A Technical note about the Industrial security

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Let,

Foreign unknown source = F

Political influences = P

Industrial officers and workers = IOW

Local business cartels = LBC

Influences from the Government officials = IGO

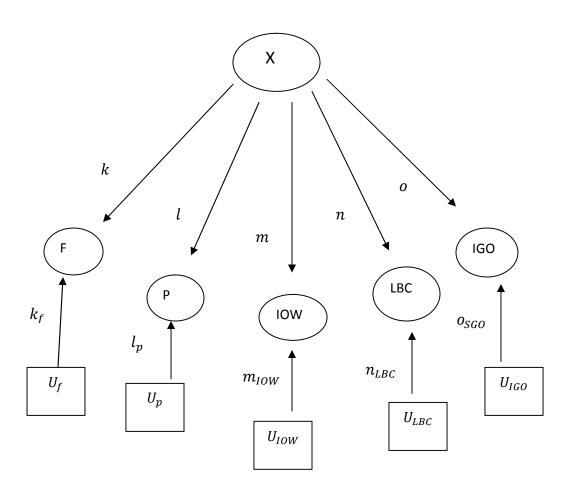
An unknown common latent factor = X

$$F = k X + k_f u_f$$
 $P = l X + k_f u_p$
 $IOW = m X + m_f u_{IOW}$
 $LBC = n X + n_f u_{LBC}$
 $IGO = o X + o_f u_{SGO}$

One Factor and Five Indicators

	F	P	IOW	LBC	IGO
F	a ₁₁	a ₁₂	a ₁₃	a ₁₄	<i>a</i> ₁₅
P	a ₂₁	a ₂₂	a_{23}	a ₂₄	a_{25}
IOW	a ₃₁	a ₃₂	a ₃₃	a ₃₄	a_{35}
LBC	a_{41}	a_{42}	a_{43}	a_{44}	a_{45}
IGO	a_{51}	a_{52}	a_{53}	a_{54}	a_{55}

Cross Correlati on Matrix



Different framework is possible

$$F = k.X + a.P + b.LBC + c.IOW + d.IGO + \gamma_f U_f'$$

$$LBC = k_{LBC}.X + a_{LBC}.P + b_{LBC}.LBC + c_{LBC}.IOW + d_{LBC}.IGO + \gamma_f U_f'$$

$$IOW = c_{IOW}.LBC$$

The whole framework will have an impact on the industrial production

Let,

Industrial production = Y

Political dummy = D_{pt}

Activity Level = $a_1 o D_p = 0$

Activity Level = $a_2 \rightarrow D_p \neq 0$

Working hour of the group of worker and officer $= WH_k$, $k = 1 \dots n$

$$Y = \beta_1 D_{pt} + \beta_2 \left(\frac{NO_2}{CO_2} \right) + \beta_3 \left(\frac{CaCl_2}{O_2 H} \right) + \beta_{41} (WH_1) + \dots + \beta_{4k} (WH_k) + U_Y$$

A possible linear regression model

$$\frac{NO_2}{cO_2} \rightarrow NO_2$$
 , CO_2 ratio in Air

$$\frac{CaCl_2}{H_2O} \rightarrow CaCl_2$$
, H_2O ratio in Water

For the classification of the worker and officer it is possible to use for example:

- 1. Region
- 2. Education
- 3. Expertise (need to define)
- 4. Their religious activities (need to define the activity level)
- 5. Number of conflict (fighting attitude) Category of the conflict ->
 - 1. Protest
 - 2. Crime
- 6. Married /Unmarried
- 7. Number of Children
- 8. Extra Curriculum
- 9. Hobby

..... etc.

We can also analysis the framework by using the constantelasticity -of-substitution model of the production.

Production function of the two factor case:

Two Factor CES Production Function

$$Y' = \gamma' [k'X'_{1}^{-\alpha} + (1 - k')X'_{1}^{-\alpha}]^{-\frac{r}{\alpha}}$$

 $Y' \rightarrow Output$

 $X'_1 \rightarrow Factor 1$

 $X'_2 \rightarrow Factor 2$

 $\gamma' \rightarrow Denotes \ the \ efficiency \ of \ a \ Production \ function$

 $r \rightarrow Homogenity parameter$; Representing the Degree of returns to scale

 $r > 1 \rightarrow Economics of scale$

 $r = 1 \rightarrow Constant\ returns$

 $r < 1 \rightarrow \textit{Diseconomics of scale}$

 $k' \rightarrow Intensity Parameter$

$$\alpha = \frac{1}{\sigma} - 1$$

We can include more factors:

Generalized CES Production Function

$$Y' = \gamma' [k'_1 X'_1^{-\alpha} + k'_2 X'_2^{-\alpha} + k'_3 X'_3^{-\alpha} + k'_4 X'_4^{-\alpha}]^{-\frac{r}{\alpha}}$$

Another Generalized CES Production Function

$$Y' = \gamma' \left[{k'}_1 {X'}_1^{-\alpha_1} + {k'}_2 {X'}_2^{-\alpha_1} \right]^{-\frac{r_1}{\alpha_1}} . \left[{k'}_3 {X'}_3^{-\alpha_2} + {k'}_4 {X'}_4^{-\alpha_2} \right]^{-\frac{r_2}{\alpha_2}}$$

 α_1 , $\alpha_2 \rightarrow Partial \ elasticity \ of \ substitution$

Let,

$$Y' = \gamma' \cdot e^{\lambda \cdot t} \cdot [k'X'_1^{-\alpha} + (1 - k')X'_2^{-\alpha}]^{-\frac{r}{\alpha}}$$

$$r = 1$$

$$Y' = \gamma' \cdot e^{\lambda \cdot t} \cdot \left[k' X'_1^{-\alpha} + (1 - k') X'_2^{-\alpha} \right]^{-\frac{1}{\alpha}}$$

 $\lambda \rightarrow rate\ of\ technical\ change$

By taking log on the both side,

$$ln(Y') = ln(\gamma') + \lambda \cdot t + b'_{2}ln(X'_{1}) + b'_{3}ln(X'_{2}) + b'_{4}ln\left(\frac{X'_{1}}{X'_{2}}\right)^{2}$$

$$b'_{2} = k'$$

$$b'_3 = 1 - k'$$

$$b'_4 = -\left(\frac{1}{2}\right)k'.(1-k').\alpha$$

We can estimate the co-efficient

Elasticity of substitution $\sigma = \frac{1}{1 + \alpha}$

Ref: Book and Research Papers (Own Collection)

We can use OLS

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Let,

LGP = Liquid - Chemical - Gas-Pressure

FGS = Frequency of the ground shake

TI = Time Interval

ED = Error of the Design

C = Maximum Capacity of the Chemical Plant

WA = Warning before the destruction of the plant (number for example)

t = Flow of the Time

where, t = 1T

mathematically, or we can use OLS separately , otherwise

$$C_t \sim I(0)$$

$$LGP_t \sim I(0)$$

.....

$$\triangle \ C_t = \ \beta_{10} + \ \beta_{11} \ \triangle \ C_{t-1} + \beta_{12} \ \triangle \ FGS_t + \beta_{13} \ \triangle \ LSP_{t-1} + \beta_{16} \ \triangle \ ED_t + \beta_{14} \ \triangle \ TI + \beta_{15}WA_t + v_t^{\ \triangle c}$$

$$\triangle \ LGP_t = \ \beta_{20} + \beta_{21} \ \triangle \ LGP_{t-1} + \beta_{22} \ \triangle \ FGS_t + \beta_{23} \ \triangle \ C_{t-1} + \beta_{24} \ \triangle \ TI + \beta_{25} \ \triangle \ WA_t + \beta_{26} \ \triangle \ ED_t + v_t^{\triangle LGP}$$

 $C_t \sim I(1)$

$$LGP_t \sim I(1)$$

.....

 \mathcal{C}_t and LGP_t are not co-integrated and so on

$$C_t \sim I(1)$$

$$LGP_t \sim I(1)$$

.....

 $\textit{C}_{\textit{t}}$ and $\textit{LGP}_{\textit{t}}$ are not co-integrated and so on

Check the impulse response

You can also check the stability of the system(Please check the standard text book)

$$\begin{bmatrix} \dot{y}_1 \\ \dot{y}_2 \end{bmatrix} = \begin{bmatrix} a_{11} & a_{12} \\ a_{21} & a_{22} \end{bmatrix} \begin{bmatrix} y_1 \\ y_2 \end{bmatrix} + \begin{bmatrix} b_1 \\ b_2 \end{bmatrix}$$
$$\dot{Y} = A \cdot Y + B$$

Complementary solution

$$y_c = \sum_{i=1}^n k_i C_i e^{r_i t} = k_1 C_1 e^{r_1 t} + k_2 C_2 e^{r_2 t}$$

 $k_i = a \ scalar \ or \ constant$

 $C_i = (2 \times 1)$ column vector of constants called an eigenvector

 $r_i = a$ scalar called the characteristic root

$$r_i = \frac{tr(A) \pm \sqrt{|tr(A)|^2 - 4|A|}}{2}$$

$$(A - r_i.I)C_i = 0$$

$$(A - r_i.I) = \begin{bmatrix} a_{11} & a_{12} \\ a_{21} & a_{22} \end{bmatrix} - r_i \begin{bmatrix} 1 & 0 \\ 0 & 1 \end{bmatrix}$$

$$= \begin{bmatrix} a_{11} - r_i & a_{12} \\ a_{21} & a_{22} - r_i \end{bmatrix}$$

 k_i is a scalar

$$(A-r_i.I)\mathcal{C}_i=0$$
 is a Eigen-value problem

If we solve this Eigen value problem we will find the Eigen vector.

Intertemporal and the steady-state solution is,

$$y_p = \overline{Y} = -A^{-1} B$$

The complete general solution,

$$y(t) = y_c + y_p$$

If all $r_i < 0$ -> The model is dynamically stable

If all $r_i > 0$ -> The model is dynamically unstable

If r_i have different sings

-> The solution is at a saddle - point equilibrium and the model is unstable

Ref: Books, Research Papers (My own collection)

Contact:

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