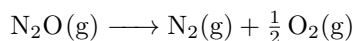


3 Rate Laws II / Mechanisms

Chapter 28

From McQuarrie and Simon (1997).

4/25: **28-31.** The following data were obtained for the reaction



$\frac{[\text{N}_2\text{O}]_0/\text{mol dm}^{-3}}{t_{1/2}/\text{s}}$	1.674×10^{-3}	4.458×10^{-3}	9.300×10^{-3}	1.155×10^{-2}
	1200	470	230	190

Assume the rate law for this reaction is

$$-\frac{d[\text{N}_2\text{O}]}{dt} = k[\text{N}_2\text{O}]^n$$

and use the equation for the half-life of an n^{th} -order reaction to determine the reaction order of N_2O by plotting $\ln t_{1/2}$ against $\ln[\text{A}]_0$. Calculate the rate constant for this decomposition reaction.

Answer. We have that

$$\begin{aligned} \ln(kt_{1/2}) &= \ln\left(\frac{1}{n-1} \frac{2^{n-1} - 1}{[\text{A}]_0^{n-1}}\right) \\ \ln k + \ln t_{1/2} &= -\ln(n-1) + \ln(2^{n-1} - 1) - (n-1) \ln[\text{A}]_0 \\ \ln t_{1/2} &= -(n-1) \ln[\text{A}]_0 + C \end{aligned}$$

where $C = \ln(2^{n-1} - 1) - \ln(n-1) - \ln k$ is a constant. Thus, we can determine n by performing a linear regression on a plot of $\ln t_{1/2}$ vs. $\ln[\text{N}_2\text{O}]_0$. The resultant line of best fit has slope $m = -0.96$, which means that

$$\begin{aligned} -(n-1) &\approx -0.96 \\ n-1 &\approx 0.96 \\ n &\approx 1.96 \\ \boxed{n=2} \end{aligned}$$

It follows by plugging our four data points back into the equation

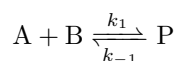
$$k = \frac{1}{(2-1)t_{1/2}} \frac{2^{2-1} - 1}{[\text{N}_2\text{O}]_0^{2-1}} = \frac{1}{t_{1/2} \cdot [\text{N}_2\text{O}]_0}$$

and averaging the results that

$$\boxed{k = 0.47 \frac{\text{L}}{\text{mol s}}}$$

□

28-33. Consider the general chemical reaction



If we assume that both the forward and reverse reactions are first order in their respective reactants, the rate law is given by

$$\frac{d[\text{P}]}{dt} = k_1[\text{A}][\text{B}] - k_{-1}[\text{P}]$$

Now consider the response of this chemical reaction to a temperature jump. Let $[A] = [A]_{2,\text{eq}} + \Delta[A]$, $[B] = [B]_{2,\text{eq}} + \Delta[B]$, and $[P] = [P]_{2,\text{eq}} + \Delta[P]$, where the subscript “2,eq” refers to the new equilibrium state. Now use the fact that $\Delta[A] = \Delta[B] = -\Delta[P]$ to show that the above rate law becomes

$$\frac{d\Delta[P]}{dt} = k_1[A]_{2,\text{eq}}[B]_{2,\text{eq}} - k_{-1}[P]_{2,\text{eq}} - \{k_1([A]_{2,\text{eq}} + [B]_{2,\text{eq}}) + k_{-1}\}\Delta[P] + O(\Delta[P]^2)$$

Show that the first terms on the right side of this equation cancel and that the following two equations result.

$$\Delta[P] = \Delta[P]_0 e^{-t/\tau} \qquad \tau = \frac{1}{k_1([A]_{2,\text{eq}} + [B]_{2,\text{eq}}) + k_{-1}}$$

Answer. We have that

$$\begin{aligned} \frac{d}{dt}([P]_{2,\text{eq}} + \Delta[P]) &= k_1([A]_{2,\text{eq}} + \Delta[A])([B]_{2,\text{eq}} + \Delta[B]) - k_{-1}([P]_{2,\text{eq}} + \Delta[P]) \\ \frac{d\Delta[P]}{dt} &= k_1([A]_{2,\text{eq}}[B]_{2,\text{eq}} + [A]_{2,\text{eq}}\Delta[B] + \Delta[A][B]_{2,\text{eq}} + \Delta[A]\Delta[B]) - k_{-1}([P]_{2,\text{eq}} + \Delta[P]) \\ &= k_1([A]_{2,\text{eq}}[B]_{2,\text{eq}} - [A]_{2,\text{eq}}\Delta[P] - \Delta[P][B]_{2,\text{eq}} + \Delta[P]\Delta[P]) - k_{-1}([P]_{2,\text{eq}} + \Delta[P]) \\ &= k_1[A]_{2,\text{eq}}[B]_{2,\text{eq}} - k_{-1}[P]_{2,\text{eq}} - \{k_1([A]_{2,\text{eq}} + [B]_{2,\text{eq}}) + k_{-1}\}\Delta[P] + O(\Delta[P]^2) \end{aligned}$$

as desired, where $d[P]_{2,\text{eq}}/dt = 0$ because $[P]_{2,\text{eq}}$ is a constant, and we have bundled $k_1\Delta[P]^2$ into the $O(\Delta[P]^2)$ term.

Moreover, the first two terms on the right side of the bottom equation above equal zero since at equilibrium under the new conditions,

$$\frac{d[P]}{dt} = 0 = k_1[A]_{2,\text{eq}}[B]_{2,\text{eq}} - k_{-1}[P]_{2,\text{eq}}$$

Thus, ignoring the $O(\Delta[P]^2)$ term, we have that

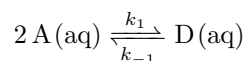
$$\begin{aligned} \frac{d\Delta[P]}{dt} &= -\{k_1([A]_{2,\text{eq}} + [B]_{2,\text{eq}}) + k_{-1}\}\Delta[P] \\ \frac{d\Delta[P]}{\Delta[P]} &= -\frac{dt}{1/\{k_1([A]_{2,\text{eq}} + [B]_{2,\text{eq}}) + k_{-1}\}} \\ \int_{\Delta[P]_0}^{\Delta[P]} \frac{d\Delta[P]}{\Delta[P]} &= \int_0^t -\frac{dt}{\tau} \\ \ln \frac{\Delta[P]}{\Delta[P]_0} &= -\frac{t}{\tau} \\ \Delta[P] &= \Delta[P]_0 e^{-t/\tau} \end{aligned}$$

where

$$\tau = \frac{1}{k_1([A]_{2,\text{eq}} + [B]_{2,\text{eq}}) + k_{-1}}$$

as desired. □

28-36. Consider the chemical reaction described by



If we assume the forward reaction is second order and the reverse reaction is first order, the rate law is given by

$$\frac{d[D]}{dt} = k_1[A]^2 - k_{-1}[D]$$

Now consider the response of this chemical reaction to a temperature jump. Let $[A] = [A]_{2,\text{eq}} + \Delta[A]$ and $[D] = [D]_{2,\text{eq}} + \Delta[D]$, where the subscript “2,eq” refers to the new equilibrium state. Now use the fact that $\Delta[A] = -2\Delta[D]$ to show that the rate law becomes

$$\frac{d\Delta[D]}{dt} = -(4k_1[A]_{2,\text{eq}} + k_{-1})\Delta[D] + O(\Delta[D]^2)$$

Show that if we ignore the $O(\Delta[D]^2)$ term, then

$$\Delta[D] = \Delta[D]_0 e^{-t/\tau}$$

where $\tau = 1/(4k_1[A]_{2,\text{eq}} + k_{-1})$.

Answer. Proceeding as in Problem 28-33, we have that

$$\begin{aligned} \frac{d}{dt}([D]_{2,\text{eq}} + \Delta[D]) &= k_1([A]_{2,\text{eq}} + \Delta[A])^2 - k_{-1}([D]_{2,\text{eq}} + \Delta[D]) \\ \frac{d\Delta[D]}{dt} &= k_1([A]_{2,\text{eq}}^2 + 2[A]_{2,\text{eq}}\Delta[A] + \Delta[A]^2) - k_{-1}([D]_{2,\text{eq}} + \Delta[D]) \\ &= k_1(-4[A]_{2,\text{eq}}\Delta[D] + 4\Delta[D]^2) - k_{-1}\Delta[D] \\ &= -(4k_1[A]_{2,\text{eq}} + k_{-1})\Delta[D] + O(\Delta[D]^2) \end{aligned}$$

so that integrating yields

$$\Delta[D] = \Delta[D]_0 e^{-t/\tau}$$

where $\tau = 1/(4k_1[A]_{2,\text{eq}} + k_{-1})$. □

28-46. Show that if A reacts to form either B or C according to



then E_a , the observed activation energy for the disappearance of A, is given by

$$E_a = \frac{k_1 E_1 + k_2 E_2}{k_1 + k_2}$$

where E_1 is the activation energy for the first reaction and E_2 is the activation energy for the second reaction.

Answer. We have that

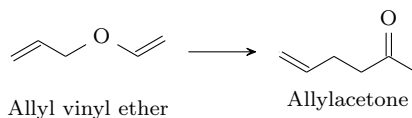
$$k_1 = A_1 e^{-E_1/RT} \qquad k_2 = A_2 e^{-E_2/RT}$$

Thus, since $k = k_1 + k_2$, we can plug into the original form of the Arrhenius equation to determine that

$$\begin{aligned} \frac{E_a}{RT^2} &= \frac{d \ln(k_1 + k_2)}{dT} \\ &= \frac{1}{k_1 + k_2} \frac{d}{dT} (A_1 e^{-E_1/RT} + A_2 e^{-E_2/RT}) \\ &= \frac{1}{k_1 + k_2} \left(A_1 e^{-E_1/RT} \cdot \frac{E_1}{RT^2} + A_2 e^{-E_2/RT} \cdot \frac{E_2}{RT^2} \right) \\ E_a &= \frac{1}{k_1 + k_2} (k_1 \cdot E_1 + k_2 \cdot E_2) \\ &= \frac{k_1 E_1 + k_2 E_2}{k_1 + k_2} \end{aligned}$$

as desired. □

28-48. The gas-phase rearrangement reaction



has a rate constant of $6.015 \times 10^{-5} \text{ s}^{-1}$ at 420 K and a rate constant of $2.971 \times 10^{-3} \text{ s}^{-1}$ at 470 K. Calculate the values of the Arrhenius parameters A and E_a . Calculate the values of $\Delta^\ddagger H^\circ$ and $\Delta^\ddagger S^\circ$ at 420 K. Assume ideal-gas behavior.

Answer. Let

$$k_1 = 6.015 \times 10^{-5} \text{ s}^{-1}$$

$$k_2 = 2.971 \times 10^{-3} \text{ s}^{-1}$$

$$T_1 = 420 \text{ K}$$

$$T_2 = 470 \text{ K}$$

Then

$$k_1 = Ae^{-E_a/RT_1}$$

$$k_2 = Ae^{-E_a/RT_2}$$

so that

$$\begin{aligned} \frac{k_1}{k_2} &= \frac{Ae^{-E_a/RT_1}}{Ae^{-E_a/RT_2}} \\ &= e^{E_a/RT_2 - E_a/RT_1} \\ \ln \frac{k_1}{k_2} &= \frac{(T_1 - T_2)E_a}{RT_1T_2} \\ E_a &= \frac{RT_1T_2}{T_1 - T_2} \ln \frac{k_1}{k_2} \\ \boxed{E_a = 128.0 \frac{\text{kJ}}{\text{mol}}} \end{aligned}$$

and

$$\begin{aligned} A &= \frac{k_1}{e^{-E_a/RT_1}} \\ \boxed{A = 5.0 \times 10^{11} \text{ s}^{-1}} \end{aligned}$$

Additionally, since this is a unimolecular reaction, we have that

$$\begin{aligned} E_a &= \Delta^\ddagger H^\circ + RT \\ \Delta^\ddagger H^\circ &= E_a - RT \\ \boxed{\Delta^\ddagger H^\circ = 124.5 \frac{\text{kJ}}{\text{mol}}} \end{aligned}$$

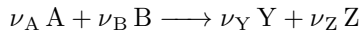
and

$$\begin{aligned} A &= \frac{ek_B T}{h} e^{\Delta^\ddagger S^\circ / R} \\ \Delta^\ddagger S^\circ &= R \ln \frac{Ah}{ek_B T} \\ \boxed{\Delta^\ddagger S^\circ = -32.1 \frac{\text{J}}{\text{mol K}}} \end{aligned}$$

at 420 K.

□

- 28-49.** The kinetics of a chemical reaction can be followed by a variety of experimental techniques, including optical spectrometry, NMR spectroscopy, conductivity, resistivity, pressure changes, and volume changes. When using these techniques, we do not measure the concentration itself but we know that the observed signal is proportional to the concentration; the exact proportionality constant depends on the experimental technique and the species present in the chemical system. Consider the general reaction given by



where we assume that A is the limiting reagent so that $[A] \rightarrow 0$ as $t \rightarrow \infty$. Let p_i be the proportionality constant for the contribution of species i to S , the measured signal from the instrument. Explain why at any time t during the reaction, S is given by

$$S(t) = p_A[A] + p_B[B] + p_Y[Y] + p_Z[Z] \quad (1)$$

Show that the initial and final readings from the instrument are given by

$$S(0) = p_A[A]_0 + p_B[B]_0 + p_Y[Y]_0 + p_Z[Z]_0 \quad (2)$$

and

$$S(\infty) = p_B \left([B]_0 - \frac{\nu_B}{\nu_A} [A]_0 \right) + p_Y \left([Y]_0 + \frac{\nu_Y}{\nu_A} [A]_0 \right) + p_Z \left([Z]_0 + \frac{\nu_Z}{\nu_A} [A]_0 \right) \quad (3)$$

Combine Equations 1-3 to show that

$$[A] = [A]_0 \frac{S(t) - S(\infty)}{S(0) - S(\infty)}$$

(Hint: Be sure to express $[B]$, $[Y]$, and $[Z]$ in terms of their initial values, $[A]$ and $[A]_0$.)

Answer. If only species X exists *in situ* at time t , then $S(t) \propto [X]$ with proportionality constant p_X , where $[X]$ denotes the concentration of species X at time t . Therefore, since the total signal is the sum of all of the partial signals,

$$S(t) = \sum_X p_X [X] = p_A[A] + p_B[B] + p_Y[Y] + p_Z[Z]$$

It follows by direct substitution that

$$S(0) = p_A[A]_0 + p_B[B]_0 + p_Y[Y]_0 + p_Z[Z]_0 \quad (4)$$

where $[X]_0$ denotes the concentration of species X at time $t = 0$. Additionally, at time $t = \infty$, all of A (the limiting reagent) will have been consumed, and a proportional amount of all other species will have been created or consumed. For instance, if V is the volume of the reaction domain, then dimensional analysis tells us that $[A]_0 \cdot V$ moles of A will react with

$$\frac{[A]_0 \cdot V \text{ moles A}}{1} \times \frac{\nu_B \text{ moles B}}{\nu_A \text{ moles A}} = \frac{\nu_B}{\nu_A} [A]_0 \cdot V \text{ moles B}$$

Another way of looking at this is that the concentration of B will decrease by $\frac{\nu_B}{\nu_A} [A]_0$ over the course of the reaction, i.e., that the final concentration $[B]_\infty$ of B will be given by

$$[B]_\infty = [B]_0 - \frac{\nu_B}{\nu_A} [A]_0$$

Similarly, the concentration of the products will increase by a proportional amount. Thus, we have that

$$\begin{aligned} S(\infty) &= p_A[A]_\infty + p_B[B]_\infty + p_Y[Y]_\infty + p_Z[Z]_\infty \\ &= p_A \cdot 0 + p_B \left([B]_0 - \frac{\nu_B}{\nu_A} [A]_0 \right) + p_Y \left([Y]_0 + \frac{\nu_Y}{\nu_A} [A]_0 \right) + p_Z \left([Z]_0 + \frac{\nu_Z}{\nu_A} [A]_0 \right) \\ &= p_B \left([B]_0 - \frac{\nu_B}{\nu_A} [A]_0 \right) + p_Y \left([Y]_0 + \frac{\nu_Y}{\nu_A} [A]_0 \right) + p_Z \left([Z]_0 + \frac{\nu_Z}{\nu_A} [A]_0 \right) \end{aligned}$$

as desired.

To derive an expression for $[A]$ as a function of $S(t)$, we can first note that there are a number of similar terms between Equations 1, 2, and 3 that would cancel when adding or subtracting. As such, we can determine that

$$\begin{aligned} S(\infty) - S(0) &= p_B \left([B]_0 - \frac{\nu_B}{\nu_A} [A]_0 \right) + p_Y \left([Y]_0 + \frac{\nu_Y}{\nu_A} [A]_0 \right) + p_Z \left([Z]_0 + \frac{\nu_Z}{\nu_A} [A]_0 \right) \\ &\quad - p_A [A]_0 - p_B [B]_0 - p_Y [Y]_0 - p_Z [Z]_0 \\ &= -p_B \frac{\nu_B}{\nu_A} [A]_0 + p_Y \frac{\nu_Y}{\nu_A} [A]_0 + p_Z \frac{\nu_Z}{\nu_A} [A]_0 - p_A [A]_0 \\ S(0) - S(\infty) &= (p_A \nu_A + p_B \nu_B - p_Y \nu_Y - p_Z \nu_Z) \frac{[A]_0}{\nu_A} \end{aligned}$$

and

$$\begin{aligned} S(t) - S(0) &= p_A ([A] - [A]_0) + p_B ([B] - [B]_0) + p_Y ([Y] - [Y]_0) + p_Z ([Z] - [Z]_0) \\ &= p_A \cdot \frac{\nu_A}{\nu_A} ([A] - [A]_0) + p_B \cdot \frac{\nu_B}{\nu_A} ([A] - [A]_0) - p_Y \cdot \frac{\nu_Y}{\nu_A} ([A] - [A]_0) - p_Z \cdot \frac{\nu_Z}{\nu_A} ([A] - [A]_0) \\ &= (p_A \nu_A + p_B \nu_B - p_Y \nu_Y - p_Z \nu_Z) \frac{[A] - [A]_0}{\nu_A} \end{aligned}$$

It follows that

$$\begin{aligned} S(t) - S(\infty) &= [S(t) - S(0)] + [S(0) - S(\infty)] \\ &= (p_A \nu_A + p_B \nu_B - p_Y \nu_Y - p_Z \nu_Z) \frac{[A]}{\nu_A} \end{aligned}$$

so that

$$\begin{aligned} \frac{S(t) - S(\infty)}{S(0) - S(\infty)} &= \frac{(p_A \nu_A + p_B \nu_B - p_Y \nu_Y - p_Z \nu_Z) [A] / \nu_A}{(p_A \nu_A + p_B \nu_B - p_Y \nu_Y - p_Z \nu_Z) [A]_0 / \nu_A} \\ &= \frac{[A]}{[A]_0} \\ [A] &= [A]_0 \frac{S(t) - S(\infty)}{S(0) - S(\infty)} \end{aligned}$$

as desired. □

Chapter 29

From McQuarrie and Simon (1997).

29-5. Solve the differential equation

$$\frac{d[A]}{dt} = -k_1[A]$$

to obtain $[A] = [A]_0 e^{-k_1 t}$, and substitute this result into the differential equation

$$\frac{d[I]}{dt} = k_1[A] - k_2[I]$$

to obtain

$$\frac{d[I]}{dt} + k_2[I] = k_1[A]_0 e^{-k_1 t}$$

This equation is of the form (see the Zwillinger (2003), for example)

$$\frac{dy(x)}{dx} + p(x)y(x) = q(x)$$

a linear, first-order differential equation whose general solution is

$$y(x)e^{h(x)} = \int q(x)e^{h(x)} dx + c$$

where $h(x) = \int p(x) dx$ and c is a constant. Show that this solution leads to

$$[I] = \frac{k_1}{k_2 - k_1} [A]_0 (e^{-k_1 t} - e^{-k_2 t})$$

Answer. As in Problem 28-33, we can integrate

$$\frac{d[A]}{dt} = -k_1[A]$$

to obtain $[A] = [A]_0 e^{-k_1 t}$. Substituting this into the rate law for the intermediate I yields

$$\begin{aligned} \frac{d[I]}{dt} &= k_1[A]_0 e^{-k_1 t} - k_2[I] \\ \frac{d[I]}{dt} + k_2[I] &= k_1[A]_0 e^{-k_1 t} \end{aligned}$$

Noting that this equation is of the described form with $y(x) = [I](t)$, $p(x) = k_2$, and $q(x) = k_1[A]_0 e^{-k_1 t}$, we can determine that

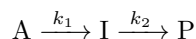
$$\begin{aligned} h(x) &= \int_0^x k_2 dx \\ &= k_2 x \end{aligned}$$

and thus that the general solution is

$$\begin{aligned} [I] \cdot e^{k_2 t} &= \int_0^t k_1[A]_0 e^{-k_1 t} \cdot e^{k_2 t} dt \\ [I] e^{k_2 t} &= k_1[A]_0 \int_0^t e^{(k_2 - k_1)t} dt \\ [I] e^{k_2 t} &= \frac{k_1[A]_0}{k_2 - k_1} (e^{(k_2 - k_1)t} - 1) \\ [I] &= \frac{k_1}{k_2 - k_1} [A]_0 (e^{-k_1 t} - e^{-k_2 t}) \end{aligned}$$

as desired. □

29-7. Consider the reaction mechanism

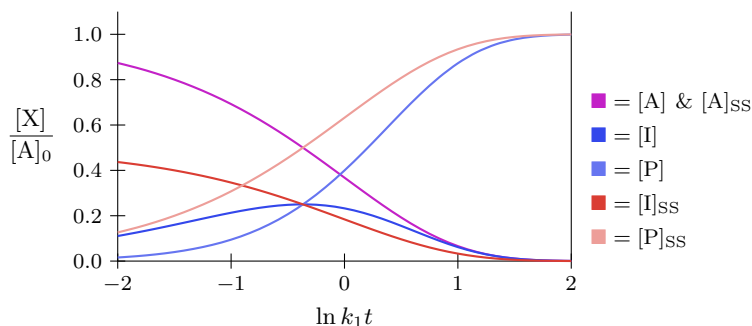


where $[A] = [A]_0$ and $[I]_0 = [P]_0 = 0$ at time $t = 0$. Use the exact solution to this kinetic scheme (below) to plot the time dependence of $[A]/[A]_0$, $[I]/[A]_0$, and $[P]/[A]_0$ versus $\log k_1 t$ for the case $k_2 = 2k_1$.

$$\begin{aligned} [A] &= [A]_0 e^{-k_1 t} \\ [I] &= \frac{k_1}{k_2 - k_1} [A]_0 (e^{-k_1 t} - e^{-k_2 t}) \\ [P] &= [A]_0 - [A] - [I] = [A]_0 \left\{ 1 + \frac{1}{k_1 - k_2} (k_2 e^{-k_1 t} - k_1 e^{-k_2 t}) \right\} \end{aligned}$$

On the same graph, plot the time dependence of $[A]/[A]_0$, $[I]/[A]_0$, and $[P]/[A]_0$ using the expressions for $[A]$, $[I]$, and $[P]$ obtained using the steady-state approximation for $[I]$. Based on your results, can you use the steady-state approximation to model the kinetics of this reaction mechanism when $k_2 = 2k_1$?

Answer.



Based on the above graph, the steady-state approximation is not a good model in this case. As we can see, there are substantial differences in the values for $[P]$, and the two curves describing $[I]$ do not even have similar shapes. \square

Application

- 1) Name one HW problem you would like to develop into a thought experiment or relate to a literature article.
- 2) Describe how the idea or conclusion from the HW problem applies to the research idea in 1-2 paragraphs (word limit: 300). Once again, this can either be a thought experiment or an experiment found in the literature.
- 3) You do not need to derive any equations in this short discussion. Use your intuition and focus on the big picture.
- 4) Please cite the literature if you link the HW problem to anyone (author names, titles, journal name, volume numbers, and page numbers).

Answer. I would like to deepen my understanding of Problem 28-46, which considers the observed activation energy as a function of the component activation energies for parallel reactions. One of the first things I noticed when looking at this problem was that the expression I'm deriving is a weighted average of the two component activation energies by the speeds at which said reactions occur. This should make intuitive sense. Consider how often E_1 being supplied to the system results in the formation of a molecule of B. This relative rate should be summed up somewhat by k_1 . A similar statement holds for E_2 , C, and k_2 . Moreover, if we take $k_2 = 2k_1$ and $E_2 > E_1$ for the sake of having something tangible to work with, we should be able to imagine that supplying E_2 to the system means we are twice as likely to generate a molecule of C as we would be likely to generate a molecule of B upon supplying E_1 to the system. Thus, assuming all quantities of energy are supplied equally, we would observe that supplying slightly more than $(E_1 + E_2)/2$ results in the reaction happening at the optimum production-to-energy input ratio, as predicted by the expression given in Problem 28-46. \square