

C44 08/12/44
化 I = 9
戴郁庭

12.5 Evaluate and compare with the exact solution δ , C_{fx} , and C_{fL} for the laminar boundary layer over a flat plate, using the velocity profile

$$v_x = \alpha \sin by.$$

$$\left\{ \begin{array}{l} U_x \frac{\partial V_x}{\partial x} + V_y \frac{\partial V_x}{\partial y} = \nu \frac{\partial^2 V_x}{\partial y^2} \\ \frac{\partial V_x}{\partial x} + \frac{\partial V_y}{\partial y} = 0 \end{array} \right. \rightarrow \text{stream function } \Psi(x, y) \Rightarrow \frac{\partial \Psi}{\partial x} = -V_y, \quad \frac{\partial \Psi}{\partial y} = U_x$$

$$\text{B.C. } \partial V_x(0) = 0$$

$$\textcircled{2} \quad V_x(\delta) = V_\infty = \alpha \sin(b\delta)$$

$$\textcircled{3} \quad \frac{dV_x(\delta)}{dy} = 0 = \alpha b \cos(b\delta)$$

$$\cos b\delta = \cos \frac{\pi y}{2}$$

$$b = \frac{\pi}{2\delta} \text{ 代入 } \textcircled{3} \text{ 得 } \alpha = V_\infty$$

$$\therefore V_x = V_\infty \sin\left(\frac{\pi y}{2\delta}\right)$$

von Kármán integral e.g.

$$\frac{T_0}{\rho} = \left(\frac{d}{dx} V_\infty \right) \int_0^\delta (V_\infty - V_x) dy + \frac{d}{dx} \int_0^\delta V_x (V_\infty - V_x) dy$$

$$\Rightarrow \frac{T_0}{\rho} = \frac{d}{dx} \int_0^\delta V_x (V_\infty - V_x) dy$$

$$= \frac{d}{dx} \int_0^\delta \left[V_\infty^2 \sin\left(\frac{\pi y}{2\delta}\right) - V_\infty^2 \sin^2\left(\frac{\pi y}{2\delta}\right) \right] dy$$

$$= \frac{d}{dx} V_\infty^2 \int_0^\delta \left[\sin\frac{\pi y}{2\delta} - \left(\frac{1 - \cos\left(\frac{\pi y}{2\delta}\right)}{2} \right) \right] dy$$

$$= \frac{d}{dx} V_\infty^2 \left[-\frac{2\delta}{\pi} \cos\frac{\pi y}{2\delta} - \frac{1}{2}y + \frac{\delta}{2\pi} \sin\frac{\pi y}{2\delta} \right]_0^\delta$$

$$= \frac{d}{dx} V_\infty^2 \left[\left(-\frac{2\delta}{\pi} \left(\cos\frac{\pi}{2} - 1 \right) \right) + \left(-\frac{1}{2}\delta \right) + \left(\frac{\delta}{2\pi} \right) (\sin\pi - 0) \right]$$

$$= \frac{d}{dx} V_\infty^2 \left(\frac{2\delta}{\pi} - \frac{\delta}{2} \right) = \frac{d}{dx} V_\infty^2 \left(\frac{\pi}{2} - \frac{1}{2} \right) \quad \boxed{\text{equal}}$$

$$\text{also } \frac{T_0}{\rho} = \frac{M}{\rho} \frac{dV_x}{dy} \Big|_{y=0} = \frac{M}{\rho} \alpha b (\cos b y) = \frac{M}{\rho} V_\infty \frac{\pi}{2\delta}$$

$$\frac{d\delta}{dx} V_\infty^2 \left(\frac{\pi}{2} - \frac{1}{2} \right) = \frac{M}{\rho} V_\infty \frac{\pi}{2\delta}$$

$$\int \delta d\delta = \int \frac{M}{\rho V_\infty^2} \frac{2\pi^2}{(4-\pi)^2} dx$$

$$\frac{1}{2}\delta^2 = \frac{M\pi^2 x}{\rho V_\infty^2 (4-\pi)}$$

$$\delta = \sqrt{\frac{2M\pi^2 x}{\rho V_\infty^2 (4-\pi)}} = \sqrt{\frac{2M\pi^2 x}{\rho V_\infty^2 (4-\pi)}} = \sqrt{\frac{2\pi^2}{4-\pi}} \frac{x}{\sqrt{Rex}} = 4.788 \frac{x}{\sqrt{Rex}} \quad \times$$

$$\therefore T_0 = M V_\infty \frac{\pi}{2} \sqrt{\frac{V_\infty \rho (4-\pi)}{2M\pi^2 x}}$$

$$\text{for } C_{fx} = \frac{2T_0}{\rho V_\infty^2} = \frac{2 \cdot M \cdot V_\infty \frac{\pi}{2}}{\rho V_\infty^2} \sqrt{\frac{V_\infty \rho (4-\pi)}{2M\pi^2 x}} = \sqrt{\frac{M \cdot \pi^2 \cdot V_\infty \cdot x \cdot (4-\pi)}{\rho \cdot V_\infty^2 \cdot 2M\pi^2 x}} = \sqrt{\frac{M}{\rho V_\infty x}} \cdot \sqrt{\frac{4-\pi}{2}} = \frac{0.655}{\sqrt{Rex}} \quad \times$$

$$\text{for } C_{fL} = \frac{1}{L} \int_0^L C_{fx} dx = \frac{1}{L} \int_0^L \sqrt{\frac{M}{\rho V_\infty x}} \sqrt{\frac{4-\pi}{2}} dx = \frac{1}{L} \sqrt{\frac{M}{\rho V_\infty}} \sqrt{\frac{4-\pi}{2}} \int_0^L x^{-\frac{1}{2}} dx = \frac{2}{L} \sqrt{\frac{M}{\rho V_\infty}} \sqrt{\frac{4-\pi}{2}} \int_0^L x^{-\frac{1}{2}} dx = \frac{2}{L} \sqrt{\frac{M}{\rho V_\infty}} \sqrt{\frac{4-\pi}{2}} \frac{1}{\sqrt{2}} = \frac{\sqrt{\frac{M}{\rho V_\infty L}} \sqrt{\frac{4(4-\pi)}{2}}}{\sqrt{2}} = \frac{1.311}{\sqrt{Rex}} \quad \times$$

sphere

12.17 A baseball has a circumference of $9\frac{1}{4}$ in. and a weight of $5\frac{1}{4}$ ounces. At 95 mph determine

- the Reynolds number
- the drag force
- the type of flow (see the illustration for Problem 12.7)

$$V = 95 \text{ mph} = 139.3 \frac{\text{ft}}{\text{s}}$$

$$C = 9.25 \text{ in} = 0.77 \text{ ft}$$

$$D = \frac{C}{\pi} = \frac{0.77}{\pi} = 0.245 \text{ ft}$$

↓
diameter

查表 $T = 80^\circ\text{F}$, $\nu = \frac{\mu}{\rho} = 0.169 \times 10^{-3} \frac{\text{ft}^2}{\text{s}}$

$$\rho = 0.0735 \frac{\text{lbf}}{\text{ft}^3}$$

$$(a) Re = \frac{\rho V D}{\mu} = \frac{\nu \cdot D}{\mu} = \frac{(139.3) \cdot (0.245)}{0.169 \times 10^{-3}} = 201903.789 \div 2 \times 10^5 *$$

(b)

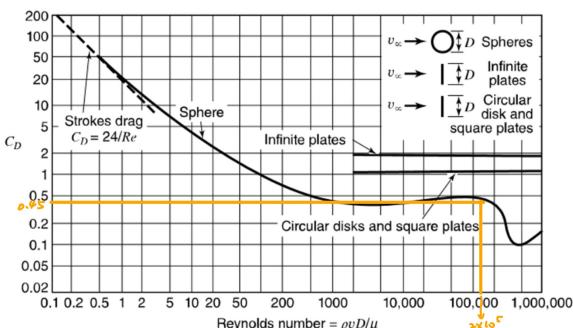


Figure 12.4 Drag coefficient versus Reynolds number for various objects.

$$\begin{aligned} \frac{F}{A_p} &= C_D \frac{\rho V_\infty^2}{2} \\ F &= A_p C_D \frac{\rho V_\infty^2}{2} \\ &= \left(\frac{\pi}{4} D^2 \right) C_D \frac{1}{2} \rho V_\infty^2 = \frac{\pi}{4} \cdot (0.0735) \cdot (0.45) \cdot \left(\frac{1}{2} \right) (0.0735) (139.3)^2 \\ &= 15.1 \frac{\text{lbf} \cdot \text{ft}}{\text{s}^2} \\ &= 0.47 \text{ lbf. *} \end{aligned}$$

(c)

- $Re_x < 2 \times 10^5$ the boundary layer is laminar
- $2 \times 10^5 < Re_x < 3 \times 10^6$ the boundary layer may be either laminar or turbulent
- $3 \times 10^6 < Re_x$ the boundary layer is turbulent

flow is near transition.

12.26 For a thin plate 6 in. wide and 3 ft long, estimate the friction force in air at a velocity of 40 fps, assuming

- turbulent flow
- laminar flow

The flow is parallel to the 6-in. dimension.

$$w = 6 \text{ in} = 0.5 \text{ ft}$$

$$L = 3 \text{ ft}$$

$$V = 40 \text{ fps.}$$

$$T = 80^\circ F$$

$$U = \frac{\mu}{\rho} = 0.169 \times 10^{-3} \frac{\text{lbm}}{\text{ft}^2 \cdot \text{s}}$$

$$\rho = 0.0735 \frac{\text{lbm}}{\text{ft}^3}$$

$$Re_x = \frac{\rho V w}{\mu} = \frac{0.0735 \times 0.5}{0.169 \times 10^{-3}} = 118343 \Rightarrow Re < 10^7$$

(a) for turbulent flow

by $\frac{1}{7}$ power law for turbulent boundary layer

$$\left\{ \begin{array}{l} \frac{V_x}{V_{x \max}} = \left(\frac{y}{\delta}\right)^{\frac{1}{7}} \\ T_0 = 0.0225 \rho V_{x \max}^2 \left(\frac{V}{V_{x \max} \delta}\right)^{\frac{1}{4}} \end{array} \right.$$

$$\text{fit } \lambda \text{ von Kármán integral eq } \frac{T_0}{\rho} = \left(\frac{d}{dx} V_\infty \right) \int_0^{\delta} (V_\infty - V_x) dy + \frac{d}{dx} \int_0^{\delta} V_x (V_\infty - V_x) dy$$

flat plat V_∞ is const.

$$0.0225 V_\infty^2 \left(\frac{V}{V_{x \max} \delta}\right)^{\frac{1}{4}} = \frac{d}{dx} \int_0^{\delta} V_\infty \left[\left(\frac{y}{\delta}\right)^{\frac{1}{7}} - \left(\frac{y}{\delta}\right)^{\frac{3}{7}} \right] dy$$

$$\Rightarrow 0.0225 \left(\frac{V}{V_{x \max} \delta}\right)^{\frac{1}{4}} = \frac{d}{dx} \int_0^{\delta} \left[\left(\frac{y}{\delta}\right)^{\frac{1}{7}} - \left(\frac{y}{\delta}\right)^{\frac{3}{7}} \right] dy = \frac{d}{dx} \left[\frac{7}{8} \left(\frac{1}{\delta}\right)^{\frac{1}{7}} y^{\frac{8}{7}} - \frac{7}{4} \left(\frac{1}{\delta}\right)^{\frac{3}{7}} y^{\frac{10}{7}} \right]_0^{\delta} = \frac{d}{dx} \left(\frac{7}{8} \delta - \frac{7}{4} \delta \right) = \frac{d\delta}{dx} \frac{7}{2}$$

$$\Rightarrow 0.0225 \left(\frac{V}{V_{x \max} \delta}\right)^{\frac{1}{4}} = \frac{7}{2} \frac{d\delta}{dx}$$

$$\int \left(\frac{V}{V_{x \max} \delta}\right)^{\frac{1}{4}} dx = \frac{7}{2} \cdot 0.0225 \int (\delta)^{\frac{1}{7}} d\delta \Rightarrow \left(\frac{V}{V_{x \max} \delta}\right)^{\frac{1}{4}} x = 4.32 \cdot \frac{4}{5} \delta^{\frac{8}{7}} = 3.456 \delta^{\frac{5}{7}} + C \quad \text{fit } \lambda \text{ B.C. } x=0, \delta=0 \therefore C=0$$

$$\left(\frac{V}{V_{x \max} \delta}\right)^{\frac{1}{4}} = 3.45 \left(\frac{\delta}{x}\right)^{\frac{5}{7}} \Rightarrow 0.376 (Re_x)^{-\frac{1}{7}} = \frac{\delta}{x}$$

$$C_{fT} = \frac{2 T_0}{\rho V_{x \max}^2} = 0.045 \left(\frac{V_{x \max}^2}{V_\infty (0.376 \delta)}\right)^{\frac{1}{4}} = \frac{0.074}{Re_x^{\frac{1}{7}}}$$

$$C_{fT} = \frac{0.074}{Re_x^{\frac{1}{7}}} = \frac{0.074}{118343^{\frac{1}{7}}} = 0.00715$$

$$F_{fT} = A \cdot C_{fT} \frac{\rho V_{x \max}^2}{2} = (0.5) \cdot (3) \cdot (0.00715) \frac{1}{2} (0.0735) (40)^2 = 0.63 \frac{\text{lbm} \cdot \text{ft}}{\text{s}^2} = 0.02 \text{ lbft. } \star$$

(b) for laminar flow

\because thin plate fit λ The Blasius's solution for flat plate for laminar

$$C_{fL} = \frac{0.664}{\sqrt{Re_x}}$$

$$C_{fL} = \frac{1}{L} \int C_{fL} dx = \frac{1}{L} \int_0^L 0.664 \sqrt{\frac{\mu}{\rho V_{x \max} x}} dx = \frac{1.328}{\sqrt{Re_x}} = 1.328 \sqrt{\frac{\mu}{\rho V_{x \max} L}}$$

$$C_{fL} = \frac{1.328}{\sqrt{Re_x}} = \frac{1.328}{\sqrt{118343}} = 0.00386$$

$$F_{fL} = A \cdot C_{fL} \frac{\rho V_{x \max}^2}{2} = (0.5) \cdot (3) \cdot (0.00386) \cdot \frac{1}{2} (0.0735) (40)^2$$

$$= 0.34 \frac{\text{lbm} \cdot \text{ft}}{\text{s}^2}$$

$$= 0.01 \text{ lbft. } \star$$