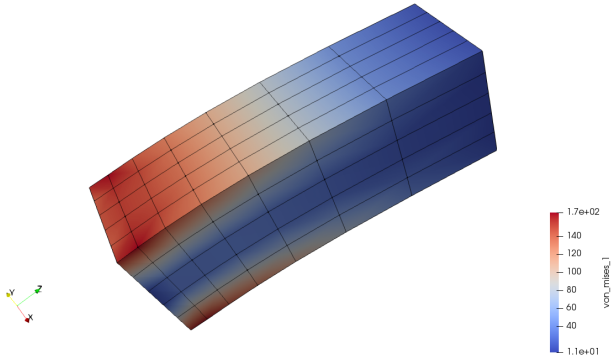
$$\begin{aligned}
 \int \nabla v^* \left(\int \lambda \mathbf{C} \lambda dt \right) \nabla v d\Omega &= \int \left(\int \hat{f}^e \mathbf{C} \lambda dt \right) \nabla v^* d\Omega, \\
 \int \lambda^* \left(\int \nabla v \mathbf{C} \nabla v d\Omega \right) \lambda dt &= \int \lambda^* \left(\int \hat{f}^e \mathbf{C} \nabla v d\Omega \right) dt.
 \end{aligned}$$

- The strain space function can be computed through the kinematic admissibility relation as $\bar{\varepsilon} = \nabla v$.
- Local stage
 - The stress is taken from the last global stage
 - The damage evolution is computed

$$\dot{D} = \frac{\partial \varphi_d}{\partial Y} = k_d \langle f^d \rangle_+^{n_d}$$

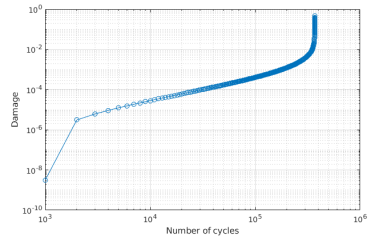
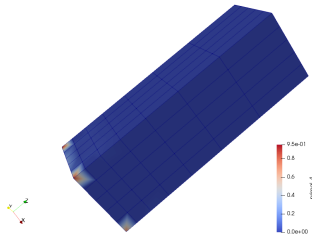
Brittle damage example

- Constant amplitude loading and adaptive time jumps



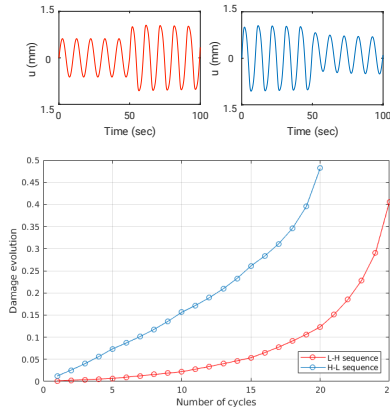
Brittle damage example

- Constant amplitude loading and adaptive time jumps



Variable loading

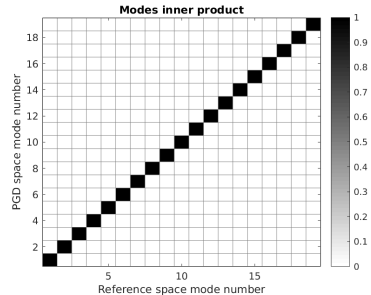
■ L-H and H-L sequence



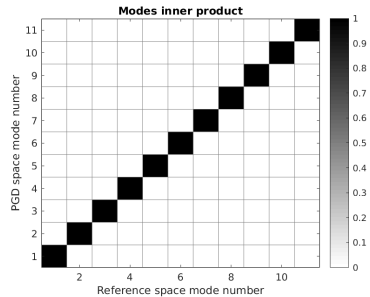
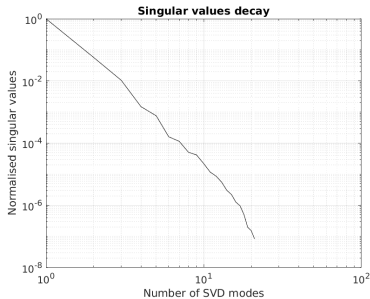
■ Time modes are scaled to have a better initialisation

Modes optimisation

■ Modified Gram Schmidt and SVD



Modes truncation



Conclusion and current research

- MOR approach for HCF
- It works for variable loading

Current objectives

- Virtual S-N curves
- Modes selection and optimisation for variable loading
- Reference point method or hyper-reduction
- Parametric loading
- Time homogenisation



Milestone plan

- First year
Constitutive modelling, LATIN-PGD and Two-time scale
- Second year
Brittle damage and different amplitudes and RPM
- Third year
Parametric PGD and Computations and thesis writing

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Thank you for your attention!

■ Time comparison

D. Néron et al, Time-space PGD for the rapid solution of 3D nonlinear parametrized problems in the many-query context, *IJNME*, 2015.

■ LATIN convergence conditions

Ladeveze 1999 [p84]

■ PGD existence and convergence

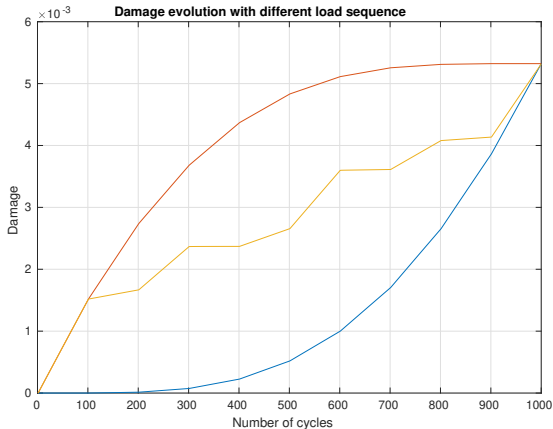
Ladeveze 1999 [p119]

■ PGD for solving PDE

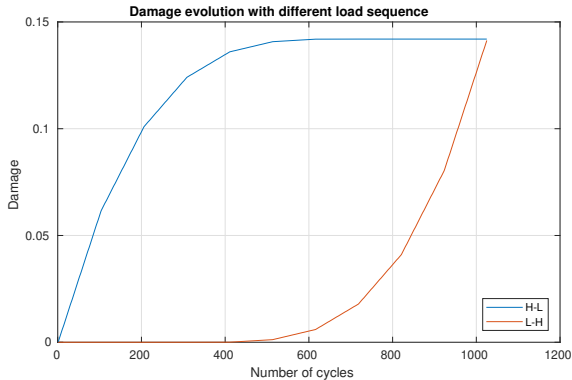
A. Nouy. A priori model reduction through proper generalized decomposition for solving time-dependent partial differential equations. Computer Methods In Applied Mechanics and Engineering, 199(23- 24):1603–1626, 2010.

Antonio Falco

Different loading sequence



Different loading sequence with elastic loading



The used mesh

