

The Shallow Water Model

- * primitive equations with simplified representation of stratification
- * thin layers of constant density with no vertical variation in horizontal velocities:

In each layer : $\rho = \text{constant}$

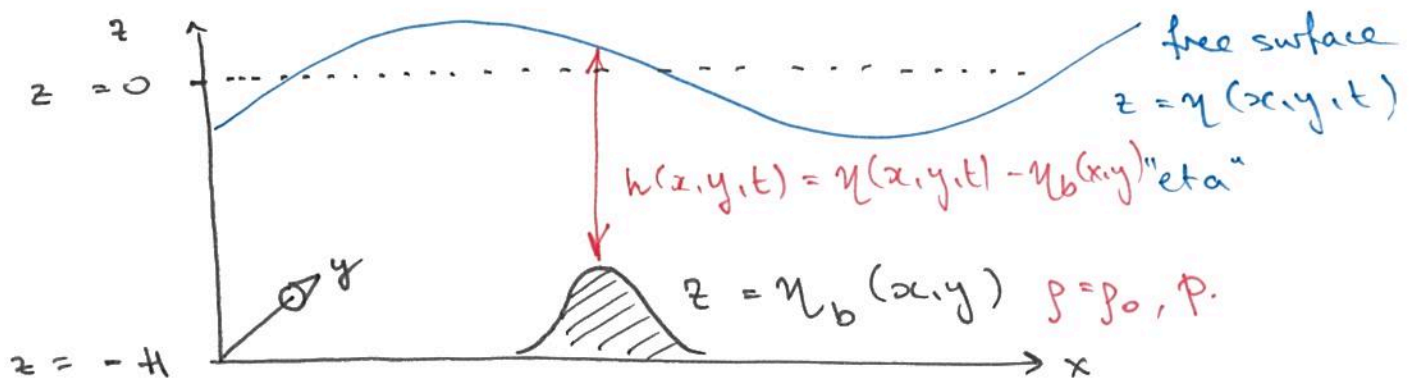
$$u = u(x, y, t)$$

$$v = v(x, y, t)$$

$$\phi = \phi(x, y, z, t)$$

- * horizontal scales \gg depth ("shallow water")

Single-layer SW model



Conservation of Mass

$\rho_0 = \text{constant} \Rightarrow$ fluid is incompressible in 3D.

$$\nabla \cdot \underline{v} = 0 = \frac{\partial u}{\partial x} + \frac{\partial v}{\partial y} + \frac{\partial w}{\partial z}$$

3D velocity

$$\Rightarrow \left[\frac{\partial w}{\partial z} = - \nabla_z \cdot \underline{u} \right] \quad \begin{array}{l} \nabla_z = (\partial_x, \partial_y) \\ \underline{u} = (u, v) \end{array}$$

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Integrate from bottom to top:

$$\int_{\eta_b}^{\eta} \frac{dw}{dz} dz = w(\eta) - w(\eta_b)$$

$$= \int_{\eta_b}^{\eta} -\underline{\nabla}_z \cdot \underline{u} dz$$

u, v don't depend on z .

$$= -\underline{\nabla}_z \cdot \underline{u} (\eta - \eta_b)$$

$$= -(\underline{\nabla}_z \cdot \underline{u}) h$$

But position of the fluid at the top and bottom.

$$w(\eta) = \frac{D\eta}{Dt}$$

$$w(\eta_b) = \frac{D\eta_b}{Dt} = \underline{u} \cdot \underline{\nabla}_z \eta_b$$

$$w(\eta) - w(\eta_b) = \frac{D}{Dt} (\underbrace{\eta - \eta_b}_h) = -(\underline{\nabla}_z \cdot \underline{u}) (\underbrace{\eta - \eta_b}_h)$$

$$\Rightarrow \boxed{\frac{Dh}{Dt} = -\underline{\nabla}_z \cdot \underline{u} h.} \quad \text{Conservation of mass.}$$

compare with 3D conservation of mass:

$$\frac{D\rho}{Dt} = -\underline{\nabla} \cdot \underline{v} \cdot \rho \quad \begin{array}{l} \underline{v} \rightarrow \underline{u} \\ \rho \rightarrow h \end{array}$$

Lagrangian form: $\frac{Dh}{Dt} = -h \underline{\nabla}_z \cdot \underline{u}$

Eulerian form: $\frac{\partial h}{\partial t} + \underline{u} \cdot \underline{\nabla}_z (h) = -\underline{\nabla}_z \cdot (\underline{u} h)$

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Pressure from hydrostatic balance.

$$\frac{\partial \phi}{\partial z} = -\rho_0 g \quad \rho_0 = \text{constant}$$

Integrate:

$$\int_{\phi(z)}^{\phi_0} \frac{\partial \phi}{\partial z} dz = - \int_z^{\eta} \rho_0 g dz \quad z < 0$$

$$\phi_0 - \phi(z) = -\rho_0 g (\eta - z)$$

$$\phi(z) = \underbrace{\phi_0}_{\text{surface pressure}} + \underbrace{\rho_0 g (\eta - z)}_{\text{mass of fluid above depth } z}$$

Pressure gradient force:

$$-\frac{1}{\rho_0} \nabla_z \phi = -g \nabla_z \eta.$$

Momentum balance:

$$\frac{D\underline{u}}{Dt} + \underline{f} \times \underline{u} = -\frac{1}{\rho_0} \nabla_z \phi = -g \nabla_z \eta.$$

$$\uparrow$$
$$\frac{\partial \underline{u}}{\partial t} + u \frac{\partial \underline{u}}{\partial x} + v \frac{\partial \underline{u}}{\partial y}$$

$$(w \frac{\partial \underline{u}}{\partial z} = 0).$$

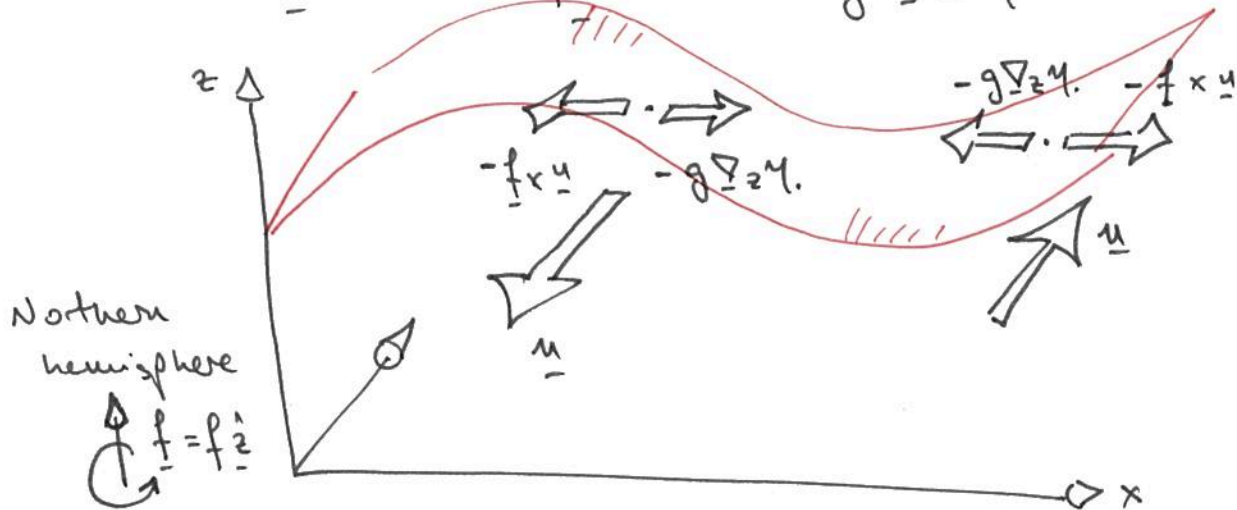
Geostrophic balance in the SW model.

$R_0 \ll 1 \Rightarrow$ neglect inertial terms.

$$\underline{f} \times \underline{u} = -g \nabla_z \eta.$$

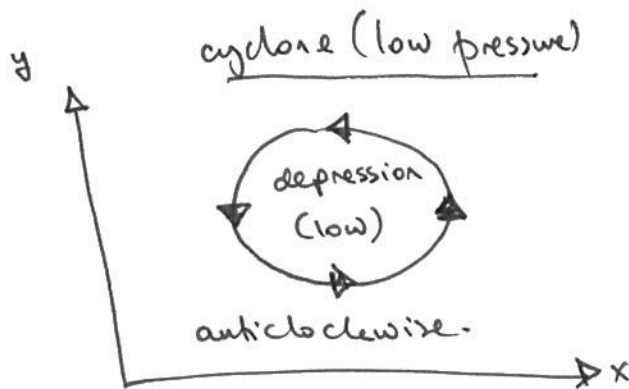
Rewrite this as a force balance.

$$0 = -\underline{f} \times \underline{u} - g \nabla_z \eta.$$

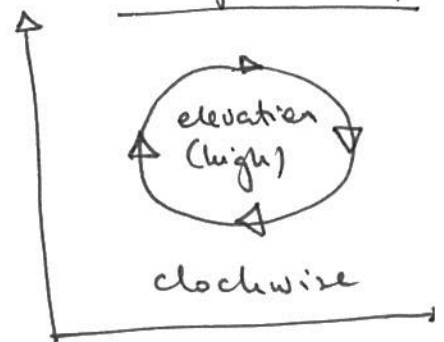


From above

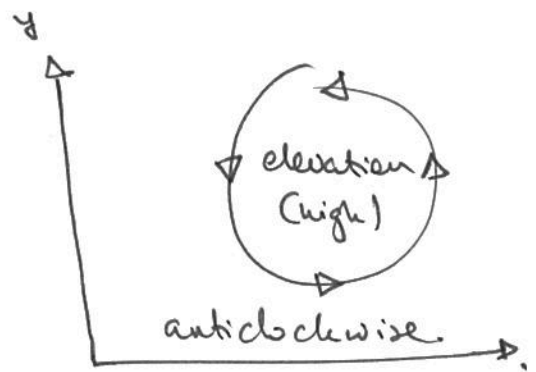
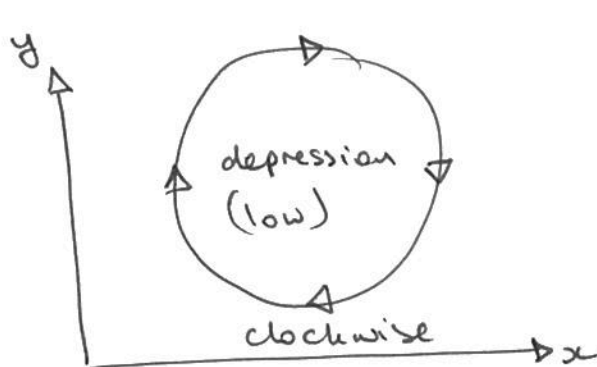
Northern hemisphere
 $(f > 0)$



anticyclone (high)

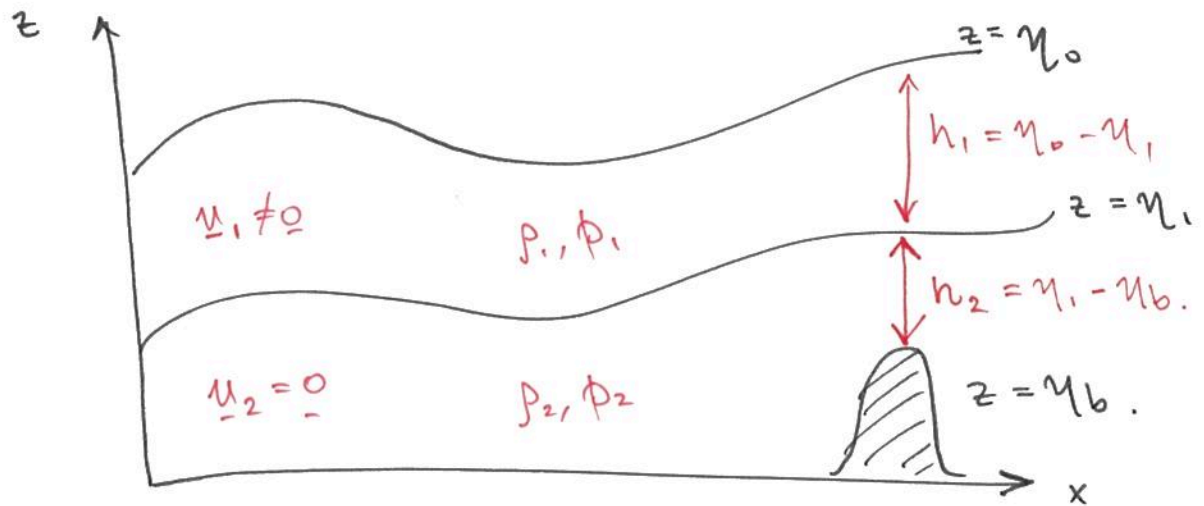


Southern hemisphere
 $(f < 0)$



1½ layer shallow water model

* "active layer" ($\underline{u} \neq 0$) on top of "quiescent layer" ($\underline{u} = 0$).



Continuity equation in upper layer:

$$\frac{Dh_1}{Dt} + h_1 \nabla_z \cdot \underline{u} = 0$$

Pressure gradient:

In layer 1:

$$\phi_1(z) = \phi_0 + \rho_1 g (\eta_0 - z), \quad \eta_0 \leq z \leq \eta_1.$$

In layer 2:

$$\phi_2(z) = \phi_0 + \rho_1 g (\eta_0 - \eta_1) + \rho_2 g (\eta_1 - z), \quad \eta_1 \leq z \leq \eta_b.$$

$$\Rightarrow \underline{f}_{\text{pres},1} = -\frac{1}{\rho_1} \nabla_z \phi_1 = -g \nabla_z \eta_0.$$

$$\underline{f}_{\text{pres},2} = -\frac{1}{\rho_2} \nabla_z \phi_2 = -\frac{\rho_1}{\rho_2} g \nabla_z (\eta_0 - \eta_1) - g \nabla_z \eta_1.$$

Momentum equation in each layer:

In layer 1: $\frac{D\underline{u}}{Dt} + \underline{f} \times \underline{u} = -g \nabla_z \eta_0$

In layer 2: $0 + 0 = -\frac{\rho_1}{\rho_2} g \nabla_z (\eta_0 - \eta_1) - g \nabla_z \eta_1$

$$\Rightarrow \nabla_z \eta_0 = -\frac{\rho_2}{\rho_1} \nabla_z \eta_1 + \nabla_z \eta_1 = -\frac{\rho_2 - \rho_1}{\rho_1} \nabla_z \eta_1$$

$$\Rightarrow \frac{D\underline{u}}{Dt} + \underline{f} \times \underline{u} = g \frac{\rho_2 - \rho_1}{\rho_1} \nabla_z \eta_1 \quad \rho_2 > \rho_1$$

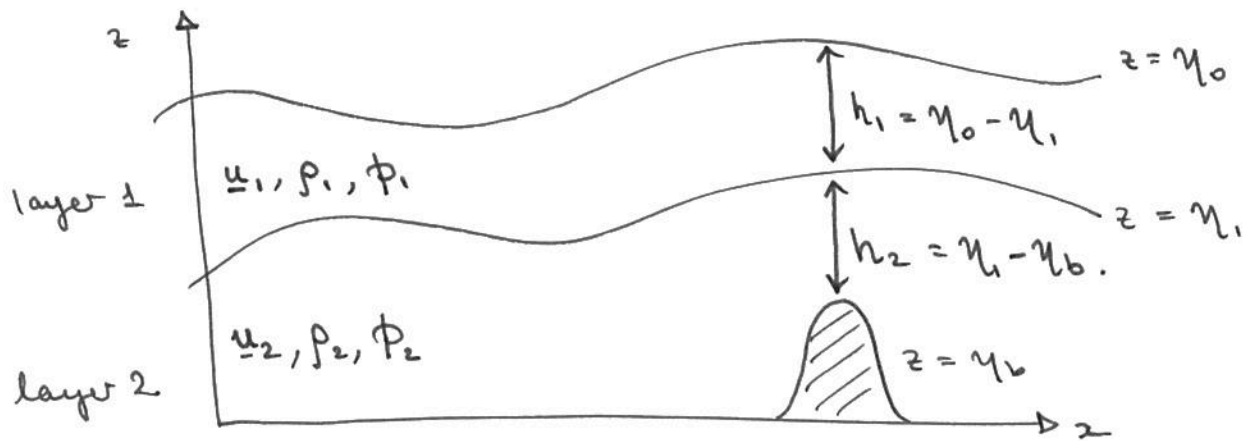
$$= g' \nabla_z \eta_1$$

reduced gravity.

$$g' = g \frac{\rho_2 - \rho_1}{\rho_1} \ll g$$

$$\Rightarrow |\nabla_z \eta_1| \gg |\nabla_z \eta_0|$$

TWO LAYER SHALLOW WATER MODEL



Continuity eqns for each layer:

$$\frac{D_1 h_1}{Dt} + h_1 \nabla_z \cdot \underline{u}_1 = 0$$

$$\frac{D_2 h_2}{Dt} + h_2 \nabla_z \cdot \underline{u}_2 = 0.$$

$$\frac{D_1}{Dt} = \frac{\partial}{\partial t} + \underline{u}_1 \cdot \nabla_z$$

$$\frac{D_2}{Dt} = \frac{\partial}{\partial t} + \underline{u}_2 \cdot \nabla_z$$

Pressure gradient + forces:

$$\phi_1 = \phi_0 + \rho_1 g (\eta_0 - z)$$

$$\eta_0 \geq z \geq \eta_1$$

$$\phi_2 = \phi_0 + \rho_1 g (\eta_0 - \eta_1) + \rho_2 g (\eta_1 - z) \quad \eta_1 \geq z \geq \eta_b$$

$$\Rightarrow \underline{f}_{\text{pres},1} = -g \nabla_z \eta_0$$

$$\underline{f}_{\text{pres},2} = -g \frac{\rho_1}{\rho_2} \nabla_z (\eta_0 - \eta_1) - g \nabla_z \eta_1$$

$$= \frac{\rho_1}{\rho_2} (-g \nabla_z \eta_0 - g' \nabla_z \eta_1)$$

reduced gravity

$$\approx -g \nabla_z \eta_0 - g' \nabla_z \eta_1$$

$\frac{\rho_1}{\rho_2} \approx 1$
in Boussinesq approx.

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Geostrophic balance in each layer ($R_0 \ll 1$).

$$\underline{f} \times \underline{u}_1 = -g \nabla_z \eta_0 \quad (1)$$

$$\underline{f} \times \underline{u}_2 = -g \nabla_z \eta_0 - g' \nabla_z \eta_1 \quad (2)$$

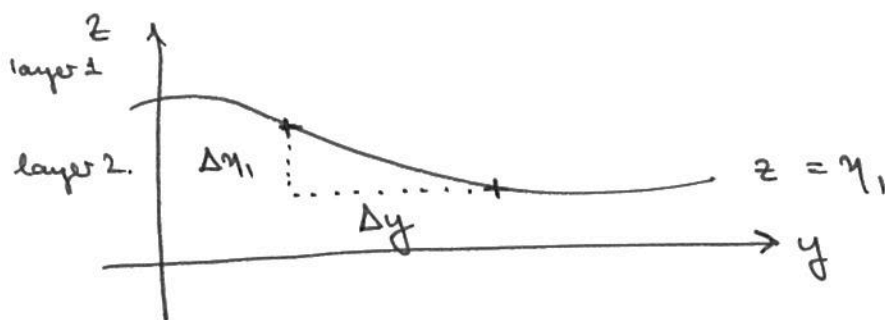
Thermal wind balance in SW system:

(1) - (2)

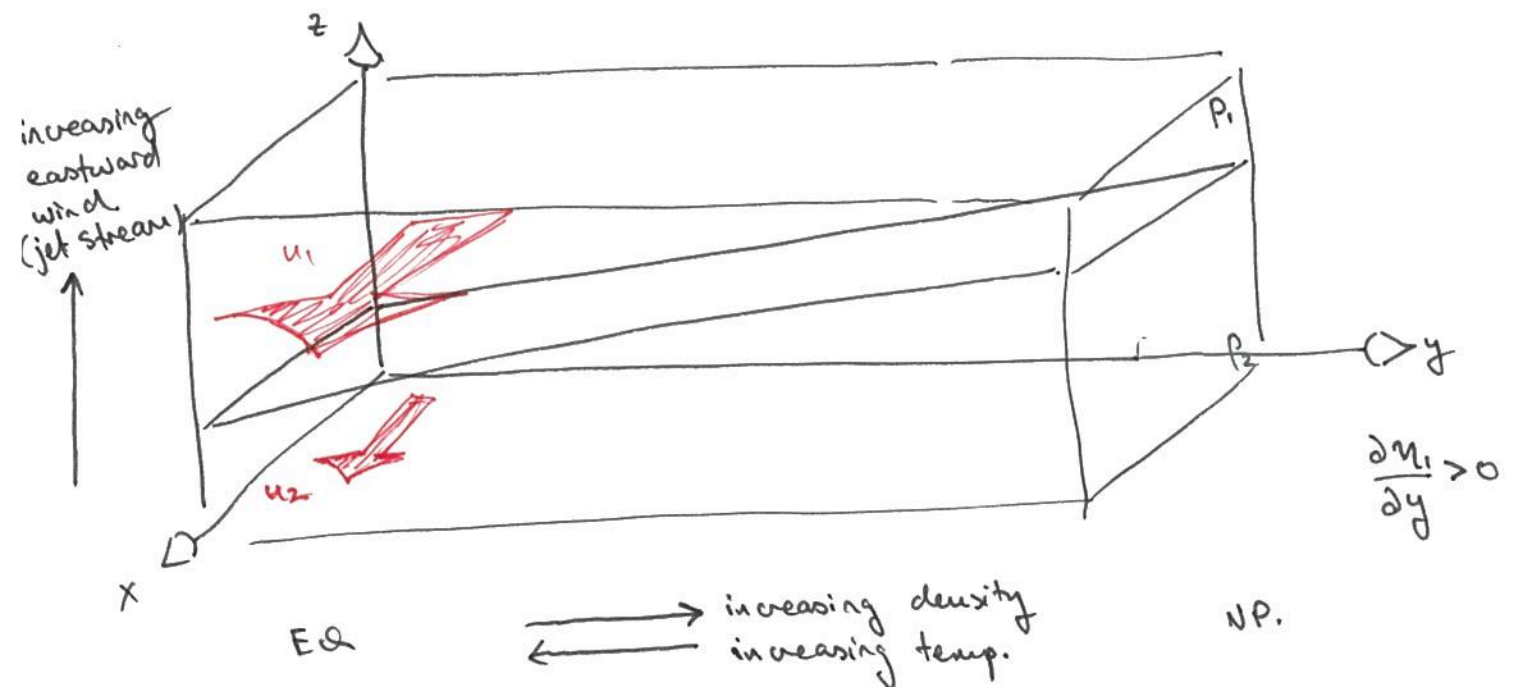
$$\underline{f} \times (\underline{u}_1 - \underline{u}_2) = g' \nabla_z \eta_1 \quad \underline{f} = f_0 \hat{z}$$

$$u_1 - u_2 = \frac{g'}{f_0} \frac{\partial \eta_1}{\partial y}$$

$$v_1 - v_2 = -\frac{g'}{f_0} \frac{\partial \eta_1}{\partial x}$$



$\frac{\partial \eta_1}{\partial y} \approx \frac{\Delta \eta_1}{\Delta y} \Rightarrow$ horizontal gradients in pressure (height)
 \Updownarrow
 sloping interfaces.



Rearrange :

$$\underbrace{\frac{\partial \underline{u}}{\partial t}}_{(1)} + \underbrace{\underline{\omega} \times \underline{u}}_{(2)} + \underbrace{\underline{f} \times \underline{u}}_{(3)} = \underbrace{-\nabla (g\eta + \frac{1}{2} \underline{u} \cdot \underline{u})}_{(4)}$$

Take curl term-by-term :

$$(1) \quad \nabla \times \frac{\partial \underline{u}}{\partial t} = \frac{\partial}{\partial t} \nabla \times \underline{u} = \frac{\partial \underline{\omega}}{\partial t} = \frac{\partial \zeta}{\partial t} \hat{z}$$

$$(2) \quad \nabla \times (\underline{\omega} \times \underline{u}) \stackrel{\#3}{=} \underline{\omega} (\nabla \cdot \underline{u}) + (\underline{u} \cdot \nabla) \underline{\omega} - \underline{u} (\nabla \cdot \underline{\omega}) - (\underline{\omega} \cdot \nabla) \underline{u}$$

#1. $\nabla \cdot \underline{\omega} = \nabla \cdot (\nabla \times \underline{u}) = 0$

$\zeta \frac{\partial \underline{u}}{\partial z} = 0$

\underline{u} has no z -dependence.

$$(3) \quad \nabla \times (\underline{f} \times \underline{u}) \stackrel{\#3}{=} \underline{f} (\nabla \cdot \underline{u}) + (\underline{u} \cdot \nabla) \underline{f} - \underline{u} (\nabla \cdot \underline{f}) - (\underline{f} \cdot \nabla) \underline{u}$$

$\nabla \cdot \underline{f} = \frac{\partial}{\partial z} f(y) = 0$

$f \frac{\partial \underline{u}}{\partial z} = 0$

$$(4) \quad \nabla \times \nabla (g\eta + \frac{1}{2} \underline{u} \cdot \underline{u}) = 0 \quad (\text{Identity \#4 } \nabla \times \nabla \phi = 0)$$

Thus

$$\underbrace{\frac{\partial \underline{\omega}}{\partial t}}_{(1)} + \underbrace{\underline{\omega} (\nabla \cdot \underline{u}) + (\underline{u} \cdot \nabla) \underline{\omega}}_{(2)} + \underbrace{\underline{f} (\nabla \cdot \underline{u}) + (\underline{u} \cdot \nabla) \underline{f}}_{(3)} = \underbrace{0}_{(4)}$$

$$\frac{\partial}{\partial t} \zeta \hat{z} + \zeta (\nabla \cdot \underline{u}) \hat{z} + (\underline{u} \cdot \nabla \zeta) \hat{z} + f (\nabla \cdot \underline{u}) \hat{z} + (\underline{u} \cdot \nabla f) \hat{z} = 0$$

Take z -component :

$$\frac{\partial}{\partial t} (\zeta + f) + (\underline{u} \cdot \nabla) (\zeta + f) + (\zeta + f) (\nabla \cdot \underline{u}) = 0$$

$\frac{\partial f}{\partial t} = 0$

$$\frac{\partial h}{\partial t} + \underline{u} \cdot \underline{\nabla} h + h \underline{\nabla} \cdot \underline{u} = 0$$

$$\eta = \eta(x, y, t) \quad u = u(x, y, t) \quad v = v(x, y, t)$$

$$\underline{f} = f \hat{\underline{e}}_1 = (f_0 + \beta y) \hat{\underline{e}}_1$$

$\vec{\omega} = \nabla \times \vec{u}$
 "omega" ∇ 3D \vec{u} 2D $(u, v, 0)$

$$= \begin{pmatrix} \cancel{u_y} - \cancel{v_z} \\ \cancel{u_z} - \cancel{v_x} \\ v_x - u_y \end{pmatrix} = \begin{pmatrix} 0 \\ 0 \\ v_x - u_y \end{pmatrix} = \hat{z} \text{ "zeta"}$$

Some vector calculus identities:

$$4. \nabla \times (\underline{A} \times \underline{B}) = \underline{A}(\nabla \cdot \underline{B}) + (\underline{B} \cdot \nabla)\underline{A} - \underline{B}(\nabla \cdot \underline{A}) - (\underline{A} \cdot \nabla)\underline{B}$$

#3 with $A = u$:

$$\frac{1}{2} \nabla \cdot \mathbf{u} = \frac{1}{2} \nabla \cdot (\mathbf{u} \times (\nabla \times \mathbf{u}))$$

$$\Rightarrow \frac{\partial \underline{u}}{\partial t} - \underline{u} \times \underline{\omega} + \frac{1}{2} \nabla (\underline{u} \cdot \underline{u}) + \underline{f} \times \underline{u} = -g \nabla_z \eta.$$

Rearrange:

$$\underbrace{\frac{\partial \underline{u}}{\partial t}}_{(1)} + \underbrace{\underline{\omega} \times \underline{u}}_{(2)} + \underbrace{\underline{f} \times \underline{u}}_{(3)} = - \underbrace{\nabla_z (g\eta + \frac{1}{2} \underline{u} \cdot \underline{u})}_{(4)}$$

Take curl term-by-term:

$$(1) \quad \nabla \times \frac{\partial \underline{u}}{\partial t} = \frac{\partial}{\partial t} \nabla \times \underline{u} = \frac{\partial \underline{\omega}}{\partial t}$$

$$(2) \quad \nabla \times (\underline{\omega} \times \underline{u}) \stackrel{\#4}{=} \underline{\omega} (\nabla \cdot \underline{u}) + (\underline{u} \cdot \nabla) \underline{\omega} - \underline{u} (\nabla \cdot \underline{\omega}) - (\underline{\omega} \cdot \nabla) \underline{u}$$

$\nabla \cdot \underline{\omega} = \nabla \cdot (\nabla \times \underline{u}) = 0$
 $\underline{\omega} \cdot \nabla \underline{u} = \zeta \frac{\partial \underline{u}}{\partial z} = 0$

$$(3) \quad \nabla \times (\underline{f} \times \underline{u}) \stackrel{\#4}{=} \underline{f} (\nabla \cdot \underline{u}) + (\underline{u} \cdot \nabla) \underline{f} - \underline{u} (\nabla \cdot \underline{f}) - (\underline{f} \cdot \nabla) \underline{u}$$

$\nabla \cdot \underline{f} = \frac{df}{dz} = 0$
 $\underline{f} \cdot \nabla \underline{u} = f \frac{\partial \underline{u}}{\partial z} = 0$

$$(4) \quad \nabla \times (\nabla (\dots)) \stackrel{\#1}{=} 0$$

Thus:

$$\underbrace{\frac{\partial \underline{\omega}}{\partial t}}_{(1)} + \underbrace{\underline{u} \cdot \nabla \underline{\omega}}_{(2)} + \underbrace{\underline{\omega} (\nabla \cdot \underline{u})}_{(3)} + \underbrace{\underline{u} \cdot \nabla \underline{f}}_{(3)} + \underbrace{f (\nabla \cdot \underline{u})}_{(4)} = 0$$

$$\frac{\partial \zeta}{\partial t} \hat{z} + (\underline{u} \cdot \nabla) \zeta \hat{z} + \zeta \hat{z} (\nabla \cdot \underline{u}) + (\underline{u} \cdot \nabla) f \hat{z} + f \hat{z} (\nabla \cdot \underline{u}) = 0$$

Take z-component

$$\frac{\partial \zeta}{\partial t} + (\underline{u} \cdot \nabla) (\zeta + f) + (\zeta + f) \nabla \cdot \underline{u} = 0$$

Write as : $q = \zeta + f$ = absolute vorticity

ζ = relative vorticity

f = planetary vorticity

The SW system can be rewritten as

$$\begin{aligned} \frac{\partial q}{\partial t} + (\underline{u} \cdot \underline{\nabla}) q + q(\underline{\nabla} \cdot \underline{u}) &= 0. \\ \frac{\partial h}{\partial t} + (\underline{u} \cdot \underline{\nabla}) h + h(\underline{\nabla} \cdot \underline{u}) &= 0. \end{aligned} \quad \left(\begin{aligned} \frac{\partial q}{\partial t} &= \frac{\partial \zeta}{\partial t} \\ \frac{\partial f}{\partial t} &= 0 \end{aligned} \right)$$

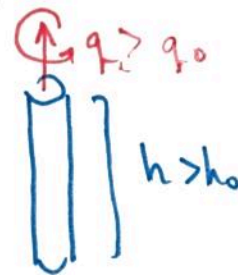
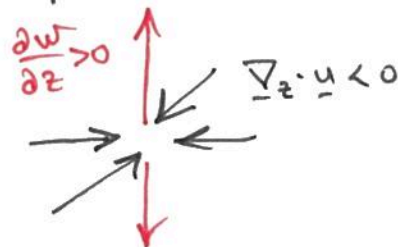
OR

$$\frac{Dq}{Dt} = -q(\underline{\nabla} \cdot \underline{u}), \quad \frac{Dh}{Dt} = -h(\underline{\nabla} \cdot \underline{u})$$

* For horizontally non-divergent flow ($\underline{\nabla} \cdot \underline{u} = 0$) both height and vorticity are conserved.

$$\frac{Dq}{Dt} = 0 \quad \frac{Dh}{Dt} = 0.$$

* Horizontally diverging / converging flows will change both q & h :



* Can change $q = \zeta + f$ by

- spinning the flow (change ζ)

- moving the column north/south (change f)

Potential Vorticity in SW system

Combine effects of q & h into a single quantity:

$$Q = \frac{q}{h} = \frac{\zeta + f}{h} = \frac{\text{relative} + \text{planetary vorticity}}{\text{height}}$$

= "potential vorticity" ~~$[s^{-1}]$~~ !

$$\begin{aligned} \frac{DQ}{Dt} &= \frac{D}{Dt} \left(\frac{q}{h} \right) = \frac{1}{h} \frac{Dq}{Dt} + q \frac{D}{Dt} \left(\frac{1}{h} \right) \\ &= \frac{1}{h} \frac{Dq}{Dt} - \frac{q}{h^2} \frac{Dh}{Dt} \\ &= \frac{1}{h} \left(-q \nabla_z \cdot \underline{u} \right) - \frac{q}{h^2} \left(-h \nabla_z \cdot \underline{u} \right) \\ &= -\frac{q}{h} \nabla_z \cdot \underline{u} + \frac{q}{h} \nabla_z \cdot \underline{u} = 0. \end{aligned}$$

$\frac{DQ}{Dt} = 0$	$Q = \frac{\zeta + f}{h}$
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Conservation of potential vorticity (PV)

Q is conserved following the flow.