



## NOTES CORNER

### Diffraktion

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According to geometrical optics, light travels along a rectilinear path in a homogenous and isotropic medium. However, a minute investigation of this fact reveals that, light suffers some deviation from its straight path in passing close to the edges of opaque obstacles and narrow slits. Some of the light bends into the region of geometrical shadow and its intensity falls off rapidly. This deviation from rectilinear propagation is extremely small when the wavelength of light is small in comparison to the dimensions of an obstacle or aperture and is more pronounced when dimension of slit, aperture or boundary of obstacle are comparable with the wavelength of light. This indicates that, light after passing through a narrow slit or across a sharp edge (like razor blade), it spreads and enters into regions that could be in shadow if light travelled in straight lines. This phenomenon where light spreads around the edges of a barrier is called as diffraction. Thus diffraction broadly may be defined as:-

"When light falls on obstacles or small apertures whose size is comparable with the wavelength of light, there is a departure from straightline propagation and the light bends round the corners of the obstacles or apertures and enters into the geometrical shadow. This bending of light is called as diffraction".

Under ordinary circumstances, we seldom notice the diffraction of light because such

as incandescent bulbs or the sun. These are not the monochromatic point sources, and the diffraction pattern due to different parts of the source and to different wavelengths usually overlap and obscure each other.

Diffraction limits geometrical optics, in which we represent an electromagnetic wave with a ray. If we try to form a ray by bending light through a narrow slit or through a series of narrow slits, diffraction will always defeat our effort, because it always causes light to spread. Indeed, the narrower we make the slit in the hope of producing a narrower beam, the greater the spreading is.

Fresnel attributed the phenomenon of diffraction to be due to the mutual interference of secondary wavelets, originating from various points of the wavefront, which are not blocked off by an obstacle or are allowed to pass by a slit. That is, instead of finding the new wavefront by constructing the envelope of these secondary wavelets, we must find by principle of superposition, their resultant on every point of the screen taking due account of their relative amplitudes and phases. Fresnel thus applied Huygen's principle of secondary wavelets in conjunction with the

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principle of interference and calculated the position of fringes in general agreement with the observed diffraction pattern.

Here it should be emphasized that, the process responsible for the production of diffraction phenomena is going on continuously during the propagation of every wavefront. But the diffraction effects are observed only when a portion of the wavefront is cut off by some obstacle.

Note: → Every optical instrument (even eye) in fact, make use of only a limited portion of the wavefront. A telescope or a microscope for example utilizes only a limited portion of the wavefront transmitted by the objective lens. Therefore, some diffraction is always present in the image. (This reduces the resolution of the optical instrument).

### Two classes of diffraction phenomena: →

Diffraction phenomena which arise as a result of some limitation on the width of wavefront are divided into two classes known on historical reasons as: →

- 1 → Fraunhofer diffraction.
- 2 → Fresnel diffraction.

### 1 → Fraunhofer diffraction: →

In this class, the source of light and the screen are effectively at infinite distance from the obstacle or aperture causing the diffraction. This means that, the wavefront incident on the obstacle or aperture is plane wavefront. The second - any wavelets which we consider as originating

From the unblocked portion of the wavefront at the moment it just touches the aperture, all start at the same instant of time. In other words, the phase of the secondary wavelets is the same at every point of the aperture. The screen is at infinity. Therefore, we have to consider the interference as taking place between parallel diffracted rays which can be brought into focus by placing a convergent lens behind the aperture. Thus, it is very conveniently observed by employing two convergent lenses (i) one to render the light from the source parallel before its incidence on the aperture and (ii) the other to unite the parallel diffracted rays in focus on the screen, an arrangement which effectively removes the source and screen to infinity.

2) Fresnel class: → In this class of diffraction, the source of light on the screen or both are at finite distances from the obstacle or aperture but no lenses are employed for rendering the rays parallel or convergent. Therefore, the incident wavefront is spherical or cylindrical instead of being plane. As a consequence of this, the phase of secondary wavelets is not same at all points in the plane of aperture causing diffraction. The resultant amplitude at any point, however, is obtained by mutual interference of secondary wavelets.

from different element of unblocked portion of the wavefront.

Here we shall limit ourselves to the Fraunhofer class of diffraction only.

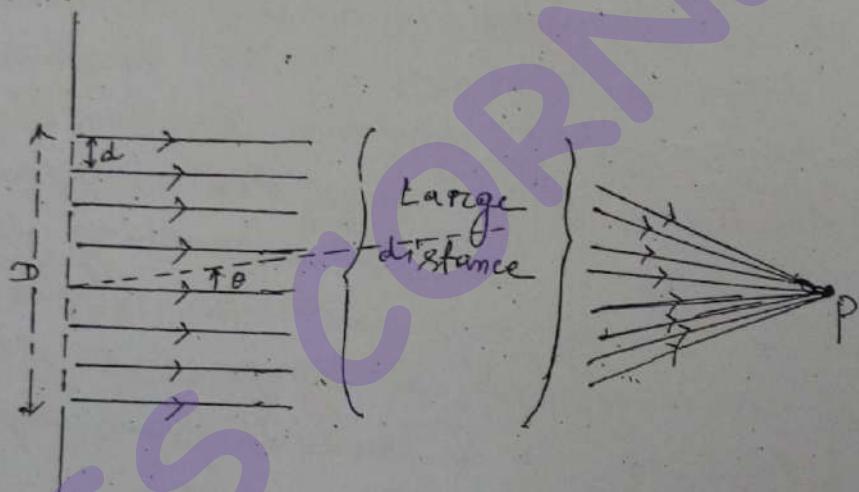
### Fraunhofer class of diffraction

In Fraunhofer class of diffraction all the secondary waves start from the plane of aperture with same phase at any instant of time. At the point of superposition on the screen, they meet at different phases. Since, in this class of diffraction the distance between the slits and field point P is large, the variation of amplitude of successive disturbances reaching the point P can be safely neglected. So, in this class, actually the resultant wave at any point on screen is obtained due to large no. of waves of same amplitude but different phases.

So let us first mathematically find out the resultant wave due to superposition of large no. of simple vibrations of equal amplitudes, same period and phases increasing in an arithmetic progression. [ Such a situation arises, when we consider the diffraction pattern due to  $n$ -identical and uniformly spaced narrow slits ].

b) Superposition of large no. of simple vibrations of equal amplitudes, same period and phases increasing in an arithmetic progression: →

Consider the superposition of  $n$  ( $\rightarrow \infty$ ) waves coming from  $n$  identical and uniformly spaced narrow slits at a point 'P' far away from the slits.



We shall suppose that, the distance between the centre lines of two consecutive slits is 'd' and that between the first and last is 'D'. Then we can write,

$$D = (n-1)d.$$

When a plane wave falls on this array of fine slits, the entire wavefront excepting the parts illuminating the  $n$ -slits is blocked. Each of the slits then become the source of secondary wavelets having same amplitude and same initial phase.

Let us find out the resultant effect due to superposition of all the secondary waves along a direction

to the axis of the system at a distant bold<sup>7</sup>  
 point P.  
 While superposing at 'P', the waves will have  
 same amplitudes (since P is at large distance, the  
 variation of amplitudes of successive disturbances  
 reaching the point P can be safely neglected) but  
 the phase difference between the waves from two  
 successive slits reaching at P will have a phase diff.  
 -ence given by : -

$$\alpha = \phi_{i+1} - \phi_i \\ = \frac{2\pi}{\lambda} (d \sin \theta)$$

[path difference between two  
 consecutive waves in the  
 direction of "d sinθ".]

Hence at 'P' large no. of waves of equal  
 amplitudes but phases varying in arithmetic  
 progression of  $\alpha$  ( $= \frac{2\pi}{\lambda} d \sin \theta$ ) superposes.

The resultant of all these vibrations  
 can be obtained by phasor addition method  
 etc. Using the method of complex addition,  
 let us assume that, Secondary waves  
 have amplitude 'a' at point of superposition  
 'P' and the angular frequency of vibration  
 is. Assuming each to be sinusoidal wave,

The resultant wave at P is : →

$$y = a \sin \omega t + a \sin(\omega t + \alpha) + a \sin(\omega t + 2\alpha) + \dots + a \sin \{ \omega t + (n-1)\alpha \}$$

$$= a [ \sin \omega t + \sin(\omega t + \alpha) + \sin(\omega t + 2\alpha) + \dots + \sin \{ \omega t + (n-1)\alpha \} ]$$

Now  $\sin \omega t$ ,  $\sin(\omega t + \alpha)$ , etc. can be considered as the imaginary parts of the complex functions  $e^{i\omega t}$ ,  $e^{i(\omega t + \alpha)}$ , etc.

$$\text{Then } \sin \omega t + \sin(\omega t + \alpha) + \sin(\omega t + 2\alpha) + \dots + \sin \{ \omega t + (n-1)\alpha \}$$

$$= \operatorname{Im} [ e^{i\omega t} + e^{i(\omega t + \alpha)} + \dots + e^{i\{ \omega t + (n-1)\alpha \}} ]$$

$$= \operatorname{Im} [ e^{i\omega t} \{ 1 + e^{i\alpha} + e^{2i\alpha} + \dots + e^{i(n-1)\alpha} \} ]$$

Now using the identity :-

$$1 + x + x^2 + \dots + x^m = \frac{1 - x^{m+1}}{1 - x}, \text{ We get}$$

$$y = \operatorname{Im} [ a e^{i\omega t} \cdot \frac{1 - e^{i(n-1)\alpha}}{1 - e^{i\alpha}} ]$$

$$= \operatorname{Im} [ a e^{i\omega t} \cdot \frac{e^{i(n-1)\alpha} - 1}{e^{i\alpha} - 1} ]$$

$$= \operatorname{Im} [ a e^{i\omega t} \cdot \frac{e^{\frac{i(n-1)\alpha}{2}} \{ e^{\frac{i\alpha}{2}} - e^{-\frac{i\alpha}{2}} \}}{e^{\frac{i\alpha}{2}} \{ e^{\frac{i\alpha}{2}} - e^{-\frac{i\alpha}{2}} \}} ]$$

$$= \operatorname{Im} [ a e^{i\omega t} \cdot e^{\frac{i(n-1)\alpha}{2}} \cdot \frac{2 i \sin \frac{n\alpha}{2}}{2 i \sin \frac{\alpha}{2}} ]$$

$$= \operatorname{Im} [ a \cdot \frac{\sin \frac{n\alpha}{2}}{\sin \frac{\alpha}{2}} \cdot e^{i \{ \omega t + \frac{n-1}{2}\alpha \}} ]$$

So

$$y = a \frac{\sin \frac{n\alpha}{2}}{\sin \frac{\alpha}{2}} \cdot \sin \left[ \omega t + \frac{n-1}{2}\alpha \right]$$

Substituting a  $\frac{\sin \frac{n\alpha}{2}}{\sin \frac{\alpha}{2}} = R$ , we get: → ①

$$y = R \sin \left[ \omega t + \frac{(n-1)}{2} \alpha \right] \quad \text{--- ②}$$

This represents a sinusoidal wave of amplitude  $R$  and phase  $\omega t + \beta$ , where

$$\beta = \frac{(n-1)}{2} \alpha \quad \text{--- ③}$$

This  $\beta$  is the average of the phases of the first and  $n$ th wave on arrival at point P.

putting  $\alpha = \frac{2\pi}{\lambda} \cdot d \sin \theta$ , eqn. ① gives: →

$$\begin{aligned} R &= a \cdot \frac{\sin \left[ \frac{1}{2} n \left( \frac{2\pi}{\lambda} d \sin \theta \right) \right]}{\sin \left[ \frac{1}{2} \left( \frac{2\pi}{\lambda} d \sin \theta \right) \right]} \\ &= a \cdot \frac{\sin \left[ n \left( \frac{\pi}{\lambda} \right) d \sin \theta \right]}{\sin \left[ \left( \frac{\pi}{\lambda} \right) d \sin \theta \right]} \quad \text{--- ④} \end{aligned}$$

Again since  $D = (n-1)d$ , We can write eqn. ④ as: →

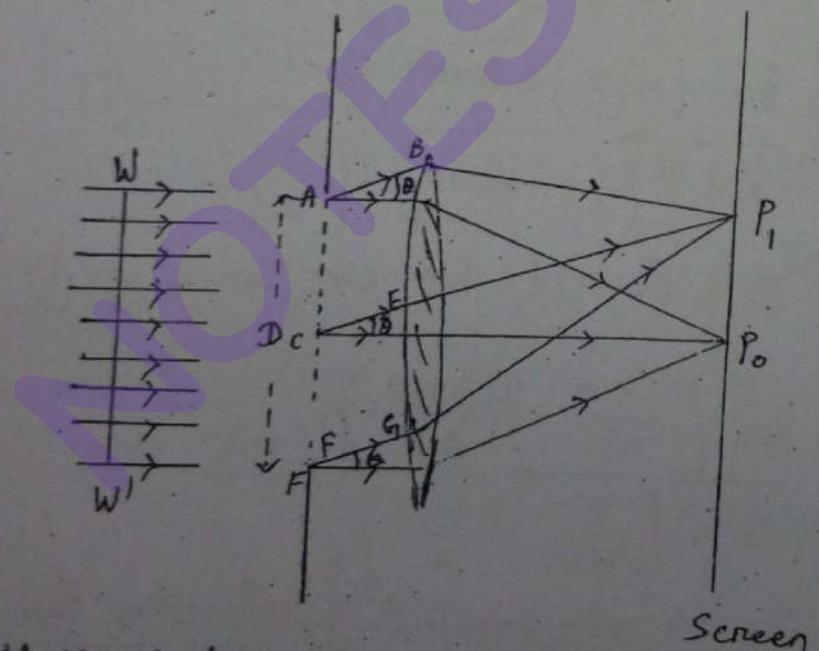
$$R = a \frac{\sin \left[ \frac{n\pi}{n-1} \frac{D \sin \theta}{\lambda} \right]}{\sin \left[ \frac{\pi}{n-1} \frac{D \sin \theta}{\lambda} \right]} \quad \text{--- ⑤}$$

This formulation is of general application for any number of slits starting from  $n=2$ . We can also use it for finding the diffraction pattern of a single slit with a neat little trick.

## Diffraktion by a Single Slit

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Consider a beam of parallel monochromatic light incidenting normally on an opaque plate in which there is a long narrow slit. The light beam after transmitted through the slit spreads out perpendicularly to the length of the slit. Therefore, when it is focused on the screen by a lens, what is observed is a diffraction pattern. It consists of central band, much wider than the slit width, situated directly opposite to the slit and bounded by dark and bright bands of decreasing intensity. The central bright band is extremely intense and its width is twice as great as that of the fainter sidebands.



AF → Section of slit of width D in the plane of paper.

WW' → plane wavefront of monochromatic light of wavelength  $\lambda$  propagating normally to the slit.

At the instant,

When the unblocked portion of the incident plane wavefront is in the plane of slit, e.g., point of the wavefront in the plane of slit as dotted wave

These secondary wavelets spread out to the right in all directions. The parts of each wavefront travelling normal to slit (i.e. in the direction of incident wave) are brought to focus at  $P_0$  (by the lens). Those travelling at an angle  $\theta$  with normal are brought to focus at  $P_1$  and so on.

The resultant intensity at  $P_1$  can be obtained by using eqn. ⑤.

Let us assume in this case that ~~n~~  $n$  is made very large keeping the distance  $D$  fixed. Then the distance  $a$  between consecutive slits will become very small and in the limit when  $n \rightarrow \infty$ , the distance  $a$  will tend to zero and we shall be left with a single slit of width  $D$ .

When  $n \rightarrow \infty$ , we can write the numerator and denominator of eqn. ⑤ as: →

$$\sin\left[\frac{n\pi}{n-1}, \frac{D\sin\theta}{\lambda}\right] = \sin\left(\frac{\pi D \sin\theta}{\lambda}\right)$$

$$\text{and } \sin\left(\frac{\pi}{n-1}, \frac{D\sin\theta}{\lambda}\right) = \sin\left(\frac{\pi}{n}, \frac{D\sin\theta}{\lambda}\right) = \frac{\pi}{n} \times \frac{D\sin\theta}{\lambda}$$

$$\text{So } R = a \frac{\sin\left(\frac{\pi D \sin\theta}{\lambda}\right)}{\frac{\pi}{n} \times \frac{D\sin\theta}{\lambda}} \quad \begin{matrix} \text{Measuring} \\ \text{all angles} \\ \text{in radians} \end{matrix} \quad - ⑥$$

$$\Rightarrow R = n a \frac{\sin\left(\frac{\pi D \sin\theta}{\lambda}\right)}{\left(\frac{\pi D \sin\theta}{\lambda}\right)}$$

Substituting  $na = A$  and  $\frac{\pi D \sin\theta}{\lambda} = \beta$ , we get,

$$R = A \frac{\sin\beta}{\beta} \quad \text{--- (7)}$$

The resultant intensity at  $P_1$  being proportional to the square of the resultant amplitude  $R$ , hence

$$I = KR^2 = KA^2 \frac{\sin^2\beta}{\beta^2} \quad \text{--- (8)}$$

$$= I_0 \frac{\sin^2\beta}{\beta^2} \quad \text{--- (9)}$$

(Substituting  $I_0 = KA^2$ )

Now let us proceed to analyse the intensity distribution on the Screen.

Principal Maxima: →

The maximum value of  $\frac{\sin\beta}{\beta}$  is 1. At this  $\beta$ ,  $I$  is maximum and its equal to  $I_0$ .

But  $\frac{\sin\beta}{\beta} = 1$  when  $\beta = 0$

$$\Rightarrow \frac{\pi D}{\lambda} \sin\theta = 0$$

$$\Rightarrow \theta = 0.$$

The condition  $\theta = 0$  simply means that this maximum is formed by parts of secondary wavelets which travel normally to the slit. The position of this maximum is therefore directly opposite to the slit. This Maximum is called as principal Maximum and it is formed at  $P_0$ .

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### Condition of Minima and Minimum Intensity Positions -

The intensity  $I$  will be zero at the positions for which  $\sin \beta = 0$  but  $\beta \neq 0$

$$\Rightarrow \beta = \pm \pi, \pm 2\pi, \pm 3\pi, \dots \text{etc} = \pm n\pi$$

$$\Rightarrow \frac{\pi D \sin \theta}{\lambda} = \pm n\pi$$

$$\Rightarrow \sin \theta = \pm \frac{n\lambda}{D} \quad \text{--- (9)}$$

where  $n = 1, 2, \dots \text{etc}$

[Note:  $\rightarrow n=0$  is not admissible as that is the condition of principal Maxima].

Eqn. (9) can be written as:-

$$D \sin \theta = \pm n\lambda \quad \text{--- (10)}$$

i.e. the rays diffracted at an angle  $\theta$  interfere destructively if the path difference between the extreme diffracted rays is an integral multiple of  $\lambda$ .

From eqn. (9), the minima are located on both sides of the principal Maxima at:-

$$\sin \theta = \pm \frac{1}{D}, \pm \frac{2}{D}, \pm \frac{3}{D}, \dots \text{etc.}$$

### Secondary Maxima:-

With one principal Maximum and a number of minima, it is obvious that, there should also be secondary maxima in between minima. The intensity of these secondary maxima are less than that of the principal Maximum. The following procedure will tell

as the position and intensity of these secondary maximum.

$$I \text{ at any point } \Rightarrow I = I_0 \cdot \frac{\sin^2 \beta}{\beta^2}$$

The positions of maxima and minima corresponds to

$$\frac{dI}{d\beta} = 0 \Rightarrow \frac{d}{d\beta} \left[ I_0 \left( \frac{8m\beta}{\rho} \right)^2 \right] = 0$$

$$\Rightarrow I_0 \cdot 2 \cdot \frac{\sin \beta}{\beta} \left[ \frac{\beta \cos \beta - \sin \beta}{\beta^2} \right] = 0$$

This relation is satisfied if either (i)  $\sin \beta = 0$   
or (ii)  $\beta \cos \beta - 8 \sin \beta = 0$

The first condition, that is  $\frac{d\sin\beta}{d\beta} = 0$  gives (i) the condition for principal Maximum when  $\beta = 0$  and (ii) minimum when  $\beta = \pi n$ .

Hence the Second condition  $\beta \cos \beta - \sin \beta = 0$  is  
for Secondary Maxima. For this therefore,

$$\beta \cos \beta - \sin \beta = 0$$

$$\Rightarrow \tan \beta = \beta \quad \text{---} \quad (11)$$

The values of  $\beta$  satisfying the condition ① are obtained graphically by plotting  $y = \beta$  and  $y = \text{temp}$  together. (See figure in next page).

The points of intersection of these plots are (approximately)  $x = -5$  and  $x = 1$ .

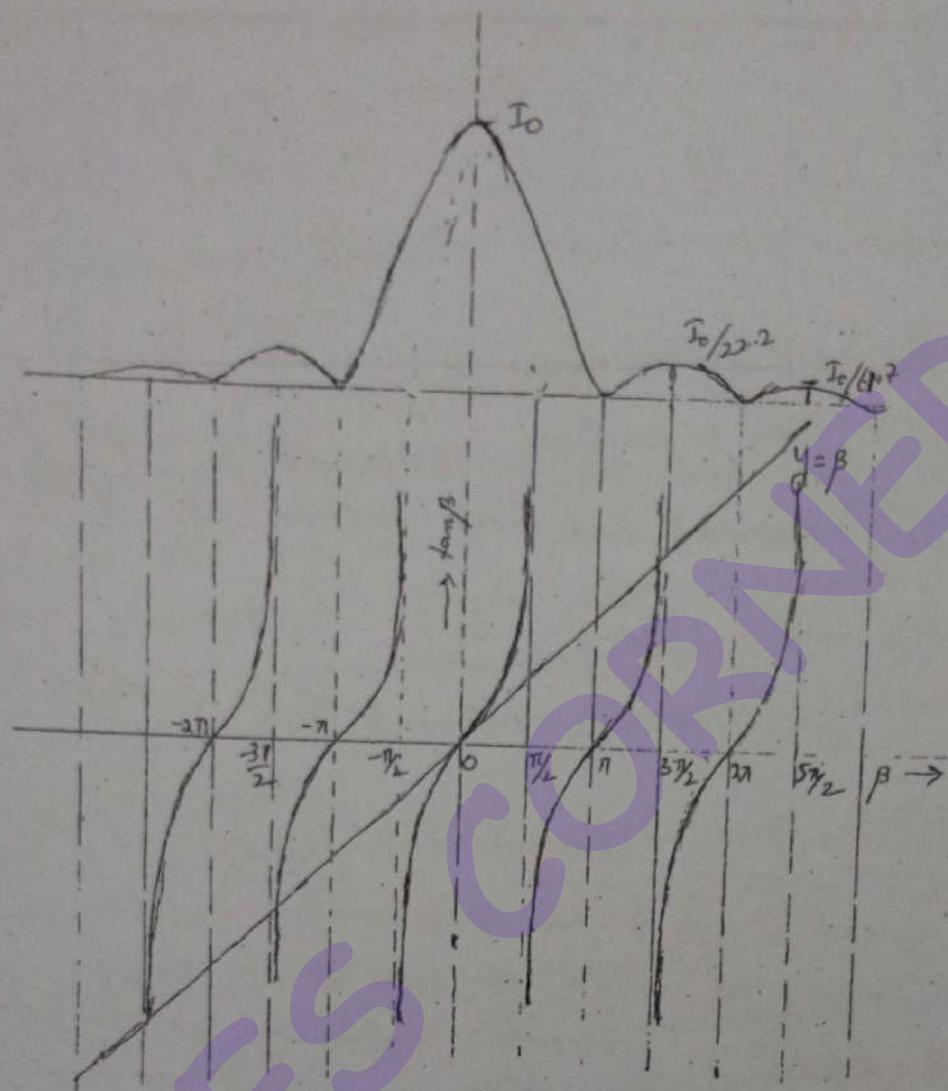
$$\beta = 0, \pm \frac{3\pi}{2}, \pm \frac{5\pi}{2}, \dots, \pm \left(2n+1\right) \frac{\pi}{2} \quad \text{or}$$

more exactly,

$$\beta = 0, \pm 1.430\pi, \pm 2.462\pi, \pm 3.471\pi, \dots$$

$\beta = 0$  gives the principal Maximum and rest gives the condition for secondary maximum.

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Intensity of Maxima  $\rightarrow$

$$I = I_0 \frac{8m\beta}{\beta^2}$$

putting  $\beta = 0$ , limit  $\frac{8m\beta}{\beta} = 1$

$\therefore I = I_0$

$\therefore I_0$  is the intensity of principal Maxima.

putting  $\beta = \frac{3\pi}{2}$ ,  $\frac{8m\beta}{\beta} = \frac{8(-1)}{3\pi/2}$

$\therefore I_r = I_0 \left( \frac{8m\beta}{\beta} \right)^2 = I_0 \times \frac{4}{9\pi^2} = \frac{I_0}{22.2}$

$$\text{For } \beta = \frac{\pi n}{2}, I_2 = I_0 \left(\frac{1}{5\gamma_2}\right)^2 = \frac{4}{25\gamma_2^2} \times I_0 \\ \approx \frac{I_0}{61.7}$$

Similarly,  $I_3 = \frac{I_0}{121}$  & so on.

So the ratio of intensities of principal Maxima, 1st order Maxima, 2nd order Maxima etc is

$$1 : \frac{1}{82.2} : \frac{1}{61.7} : \frac{1}{121}$$

$$\Rightarrow 1 : 0.0469 : 0.068 : 0.0083 : 0.0050 \\ \text{etc.}$$

Note: → (1) It should be pointed out that the angular spread of principal Maxima (i.e. the distance between 1st minima in left to 1st minima in right  $= \frac{2\lambda}{D}$ ) is inversely proportional to the width of the slit. Moreover if  $D = \lambda$  and  $\sin\theta = 1$  in eqn (2) then  $\sin\theta = \pm 1 \Rightarrow \theta = \pm \frac{\pi}{2}$ , that is, the first minimum occurs at  $90^\circ$  with the normal (i.e. the incident direction). Under this condition, the length after traversing the slit spreads out in all directions, with an intensity which decreases steadily as  $\theta$  increases. There is no maxima and minima in this case, the slit will become just a sum of secondary waves.

(2) If  $D < \lambda$ , then the original condition  $D \sin\theta = \lambda$ , for the 1st minima (i.e.  $\sin\theta = \frac{\lambda}{D}$ ) gives  $\sin\theta > 1$ , which is impossible. Therefore the eqn (2) for intensity does not hold good when

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The slit width becomes less than one wavelength.  
The treatment breaks up.

Questions : -

1. Differentiate between Fresnel and Fraunhofer type of diffraction.
2. What do you mean by diffraction of light?
3. Differentiate between diffraction and interference.
4. Discuss the features of Fraunhofer diffraction pattern through a single slit when it is illuminated by a monochromatic light. Draw separately the intensity distribution in Fraunhofer single slit diffraction pattern.
5. What happens to the single slit diffraction pattern when the size of slit is:-
  - (i) equal to the wavelength?
  - (ii) smaller than the wavelength?
  - (iii) much larger than the wavelength?
6. What is the significance of secondary maxima in the diffraction pattern due to a single slit? Where are they located?
7. What is the effect of increase in wavelength in a Fraunhofer single slit diffraction pattern?
8. Describe the change in Fraunhofer single slit diffraction pattern, as the slit width is narrowed.
9. Describe the change in Fraunhofer single slit diffraction pattern if the slit width is gradually increased.
10. What happens to the Fraunhofer diffraction

pattern through a single slit on a screen if water replaces air in the space between the slit and screen.

11. Deduce the expression for the angular radius of the central peak of a Fraunhofer single slit diffraction pattern.

Numericals: →

1) A single narrow slit is illuminated by monochromatic light of wavelength  $6330\text{ Å}$ . If the angular width of the principal Maxima is  $1.2^\circ$ , find the slit width. (Given  $\sin(0.6^\circ) = 0.0105$ ).

2) A monochromatic light beam of wavelength  $597\text{ nm}$  is incident normally on a slit of width  $0.04\text{ cm}$ . The diffracted beam is focused on a screen by a convex lens of focal length  $80\text{ cm}$ . Find the distance on the screen between the first minimum and centre of diffraction pattern.

3) Light of wavelength  $500\text{ nm}$  is incident on a slit having a width of  $2.5\text{ mm}$ . Find the positions of the first minima and width of the central Maxima on a screen  $2\text{ m}$  from the slit.

4) A single slit is illuminated by light of wavelength  $\lambda_1$  and  $\lambda_2$  such that the first diffraction minimum of  $\lambda_1$  coincides with the second minimum of  $\lambda_2$  component.

- What relationship exists between the two wavelengths?
- Do any other minima in the two diffraction patterns coincide?

## Magnetic Circuits

- What is the requirement of magnetic circuit?
- Some important terms in magnetic "
- Comparison b/w electric & magnetic "
- Series magnetic circuit & numericals
- B-H Curve & Hysteresis Loop.

$$F = -N \frac{d\phi}{dt}, \quad H = \frac{NI}{l}, \quad B = \mu H$$

$$\phi = BA, \quad \text{Eq} = \frac{\phi ZN}{E_0} \xrightarrow[A]{P}$$

MMF — Magneto motive Force (EMF) =  $N \times I$   
 Magnetic Field Intensity ( $H$ ), Magnetising Force.

Reluctance (Resistance)

$$\frac{1}{S} = \text{Permeance (Conductance)}$$

→ EMF - Amt of work done required to carry a unit magnetic pole once around a magnetic circuit

$$\Rightarrow H = \frac{NI}{l} \quad (l - \text{length of magnetic circuit}).$$

→ Opposition to the flow of magnetic flux is called as reluctance ( $S$ ).

$\text{EMF} = \text{Current} \times \text{Resistance}$

$\text{MMF} = \text{Flux} \times \text{Resistance}$

Let  $S = S_1 + S_2 + S_3$

$$\boxed{S = \frac{l}{A\mu}}$$

$$, \mu = \mu_0 \times \mu_r \quad (\mu_0 = 4\pi \times 10^{-7})$$

$\mu_r$  = Relativile

permability

Defined as

Permeability of a material is its ability of conducting magnetic lines of force on the ratio magnetic flux density by magnetic field intensity.

$$\boxed{\mu = \frac{B}{H}}$$

Relative permeability is defined as the ratio of flux density produced in the material to the flux density produced in air by the same magnetic field intensity

$$\boxed{B = \mu_r \mu_0 H}$$

Q: A coil of 600 turns and of resistance 20 ohms is wound uniformly over a steel ring of circumference 30 cm and cross-sectional area 9 cm<sup>2</sup>. It is connected to supply of 20V DC. If the relative permeability of the ring is 1800. Find the reluctance, MF Intensity, MMF, Magnetic Flux.

$$N = 600, R = 20$$

$$S = \frac{l}{\mu_0 \mu_r A}, H = \frac{NI}{l}$$

$$MMF = N \times I$$

Q: A steel ring having a cross-sectional area of 400 mm<sup>2</sup> and mean circumference of 400 mm has a coil of 200 turns wound uniformly around it. ( $\mu_r = 300$ ). Calculate the reluctance of the ring. (ii) The current req. to produce a flux of 800 mWb in the ring.

$$A = 400, N = 200$$



Total MMF in a circuit. (series)

$$MMF = H_1 l_1 + H_2 l_2 + H_3 l_3 + H_4 l_4 + H_5 l_5$$

$$\downarrow NI$$

$H$  = Magnetic field intensity  
 $l$  = length of magnetic circuit

$$H = \frac{NI}{l}$$

$$MMF = \phi \left[ \frac{\phi_1 l_1}{a_1 \mu_0 \mu_{r1}} + \frac{l_2 \phi_2}{a_2 \mu_0 \mu_{r2}} \right]$$

Q A iron ring of circular cross-sectional area  $5 \times 10^{-4} \text{ m}^2$  has a mean circumference of 2 m. It has a saw cut of  $2 \times 10^{-3} \text{ m}$  length and is wound with 800 turns of wire. Determine the exciting current when the flux in the air gap is  $0.5 \times 10^{-3} \text{ Wb}$ .  $\mu_r(\text{iron}) = 600$  and leakage factor = 1.2.  $I = 5.9$

$$\Rightarrow \phi_{\text{in iron}} = \phi_{\text{in airgap}} \times \text{Leakage Current}$$

$$\text{MMF} = NI = \oint \left[ \frac{\phi_1 l_1}{a_1 \mu_0 \mu_{r1}} + \frac{\phi_2 l_2}{a_2 \mu_0 \mu_{r2}} \right]$$

$$600 \times I = \frac{0.6 \times 10^{-3} \times 2}{5 \times 10^{-4} \times 4 \times 10^{-7} \times 600 \times 3.14} + \begin{cases} \phi_1 = 0.5 \times 10^{-3} \times 1/2 \\ = 0.6 \times 10^{-3} \end{cases}$$

$$\frac{0.5 \times 10^{-3} \times 2 \times 10^{-3}}{5 \times 10^{-4} \times 4 \times 10^{-7} \times 13.14}$$

$$= \frac{1.2 \times 10^{-3}}{12 \times 10^3 \times 10^{-14} \times 3.14} + \frac{10^{-6}}{2 \times 10 \times 10^{-11} \times 3.14}$$

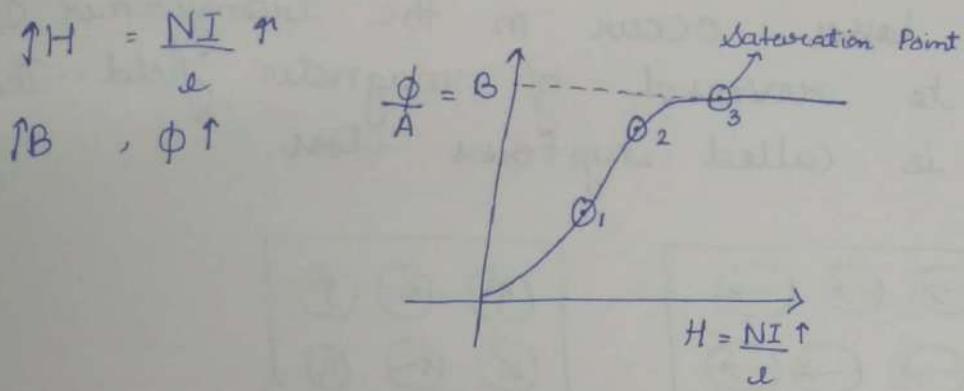
$$= \frac{0.1 \times 10^{-3} \times 10^8}{3.14} + \frac{0.5 \times 10^6 \times 10^{10}}{3.14}$$

$$= \frac{0.1 \times 10^5}{3.14} + \frac{0.5 \times 10^4}{3.14}$$

$$I = \frac{10000 + 5000}{600} \quad 0.03184 \times 10^5 + 0.1592$$

$$= \frac{3184 + 1592}{600} =$$

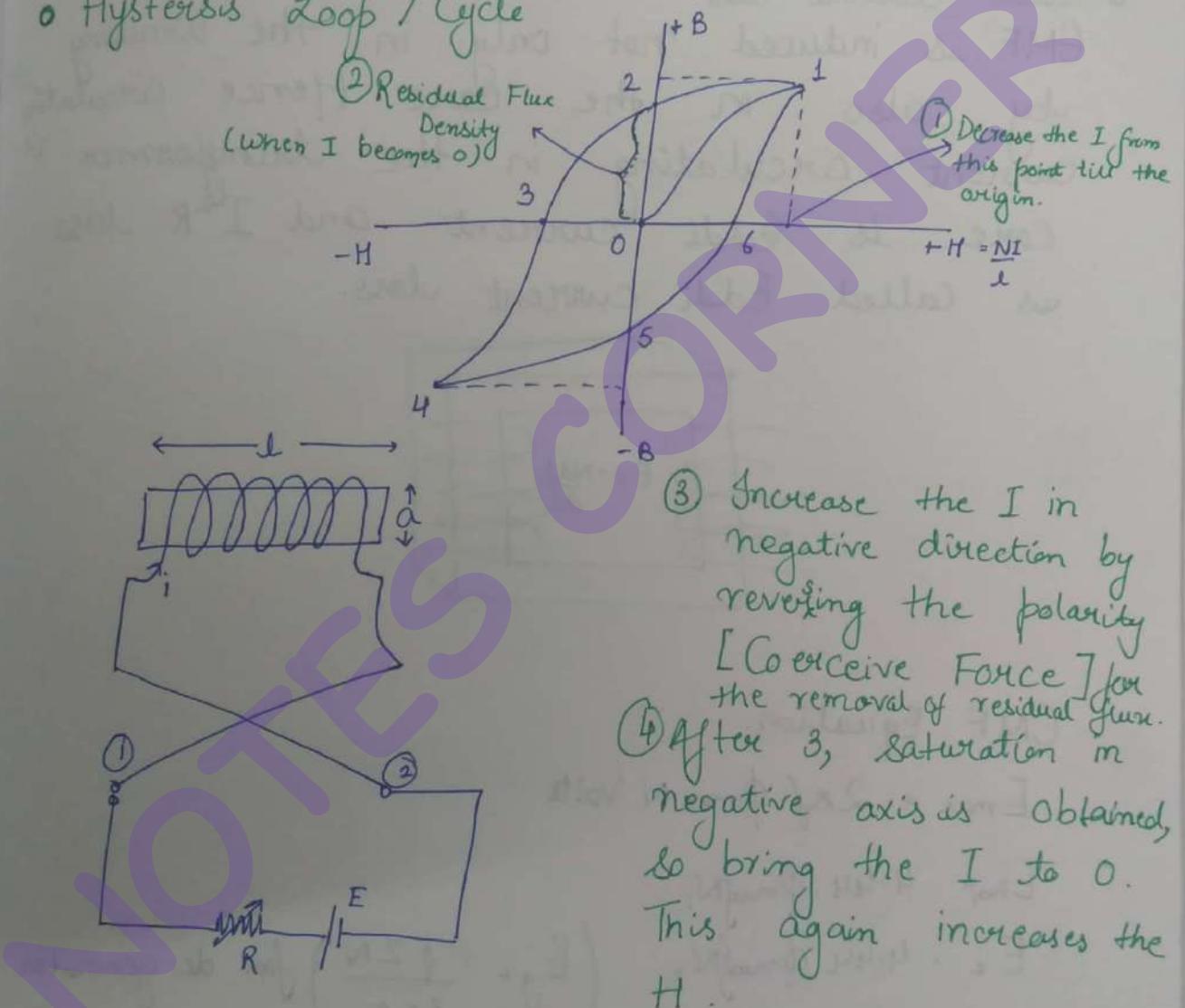
## o B-H Curve: Hysteresis Loop



## o Hysteresis Loop / Cycle

② Residual Flux Density (when I becomes 0)

① Decrease the I from this point till the origin.



- ③ Increase the I in negative direction by reversing the polarity [Coercive Force] for the removal of residual flux.
- ④ After 3, saturation in negative axis is obtained, so bring the I to 0. This again increases the H.

## Residual Flux Density

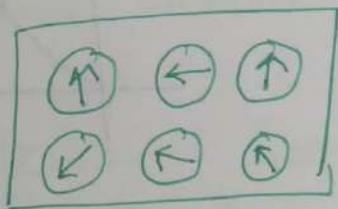
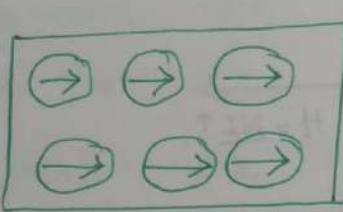
The value of magnetism, inside the magnetic material when the I supply is completely withdrawn.

## Coercive Force

It is the magnetising force required to remove the residual flux completely.

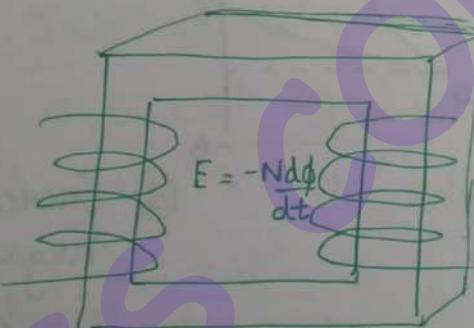
### • Hysteresis Loss

Some losses occur in the transformer core due to reversal of magnetic field. That loss is called hysteresis loss.



### • Eddi Current loss

EMF is induced not only in the winding but also in the core. Hence circulating current circulating in the transformer core is Eddi current and  $I^2R$  loss is called Eddi current loss.



EMF Equation.

$$E_{max} = 2\pi f \phi_{max} N \text{ Volts}$$

$$E_{max} = 4.44 \cdot \phi_{max} f N,$$

$$E_2 = 4.44 \phi_{max} f N_2$$

$$\left( E_g = \frac{P \phi Z N}{60A} \right) \text{ for dc generator.}$$

- Constructing
- Working Principle
- Types
- Formula based Numericals

$A = 2$  = full wave Winding

-  $P$  for lap winding

$Z$  = No. of armature Coils

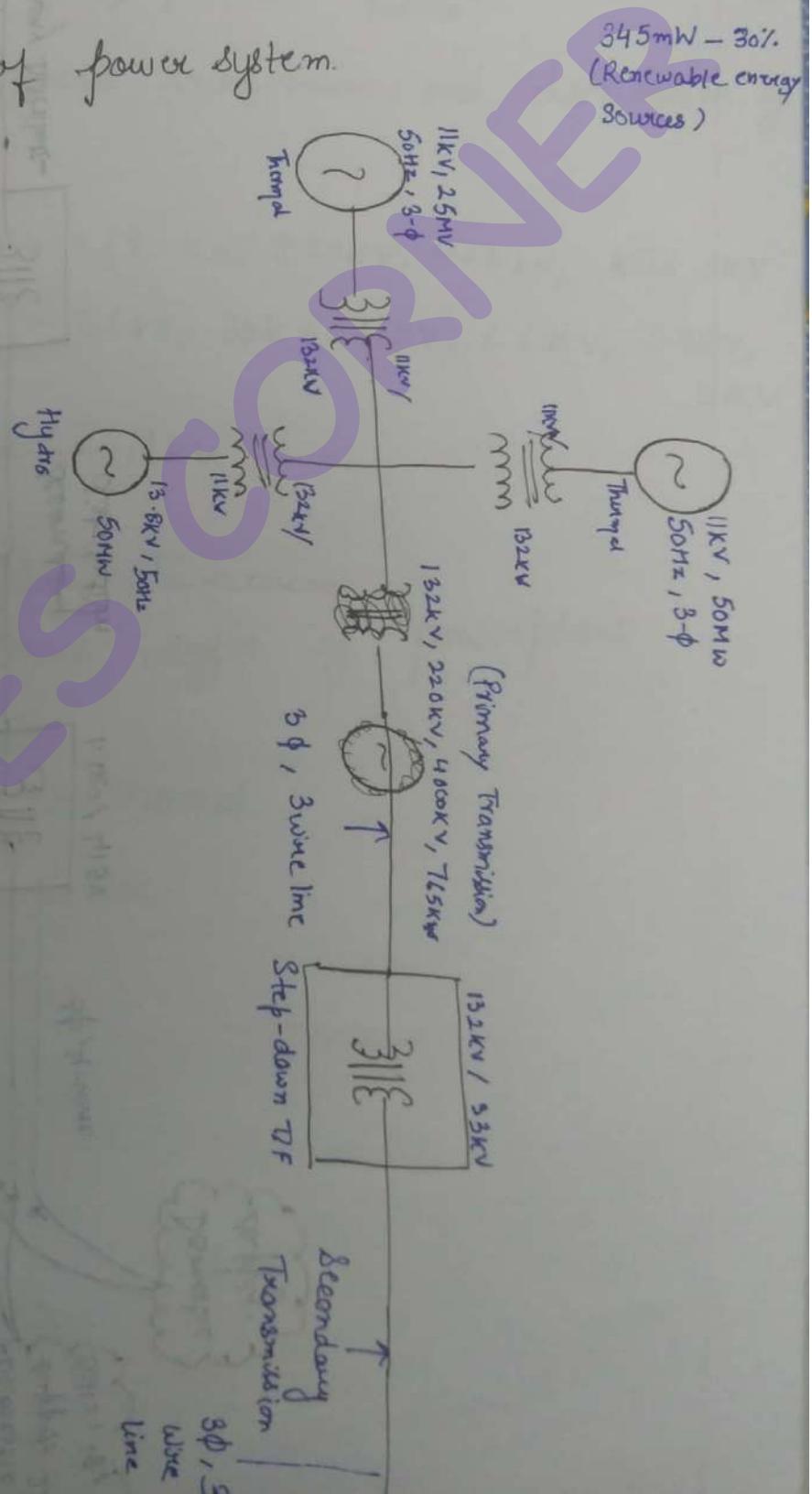
$\phi$  - Flux

## Power System

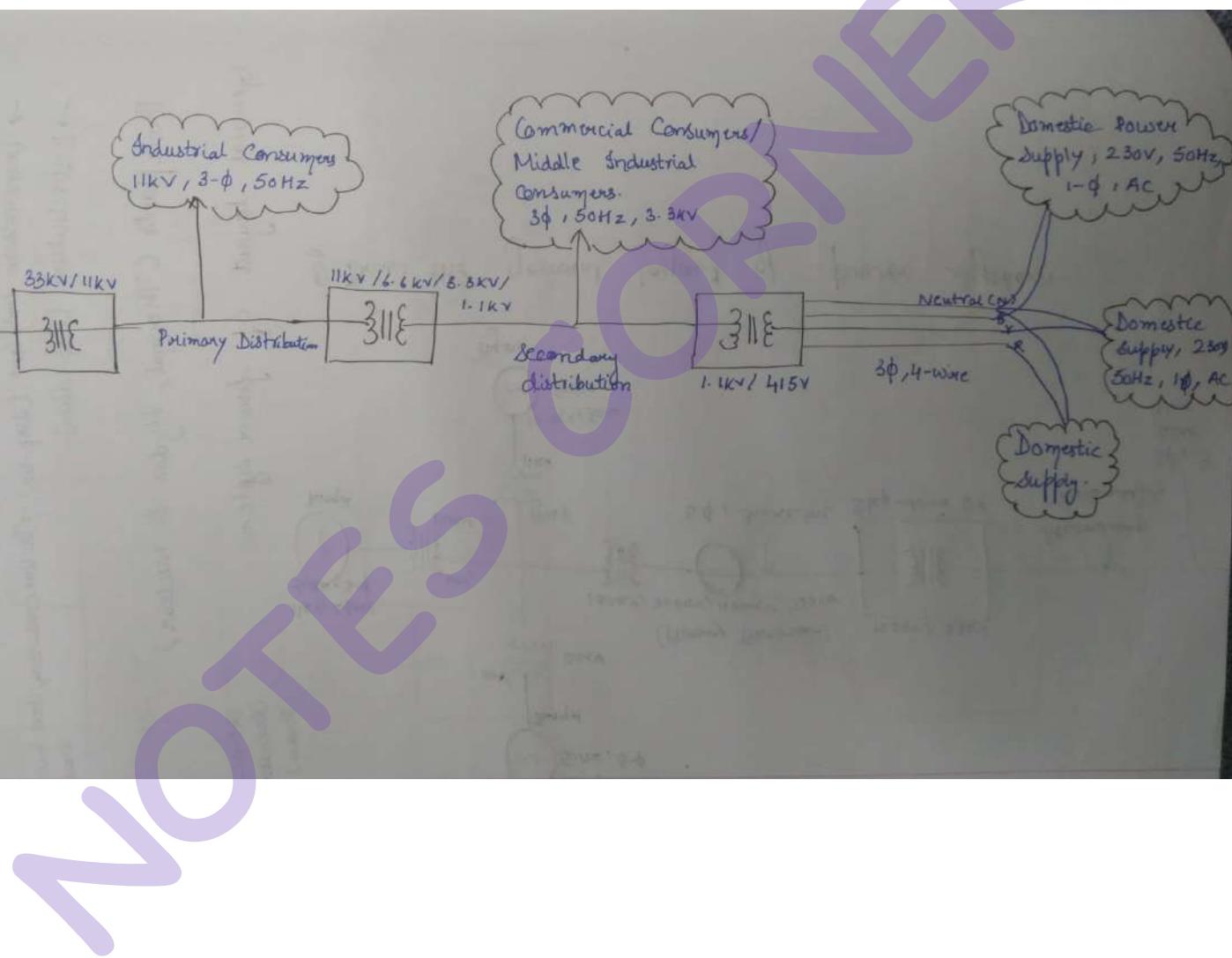
- Generation → Different types of powerplants
  - Transmission Only Govt. (Step-up) → Tr. line conductors, steel towers, Insulators
  - Distribution (Step-down)

## Powerplants (Thermal, Hydro & nuclear)

## General layout of power system.



Q Draw the general layout of power system.



Q. What are the components of power system?

1. Power station / Power supply
2. Step-up transformers
3. Transmission lines
4. Sub-stations
5. Step-down transformers
6. Other supplementary equipments (switch gear and protection devices)

Q. What are the different transmission and distribution of voltages in India?

Transmission Voltages - 132 kV, 220 kV, 400 kV, 476.5 kV

Distribution Voltages - 66 kV, 33 kV, 11 kV, 6.6 kV, 3.3 kV, 1 kV

Generation voltage - 11 kV

• Conductors - Copper, aluminium

Q. Comparison b/w different types of power plant.

Initial Setup Cost

Nuclear > Hydro > Thermal

Cleanest one → Hydro

- Q. What are the different types of energy sources?
1. Renewable and non-renewable
  2. Commercial and non-commercial
  3. Conventional and non-Conventional
  4. Primary and Secondary source of energy  
Comparison b/w nuclear, thermal & hydro power plant
- Q. What are the diff. types of wiring techniques?
- Q. What is the requirement and different types of earthing.
- Q. What are the electrical safety rules for the industry
- Q. Give the classification of different types of energy sources

# OSCILLATION & WAVES

with companion

## (1) Free Oscillation

The to and fro motion of a body about a mean position, maintaining the amplitude constant with respect to time is called as free oscillation.

In free oscillation generally there is no loss of energy. A body undergoing free oscillation experiences two type of forces.

- i) Inertial force ( $F_I$ )
- ii) Restoring force ( $F_R$ )

### Inertial Force

The inertial force is directly proportional to the acceleration.

$$F_I = M \frac{dy}{dt^2}$$

, where,  $m$  = mass of oscillating body  
 $y$  = displacement

### Restoring Force

Once the body is displaced from the equilibrium position it has tendency to come back to the equilibrium position.

Generally it comes with a force called restoring force. It is directly proportional to the displacement and acts in the direction opposite to the displacement.  
So it is expressed by.

$$F_R = -Ky \quad , \text{where } k = \text{const (gains/restoring)}$$

→ For equilibrium,  $F_I = F_R$   
 $\rightarrow M \frac{dy}{dt^2} = -ky$

$$\Rightarrow \frac{d^2y}{dt^2} = -\frac{k}{m} y.$$

$$\Rightarrow \boxed{\frac{d^2y}{dt^2} + \frac{k}{m} y = 0} \rightarrow \text{Basic equation for free oscillation}$$

The solution of this equation becomes,

$$y = A \sin(\omega t + \phi) \quad \begin{aligned} A &\rightarrow \text{Amplitude} \\ \phi &\rightarrow \text{phase difference} \end{aligned}$$

$$\text{Here, } \omega^2 = \frac{k}{m} \quad \omega \rightarrow \text{Angular freq.}$$

So, the differential equation for free oscillation can also be written as,

$$\boxed{\frac{d^2y}{dt^2} + \omega^2 y = 0}$$

Here,  
 $\omega$  = Natural Angular freq. of the oscillation

$$\Rightarrow \omega = 2\pi f = \frac{2\pi}{T}$$

$$\phi = \text{initial phase} \Rightarrow \phi = kx.$$

$$\boxed{y = A \sin(\omega t + kx)}$$

## ② Damped Oscillation:

In the damped oscillation, the oscillating body continuously loses its energy to overcome the opposing forces like friction. In this case, the body experiences three type of forces.

- (i) Inertial force ( $F_I$ )
- (ii) Restoring Force ( $F_R$ )
- (iii) Damping Force ( $F_D$ )

Ans.

Inertial force

Inertial force is directly proportional to acceleration

$$F_I = \frac{M d^2y}{dt^2}, \text{ where } M = \text{mass of oscillating body}$$

$y$  = displacement

Restoring force

Once the body is displaced from the equilibrium position it has tendency to come back to equilibrium position.

$$F_R = -ky, \quad k = \text{gas/restoring const.}$$

Damping force

This force tries to oppose the motion. It is directly proportional to the velocity and is given by,

$$F_D = -\alpha \frac{dy}{dt}$$

$\alpha$  = damping const.

→ In equilibrium

$$F_I = F_R + F_D \Rightarrow M \frac{d^2y}{dt^2} = -ky - \alpha \frac{dy}{dt}$$

$$\Rightarrow M \frac{d^2y}{dt^2} + ky + \alpha \frac{dy}{dt} = 0$$

$$\boxed{\frac{d^2y}{dt^2} + \left(\frac{\alpha}{m}\right) \frac{dy}{dt} + \left(\frac{k}{m}\right)y = 0}$$

$$\boxed{\frac{d^2y}{dt^2} + 2b \frac{dy}{dt} + \omega^2 y = 0} \rightarrow \text{diff eqn for damped oscillation.}^{(1)}$$

here,  $2b = \frac{\alpha}{m}, \quad \omega^2 = \frac{k}{m}$

The solution to the above equation can be as follows:

$$y = Ae^{\alpha t}$$

So

$$\frac{dy}{dt} = A\alpha e^{\alpha t}$$

$$\Delta \quad \frac{d^2y}{dt^2} = A\alpha^2 Ae^{\alpha t}$$

Putting these values in eq^n ①

$$\Rightarrow A\alpha^2 e^{\alpha t} + 2A\alpha e^{\alpha t} + \omega^2 A e^{\alpha t} = 0$$

$$\Rightarrow \alpha^2 + 2\alpha + \omega^2 = 0$$

$$\Rightarrow \alpha = \frac{-2b \pm \sqrt{4b^2 - 4\omega^2}}{2}$$

$$\Rightarrow \alpha = \frac{-2b \pm 2\sqrt{b^2 - \omega^2}}{2}$$

$$\Rightarrow \boxed{\alpha = -b \pm \sqrt{b^2 - \omega^2}}$$

Soln for displacement is

$$\boxed{y = A_1 e^{(-b+\sqrt{b^2-\omega^2})t} + A_2 e^{(-b-\sqrt{b^2-\omega^2})t}}$$

→ General solution  
of displacement  
for damped oscillation

Q)i) Formulate the equation for damped harmonic oscillation and find out its general solution.

ii) Discuss the case of overdamping / underdamping / critical damping.

The solutions depend on the different cases.

i) Overdamping ( $b > \omega$ )

(ii) Critical damping ( $b = \omega$ )

(iii) Under damping ( $b < \omega$ )

(i) Pseudodamping ( $b > \omega$ ):-

In this case  $\sqrt{b^2 - \omega^2}$  is a real positive number where value is less than  $b$ .

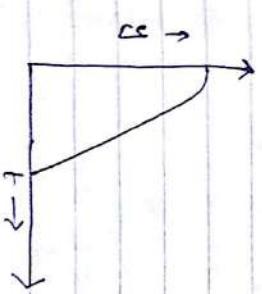
So,  
 $(-b + \sqrt{b^2 - \omega^2})$  is a negative number and  $(-b - \sqrt{b^2 - \omega^2})$  is a more negative number.

"The displacement is governed by the first term of eqn (2).

$$y = A_1 e^{(-b + \sqrt{b^2 - \omega^2})t}$$

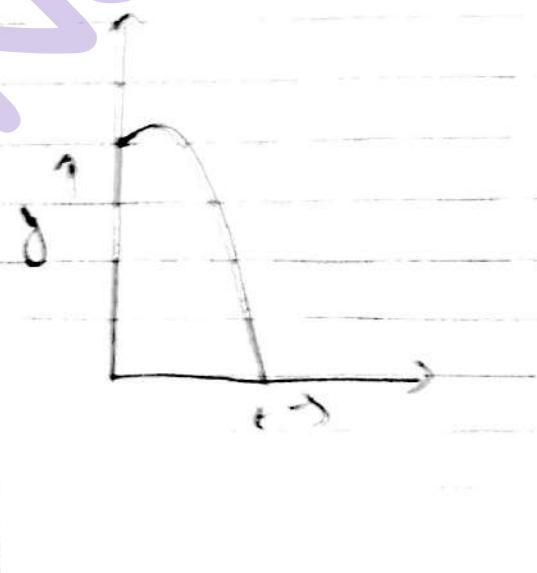
This eqn represent that with increase in time displacement will go on decreasing (As  $-b + \sqrt{b^2 - \omega^2}$  is a -ve no.)

So, in this case the displacement with respect to time can be shown in the graph as below.



Ques Define Half Time  
2. Explain Half Time  
3. Explain Half Time  
4. Explain Half Time  
5. Explain Half Time  
6. Explain Half Time  
7. Explain Half Time  
8. Explain Half Time

These are the Definitions of Half Time  
in Half Time Decay Law



iii) Underdamping ( $b < \omega$ ) :-

In this case  $\sqrt{b^2 - \omega^2}$  is an imaginary number.

Let,

$$\sqrt{b^2 - \omega^2} = i\beta$$

$$\beta = \sqrt{\omega^2 - b^2}$$

$$i = \sqrt{-1}$$

In this case, the general solution for displacement is as follows.

$$y = A_1 e^{(b + \sqrt{b^2 - \omega^2})t} + A_2 e^{(-b - \sqrt{b^2 - \omega^2})t}$$

$$\Rightarrow y = A_1 e^{(b + i\beta)t} + A_2 e^{(-b - i\beta)t}$$

$$\Rightarrow y = e^{-bt} \times (A_1 e^{i\beta t} + A_2 e^{-i\beta t})$$

$$\Rightarrow y = e^{-bt} \times [A_1 (\cos \beta t + i \sin \beta t) + A_2 (\cos \beta t - i \sin \beta t)]$$

$$\Rightarrow y = e^{-bt} [(A_1 + A_2) \cos \beta t + i(A_1 - A_2) \sin \beta t]$$

$$\text{Let } (A_1 + A_2) = \sin \phi$$

$$i(A_1 - A_2) = \cos \phi$$

Under this assumption,

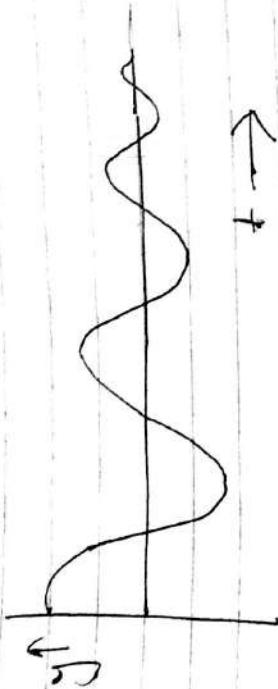
$$\Rightarrow y = e^{-bt} [\sin \phi \cos \beta t + \cos \phi \sin \beta t]$$

$$\Rightarrow y = e^{-bt} \sin(\beta t + \phi)$$

$\rightarrow$  Soln for displacement in underdamping condition.

From this equation, it is clear that in the underdamping condition, the displacement will be oscillatory with decreasing amplitude.

This can be represented as follows:-



This oscillation have angular frequency  $\beta$ .  
Let the time period  $T'$

$$\Rightarrow \frac{2\pi}{T'} = \beta$$

$$\therefore T' = \frac{2\pi}{\beta}$$

$$\Rightarrow T' = \boxed{\frac{2\pi}{\sqrt{\omega^2 - \beta^2}}}$$

From this expression it is clear that the time period of oscillation increases.

### ③ Forced Oscillation :-

When a body is capable of oscillation is subjected to external periodic force then the body oscillates with the frequency other than the natural frequency. Such type of oscillation is called as forced oscillator. When a body is subjected to forced oscillation, the oscillation in presence of damping then it experiences

the following forces:-

- (i) Inertial force
- (ii) Restoring force
- (iii) Damping force
- (iv) External force.

### (i) Inertial force :-

Inertial force is directly proportional to acceleration.

$$F_I = M \frac{dy}{dt^2}, \text{ where } m = \text{mass of oscillating body}$$

$y$  - displacement,

### (ii) Restoring force :-

Once the body is displaced from the equilibrium position, it has tendency to come back to equilibrium position. It is opposite and proportional to displacement.

$$F_R = -Ky, \quad k = \text{gain/restoring constant.}$$

### (iii) Damping force :-

This force tends to oppose the motion. It is directly proportional to the velocity and is given by:-

$$F_D = -rdy \quad , \quad r = \text{damping const.}$$

### (iv) External force :-

The periodic external force can be defined as.

$$F_{ext} = F \sin pt, \quad \text{where}$$

$F$  = Amplitude of ext. force

$p$  = Angular freq of ext. force

In equilibrium condition,

$$F_I = F_R + F_D + F_{Ex}$$

$$\Rightarrow m \frac{d^2y}{dt^2} = -ky - \frac{dy}{dt} + F_{\text{sinpt.}}$$

$$\Rightarrow M \frac{d^2y}{dt^2} + \frac{ky}{m} \frac{dy}{dt} + ky = F_{\text{sinpt.}}$$

$$\Rightarrow \frac{d^2y}{dt^2} + \left(\frac{k}{m}\right) \frac{dy}{dt} + \left(\frac{k}{m}\right)y = \left(\frac{F}{m}\right)_{\text{sinpt.}}$$

$$\Rightarrow \boxed{\frac{d^2y}{dt^2} + 2b \frac{dy}{dt} + \omega^2 y = f_{\text{sinpt.}}}$$

$$2b = \frac{1}{m}, \omega^2 = \frac{k}{m}$$

→ Equation of motion for forced oscillation in presence of damping.

The solution of above equation can be as follows:

$$|y = A \sin(pt - \phi)|$$

where  $A$  = Amplitude of forced oscillation

$$A = \frac{f}{\sqrt{(\omega^2 - p^2)^2 + 4b^2 p^2}}$$

$\phi$  = phase lag between displacement and applied force.

Generally, when there is external force is there the body takes some time to follow it. This time is reflected in terms of phase lag.

Generally,  $\phi$  is given by,

$$\boxed{\phi = \tan^{-1} \left( \frac{2Bp}{w^2 - p^2} \right)}$$

### Amplitude Resonance :-

This is a condition of forced oscillations where the amplitude is extremely large.

### Derivation of Condition for Amplitude Resonance :-

We know in forced oscillation,

$$A = \frac{f}{\sqrt{(w^2 - p^2)^2 + 4b^2 p^2}}$$

for maximum value of A (Amplitude Resonance)

$$\frac{d}{dp} [(w^2 - p^2)^2 + 4b^2 p^2] = 0$$

$$\boxed{p = \sqrt{w^2 - 2b^2}} \rightarrow \text{cond for resonance.}$$

$$\Rightarrow 2(w^2 - p^2) \times \frac{d}{dp} (w^2 - p^2) + 8b^2 p = 0$$

$$\boxed{p = \sqrt{w^2 - 2b^2}} \rightarrow \text{cond of resonance in absence of damping}$$

If no damping, i.e.  $b = 0$

$\Rightarrow [p = \omega] \rightarrow$  cond<sup>n</sup> of resonance p.  
absence of damping

expression for amplitude in resonance condition

We know

$$A = \frac{f}{\sqrt{(B^2 - (\omega^2 - p^2))^2 + 4b^2 p^2}}$$

In the resonance cond<sup>n</sup>,  $p^2 = \omega^2 - 2b^2$

$$A_{res} = A_{max} = \frac{f}{\sqrt{(\omega^2 - \omega^2 + 2b^2)^2 + 4b^2(\omega^2 - 2b^2)}}$$

$$\begin{aligned} &= \frac{f}{\sqrt{4b^4 + 4b^2\omega^2 - 8b^4}} \\ &= \frac{f}{\sqrt{4b^2\omega^2 - 4b^4}} \end{aligned}$$

$$A_{res} = A_{max} = \frac{f}{2b\sqrt{\omega^2 - b^2}}$$

expression for  
amplitude at  
resonance in  
presence of damping.

In absence of damping ( $b = 0$ )

$$A_{max} \rightarrow \infty$$

## Sharpness of Resonance

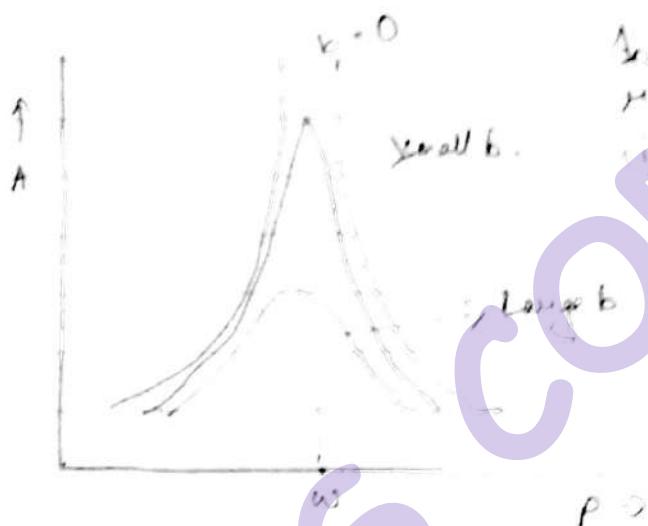
(B)

QUESTION

The rate of decrease of amplitude with respect to frequency of external force around natural frequency defines the sharpness of resonance.

More the rate of decrease of amplitude sharper is the resonance (sharpness of resonance).

The resonance can be graphically as the figure below



i. If the sharpness of resonance is

(i) maximum :  $b = 0$ ,  
sharpness decreases,  
for increasing  $b$ .

ii) for large value of  $b$   
resonance get flattened down.  
For useful application  
one needs sharp resonance

P:

Q) Formulate the eq' of motion for forced oscillation (damping)  
(i) write down general sol. of amplitude  
(ii) Discuss geo amplitude record.

Q) What do you mean by sharpness of resonance

## Waves

Differential form of wave equation :-

Let, a wave is represented by the equation

$$y = A \sin(\omega t + kx)$$

here  $A$  = Amplitude

$$\omega = 2\pi f$$

$\omega \rightarrow$  freq. of wave

$$k = \frac{2\pi}{\lambda}$$

$\lambda \rightarrow$  wavelength  
wave

$$\frac{dy}{dt} = \omega A \cos(\omega t + kx)$$

$V = \lambda f = \text{velocity of wave}$

$$\frac{dy}{dt} = A \cos(\omega t + kx) \left[ 1 + \frac{dx}{dt} \right]$$

$$\boxed{\frac{d^2y}{dt^2} = -\omega^2 y} \quad \text{--- (1)}$$

$$\frac{dy}{dx} = kA \cos(\omega t + kx)$$

$$\frac{d^2y}{dx^2} = -k^2 A \sin(\omega t + kx)$$

$$\boxed{\frac{d^2y}{dx^2} = -k^2 y} \quad \text{--- (2)}$$

$$\Rightarrow \frac{\left(\frac{d^2y}{dt^2}\right)}{\left(\frac{d^2y}{dx^2}\right)} = \left(\frac{\omega}{k}\right)^2$$

$$\Rightarrow \frac{d^2y}{dt^2} = \left(\frac{2\pi f}{\lambda}\right)^2 \left(\frac{d^2y}{dx^2}\right)$$

$$\Rightarrow \frac{d^2y}{dt^2} = v^2 \frac{d^2y}{dx^2}$$

$$\Rightarrow \frac{d^2y}{dt^2} = \frac{d^2y}{dx^2} = \frac{1}{v^2} \frac{d^2y}{dt^2} \rightarrow \text{diff. eqn of wave.}$$

*v = velocity of wave.*

~~08-12-16~~

## Interference

The redistribution of energy or intensity due to superposition of two coherent sources/waves is called as interference.

### Cohherent waves :-

Two waves having same wavelength and frequency and a constant phase difference are called as coherent waves or coherent wave source

### Example of coherent sources :-

- Two coherent sources can be generated from a single source of <sup>monochromatic</sup> light like Sodium lamp.
- Two independent sources can never be coherent.

The coherent sources can be generated from a single source by the principle of division of amplitude.

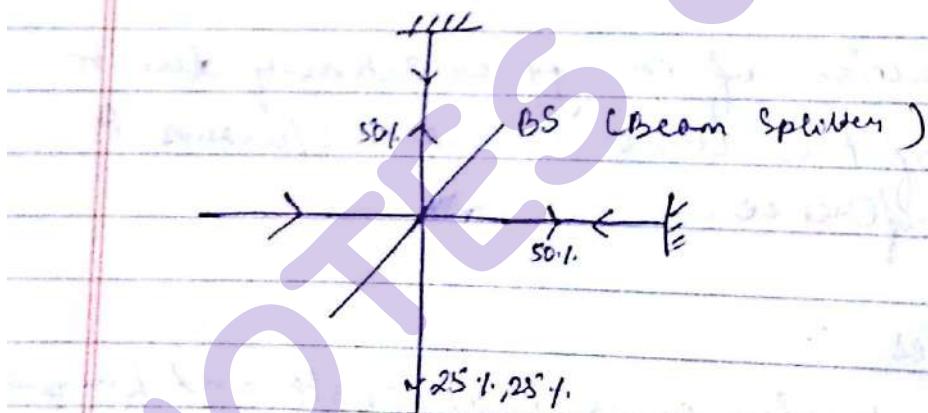
& (ii) division of wavefront

Division of amplitude:-

Notes

Michelson Interferometer is based on Newton's Ring and division of amplitude. In this type of experiment two coherent sources are created by division of amplitude.

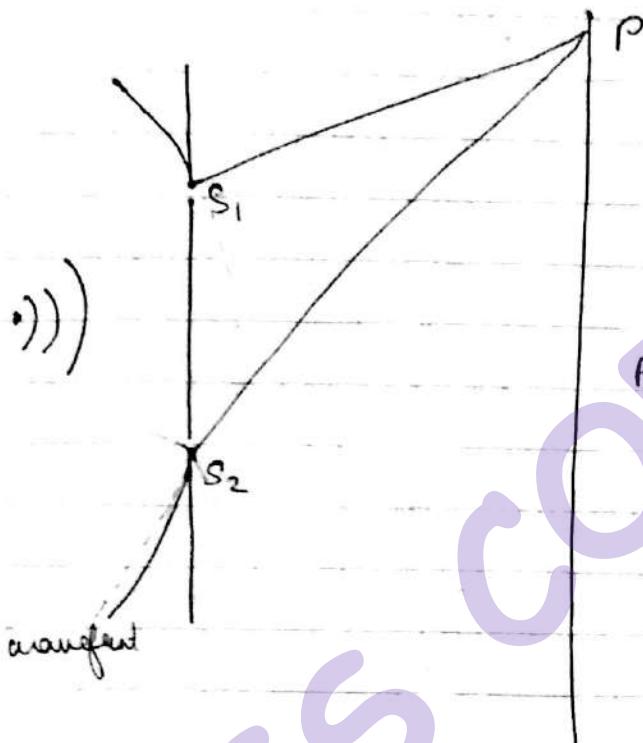
Michelson Interferometer:-



Schematic diagram of MI.

Division of waveform :-

Young's Double Slit Expt. is one example of Interference due to division of waveforms.



$$\text{Path diff } S_2P - S_1P$$

$$\text{Phase diff} = \frac{2\pi}{\lambda} \times \text{path diff}$$

\* Analytical Treatment of Interference. ~~Derivation of~~

Derivation for resultant intensity,  
Condition for maxima & minima,  
Energy distribution curves in interference, etc.

Derivation of resultant intensity in Interference

Consider two waves coherent wave sources as follows.

$$y_1 = a_1 \sin(\omega t)$$

$$y_2 = a_2 \sin(\omega t + \delta)$$

$\delta$  = phase difference.

The resultant wave due to superposition of

$$y = y_1 + y_2 \quad (\text{Superposition principle})$$

$$y = a_1 \sin(\omega t) + a_2 \sin(\omega t + \delta)$$

$$y = a_1 \sin(\omega t) + a_2 \sin(\omega t) \cos \delta + a_2 \cos(\omega t) \sin \delta$$

$$y = \sin \omega t (a_1 + a_2 \cos \delta) + \cos \omega t \cdot a_2 \sin \delta$$

Let  $a_1 + a_2 \cos \delta = R \cos \phi \quad \text{--- } ①$

$$a_2 \sin \delta = R \sin \phi \quad \text{--- } ②$$

$$\Rightarrow y = R(\sin \omega t \cos \phi + \cos \omega t \sin \phi)$$

$$\Rightarrow \boxed{y = R \sin(\omega t + \phi)} \rightarrow \text{Resultant wave is eq}$$

Squaring and adding ① & ②,

$$\Rightarrow a_1^2 + a_2^2 \cos^2 \delta + a_2^2 \sin^2 \delta =$$

$$\Rightarrow a_1^2 + a_2^2 \cos^2 \delta + 2a_1 a_2 \cos \delta + a_2^2 \sin^2 \delta = R^2$$

$$\Rightarrow a_1^2 + a_2^2 + 2a_1 a_2 \cos \delta = R^2$$

$$\therefore \boxed{R^2 = a_1^2 + a_2^2 + 2a_1 a_2 \cos \delta}$$

Generally  $R^2$  is the Intensity (I).  
So resultant intensity for Interference is

$$\therefore \boxed{I = a_1^2 + a_2^2 + 2a_1 a_2 \cos \delta} \rightarrow \text{Resultant Intensity}$$

$$\therefore I = I_1 + I_2 + 2\sqrt{I_1 I_2} \cos \delta \quad | \text{ hence,}$$

$I_1, I_2 \rightarrow$  Intensity of 1st and 2nd wave respectively.

Condition for Maxima :-

We know in Interference the resultant intensity is given by,  $I = I_1 + I_2 + 2\sqrt{I_1 I_2} \cos \delta$ .

$$I = a_1^2 + a_2^2 + 2a_1 a_2 \cos \delta.$$

For  $I$  to be maximum,  $\cos \delta = 1$ .

$$\cos \delta = 1 \\ \Rightarrow \boxed{\delta = 2n\pi} \quad (n=0, \pm 1, \pm 2, \dots)$$

→ Condition for maximum in interference in terms of phase difference.

09-12-16

We know,

$$\delta = \frac{2\pi}{\lambda} \times \text{path diff.}$$

$$\therefore \frac{2\pi}{\lambda} \times \text{path diff.} = 2n\pi$$

$$\Rightarrow \boxed{\text{path difference} = 2n \times \frac{\lambda}{2}}$$

→ Condition for maxima in terms of path difference.

Condition for Minima :-

The intensity will be minimum for the condition

$$\cos \delta = -1$$

$$\Rightarrow \boxed{\delta = (2n+1)\pi} \quad \rightarrow \text{Condition for minima in interference in terms of phase difference.}$$

$(n = 0, 1, 2, \dots)$

$$\text{if } a_1 = a_2 = a$$

$$\text{Leverage max} \leftarrow \boxed{T_{\max} = (a_1 + a_2)^2}$$

$$T_{\max} = a_1^2 + a_2^2 + 2a_1a_2$$

$$\cos \theta = 1$$

for maximum

$$E = a_1^2 + a_2^2 + 2a_1a_2 \cos \theta$$

We have

Magnitude Idemally

$$\frac{\pi}{2}(n+1) \times \text{part area} : \text{the part}$$

$$T(n+1) = \text{part area} \times \sum_{i=1}^{n+1} \text{part}$$

we know

OD

## Intensity of Minima

$$I = a_1^2 + a_2^2 + 2a_1 a_2 \cos \delta.$$

for minima,

$$\cos \delta = -1$$

$$\therefore I_{\min} = a_1^2 + a_2^2 - 2a_1 a_2 \cos \delta$$

$\Rightarrow I_{\min}$

$$\Rightarrow [I_{\min} = (a_1 - a_2)^2] \rightarrow \text{min intensity.}$$

If  $a_1 = a_2 = a$ ,

$$\Rightarrow [I_{\min} = 0]$$

It is clear that

$$[I_{\min} < I_1 + I_2]$$

## Condition for sustainable interference :-

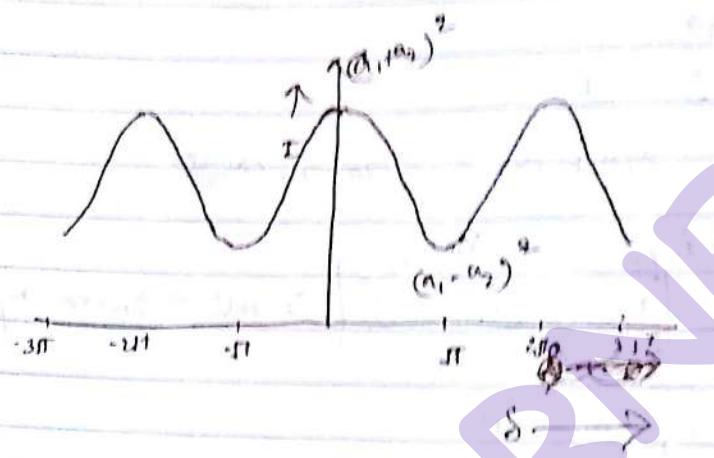
- The interfering sources should be coherent.
- The polarization of two coherent sources should be same.

## Condition for good contrast :-

- The amplitude of the interfering waves should be same for good contrast.
- The interfering sources should be point source.

Date \_\_\_\_\_

Energy / Intensity distribution curve with respect to phase difference in Interference :-



a) Show that energy is conserved in Interference.

Ans: The average Intensity in Interference over a cycle of phase difference

( $\delta$ : 0 to  $2\pi$ )

is given by,

$$I_{avg} = \frac{\int_0^{2\pi} I d\delta}{\int_0^{2\pi} d\delta}$$

$$= \frac{\int_0^{2\pi} (a_1^2 + a_2^2 + 2a_1 a_2 \cos \delta) d\delta}{\int_0^{2\pi} d\delta} = \frac{2\pi (a_1^2 + a_2^2)}{2\pi}.$$

$$= \cancel{[a_1^2 \cancel{\delta}]_0^{2\pi} + \cancel{[a_2^2 \cancel{\delta}]_0^{2\pi}}} + a_1^2 + a_2^2$$

So, the average intensity both in case of interference is constant (irrespective of Interference or absence of interference).

∴ The energy is conserved in interference.

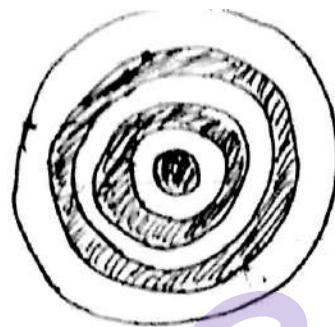
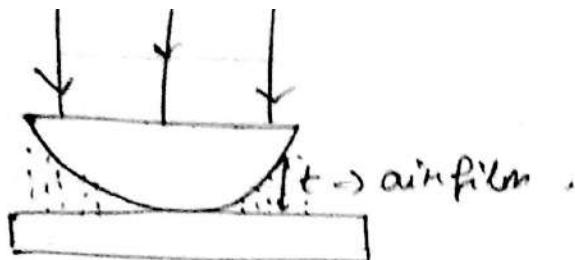
### B-12-16 Newton's Rings

When the combination of plane convex lens and glass plate (convex side in contact with glass plate ~~because~~ of curvature is large) is illuminated by monochromatic light. Then concentric light and dark ring appears in the air film enclosed between plane convex lens and glass slab. These concentric rings alternative bright and dark rings are called as Newton's Rings.

When monochromatic light fall on the glass plate combination of glass plate and plane convex lens, then there will be two reflected rays from the top and bottom of air film enclosed. These reflected light can superpose giving rise to Newton's ring.

The thickness of the film decide the maxima or minima i.e. bright and dark fringe. In this case locus of all the points having same thickness is a circle.

Therefore the fringes (bright/dark) are circular in nature.



(CNR in reflective mode)

Condition for bright ring :-

In the air film reflection, the path difference between the reflected rays is given by,

$$\text{path difference} = 2nt \cos(\theta + n) + \frac{\lambda}{2}$$

Here  $\theta$  = Angle of wedge shaped film enclosed between plane concave lens and glass lens.

For large radii of curvature  
 $\theta \rightarrow 0$ .

$n$  = Angle of refraction  
 for normal incident  $n \rightarrow 0$ .  
 So the path diff betn the two interfering waves is given by

$$\text{path diff} = 2nt \cos 0^\circ + \frac{\lambda}{2}$$

$$\boxed{\text{path diff} = 2nt + \frac{\lambda}{2}}$$

$$\rightarrow \left[ 2vt - (n+1) \frac{\lambda}{2} \right], n \text{ int}$$

$\rightarrow$  cond<sup>n</sup> for bright ring

Condition for dark ring :-

For minima or dark ring condition :-

$$\text{path diff.} = (2n+1) \frac{\lambda}{2}$$

$$\Rightarrow 2vt + \frac{\lambda}{2} = (2n+1) \frac{\lambda}{2}$$

$$\Rightarrow \boxed{2vt = 2n \frac{\lambda}{2}} \rightarrow \text{cond<sup>n</sup> for dark ring}$$

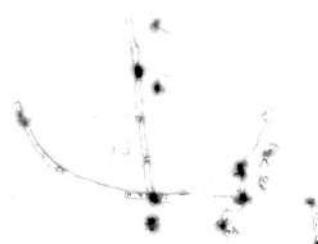
Derivation of expression for diameter of Widén Ring

Consider a circular slit shown in the figure below -

The radius of curvature of this slit will be equal to radius of curvature of place wave front.

Let  $r_0$  be the radius of

place wave front



In this case geometrical analysis is not possible but  $\sin i = \sin r$

$\Rightarrow \tan i = \frac{r}{r_0}$  Now  $i$  is called angle of semi-aperture &  $r$  is radius of semi-aperture.

$$\Rightarrow 2Rt - t^2 = P_n^2$$

$$\Rightarrow 2Rt = P_n^2$$

$$\Rightarrow 2t = \frac{P_n^2}{R}$$

$$\Rightarrow \boxed{2t = \frac{D_n^2}{4R}} \quad - \textcircled{1}$$

Expression for bright ring

We know the condition for  $n^{th}$  order bright

$$2t = (2n-1) \frac{\lambda}{2} \quad - \textcircled{2}$$

From eq<sup>n</sup>  $\textcircled{1}$  &  $\textcircled{2}$ .

We have,

$$\frac{D_n^2}{4R} = \frac{(2n-1)\lambda}{2}$$

$$\Rightarrow \boxed{D_n^2 = 2(2n-1)R\lambda}.$$

$$\Rightarrow \boxed{D_n = \sqrt{2n-1} \times \sqrt{2R\lambda}}$$

$$\Rightarrow \boxed{D_n \propto \sqrt{\text{odd no.}}}$$

$$\boxed{D_n \propto \sqrt{R}}$$
$$\boxed{D_n \propto \sqrt{\lambda}}$$

So, diameter of bright ring is directly proportional to square root of R and wavelength.

Date \_\_\_\_\_  
Page \_\_\_\_\_

$\odot$

My companion

of odd number. It is also directly proportional to square root of radius of curvature of plane-convex lens. and also  $\propto \sqrt{\text{wavelength}}$ .

Expression for dark ring :-

We condition for  $n^{\text{th}}$  dark ring is,

$$2t = \frac{2n\lambda}{2} \quad \text{--- (3)}$$

Comparing eqn ① & ③,

$$\Rightarrow \frac{D_n^2}{4R} = 2n \frac{\lambda}{2}$$

$$\Rightarrow \cancel{D_n^2 = 2n \times 2R\lambda} \quad \Rightarrow D_n^2 = 4nR\lambda$$

$$\Rightarrow \cancel{D_n = \sqrt{2n} \times \sqrt{2R\lambda}} \quad \Rightarrow D_n = 2\sqrt{n} \sqrt{R\lambda}$$

$$\begin{cases} D_n \propto \sqrt{n} \\ D_n \propto \sqrt{R} \\ D_n \propto \sqrt{\lambda} \end{cases}$$

SD, the diameter of dark Newton ring is directly proportional to sq. root of natural no, and like bright ring there are also proportional to sq. root of R &  $\lambda$ .

Q) In a given experimental set up of Newton's Ring

$$R = 200 \text{ cm}$$

$$\lambda = 5893 \text{ Å}$$

Find out diameter of ① 3rd bright ring  
 ② 3rd dark ring

$$\textcircled{1} (D_n)_b = \sqrt{2n-1} \times \sqrt{2R\lambda}$$

$$D_3 = \cancel{\sqrt{5}} \times 153.5$$

$$(D_3)_b =$$

$$(D_3)_b = 0.342 \text{ cm}$$

$$\textcircled{2} (D_n)_d = 2\sqrt{n} \sqrt{R\lambda}$$

$$(D_3)_d =$$

$$= 0.378 \text{ cm}$$

Q) In the Newton's Ring expt. containing plano convex lens of radius of curvature 200 cm, the diameter of 9th order bright ring is 1.5 cm : find out the wavelength of the light source.

$$(D_9)_b = \sqrt{17} \times \sqrt{2 \times 200 \times \lambda}$$

$$1.5 = \sqrt{17} \times \sqrt{400 \lambda}$$

$$1.5 = 17 \times 400 \lambda \Rightarrow \lambda = 3.3 \times 10^{-4} \text{ cm}$$

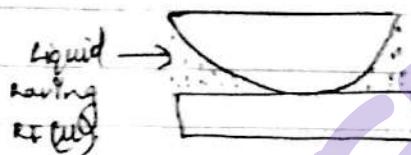
$$\Rightarrow \lambda = 3.3 \times 10^{-6} \text{ A}$$

Diameter of Newton Ring in presence of liquid film :-

In presence of liquid, the condition for bright ring is

$$2\mu t + \frac{\lambda}{2} = 2n \frac{\lambda}{2}$$

$$\Rightarrow 2\mu t = \frac{(2n-1)\lambda}{2}$$



$$\Rightarrow \frac{D_n^2}{4R} = \frac{(2n-1)\lambda}{2\mu}$$

$$\Rightarrow D_n^2 = \frac{2(2n-1)R\lambda}{\mu}$$

$$\Rightarrow (D_n)_{\text{liquid}} = \frac{1}{\sqrt{\mu}} \sqrt{2(2n-1)} \text{ times}$$

$$\Rightarrow (D_n)_{\text{liquid}} = \frac{(D_n)_{\text{air}}}{\sqrt{\mu}}$$

In presence of liquid diameter of ring is decreased by  $\frac{1}{\sqrt{\mu}}$  times.

- Q) By introducing liquid the diameter of Newton's ring for a given order reduced by 2 times find RI of liquid.

Ans:

$$\frac{(D_n)_{\text{air}}}{2} = \frac{(D_n)_{\text{air}}}{\sqrt{\mu}}$$

$$\Rightarrow \underline{\underline{\mu = 4}}$$

- Q) The phase difference between two coherent sources is  $60^\circ$ . What will be the resultant Intensity if Amplitude of each coherent source is 1 S.I unit.

$$I = a_1^2 + a_2^2 + 2a_1a_2 \cos \delta.$$

$$\Rightarrow I = 2 + 2 \cos 60^\circ$$

$$\Rightarrow I = 2 + 1$$

$$\therefore I = 3 \text{ SI. unit}$$

- Q) The path difference between two interfering waves is  $\frac{\lambda}{4}$ . What will be the resultant Intensity of Interference if ampl. of each wave is a.

$$2Mt + \frac{\lambda}{2} = \frac{\lambda}{4}$$

$$\Rightarrow 2Mt = \frac{\lambda}{4} - \frac{\lambda}{2} =$$

~~$$\cos \phi = \frac{2\pi}{\lambda} \times \frac{\lambda}{4}$$~~

$$\phi = \frac{2\pi}{\lambda} \times \frac{\lambda}{4} \Rightarrow \phi = \frac{\pi}{2}$$

$$I = a_1^2 + a_2^2 + 2a_1a_2 \cos \frac{\pi}{2} = 2a^2.$$

$$\begin{aligned} & \cancel{\frac{(D_{n+1}) - (D_n)}{\sqrt{2n+1} - \sqrt{2n-1}}} \\ & \cancel{\left( \frac{\sqrt{2n+1} - \sqrt{2n-1}}{\sqrt{2n+3} - \sqrt{2n-1}} \right) \cdot \frac{\sqrt{2n+3} * \sqrt{2n+1} * \sqrt{2n-1}}{\sqrt{2n+1} - \sqrt{2n-1}}} \\ & q(D_{n+1}) - q(D_{n+2}) \end{aligned}$$

$$= \left( \frac{1 - \sqrt{2n+1}}{1 + \sqrt{2n+1}} \right) \sqrt{2n+1}$$

$$Y_{def} \frac{1 - v_C}{1 + v_C} = Y_{def} \times \frac{1 + v_C}{1 + v_C}$$

$$(D^{n+1})^b - (D^n)^b$$

$$\frac{\partial \phi}{\partial x} + \int_{x_0}^x \psi(u) du = \phi(x)$$

$$\frac{1}{\sqrt{2n+1}} \times \sqrt{2n+1} =$$

$$\frac{1}{2\pi i} \times \int_{C_{n+1}} = \int_{C_n} \quad (1)$$

$$\text{Var}(\hat{\beta}_1) = \frac{1}{n-2} \sum_{i=1}^n (y_i - \hat{y}_i)^2$$

(a) Shows that with width of Nucleon:  $R_N = \frac{1}{2} R_{\text{had}}$   $\Rightarrow$   $R_N = \frac{1}{2} R_{\text{had}} = \frac{1}{2} R_{\text{had}} \cdot \frac{1}{2} R_{\text{had}} = \frac{1}{4} R_{\text{had}}^2$

<sup>n<sup>th</sup> order</sup>  
Ans: Consider the width of dark ring  
It is as follows:-

$$\beta = D_{n+1} - D_n$$

$$= 2\sqrt{R\lambda} \times (\sqrt{n+1} - \sqrt{n})$$

$$= 2\sqrt{R\lambda} \sqrt{n} \left[ \left( 1 + \frac{1}{n} \right)^{1/2} - 1 \right]$$

$$= 2\sqrt{R\lambda} \times \sqrt{n} \left[ 1 + \frac{1}{2n} - 1 \right]$$

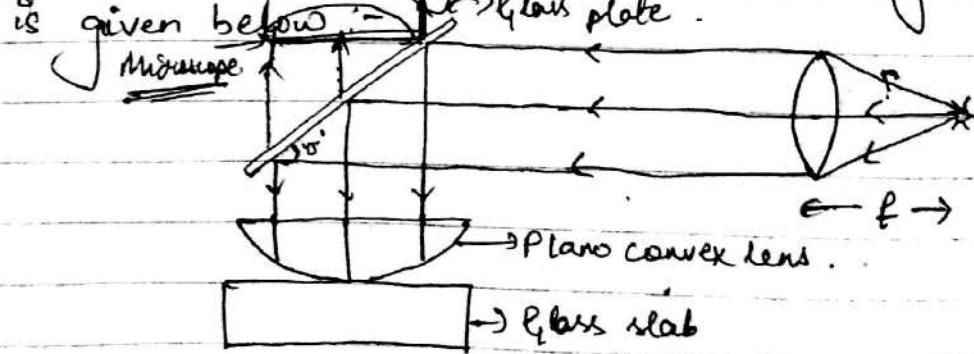
$$= \frac{2\sqrt{R\lambda}}{2\sqrt{n}}$$

$$= \frac{\sqrt{RT}}{\sqrt{n}}$$

$$\Rightarrow \beta \propto \frac{1}{\sqrt{n}}$$

Experimental arrangement for Newton's Ring :-

The schematic diagram of Newton's Ring experiment is given below :-



In this case the polarized beam of monochromatic light

To be viewed to fall on a glass plate kept at angle  $45^\circ$   
The reflected beam fall normally on the combination  
of plane convex lens and glass plate.

Two coherent beams or rays generated due to reflection  
from opposite laser interface of air film enclosed in  
between plane convex

These coherent sources interfere to give alternative  
dark and bright Newton's ring in air film.  
These rings are viewed by a microscope.

Determination of Wavelength by Newton's ring expt.

In the Newton's ring expt., the schematic diagram  
shown in above section is followed to form the Newton's  
Ring.

The diameter of  $n^{\text{th}}$  order dark ring in this case  
is given by

$$D_n^2 = 4Rn\lambda \quad \text{--- (1)}$$

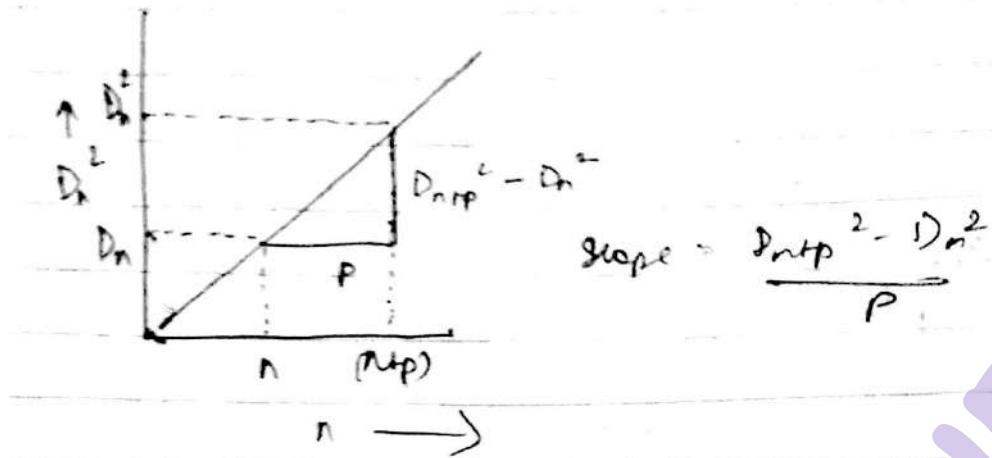
& square of diameter of  $n^{\text{th}}$  order  $(n+p)^{\text{th}}$  order ring  
is given by

$$D_{n+p}^2 = 4R(n+p)\lambda \quad \text{--- (II)}$$

$$\Rightarrow D_{n+p}^2 - D_n^2 = 4Rp\lambda$$

$$\Rightarrow \lambda = \frac{1}{4R} \left( \frac{D_{n+p}^2 - D_n^2}{p} \right) \quad \text{--- (III)}$$

From eqn (1), it is clear that the graph between  
 $D_n^2$  and  $n$  is a straight line as shown below:-



From eqn (11),

$$\lambda = \frac{l}{4R} \times \text{slope} \quad \rightarrow \text{Working formula.}$$

In this expt. diameters of various order of rings are determined by using the travelling microscope.

For this, the position (right hand side) for different order ring in left hand side are noted and the difference of this reading gives the value for diameter for different order. Finally the graph is plotted betw  $D_n^2$  and  $n$  to find out value of slope.

With the known value of  $R$  and measured value of slope one can measure the wavelength of the monochromatic light source.

Application of Newton's ring exp't for determination of RT

Working formula derivation

we know,

$$D_n^2 = \frac{4nR\lambda}{\mu} \quad \text{(for air)} \quad \text{--- (1)}$$

for liquid film.

$$D_n^2 = \frac{4nR\lambda}{\mu} \quad \text{--- (2)}$$

for  $(n+p)$  ring in presence of liquid

$$D_{n+p}^2 = \frac{4(n+p)R\lambda}{\mu} \quad \text{--- (3)}$$

Subtracting eqn (2) from (3)

$$\frac{(D_{n+p}^2 - D_n^2)_{\text{lip}}}{\mu} = \frac{4pR\lambda}{\mu}$$
$$\frac{(D_{n+p}^2 - D_n^2)_{\text{air}}}{\mu}$$

$$\Rightarrow \left[ \mu = \frac{(D_{n+p}^2 - D_n^2)_{\text{air}}}{(D_{n+p}^2 - D_n^2)_{\text{lip}}} \right] \rightarrow \text{working formula}$$

## Diffraktion :-

### Diffraktion :-

Bending of light or wave <sup>caused</sup> due to gravitational mass, when it comes across an obstacle or object whose size comparable to wavelength is called a diffraction.

The phenomena of bending of light.

This phenomena can be explained by taking Huygen's theory, which states that:-

Each part of a wavefront behaves as a source for secondary waves called wavelets. These wavelets superimpose each other to give phenomena of diffraction.

### Different types of diffraction :-

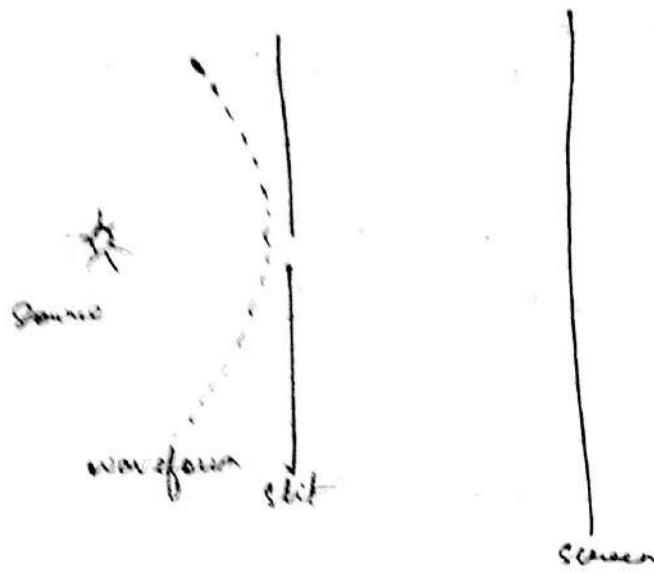
It is of two types:-

- (1) Fresnel diffraction
- (2) Fraunhofer diffraction.

#### (1) Fresnel diffraction :-

→ In this type of diffraction, the distance between source, slit and screen are finite.

→ In this case the wavefront hitting the slit is cylindrical or spherical in nature.



Q) Fraunhofer diffraction :-

- For this type of diffraction, the distance between source, slit and screen is infinite.
- In this case the wavefronts hitting slit is planar in nature.

Q) Show that superposition of  $n$  no. of waves with amplitude  $a$  and consecutive phase difference of  $\pi$  gives a resultant wave having amplitude  $R = \frac{a \sin(\frac{n\pi}{2})}{\sin(\frac{\pi}{2})}$ . (Th. Assignment - 2)

- (Q1) Distinguish between Fruenel and Fraunhofer diffraction.
- (Q2) What is diffraction and how it is different from interference of light.
- (Q3) Explain formation of Newton's ring. What will happen if the monochromatic light used is replaced with white light.
- (Q4) Why Newton's Rings are circular in nature?
- (Q5) Show that energy is conserved in interference phenomena.

### 1) Fruenel diffraction

- The distance b/w source, slit and screen are finite.
- Wavefront hitting the slit is either cylindrical or spherical in nature

### Fraunhofer diffraction

- The distance b/w source, slit and screen are infinite

→ Wavefront hitting the slit is planar in nature.

### 2) Diffraction

Bending of light or wave to the geometrical shadow region when it comes across an obstacle or slit of size comparable to its wavelength is called diffraction.

In interference of light, the energy is redistributed due to superposition of two coherent waves / sources but in diffraction each point of a waveform acts as a source for secondary waves (called as wavelets).

- 3) When the combination of plano-convex lens and glass plate is illuminated by monochromatic light. Then concentric bright and dark rings appear in the air film enclosed between convex lens and glass slab.
- 3) When monochromatic light fall on the combination of glass plate and plano convex lens, then there will be two reflected rays from the top and bottom of air film enclosed. These reflected light can superpose giving rise to Newton's ring.
- If monochromatic light is replaced by white light Newton's Rings are not formed as we know that Diameter of Newton's ring is directly proportional to square root of wavelength of light, but white light has wide range of wavelength, so Newton's ring becomes inconsistent and doesn't form Newton's ring.
- 4) The thickness of the air film decides the maxima or minima i.e. bright or dark fringe. In ~~the~~ the combination of plano convex lens and glass slab. The locus of points having same thickness is a circle.

5)

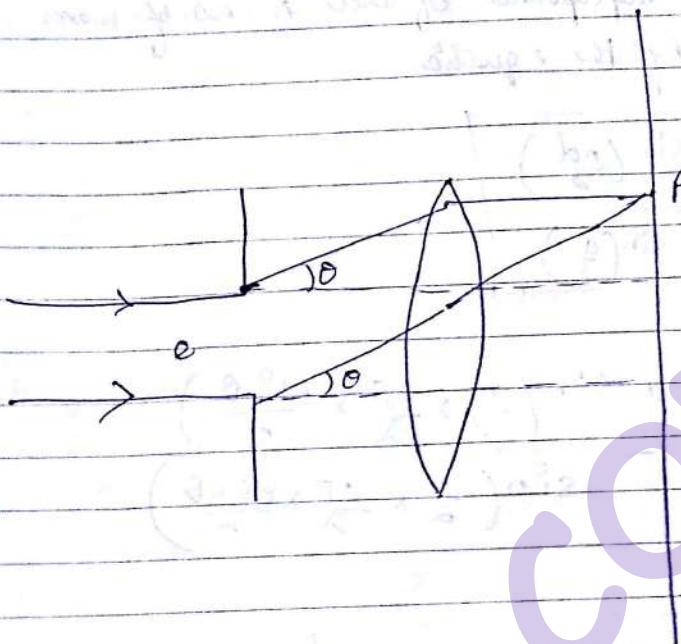
The average intensity in interference over a cycle of phase difference ( $\delta = 0 \text{ to } 2\pi$ ) is given by:-

$$\begin{aligned}
 I_{avg} &= \frac{\int_0^{2\pi} I d\delta}{\int_0^{2\pi} d\delta} \\
 &= \frac{\int_0^{2\pi} (a_1^2 + a_2^2 + 2a_1 a_2 \cos \delta) d\delta}{\int_0^{2\pi} d\delta} \\
 &= \frac{2\pi (a_1^2 + a_2^2)}{2\pi} \\
 &= a_1^2 + a_2^2
 \end{aligned}$$

So, the average intensity is constant (provided there is absence of interference).  
 As energy is conserved in interference.

## Fraunhofer diffraction for single slit :-

Consider a slit of dimension 'e' illuminated by collimated beam of light of wavelength  $\lambda$ . as shown in the figure below:-



Consider the wavefront hitting the slit is having  $n$  number of points. From these points  $n$  number of secondary wavelets will emerge and superpose at point  $P$  which is at an angle  $\theta$  with respect to angle of incident.

In this case the path difference between the wavelets coming from two extreme points of the slit is  $es \sin \theta$ . As there are  $n$  no. of points the path difference between the consecutive wavelets will be  $\frac{1}{n}(es \sin \theta)$ .

So, the phase difference between two consecutive waves is  $d = \frac{2\pi}{\lambda} \times \text{path difference}$

$$\text{path diff } (d) = \frac{2\pi}{\lambda} \times \frac{R \sin \theta}{n}$$

We know, that superposition of these  $n$ . no. of waves is represented by the equation -

$$\left[ R = \frac{a \sin \left( \frac{nd}{2} \right)}{\sin \left( \frac{d}{2} \right)} \right]$$

$$\Rightarrow R = \frac{a \sin \left( \frac{n}{2} \times \frac{2\pi}{\lambda} \times \frac{R \sin \theta}{n} \right)}{\sin \left( \frac{1}{2} \times \frac{2\pi}{\lambda} \times \frac{R \sin \theta}{n} \right)}$$

$$\Rightarrow R = \frac{a \sin \left( \frac{n \pi \sin \theta}{\lambda} \right)}{\sin \left( \frac{\pi \sin \theta}{\lambda n} \right)}$$

Let

$$\frac{\pi \sin \theta}{\lambda} = d$$

$$R = \frac{a \sin d}{\sin \left( \frac{d}{n} \right)}$$

$$R = \frac{a \sin d}{\left( \frac{d}{n} \right)} \quad \left( \because \frac{d}{n} = \text{small no.}, n \rightarrow \text{large} \right)$$

$$\left[ R = \frac{n a \sin d}{d} \right]$$

$$R = A \left( \frac{\sin \alpha}{\alpha} \right)$$

, where  $A = na$

This is the expression for resultant amplitude in single slit Fraunhofer diffraction.

Now, the resultant intensity in this case is

$$I = R^2$$

$$\Rightarrow I = A^2 \frac{\sin^2 \alpha}{\alpha^2}$$

Condition for maxima:-

For maxima,

$$\cancel{A^2} \cancel{\sin \alpha} = 1$$

$$\cancel{\alpha} = \frac{n\lambda}{2}$$

$$I = \frac{A^2}{n^2 \frac{\pi^2}{4}}$$

$$\Rightarrow I = \frac{4A^2}{n^2 \pi^2}$$

for maxima

We know the resultant amplitude is given by :-

$$R = A \left( \frac{\sin \alpha}{\alpha} \right)$$

This functn. is maxima when  $\alpha \rightarrow 0$

$$\text{As } R_{\max} = \lim_{\alpha \rightarrow 0} A \left( \frac{\sin \alpha}{\alpha} \right) = A$$

$$\boxed{R_{\max} = A}$$

So we can take condition for maxima as  
 $\alpha = 0$ . (in terms of phase).

$$\alpha = \frac{\pi e \sin \theta}{\lambda}$$

$$\frac{\pi e \sin \theta}{\lambda} = 0.$$

$$\Rightarrow \sin \theta = 0.$$

$$\Rightarrow \boxed{\theta = 0}$$

So, the maxima is lies along the direction of incident (i.e.  $\theta = 0$ ).  
This maxima is called as primary maxima or principal maxima.

Condition for minima :-

$$R = 0$$

$$\Rightarrow \frac{\sin \alpha}{\lambda} = 0$$

$$\Rightarrow \sin n\alpha = 0 \text{ as } \alpha \neq 0$$

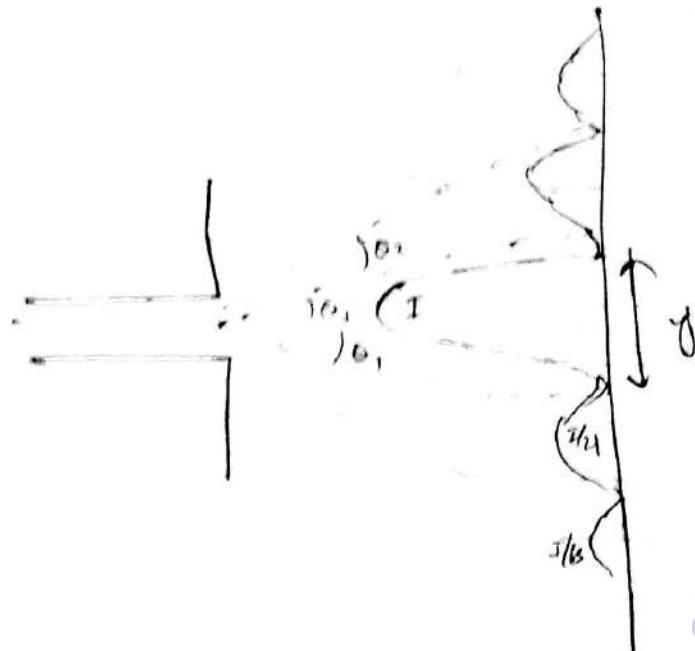
$$\Rightarrow \alpha = \pm n\pi \quad (n=1, 2, 3, \dots)$$

$$\frac{\pi e \sin \theta}{\lambda} = \pm n\pi$$

$$\Rightarrow \boxed{e \sin \theta = \pm n \lambda} \rightarrow \text{cond for minima in terms of physical parameters}$$

$n=1$  (1st order minima)

$$\boxed{e \sin \theta = \pm \lambda}$$



From this fig it is clear that there is present no. of minima defined as 1st order minima, 2nd order minima etc.

In between minima, there exist maxima. This means other than the principal maxima there exist other maxima called secondary maxima.

Q) In a Fraunhofer single slit expt. ~~size~~ of the slit is

~~size~~

$1 \times 10^{-3}$  cm. Find out the angular width of the primary maxima if the slit is illuminated by Sodium vapour lamp.

$$(\lambda = 5893 \text{ Å})$$

$$\text{Ans: } \sin \theta_1 = \frac{\lambda}{d}$$

$$\sin \theta_1 = \frac{5893 \times 10^{-8}}{1 \times 10^{-3}}$$

$$\sin \theta_1 = 5893 \times 10^{-5}$$

$$\theta_1 = 3.37^\circ$$

$$\therefore \underline{\theta_1 = 6.74^\circ}$$

So the angular width of central maxima is equal to  $2\theta_1 = 6.74^\circ$ .

(ii) If the diffraction pattern is observed by a screen kept at 1m apart from the slit. Then what will be the linear width of the 1st order maxima.

The linear width is  $2y$ , where  $y$  satisfies the relation

$$\tan \theta_1 = \frac{y}{l}$$

$$y = l \tan \theta_1$$

$$2y = 2l \tan \theta_1$$

$$2y = 2l \tan 32^\circ 7'$$

$$2y = 5.8 \text{ cm}$$

Secondary Maxima :-

The condition for secondary maxima can be found out from the following relation.

$$\frac{dI}{dx} = 0$$

$$\Rightarrow \frac{d}{dx} \left[ \frac{A^2 \sin^2 kx}{\lambda^2} \right] = 0$$

$$\Rightarrow \frac{d}{dx} \left[ \frac{\sin^2 kx}{\lambda^2} \right] = 0$$

$$\Rightarrow \frac{d \sin^2 kx}{dx} \frac{d \lambda^2}{dx} \text{ and } \frac{d \sin^2 kx}{dx} = 2 \sin kx \cos kx = 0$$

$$\Rightarrow 2x^2 \sin \alpha \cos \alpha - 2x \sin^2 \alpha = 0$$

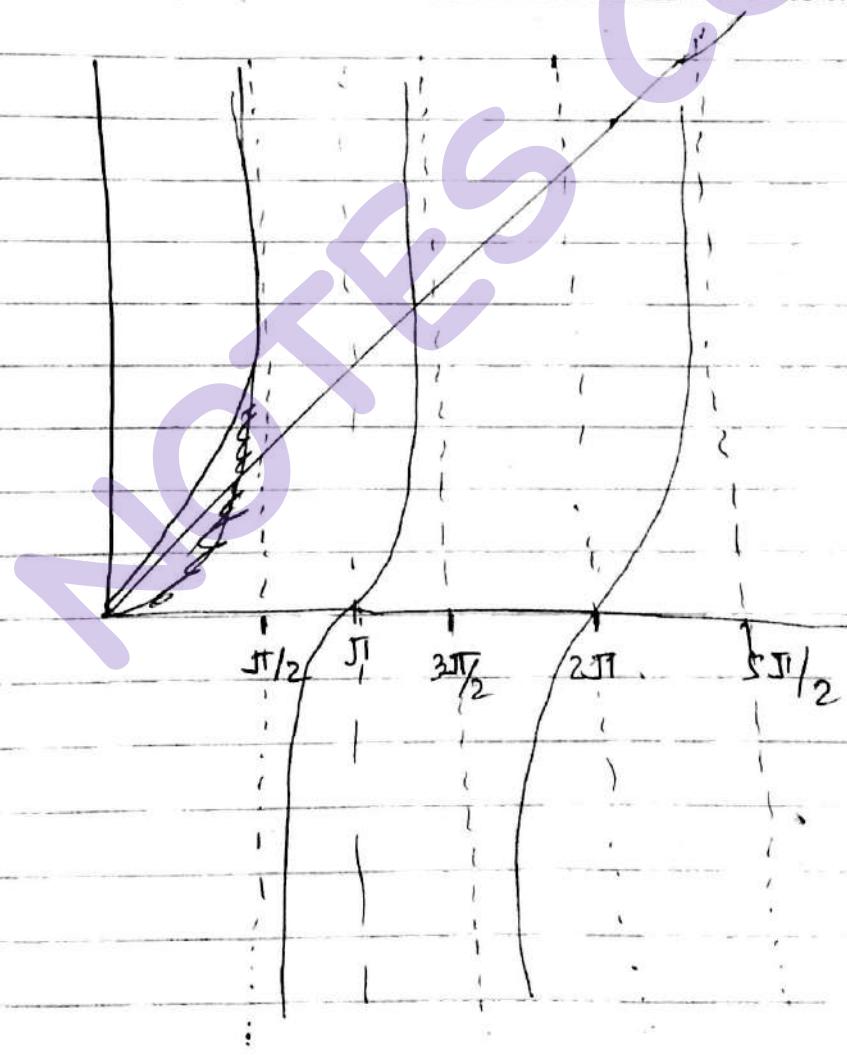
$$\Rightarrow 2x^2 \sin \alpha \cos \alpha = 2x \sin^2 \alpha$$

$$\Rightarrow x \cos \alpha = \sin \alpha$$

$\Rightarrow [x = \tan \alpha] \rightarrow \text{Condition for secondary maxima in Fraunhofer Single slit diffraction}$

The above eq<sup>n</sup> can be solved graphically by taking two equations.

$$\begin{aligned}y &= x \\ \text{and } y &= \tan \alpha\end{aligned}$$



From the graph it is clear that value of  $\alpha$  for various secondary maxima are

$$\alpha = \frac{\pi}{2}, \alpha = \pm 3, \pm 5$$

So, there are several secondary maxima.

~~$$\text{So, } \alpha = \pm \pi/2 \quad (n = 1, \text{ 1st order main maximum})$$~~

~~$$\alpha = \pm 3\pi/2 \quad (n = 3, \text{ 1st order secondary maxima})$$~~

~~Intensity of 1st order secondary maxima~~

We know,

$$I = \frac{A^2 \sin^2 \alpha}{\alpha^2}$$

~~$$I_{\text{sec}} = \frac{A^2 \sin^2(\pi/2)}{(\pi/2)^2}$$~~

~~$$I_{\text{sec}} = \frac{4A^2}{\pi^2}$$~~

~~Intensity of 1st order~~

Similarly

$$I_{SM_3} = \frac{4A^2}{25\pi^2}$$

So,

~~$I_{PM} \propto I_{SM_1} \propto I_S$~~

~~$I_{PM} : I_{SM_1} : I_{SM_2} : I_{SM_3}$~~

$$= 1 : \frac{4}{9\pi^2} : \frac{4}{9\pi^2} : \frac{4}{25\pi^2}$$

## Plane Diffraction Grating :-

A plane diffraction grating is an optical element consisting of large no. of slits of size comparable to the wavelength of the light incident on it. The slits are equispaced and equidimensional. The space between the slits is opaque.

The plane diffraction grating is generally fabricated by drawing large no. of parallel lines on the surface of a glass slide using diamond cutter. The lines in this case behave like opaque region and the region between two lines behaves like a slit.

If 'e' and 'd' are the dimension (width) of slit and opaque region respectively then (etd) is called as grating element.

(m)

$$\text{Grooving element} = \frac{15000}{8.54} = 1.69 \times 10^{-4} \text{ cm}$$

Ans: (i)

1st order Minima

$\lambda = 5893\text{A}$ ) what will be the angle for  
if the grooving is illuminated by sodium light

(ii) grooving element - Cm unit of cm.

15000 lines per inch. what will be the  
in a plane diffraction pattern there are

$$e + d = \frac{N}{8.54} \text{ cm}$$

$$e + d = \frac{N}{1} \text{ cm}$$

If we are N no. of lines per ~~inch~~ which ~~is~~  
plane diffraction grating then its grooving element is

grooving element is also defined as distance between the  
successive equivalent points of the grating  
could be the distance between two successive points

my companion \_\_\_\_\_

Q) If the size of a single slit is 5mm what will be the angle for 1st order minima (wavelength of Na light is used for diffraction exp.)

Ans:  $\sin \theta = \frac{\lambda}{d}$        $d = 0.5\text{cm}$

$$\sin \theta = \frac{\lambda}{d}$$

$$\theta = \sin^{-1} \left( \frac{\lambda}{d} \right)$$

$$= \sin^{-1} \left( \frac{5803 \times 10^{-9}}{5 \times 10^{-2}} \right)$$

$$= \sin^{-1} \left( \frac{5803 \times 10^{-9}}{5} \right)$$

$$= \sin^{-1} (1.17 \times 10^{-8})$$

$$= 6.75 \times 10^{-3}^\circ$$

Q) What is the value of angular width and linear width of Central Maxima (diffraction seen in a screen kept 1m apart)

Ans: Ang. Width =  $2\theta = 13.5 \times 10^{-3}^\circ$

For Linear Width

$$\tan \theta = \frac{y}{100}$$

$$y = 100 \tan \theta$$

$$y = 100 \tan (6.75 \times 10^{-3})$$

$$y = 0.017 = 1.17 \times 10^{-2} \text{ cm}$$

$$2y = 0.024 \text{ cm} \quad \underline{dy = 2.34 \times 10^{-2} \text{ cm}}$$

$$R = \frac{R' \sin\left(\frac{nd}{2}\right)}{\sin\left(\frac{d}{2}\right)}$$

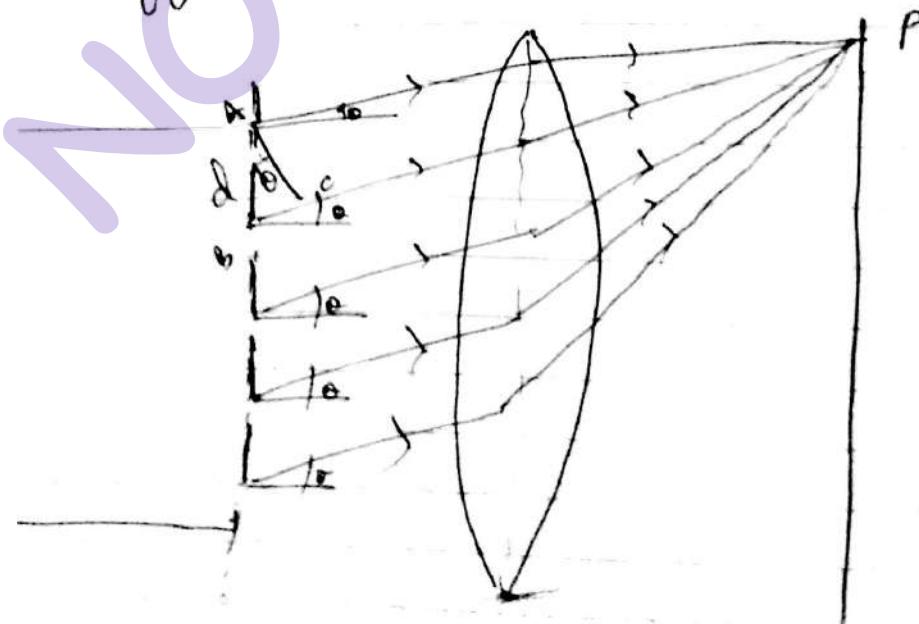
$$R = A \left( \frac{\sin x}{x} \right) \sin\left(\frac{nd}{2}\right)$$

$$d = (c + d) \cos \theta \times \frac{2\pi}{\lambda}$$

$$R = A \frac{\sin x}{x} \times \frac{\sin N\phi}{\sin \phi}$$

Analytical treatment of plane-diffraction grating:

Consider a plane diffraction grating as shown in the figure below



In this grating diffraction pattern, the maxima are separated by "aperture width of width  $a$ ".

Let a parallel beam is incident on it and  $n$  no. of slits are illuminated.

Due to diffraction at single slit, each slit will give a resultant wave of amplitude

$$R' = A \sin \frac{\alpha}{d}$$

For  $N$  no. of slits there will be  $N$  no. of waves which will again super-pose at point  $P$ . The resultant amplitude of the

~~These  $N$  no.~~ of the resultant wave at these super-positioner will be given by ~~the sum~~

$$R'' = R' \sin \left( \frac{Nd}{\lambda} \right)$$

Here,  $d$  = phase difference b/w two consecutive waves coming from two consecutive slits.

These phase differences can be given as

$$\text{phase diff. } d = \frac{2\pi}{\lambda} \times \text{path diff.}$$

$$d = \frac{2\pi}{\lambda} \times bc$$

$$= \frac{2\pi}{\lambda} \times (c + b) \sin \theta = 2\phi$$

Putting the value of  $R'$  and  $d$ ,

We get

$$R = A \left( \frac{\sin \alpha}{\alpha} \right) \left( \frac{\sin N\phi}{\sin \phi} \right)$$

$$\frac{2 \cdot R \sin^2 \theta}{\lambda}$$

This is the resultant amplitude due to Fraunhofer diffraction in diffraction grating.

So, the resultant intensity is given by

$$I = R^2 \Rightarrow I = A^2 \frac{\sin^2 \alpha}{\alpha^2} \frac{\sin^2 N\beta}{\sin^2 \beta}$$

Derivation of condition of maxima:-

Cond<sup>n</sup> for primary maxima is

$$\sin \beta = 0$$

$$\Rightarrow \beta = n\pi$$

$$\Rightarrow N\beta = N \times n\pi$$

$$\Rightarrow N\beta = P\pi$$

$$\Rightarrow \sin(N\beta) = \sin(P\pi) = 0$$

So, the cond<sup>n</sup> for primary maxima is

$$[P = n\pi]$$

$$\Rightarrow \frac{P(\text{etd}) \sin \theta}{\lambda} = n\pi$$

$$\Rightarrow [(\text{etd}) \sin \theta = n\lambda] \rightarrow \text{condition for primary maxima}$$

$n=0 \Rightarrow$  zeroth primary maxima

$n=\pm 1 \Rightarrow$  1st order ~~secondary~~ primary maxima

So,  
Intensity of primary maxima can be found out from the following limiting condition

$$\lim_{\beta \rightarrow 0^+} \left( \frac{2\pi r N \beta}{\sin \beta} \right)$$

$$\text{Ans} \quad \frac{2\pi r N \beta}{\sin \beta}$$

∴  $N$

∴ Amplitude of primary waves is given by:

$$R = \frac{4\pi r l}{\alpha} \times N$$

Now,

$$I = A^2 \frac{\sin^2 \theta}{d^2} \times N^2$$

Minima

for minima,  $I = 0$

$$\Rightarrow A^2 \frac{\sin^2 \theta}{d^2} \times \frac{2\pi r^2 N^2 \beta}{\sin^2 \beta} = 0$$

$$\Rightarrow \frac{\sin^2 N \beta}{\sin^2 \beta} = 0$$

$$\Rightarrow \frac{\sin N \beta}{\sin \beta} = 0$$

$$\Rightarrow \sin N \beta = 0 \text{ but } \sin \beta \neq 0$$

So, the condition for minima is

$$\boxed{\sin N \beta = 0 \text{ but } \sin \beta \neq 0}$$

$$\Rightarrow \sin N \beta = 0$$

$$\Rightarrow N \frac{\pi (c+d) \sin \theta}{\lambda} = m \pi$$

$\Rightarrow N(c+d) \sin \theta = m \lambda$  (Used for relation between no. of physical maxima)

$$\underline{\sin \theta = n} \rightarrow \text{transmitter, minima}$$

$$(c+d) \sin \theta = n \lambda \rightarrow P \text{ Maxima}$$

$$N(c+d) \sin \theta = m \lambda \rightarrow Q \text{ Minima}$$

From the condition of principal maxima and principal minima it is clear that (Q2)(Q) it is clear that in between two primary maxima there will be (N-1) no. of minima. This also establishes that there will be (N-2) secondary maxima if not between two consecutive primary maxima.

### $\Rightarrow$ Secondary Maxima

The condition for secondary maxima can be derived from the following relation:

$$\frac{dI}{dB} = 0$$

$$\Rightarrow \frac{d}{dB} \left( A^2 \sin^2 \frac{2\pi}{\lambda} c \sin \theta \right) = 0$$

$$\Rightarrow \frac{d}{dp} \left( \frac{\sin \alpha p}{\cos \beta p} \right) = 0$$

∴ ~~at  $\sin \alpha p = \cos \beta p$~~

$$\Rightarrow \frac{2 \sin^2 \alpha p \cos \beta p \sin^2 \beta - \cos \beta p \sin^2 \alpha p}{\sin^2 \beta p} = 0$$

$$\Rightarrow \frac{2 \sin \alpha p \cos \beta p}{\cos \beta p} = \cos \beta p \sin^2 \beta p$$

$$2 \sin \alpha p \cos \beta p = \cos \beta p \sin^2 \beta p$$

$$\Rightarrow \frac{\sin^2 \beta p \times 2 \sin \alpha p \cos \beta p - \sin^2 \beta p \sin \alpha p \cos \beta p}{\sin^2 \beta p} = 0$$

$$\Rightarrow 2 \sin \beta p \sin^2 \alpha p (\cos \alpha p \sin^2 \beta p - \sin \alpha p \cos \beta p) = 0$$

$$\Rightarrow \sin \alpha p \cos \beta p - \sin \alpha p \cos \beta p = 0$$

$$\Rightarrow \sin \alpha p \cos \beta p = \sin \alpha p \cos \beta p$$

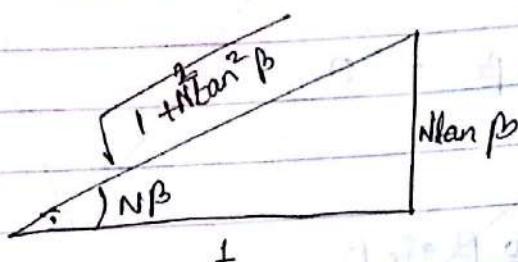
$$\Rightarrow \frac{N \sin \alpha p}{\cos \beta p} = \frac{\sin \alpha p}{\cos \beta p}$$

$$\Rightarrow \boxed{N \tan p = \tan \alpha p} \rightarrow \text{Condition to satisfy}$$

## Intensity of secondary maxima :-

Cond'n for secondary maxima is ( $N \tan\beta = \tan N\beta$ )

This cond'n can be geometrically shown as follows:-



In this triangle,

$$\sin^o N\beta = \frac{N \tan\beta}{\sqrt{1+N^2 \tan^2 \beta}}$$

Squaring,

$$\sin^2 N\beta = \frac{N^2 \tan^2 \beta}{1+N^2 \tan^2 \beta}$$

$$\Rightarrow \sin^2 N\beta = \frac{N^2}{(\cot^2 \beta + N^2)}$$

Dividing both by  $\sin^2 \beta$

$$\Rightarrow \frac{\sin^2 N\beta}{\sin^2 \beta} = \frac{N^2}{(\cot^2 \beta + N^2) \sin^2 \beta}$$

$$\Rightarrow \frac{\sin^2 N\beta}{\sin^2 \beta} = \frac{N^2}{\cos^2 \beta + N^2 \sin^2 \beta}$$

$$\Rightarrow \frac{\sin^2 N\beta}{\sin^2 \beta} = \frac{N^2}{1 - \sin^2 \beta + N^2 \sin^2 \beta}$$

$$\Rightarrow \frac{\sin^2 N\beta}{\sin^2 \beta} = \frac{N^2}{1 + \sin^2 \beta (N^2 - 1)}$$

∴ the secondary maxima intensity is :-

$$I_{\text{secondary maxima}} = A^2 \frac{\sin^2 \alpha}{\alpha^2} \times \frac{\sin^2 N\beta}{\sin^2 \beta}$$

$$I_{\text{sec max}} = \frac{A^2 \sin^2 \alpha}{\alpha^2} \times \frac{N^2}{1 + \sin^2 \beta (N^2 - 1)}$$

$$\Rightarrow I_{\text{sec max}} = \frac{I_{\text{prim max}}}{1 + \sin^2 \beta (N^2 - 1)}$$

→ Intensity of secondary maxima

$$(As; I_{\text{prim max}} = A^2 \frac{\sin^2 \alpha}{\alpha^2} \times N^2)$$

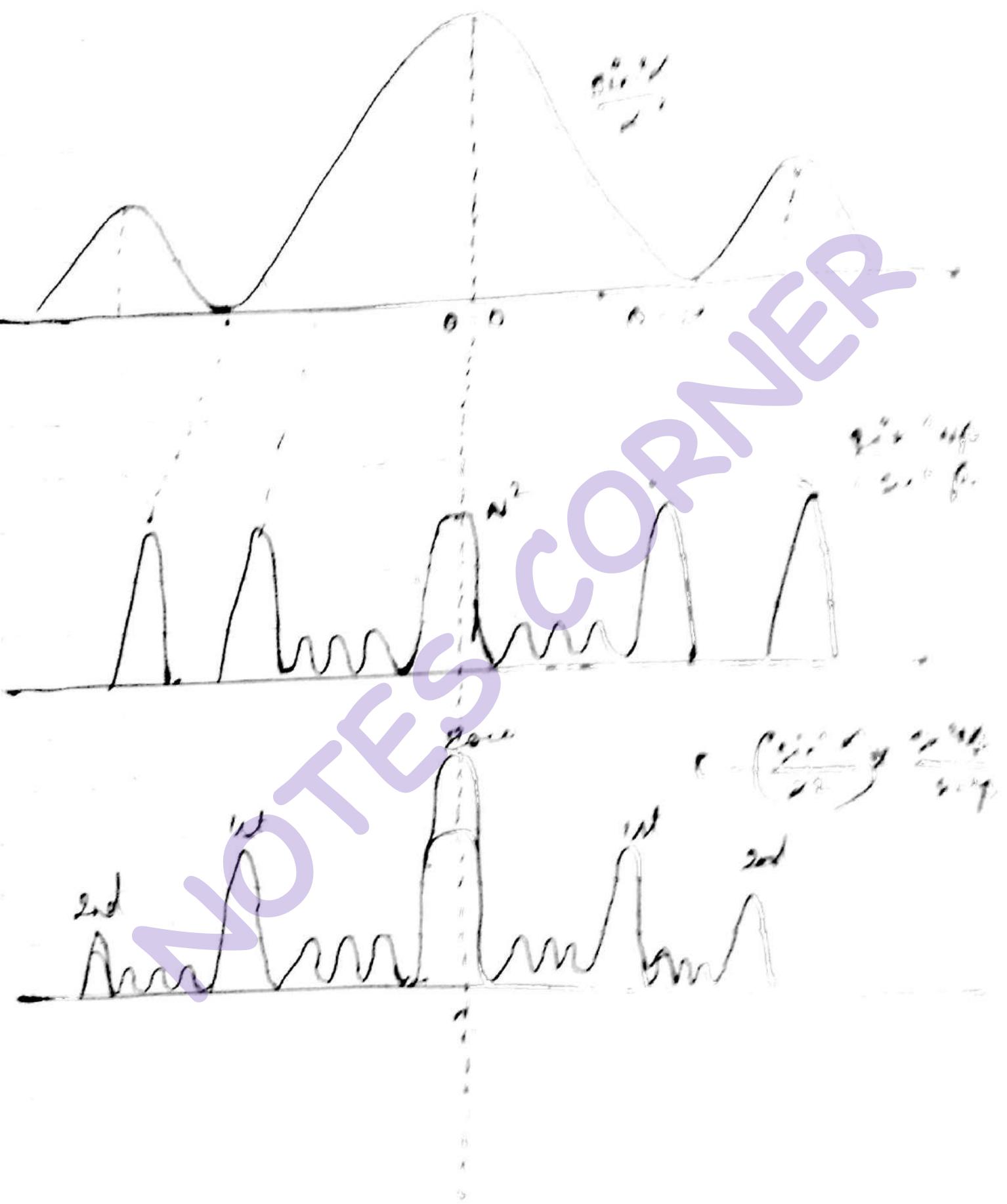
Generally,  $N$  is large. So, the secondary maxima intensity is very small as compared to primary maxima intensity.

Intensity distribution curve for Fraunhofer diffraction in plane diffraction grating :-

The intensity in Fraunhofer due to plane diffraction grating is given by.  $I = A^2 \frac{\sin^2 \alpha}{\alpha^2} \frac{\sin^2 N\beta}{\sin^2 \beta}$ .

Here the  $\alpha$  term is called as diffraction term whereas  $\beta$  term is called as interference term.

These terms individually as well as the resultant intensity ( $I$ ) can be shown graphically as figure below :-



## Missing Order

$$(e+d)\sin\theta = n\lambda \rightarrow \text{Position of } \alpha \text{ term}$$

$$e\sin\theta = m\lambda \rightarrow \text{minima of } \beta \text{ term}$$

$$\boxed{\frac{e+d}{e} = \frac{n}{m}} \rightarrow \text{cond' for missing order}$$

- In Fraunhofer diffraction due to plane diffraction grating,  
For certain angle the minima of  $\alpha$  term and maxima of  $\beta$  term coincides, in these angles some order of primary maxima will not be visible. These orders are called as missing order.
- We know in Fraunhofer diffraction due to plane diffraction grating, the minima of  $\alpha$  term satisfy the relation

$$\cancel{e\sin\theta} e\sin\theta = m\lambda \quad \text{--- ①}$$

Similarly we know maxima of  $\beta$  term ~~also~~ satisfy the relation

$$(e+d)\sin\theta = n\lambda \quad \text{--- ②}$$

Dividing eq ① by ②,

We get :-

$$\boxed{\frac{e+d}{e} = \frac{n}{m}} \rightarrow \text{cond' of missing order}$$

$n, m \rightarrow$  natural no.

### Case - 1

If  $e = d$ .

$$\frac{e+d}{e} = \frac{n}{m}$$

$$\Rightarrow \frac{2e}{e} = \frac{n}{m}$$

$$\Rightarrow \boxed{n = 2m} \quad m = 1, 2, 3, \dots$$

$\Rightarrow n = 2, 4, 6, 8, \dots$  orders will be missing

### Case - 2

If  $d = 6e$ .

$$\Rightarrow \frac{e+d}{e} = \frac{n}{m}$$

$$\Rightarrow \frac{7e}{e} = \frac{n}{m}$$

$$\Rightarrow \boxed{n = 7m}, \quad m = 1, 2, 3, \dots$$

$$\Rightarrow n = 7, 14, \dots$$

## LASER

Laser is an acronym for the physical phenomena  
Light Amplification by Stimulated Emission of Radiation

### Interaction of light with matter

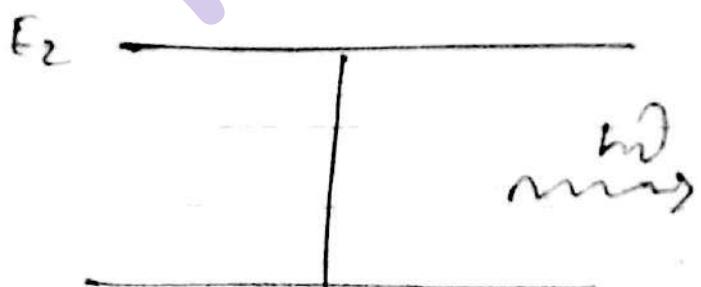
Interaction of light with matter can be described  
by the following physical phenomena

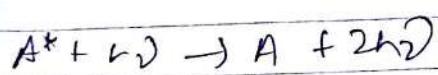
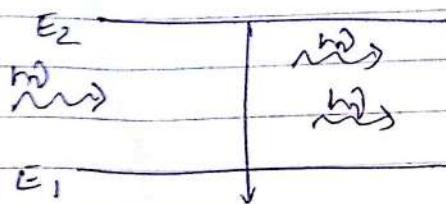
- (i) Absorption
- (ii) Spontaneous Emission
- (iii) Stimulated emission.

Ch

### Spontaneous Emission:-

The atoms in the excited state are not stable. They loose their energy in form of radiation. In this process, the electrons at the higher energy level jump back to the lower energy level by releasing its extra energy in form of photon radiation. This process is called as spontaneous emission. This is a natural process. This is governed by the life time of the electron in the excited state (the photon emitted). In this process, the radiation is omni-directional that means photon move in all possible directions. This process can be schematically shown as figure below:





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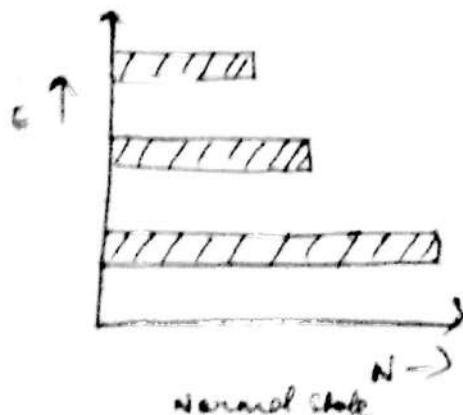
NOTES CORNER

## Difference between spontaneous emission and stimulated emission :-

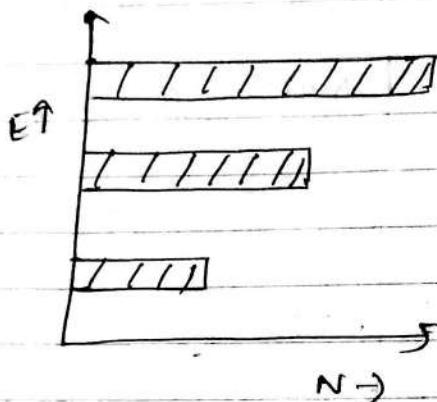
<u>Spontaneous Emission</u>	<u>Stimulated Emission</u>
→ It is a natural process	→ It is a forced process
→ It is an uncontrollable process	→ It is a controllable process
→ The emission follows the lifetime of the electron in excited state.	→ This emission is instantaneous
→ In this emission, the photons have arbitrary direction (non-directional emission)	→ In this emission the photons have same emission (directional emission)
→ All the emitted photons do not have same nature	→ All the emitted photons have same nature i.e. same wavelength, direction, polarization, momentum etc.

## Population Inversion:-

In the normal state or ground state generally more no. of atoms <sup>of a system</sup> are there in the lower energy level. With increasing its energy level, the no. of atoms decreases as shown in fig.



By giving external energy to the system more and more, no. of atoms can be switched to higher energy level as shown in figure below:-



This condition where more no. of atoms are there in higher energy level is called as population inversion.

For laser action to take place population inversion condition is mandatory.

### Pumping :-

The process of giving external energy to the system to build up the population inversion is called as pumping.

Pumping can be done by

- (i) optical means
- (ii) electrical discharge
- (iii) collision

(iv) carrier injection

## Component of LASER

\* LASER should have atleast 3 components:-

- (i) Gain medium
- (ii) Laser/Resonator cavity
- (iii) Pumping system

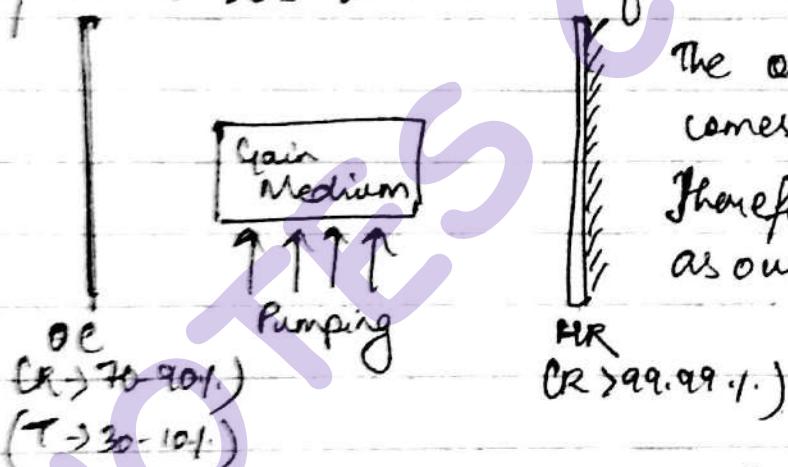
## Gain Medium :-

It is the substance in which lasing action take place i.e. in this medium <sup>more absorption,</sup> population inversion, stimulated emission takes place.

The gain medium can be solid, liquid or gas. Accordingly the lasers are named as solid state laser, gas laser or liquid state laser. Ruby (a crystal) laser is a solid state laser whereas  $\text{CO}_2$  laser is a gas laser.

## Resonator cavity / laser cavity :-

This consist of atleast two mirrors one of them is having reflectivity  $R > 99\%$  at the lasing wavelength. This mirror is called as back mirror. The other mirror has also very high reflectivity but it has also some finite value of transmittance.



The output of the laser comes out of this mirror.

Therefore this mirror is called as output Coupler.

Let  $L$  be the length of the cavity.

Then the various longitudinal modes of laser are having wavelength given by

$$\lambda_{1/2} = L$$

$$\Rightarrow \Delta = 2L$$

$$\lambda_2 = L$$

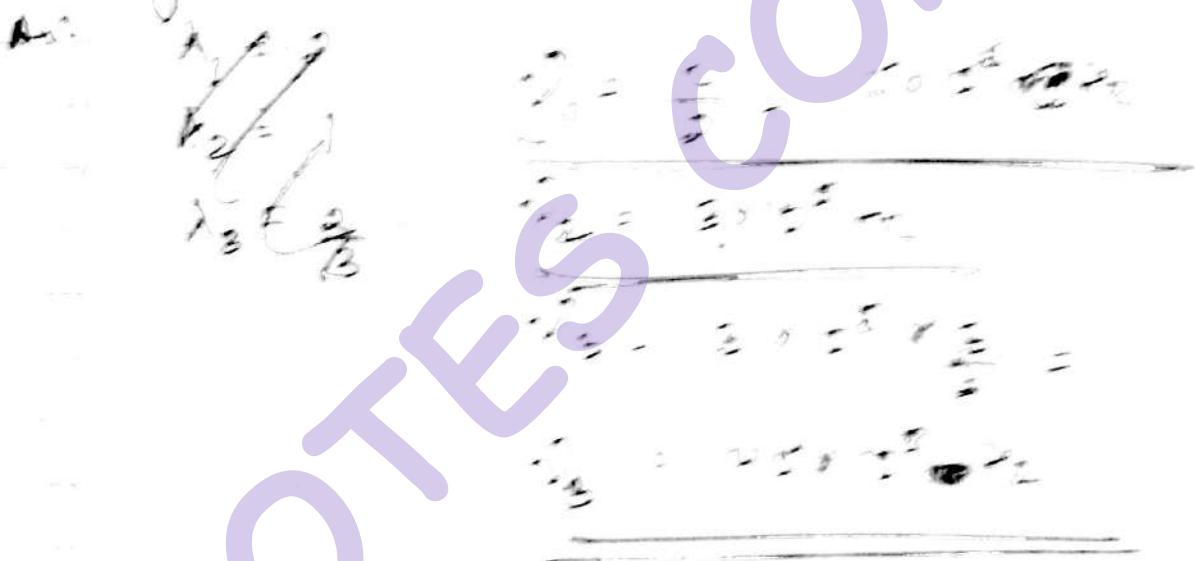
$$2\Delta - 1$$

$$D_1 = \frac{1}{2} \times \frac{1}{2}$$

$$D_2 = \frac{1}{2} \times \frac{1}{2} \times \frac{1}{2}$$

$$D_3 = \frac{1}{2} \times \frac{1}{2} \times \frac{1}{2} \times \frac{1}{2}$$

a) Let the length of bus conductor be  $L$  m. Then the time taken by longitudinal waves

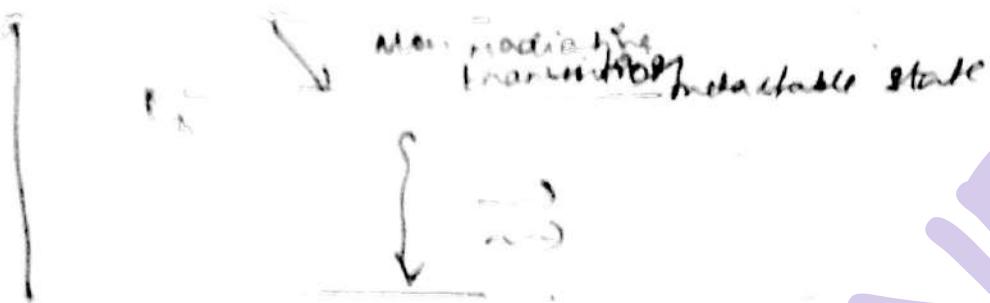


Pumping system :-

At the given rates:

Three level laser :-

The three level laser has no gain mechanism because no energy level is excited to the higher energy level. Three energy levels are shown schematically in the figure above -

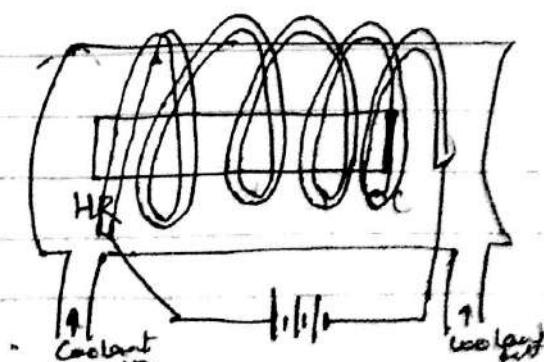


In this case the atoms transit from energy level \$E\_1\$ to \$E\_2\$ through absorption process. These atoms are not stable in this state, they quickly transit to energy level \$E\_3\$ by non radiative fast process. This type of scheme help the energy level \$E\_3\$ has very high life time therefore the atoms can stay <sup>not for</sup> long time under continuous pumping more and more no of electrons used to be trapped in energy level \$E\_3\$. This help in building up the population inversion. The energy level \$E\_3\$ is called as meta stable state. Now the stimulated emission takes place between the energy level \$E\_3\$ and \$E\_1\$.

## Ruby Laser

It is a solid state laser. Its <sup>the</sup> working principle, structure / construction is given below.

- Ruby is a crystal of  $\text{Al}_2\text{O}_3$  doped with Cr. This dopant generally exist in ion form. The concentration of this dopant is  $\approx 0.05\%$  by weight.
- The atomic concentration of the Cr Ion with 16% type of doping is  $1.6 \times 10^{25}$  per cubic meter ( $\text{cm}^{-3}$ ). This ruby crystal is the gain medium. The chromium Ion has three energy levels that is suitable for lasing action.
- The shape of the crystal is generally cylindrical having length 4 cm and width 0.5 cm.
- One of the end of this rod is polished in a such a way that it can reflect fully (high reflection). This end behaves like back mirror. The other mirror is polished to have partial transmission along with high reflecting. This end behaves like output coupler.
- This crystal is generally pumped by a helical flat lamp filled with Xenon. The 5500 Å radiation of this lamp is observed by the chromium ions. The crystal is cooled by flowing some coolant.



## Working Principle

When chromium ion <sup>absorb</sup> observe the 5500A radiation, it transit to higher energy level  $E_2$  from  $E_1$ . Ion is not stable then it quickly transit to level  $E_3$ , where the lifetime is much higher (meta-stable state). So, under continuous pumping more and more no. of ions ( $\text{Cr}^+$ ) transit to energy level  $E_2$  from  $E_1$  through  $E_2$ . The transition from  $E_2$  to  $E_3$  is generally non radiative. In this process population inversion takes place and the stimulated emission take place between the energy levels. The emission wavelength is  $6943\text{\AA}$ .



- (iv) Laser Spectroscopy  
(v) Laser gun

## Oscillations

LR

- 1) Establish or derive the eq<sup>n</sup> of motion for damped oscillation, find out general sol<sup>n</sup> and discuss the case of over damping or critical damping or under damping.
- 2) Establish or derive the eq<sup>n</sup> for forced oscillation. Write down the general sol<sup>n</sup> of amplitude and phase about condition of resonance.
- 3) Derive the eq<sup>n</sup> wave eq<sup>n</sup> in differential form. (With some numerical)
- 4) Derivation of expression for resultant Intensity, condition for maxima/minima, Maxima and minima Intensity. expressing energy distribution curve  
or  
(Analytical treatment of interference)
- 5) Show that energy remains conserved in Interference. (10 marks)
- 6) Analytical treatment of Newton's Ring.  
or  
What do you mean by Newton's ring, derive the cond<sup>r</sup> for bright and dark ring and derive their diameter expression.

7) With the experimental description discuss about Newton Ring and show how it can be used to measure  $\lambda$  / estimate wavelength and R.D.

	Order of ring (n)	Diameter ( $D_n$ )	$D_n^2$	$D_{n+1}^2 - D_n^2$	Mean $D_{n+1}^2 - D_n^2$
E <sub>1</sub>					
F <sub>n</sub>	1	X1	X1 <sup>2</sup>		
E <sub>2</sub>	2	X2	X2 <sup>2</sup>	X2 <sup>2</sup> - X1 <sup>2</sup>	X2 <sup>2</sup>
Start by the m e	3	X3	X3 <sup>2</sup>		
	4	X4	X4 <sup>2</sup>		
	5	X5	X5 <sup>2</sup>		

8) Analytical treatment for Fraunhofer diffraction due to single slit.

What do you mean by Fraunhofer diffraction due to single slit?

Derive resultant intensity expression, cond' for primary maxima, minima and secondary maxima. Show that the intensity distribution follows the relation  $I = \frac{I_0}{\pi^2} \frac{4}{25} \sin^2 \left( \frac{\pi y}{\lambda} \right)$

$$I = I_0 \frac{1}{22^2} \frac{1}{63}$$

$$I = 0.045$$

## Analytical Ques

1) Show that the width of Newton's Ring decreases with order if the glass plate is replaced by a mirror.

(2) What will happen in Newton's ring expt.

(3) What will happen if white light source is used in Newton's expt. like expt.

(4) What will happen if white light is used in single slit expt.

(5) What is the condition for sustainable and good contrast in Interference.

(6) Difference between Interference and diffraction.

(7) Write down the condn for maximum order of diffraction in single slit diffraction.

The maxm angle is  $\theta = \pi/2$ . ( $\theta = \pi/2$ ) -

8) The slit size in a Fraunhofer single slit expt is  $4\lambda$ . where  $\lambda$  be the wavelength of the light used. Find out (i) Angle for 1st order and 2nd order minima.

(ii) Maximum order of diffraction.

$$\text{Ans: } x = \frac{\pi D \sin \theta}{\lambda}$$

$$\sin \theta = 5\lambda$$

$$\Rightarrow \theta = \pi/4 \times \sin^{-1} 0$$

$$\Rightarrow \sin \theta = \pm \frac{1}{4}$$

$$\therefore \sin \theta =$$

$$\Rightarrow \theta = \sin^{-1} \left( \frac{1}{4} \right)$$

$$= 14.47^\circ$$

$$\Rightarrow \theta = \sin^{-1} \left( \frac{1}{2} \right) = \underline{\underline{30^\circ}}$$

$$\theta_{\text{max}} = n_{\text{max}} \lambda$$

$$\therefore \theta_{\text{max}} = \cancel{\pi} \frac{\pi}{2}$$

$$\Rightarrow e = 4 \lambda$$

$$\therefore 4\lambda = n_{\text{max}} \lambda$$

$$\therefore \underline{n_{\text{max}}} = 4$$

In above ques find out angle for 1st order secondary maxima.

$$\text{If } \lambda = 5893 \text{ Å}$$

$$\lambda = \frac{3\pi}{2}$$

$$\frac{1 + \sin \theta}{\lambda} = \frac{3\pi}{2}$$

$$\therefore \frac{1 + \sin \theta}{\lambda} = 3 \cancel{\pi} \frac{3}{2} \lambda$$

$$\therefore 4\lambda \sin \theta$$

$$\sin \theta = \frac{3}{2} \times 5893 \times 10^{-8}$$

$$\therefore \sin \theta = \frac{3}{8}$$

$$\therefore \theta = \sin^{-1}\left(\frac{3}{8}\right) = \underline{\underline{22.02^\circ}}$$