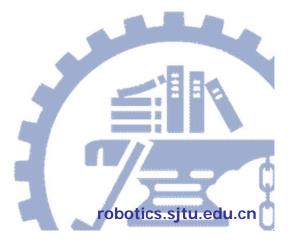


Visual Servo Control of Cabledriven Soft Robotic Manipulator

Hesheng Wang (王贺升)

Department of Automation Shanghai Jiao Tong University China





Outline

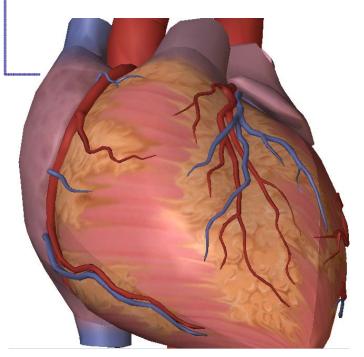
- Introduction
- Background
- System Design
- Kinematics
- Controller Design
- Experimental results
- Conclusion

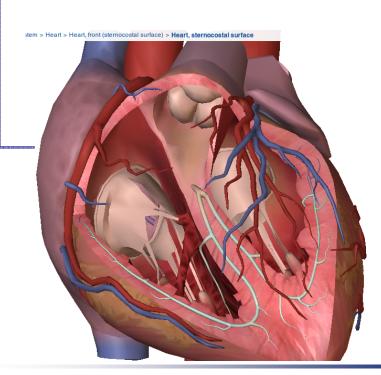


Minimally Invasive Surgery (MIS)

On the surface of the beating heart

Inside the beating heart





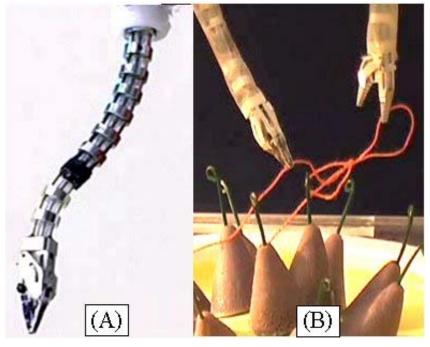




Background

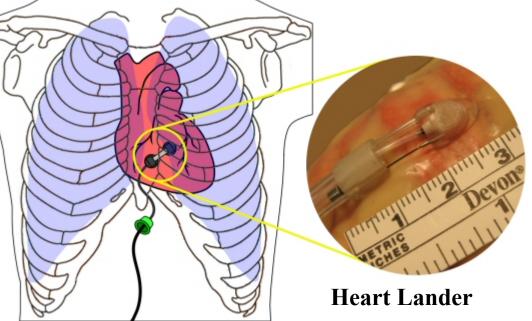






Concentric Tube Robot

HARP



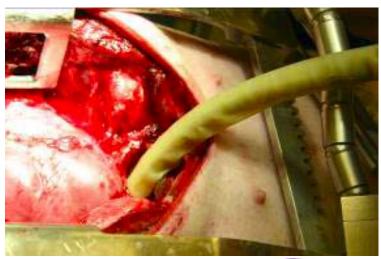


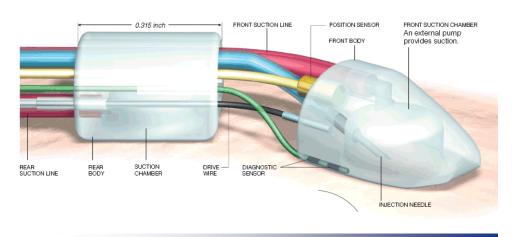


Not Soft Enough

Not Safe Enough

Not Practical Enough







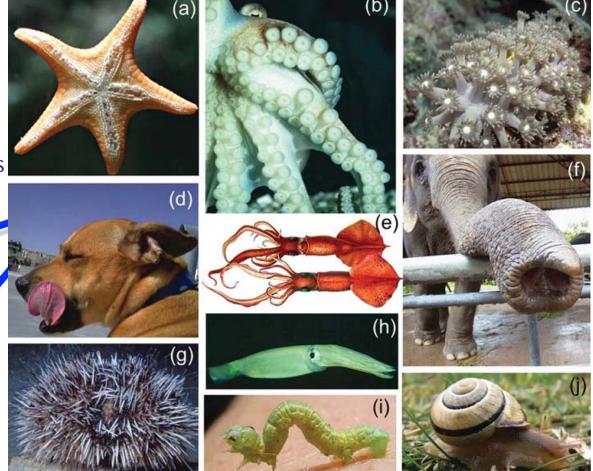


"Soft" robotic systems

-Conform to the surroundings

-Ease of operation

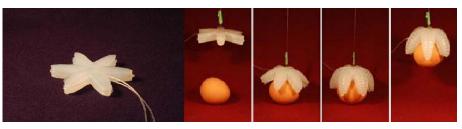
-"Fit" to Dynamic environments





Research Background

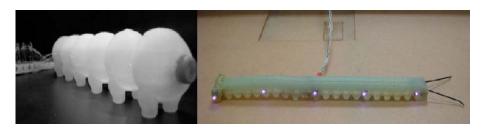
- Soft robots: material, manufacturing, Control Theory, computer simulation
- Applications: minimally invasive surgery, military, exploration, rescue...



Starfish robot



(2) Quadruped deformable robot



Caterpillar robot



(4) Mechanical octopus tentacle





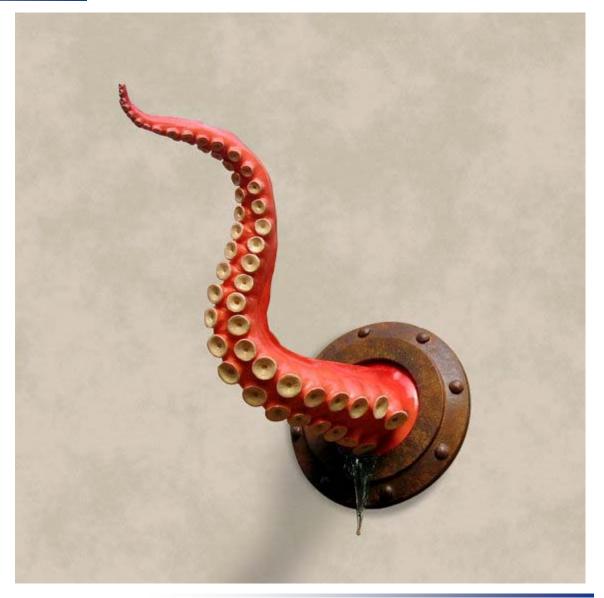
Characters of soft robot

Characters	Rigid robots	Redundant robot	Hard continuum robot	Soft robot
DOF	Small	Many	Infinite	Infinite
Material strain	None	None	Low	High
Accuracy	Very High	High	High	Low
Safety	Low	Low	Medium	High
Flexibility	Low	High	High	High
Compatibility with obstacles	None	Good	Medium	Very good
Controllability	Easy	Medium	Hard	Hard
Positioning	Easy	Medium	Hard	Hard



Soft Robotic Manipulator

■Kinematics - hyper-redundancy





System Composition

A soft manipulator

A drive base frame

Control and display system

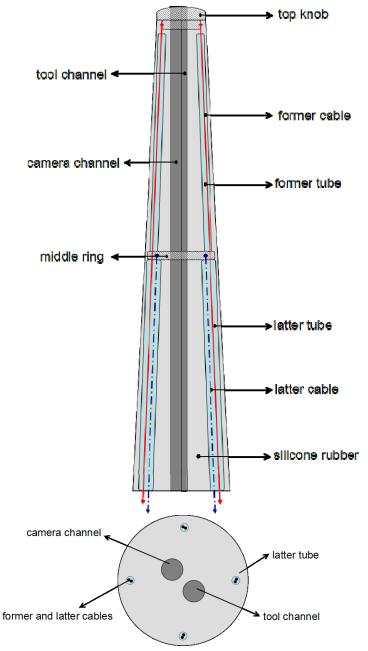




The Soft Manipulator

- 30mm
- silicone rubber (ECOFLEXTM)
- 8 non-abrasive fiber cables (DyneemaTM)
- plastic caps
- ablation tools and a micro CCD camera





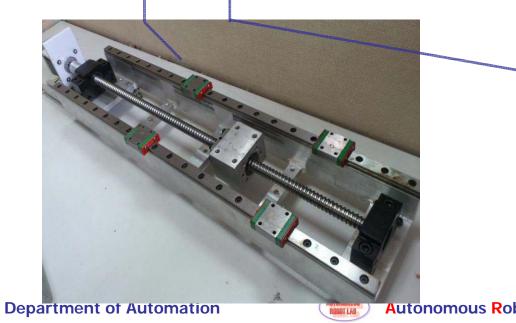


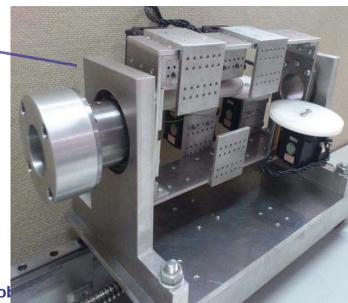
The Drive Base Frame

Linear motion system

Rotational motion system









Control and Display System

Joystick Control

Cameral Display

Control Software









System Manipulation

Manipulate method

Manual Mode

- ■The cable tension can be changed by setting the Head angle
- •Adding functional buttons
 - functional buttons for each behavior
 - buttons for selecting which cables are being controlled
 - buttons for emergency

Automatic Mode

■Path planning & Localization on the surface of the heart



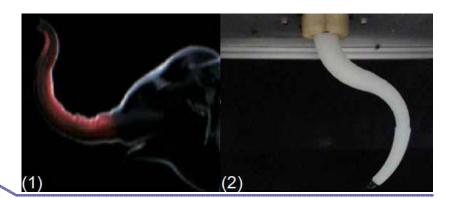
System Manipulation

Behavior Implementation

- 1. Blending
- 2. Contracting
- 3. Advancing/Retreating

(1) (2) (3)

- 4. Wriggling
- 5. Blending and Wriggling partly
- 6. S shape





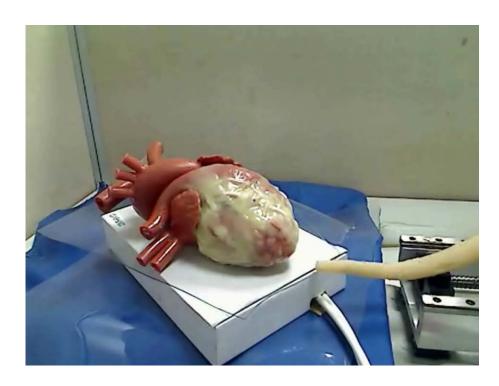


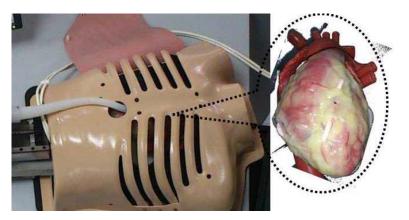


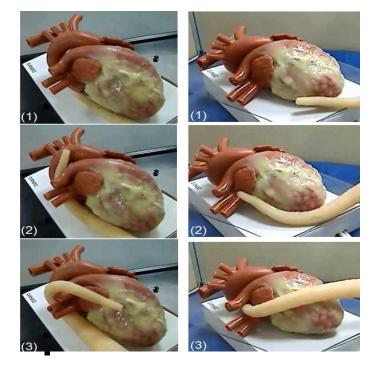
Experiments

Unconstrained Environment

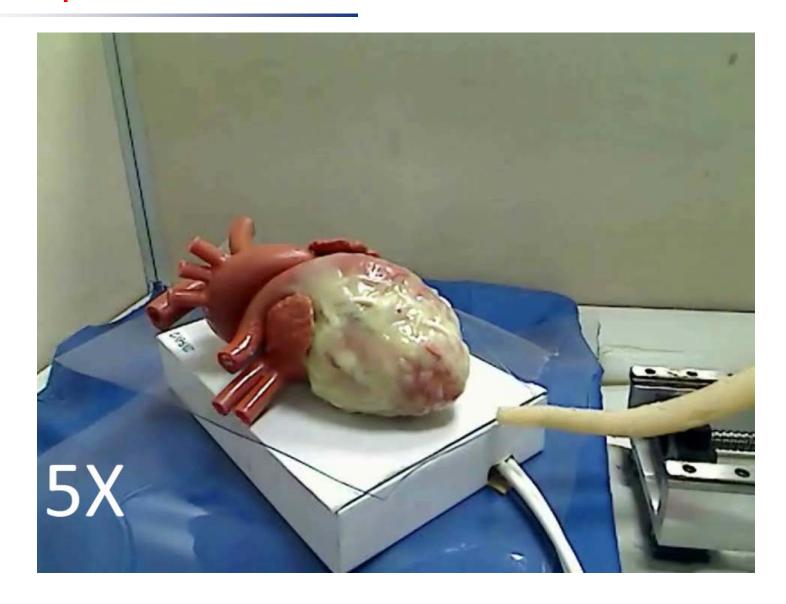
- -with a plastic thorax and a silicone heart
- -different simulated paths on the surface
- -to identify the geometrical shape and flexibility







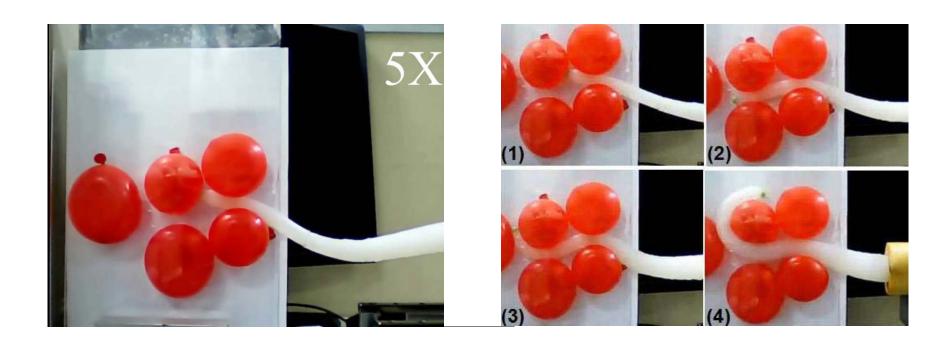




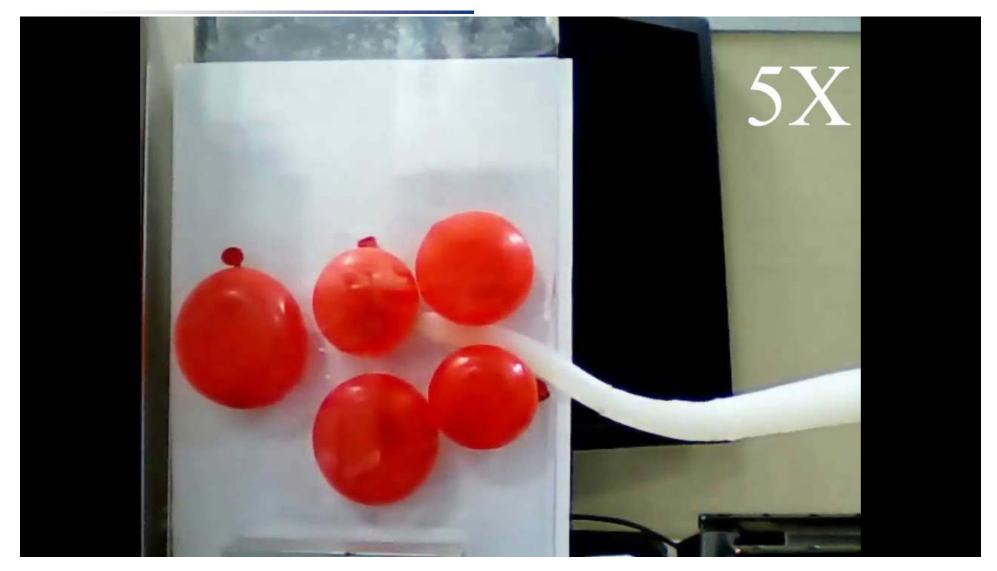


Limited Environment

- made of balloons to imitate the human tissue
- complicated path to guide the soft probe
- effects of the gravity and surroundings

















System Manipulation

KEY ISSUES

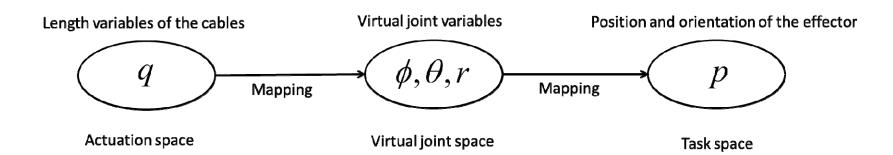
- Kinematics Modeling
- Influence of gravity
- Influence of Surroundings Environment
- Dynamics Modeling
- Modeling Method
- Calculation efficiency
- Controller



Constant curvature hypothesis

Constant curvature hypothesis: dividing the whole body of the soft robotic manipulator into n segments, and each segment can be treated as a cylinder that the radius of section is constant

three spaces and two mappings



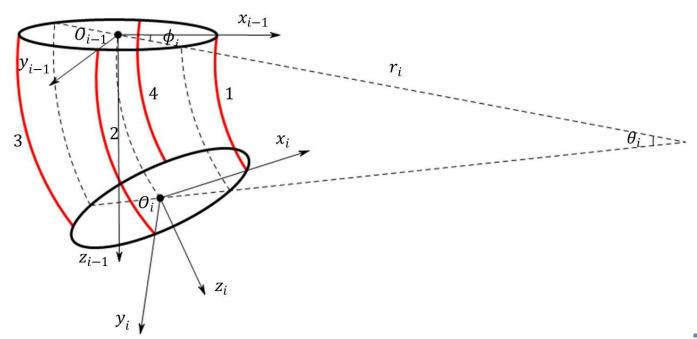
- denotes the angle between the bending plane and the positive direction of x axis,
- θ denote the curvature angle of the bending plane respectively.
- denote the curvature radius of the bending plane respectively.



Kinematics

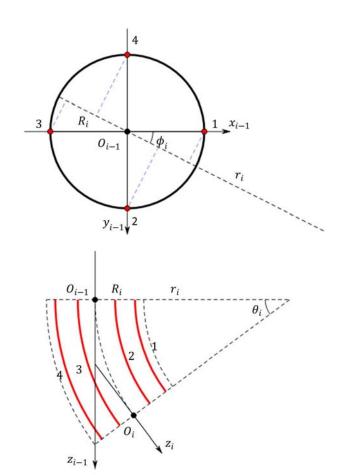
For i-th segment

- the length variables of 4 cables: q_1, q_2, q_3, q_4
- the current length of 4 cables: $\frac{l_1}{n}, \frac{l_2}{n}, \frac{l_3}{n}, \frac{l_4}{n}$
- the central axis of the i-th segment $\frac{l}{n}$





Actuation space - Virtual joint space



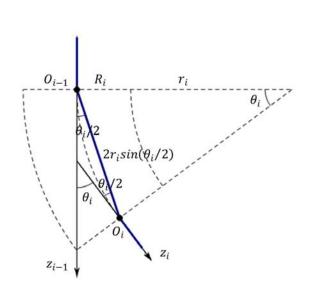
$$\phi_i = \tan^{-1} \frac{q_4 - q_2}{q_3 - q_1}$$

$$\theta_i = \frac{\sqrt{(q_3 - q_1)^2 + (q_4 - q_2)^2}}{2nR_i}$$

$$r_{i} = \frac{2(L-q)R_{i}}{\sqrt{(q_{3}-q_{1})^{2}+(q_{4}-q_{2})^{2}}}$$



Virtual joint space – Task space

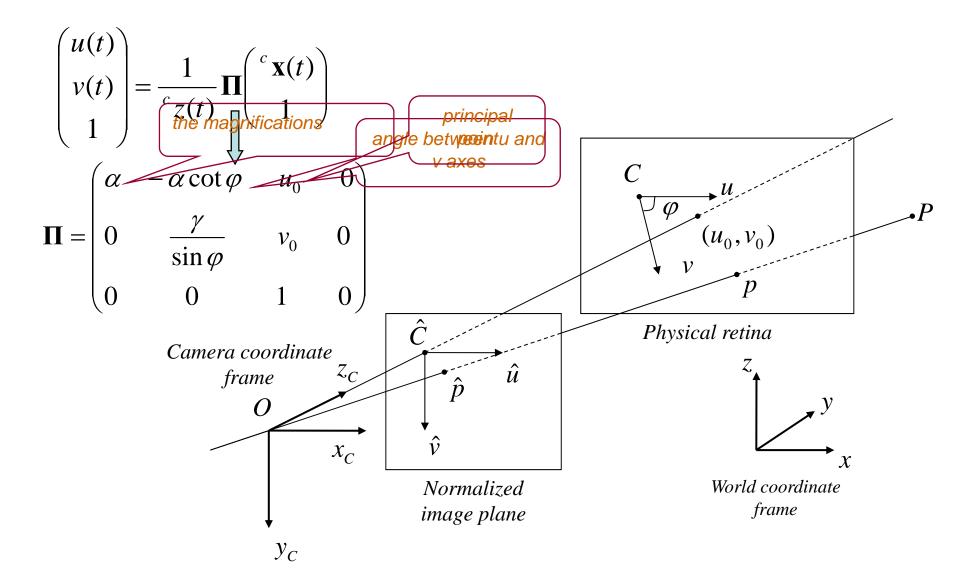


$$\begin{split} & \stackrel{i^{-1}T_i}{=} A_{i1} A_{i2} A_{i3} A_{i4} A_{i5} \\ & = \begin{bmatrix} c^2 \phi_i \left(c \theta_i - 1 \right) + 1 & s \phi_i c \phi_i \left(c \theta_i - 1 \right) & c \phi_i s \theta_i & r_i c \phi_i \left(1 - c \phi_i \right) \\ s \phi_i c \phi_i \left(c \theta_i - 1 \right) & s^2 \phi_i \left(c \theta_i - 1 \right) + 1 & s \phi_i s \theta_i & r_i s \phi_i \left(1 - c \phi_i \right) \\ - c \phi_i s \theta_i & - s \phi_i s \theta_i & c \theta_i & r_i s \theta_i \\ 0 & 0 & 0 & 1 \end{bmatrix} \end{aligned}$$

$$T = {}^{0}T_1 {}^{1}T_2 \cdots {}^{i-1}T_i$$



Perspective Projection



Projection Model

the projection of the feature point on the image plane

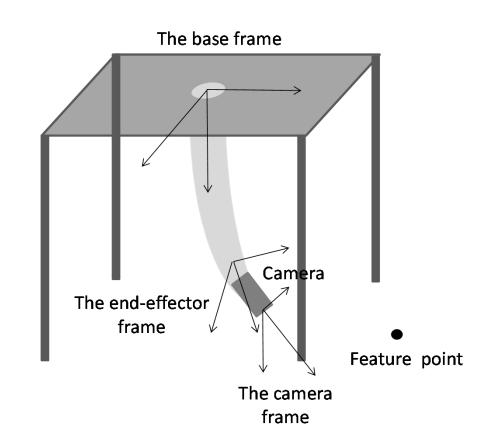
$$y(q(t)) = \frac{1}{z(q(t))} P \begin{bmatrix} {}^{e}x(t) \\ 1 \end{bmatrix}$$

$$z(q(t)) = m_3^T \begin{bmatrix} {}^e x(t) \\ 1 \end{bmatrix}$$

Interaction matrix

$$\dot{y}(q(t)) = \frac{1}{z(q(t))} A(y(t), q(t)) \begin{bmatrix} v(t) \\ w(t) \end{bmatrix}$$

$$\dot{z}(q(t)) = b(q(t)) \begin{bmatrix} v(t) \\ w(t) \end{bmatrix}$$



Property 1

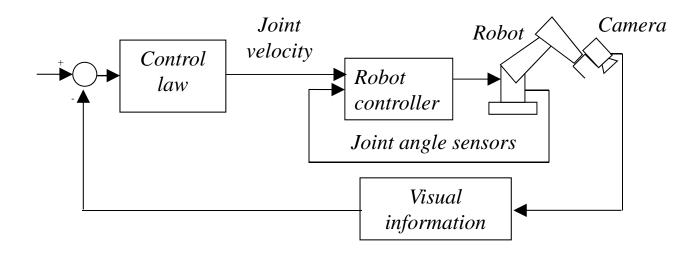
For any homogenous vector \mathbf{P} , the $\mathbf{A}^{(t)}\mathbf{P}$ product can be written in the following form:

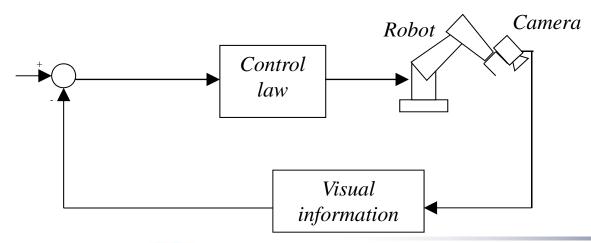
$$\mathbf{A}(t)\mathbf{\rho} = \mathbf{Q}(\mathbf{\rho}, \mathbf{y}(t))\mathbf{\theta} + \mathbf{\sigma}$$

where Q(p, y(t)) is a regressor matrix without depending on the unknown parameters.



Kinematic-based and Dyanmic Visual Servoing







Kinematic-based Visual Servoing

Kinematic-based controller

$$\dot{q}(t) = -J^{T}(q(t))\hat{A}^{T}(y(t), q(t))K_{1}\Delta y(t)$$
$$-\frac{1}{2}J^{T}(q(t))\hat{b}^{T}(q(t))\Delta y^{T}(t)K_{1}\Delta y(t)$$

Adaptive law

$$b\dot{\hat{x}}(t) = -\Gamma^{-1}Y^{T}(y(t), q(t))\dot{q}(t)$$

Stability analysis

 Applying the image-based visual servo controller and adaptive algorithm, it can be proved that the position error of the feature point on the image plane will be convergent to zero when time approaches to the infinity

$$\lim_{t\to\infty} \Delta y(t) = 0$$

– a Lyapunov-like function is defined as follows:

$$V(t) = \frac{1}{2} \Delta y^{T}(t) K_{1} z(q(t)) \Delta y(t) + \frac{1}{2} \Delta^{b} x^{T}(t) \Gamma \Delta^{b} x(t)$$

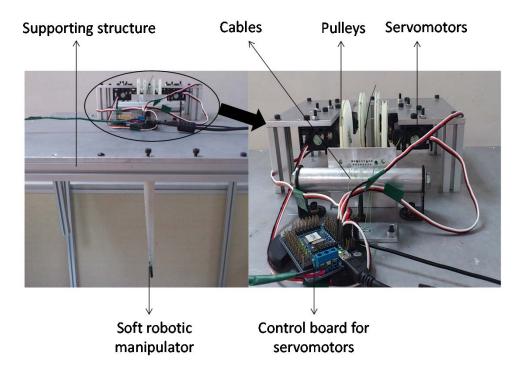
Finally

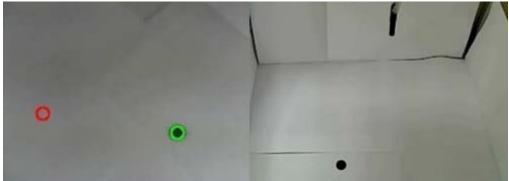
$$\dot{V}(t) = -\Delta y^{T}(t)\hat{D}^{T}(y(t), q(t))JK_{1}^{2}J^{T}\hat{D}(y(t), q(t))\Delta y(t)$$

- By Babarrat's Lemma, the stability could be proved.



Experimental system







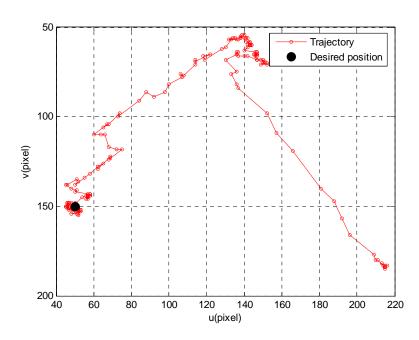
Experimental results

Image-based Visual Servo Control of Cable-driven Soft Robotic Manipulator

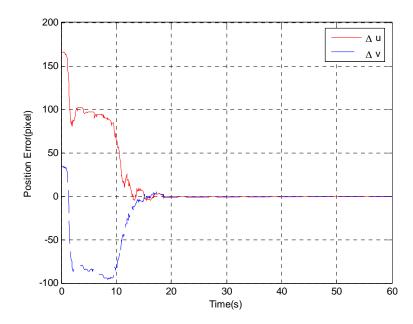
> Autonomous Robot Lab Shanghai Jiao Tong University, China http://robotics.sjtu.edu.cn

Experimental Results

- Initial position: $y(0) = (208,166)^T$
- Desired position: $y_d = (50,150)^T$
- Initial estimated feature 3D position: ${}^{b}x(0) = (0.0 \ 0.62)^{T}$
- gains: $K_1 = 3.0 \times 10^{-6}$ $\Gamma = 100$



The trajectory of the feature point on the image plane.



The image errors between current position and desired position.

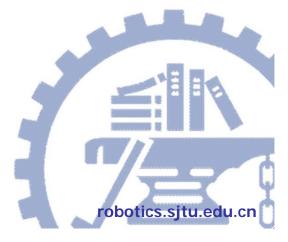


Conclusion and future work

- A cable-driven soft manipulator for cardiac ablation
 - -completely made of soft materials
 - -high degree of freedom
 - -high flexibility
- A modified behavior-based control method is presented crowded pericardial environment
- A kinematic model of the soft robotic manipulator with the concept of piecewise constant curvature is presented.
- An adaptive controller for image-based visual servoing of the soft robotic manipulator is developed.
- The performances of the proposed method are verified by experiments on a soft robotic manipulator.
- Future work includes considering dynamic visual servoing and environment effects on the robot.



Thank you!









2014 IEEE International Conference on Robotics and Biomimetics

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- Jun. 30, 2014 Submission of organized focused theme session proposals
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