

Foundations of Robotics

ROB-GY 6003

Homework 2 Answers

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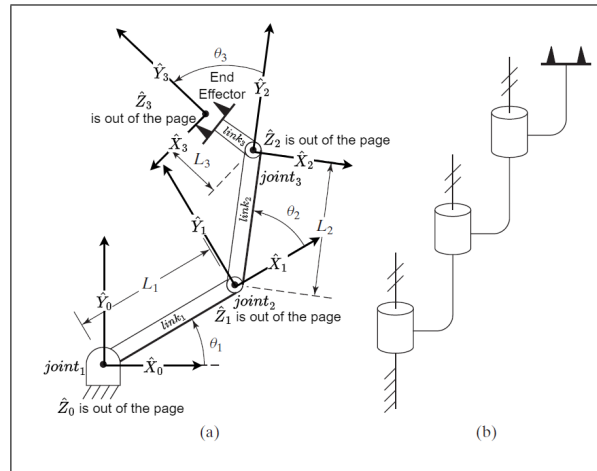
Question: 3.1**Answer:** Consider below Figure 1

Figure 1: A three-link planar arm. On the right, we show the same manipulator by means of a simple schematic notation. Hash marks on the axes indicate that they are mutually parallel.

Frames have been attached to each of the *joints* and the *end effector*. We shall now construct the DH Parameter table for this -

$joint_i$	θ_i	d_i	a_i	α_i
$joint_1$ Revolute	$\theta_1 + q_1$	0	L_1	0
$joint_2$ Revolute	$\theta_2 + q_2$	0	L_2	0
$joint_3$ Revolute	$\theta_3 + q_3$	0	L_3	0

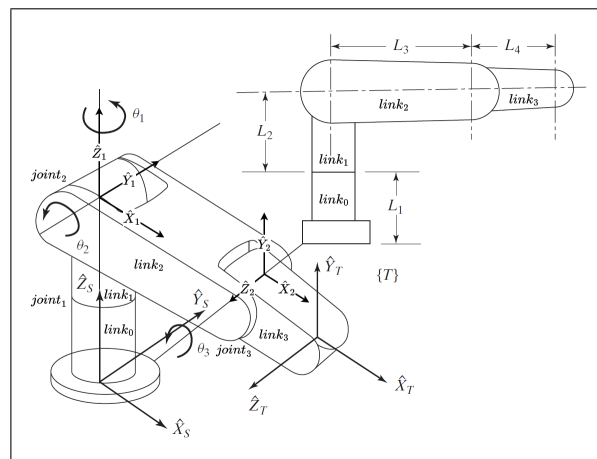
Question: 3.4**Answer:** Consider below Figure 2

Figure 2: Two views of a 3R manipulator

Frames were previously attached to $joint_1$ the *end effector*. Frames have now been attached to $joint_2$ and $joint_3$. We shall now construct the DH Parameter table for this -

$joint_i$	θ_i	d_i	a_i	α_i
$joint_1$ Revolute	$0 + q_1$	$L_1 + L_2$	0	0
$joint_2$ Revolute	$0 + q_2$	0	L_3	$\frac{\pi}{2}$
$joint_3$ Revolute	$0 + q_3$	0	L_4	0

We shall now find the transformation matrices S_1T , 1_2T and 2_TT by applying the generalised equation,

$${}^{i-1}_iT = \begin{bmatrix} \cos \theta_i & -\cos \alpha_i \sin \theta_i & \sin \alpha_i \sin \theta_i & a_i \cos \theta_i \\ \sin \theta_i & \cos \alpha_i \cos \theta_i & -\sin \alpha_i \cos \theta_i & a_i \sin \theta_i \\ 0 & \sin \alpha_i & \cos \alpha_i & d_i \\ 0 & 0 & 0 & 1 \end{bmatrix} \quad (1)$$

$$\Rightarrow {}^S_1T = \begin{bmatrix} \cos q_1 & -\sin q_1 & 0 & 0 \\ \sin q_1 & \cos q_1 & 0 & 0 \\ 0 & 0 & 1 & (L_1 + L_2) \\ 0 & 0 & 0 & 1 \end{bmatrix} \quad (2)$$

$$\Rightarrow {}^1_2T = \begin{bmatrix} \cos q_2 & 0 & \sin q_2 & L_3 \cos q_2 \\ \sin q_2 & 0 & -\cos q_2 & L_3 \sin q_2 \\ 0 & 1 & 0 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix} \quad (3)$$

$$\Rightarrow {}^2_TT = \begin{bmatrix} \cos q_3 & -\sin q_3 & 0 & L_4 \cos q_3 \\ \sin q_3 & \cos q_3 & 0 & L_4 \sin q_3 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix} \quad (4)$$

Question: 3.8

Answer: Consider below Figure 3

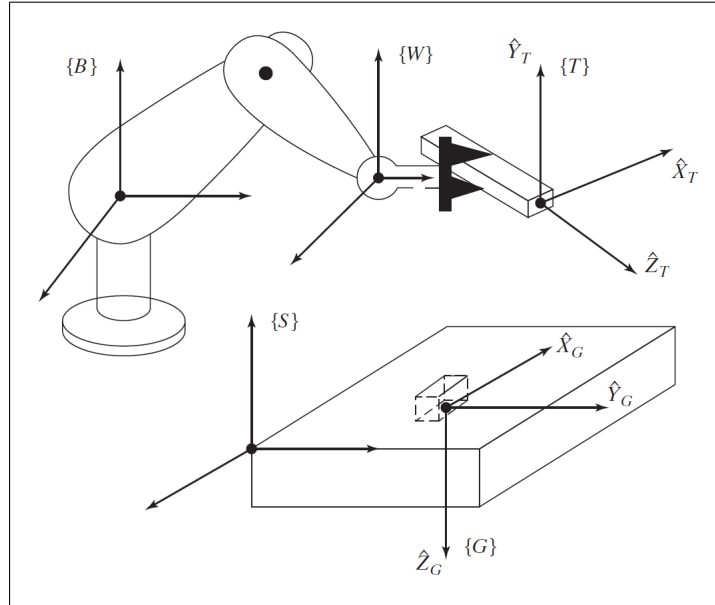


Figure 3: Determination of the tool frame

It is given that the robot feels around with the tool tip until it inserts it into the socket (or Goal). The transformation to this point can be described in two ways.

Firstly, from the perspective of the robot $= {}^B_WT \cdot {}^W_TT$

Secondly, from the perspective of the goal $= {}^B_S T \cdot {}^S_G T$

But both of these combination transforms describe the same final position, so,

$$\Rightarrow {}^B_W T \cdot {}^W_T T = {}^B_S T \cdot {}^S_G T$$

Upon multiplying both sides by ${}^B_W T^{-1}$

$$\Rightarrow {}^W_T T = {}^B_W T^{-1} \cdot {}^B_S T \cdot {}^S_G T$$

Question: 3.12

Answer: No. An arbitrary rigid-body transformation requires six parameters. Only in the case that has been described here (according to the D-H Convention) can the rigid-body transformation be expressed with four parameters.

Question: 3.16

Answer: The frames are attached as per DH convention given by Spong. See below Figure 4 -

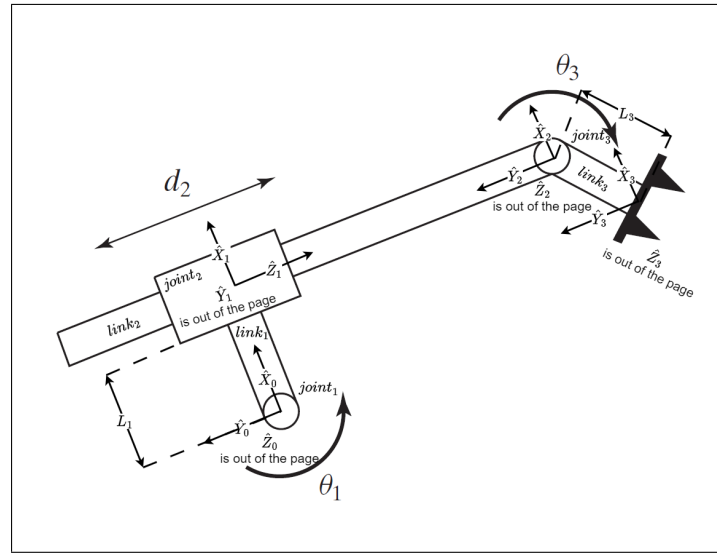


Figure 4: The *RPR* planar robot

The DH Parameter table is given below -

$joint_i$	θ_i	d_i	a_i	α_i
$joint_1$ Revolute	$0 + q_1$	0	L_1	$\frac{\pi}{2}$
$joint_2$ Prismatic	0	$d_2 + q_2$	0	$-\frac{\pi}{2}$
$joint_3$ Revolute	$\theta_3 + q_3$	0	L_3	0

Question: 3.17

Answer: The frames are attached as per DH convention given by Spong. See below Figure 5 -

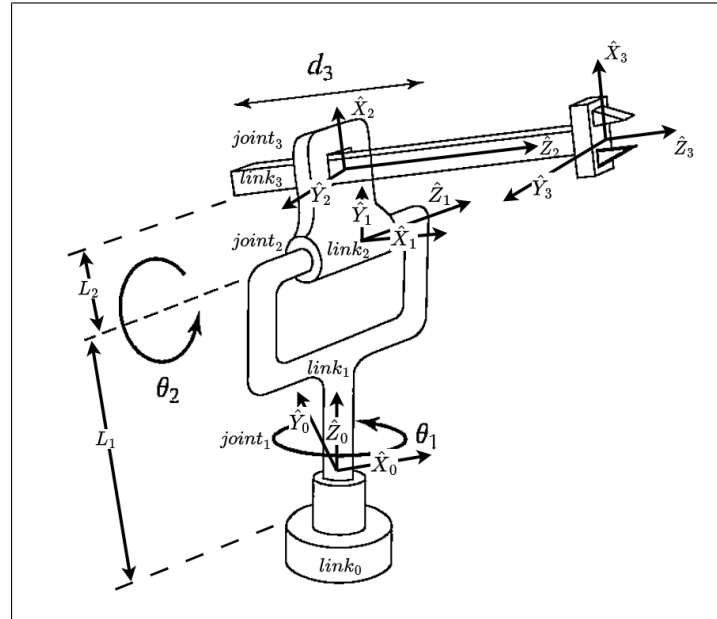


Figure 5: Three-link RRP manipulator

The DH Parameter table is given below -

$joint_i$	θ_i	d_i	a_i	α_i
$joint_1$ Revolute	$0 + q_1$	L_1	0	$-\frac{\pi}{2}$
$joint_2$ Revolute	$-\frac{\pi}{2} + q_2$	0	L_2	$-\frac{\pi}{2}$
$joint_3$ Prismatic	0	$0 + q_3$	0	0