

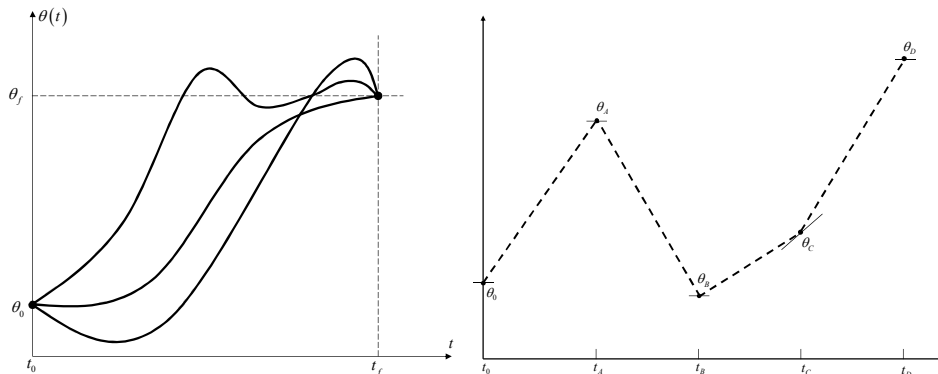
## CHAPTER 7. TRAJECTORY GENERATION

- {trajectory, motion, path (spatial)} + {generation, planning, prediction (biological systems)}
- Trajectory: desired time history of position, velocity, and acceleration for each DOF from initial to final configuration in multidimensional space; Joint space schemes vs. Cartesian space schemes
- Motions of end-effector tool frame  $\{T\}$ , relative to station frame  $\{S\}$  (inertial frame), from current value  $\{T_{initial}\}$  to a desired final value  $\{T_{final}\}$
- Via points (frames): sequence of desired intermediate points (frames) between initial and final configurations
  - Via point (in configuration space) is a frame that specifies position and orientation of tool frame relative to station frame; tool frame must pass through a set of via points.
- Path points (frames): include all via points plus initial and final points
- Path update rate: time rate at which the trajectory points are computed
- Motion of smooth function: continuous up to first (or second) derivative ( $C^1$ ,  $C^2$ )

### Joint Space Schemes

| Path shapes (in space and in time) are described in terms of (smooth) joint variable functions.

- Given: Initial, final, and via points are specified in terms of desired position/orientation, velocity, and acceleration of end-effector tool frame  $\{T\}$  relative to station frame  $\{S\}$ , and time duration
  - Converted into desired joint variables and velocities (by inverse kinematics and inverse Jacobian).
  - Calculate smooth function for each joint.
    - Time required for each segment is same for each joint; all joints reach a point at the same time.
    - No singularity problem
- Use numerical interpolation method for each joint: polynomials, piecewise polynomials, spline functions, B-splines, Hermite interpolations, Fourier transform (trigonometric), etc.
  - Calculate coefficients from initial, final, and via point conditions.



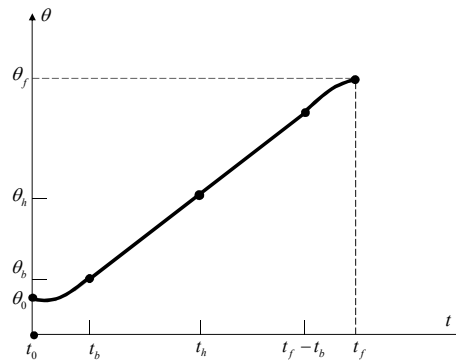
### Cubic Polynomials (Joint Space)

- General  $m$ th degree polynomial:  $\theta(t) = a_0 + a_1t + a_2t^2 \dots + a_{m-1}t^{m-1} + a_mt^m$
- Cubic ( $m = 3$ ) polynomial:  $\theta(t) = a_0 + a_1t + a_2t^2 + a_3t^3$
- Example: initial and final conditions (four constraints)  $\theta(0) = \theta_0$ ;  $\dot{\theta}(0) = \dot{\theta}_0$ ;  $\theta(t_f) = \theta_f$ ;  $\dot{\theta}(t_f) = \dot{\theta}_f$   
 - can be solved for 4 unknowns  

$$\rightarrow a_0 = \theta_0; a_1 = \dot{\theta}_0; a_2 = \frac{3}{t_f^2}(\theta_f - \theta_0) - \frac{2}{t_f}\dot{\theta}_0 - \frac{1}{t_f}\dot{\theta}_f; a_3 = -\frac{2}{t_f^3}(\theta_f - \theta_0) + \frac{1}{t_f^2}(\dot{\theta}_f + \dot{\theta}_0)$$
- If  $k$  via points are given  $\rightarrow k+1$  cubic segments
- Methods to specify desired velocity at via points
  - (1) Specified by user in terms of Cartesian linear and angular velocities of tool frame  $\{T\}$   
 $\rightarrow$  Mapped to desired joint velocities using inverse Jacobian  
 (If singular at a via point, then user is not free to assign arbitrary velocity at this point.)
  - (2) Specified automatically by the system using a suitable heuristic in Cartesian or joint space  
 $\rightarrow$  Reasonable choice of joint velocities at via points  
 $\rightarrow$  Example: via points connected with straight line segments; if slope of these lines changes sign at via point, choose zero velocity; if slope of these lines does not change sign, choose the average of the two slopes
  - (3) Specified automatically by the system such that the accelerations at via points are continuous  
 $\rightarrow$  In spline, replace two velocity constraints at the connection of two cubics with two constraints of continuous velocity and continuous acceleration  
 $\rightarrow$  For  $n$  cubic segments – tridiagonal matrix form

### Linear Function with Parabolic Blends (Joint Space)

- | Linearly interpolate to move from initial to final joint position.  
 (But generally, end-effector does not necessarily move in a straight line in space.)
- For a smooth path with continuous position and velocity
  - $\rightarrow$  linear function with a parabolic blend region at each path point
  - | During blend portion of trajectory, constant acceleration is used to change velocity smoothly.
  - | Linear function and two parabolic functions are splined together.  $\rightarrow$  continuous  $q$  and  $\dot{q}$
$$\theta_b = \theta_0 + \frac{1}{2}\ddot{\theta}t_b^2 \quad (\ddot{\theta}: \text{acceleration during blend region})$$



▪ Assume

- Parabolic blends both have same duration.
- Same constant acceleration is used during both blends.

→ Symmetric about halfway point time  $t_h$  ( $t = 2t_h$ ) and about halfway point position  $\theta_h$

▪ [Velocity at the end of blend region] = [velocity of linear section]

$$\dot{\theta}_{t_b} = \frac{\theta_h - \theta_b}{t_h - t_b} \Rightarrow \ddot{\theta} t_b^2 - \ddot{\theta} t_f t_b + (\theta_f - \theta_0) = 0 \Rightarrow t_b = \frac{t_f}{2} - \frac{\sqrt{\ddot{\theta}^2 t_f^2 - 4\ddot{\theta}(\theta_f - \theta_0)}}{2\ddot{\theta}}$$

where  $\ddot{\theta} \geq \frac{4(\theta_f - \theta_0)}{t_f^2}$

- If  $\ddot{\theta} = 4(\theta_f - \theta_0) / t_f^2 \rightarrow$  no linear portion; path is composed of two blends that connect with equivalent slope
- As  $\ddot{\theta}$  increases  $\rightarrow$  blend region decreases
- If  $\ddot{\theta} \rightarrow \infty \rightarrow$  simple linear interpolation

▪ With via points  
(skip)

### Cartesian Space Schemes

| Cartesian position and orientation as functions of time (spatial path)

- Given: initial, final, and via points are specified in terms of desired position/orientation, velocity, and acceleration of end-effector tool frame  $\{T\}$  relative to station frame  $\{S\}$ , and time duration
- Position:  ${}^0\mathbf{P}_{AORG}$
- Orientation: use angle-axis representation  $ROT({}^0\hat{K}_A, \theta_{0A}) \rightarrow {}^0\mathbf{K}_A = \theta_{0A} {}^0\hat{K}_A$   
(Note: Rotation matrices cannot be interpolated.)
- 6x1 vector of Cartesian position and orientation as a function of time:  ${}^0\chi_A = \begin{bmatrix} {}^0\mathbf{P}_{AORG} \\ {}^0\mathbf{K}_A \end{bmatrix}$
- Recall: Angle-axis orientation representation is not unique, i.e.,  $({}^0\hat{K}_A, \theta_{0A}) = ({}^0\hat{K}_A, \theta_{0A} + n360^\circ)$ .  
→ Minimize total amount of rotation  $\|{}^0\mathbf{K}_{final} - {}^0\mathbf{K}_{initial}\|$  for interpolation.

### Geometric problems with Cartesian Paths

| Workspace, singularities

- Intermediate points unreachable: Although the initial and final configuration of manipulator end-effector are within workspace, it is possible that not all points lying on a straight line connecting these two points are in the workspace.
- High joint rates near singularity: locations in workspace where it is impossible to choose finite joint rates that yield desired Cartesian velocity of end-effector  $\rightarrow$  Certain Cartesian paths are impossible  
: if manipulator approaches a singular configuration, one or more joint velocities increase toward infinity  $\rightarrow$  deviation from desired path

- Start and goal reachable in different solutions: Goal point cannot be reached in the same physical solution as the manipulator is in at the start point.
- Other problems: collision detection/avoidance, bifurcation, redundancy (optimization), etc.

